

# **Oil recovery in porous media using emulsion flooding**

by  
**Aleksey Baldygin**

A thesis submitted in partial fulfillment of the requirements for the degree of

**Doctor of Philosophy**

Department of Mechanical Engineering  
University of Alberta

©Aleksey Baldygin, 2015

# Abstract

Aiming to pursue studying enhanced oil recovery processes with an *ex-situ* produced emulsion as flooding agent, an improved core flooding experimental system was designed, constructed and commissioned. The developed system allows the use of not only emulsion, but also other flooding agents, including surfactants and polymers. The components of the experimental apparatus, including a biaxial core holder, a two-dimensional core holder, and effluent analysis system were re-designed to improve flow distribution, the packing process and reduce post-experimental analysis. To secure the conditions for experiments, custom software for system control and monitoring, and logging of all system parameters was developed. The limits and ways to improve the developed system were identified. An unconsolidated silica sand pack was chosen to represent the porous media on all experimental tests.

The initial experimental results with emulsion flooding explored the capability of the new apparatus and confirmed the efficiency of emulsion as a flooding agent during direct emulsion flooding or water flooding followed by emulsion flooding. Oil recovery was enhanced by 15 % of original oil in place in case of emulsion flooding followed by water flooding. From experimental results, it was hypothesised that emulsion moves through the sand pack with a piston-like flood front and

that an alternative technique to improve efficiency of emulsion flooding can be developed. This technique should also allow to reduce amount of emulsion used per percentage of oil recovery.

A flooding technique was proposed and established to improve the efficiency of emulsion flooding in reservoirs and reduce costs of flooding. The technique was named water-alternate-emulsion (WAE). Three different flooding ratios have been tested using a biaxial core holder. The experimental analysis showed that for 5:1 WAE flooding, the ultimate oil recovery could be up to 82 % at 0.3 PV of total emulsion injection. The analysis of physical properties of the effluent, such as viscosity, density and surface tension, revealed that alternate flooding does not affect on physical properties of liquids involved in flooding. Effluent analysis and examination of extracted sand packs after experiment completion reported that emulsion undergoes separation inside porous media during alternative flooding and moves with a post-like flood front during continuous injection. As a results, it blocks high-permeability zones and surfactant present in emulsion interacts with *in-situ* liquids. Pressure measurements identified that emulsion stimulates sand packs with internal pressure rise prior to water flooding.

Experimental flow visualization and pressure mapping analysis of emulsion flooding with horizontal and vertical wells was performed to provide additional understanding of internal processes. It was shown experimentally, that efficiency of emulsion flooding strongly depends on well configuration. The horizontal injection - horizontal production (HI-HP) configuration for injection and production well, based on data from effluent and image analysis, was found to be the most efficient for emulsion flooding. The flood front movement during emulsion flood-

ing process was estimated using code developed for image analysis. Experimental data presented in this research project suggests that stable emulsion flood front and stable pressure rise guarantees enhanced oil recovery during emulsion injection. In addition, oil drops present in an emulsion were observed with a microscope and it was hypothesised that emulsion has bimodal structure. Later it was confirmed with the membrane-base particle analysers.

As a results of this research study, emulsion flooding process was investigated experimentally. It was shown that emulsions can be used effectively to recover oil using different flooding techniques. Oil-in-water emulsion blocked highly permeable zones and redirecting following water flooding. Experimental results from multi-dimensional studies suggested that it is important to consider well configuration and physical parameters, such as pressure data, in a field trials. Collected results for the drop size distribution now can be considered in a future fundamental works for emulsion flooding process.

# Preface

This thesis is original work by Aleksey Baldygin. Chapter 3 and 4 of this thesis have been published as A. Baldygin, D. S. Nobes, and S. K. Mitra, “A new laboratory core flooding experimental system”, *Industrial & Engineering Chemistry Research*, DOI: 10.1021/ie501866e, 2014 and as A. Baldygin, D. S. Nobes, and S. K. Mitra, “Water-Alternate-Emulsion (WAE): A new technique for enhanced oil recovery”, *Journal of Petroleum Science and Engineering*, DOI:10.1016/j.petrol.2014.06.021, 2014, respectively. Chapter 5 has been prepared for submissions as publication as A. Baldygin, D. S. Nobes, and S. K. Mitra, “Experimental pressure mapping and flow visualization of emulsion flooding with horizontal and vertical wells”, *Journal of Petroleum Science and Engineering*, 2014. Appendix A-2 has been published as part of the conference paper as A. Baldygin, D. S. Nobes, and S. K. Mitra, “Oil recovery from porous media using emulsion”, *Proceedings of the ASME 2014 International Mechanical Engineering Congress & Exposition*, 2014. The initial concept of the experimental system has been presented during the biennial CSME International Congress: Symposium on Advanced Energy Systems (CSME’12 - Symposium on AES) as A. Baldygin, D. S. Nobes, and S. K. Mitra, “Novel Technique for Core Flooding Experiments”, 2012. The software with graphical user interface was developed myself and used to assist experiments in the current re-

search study. The design of core holders with appropriate drawing package was also developed myself. In addition, I was responsible for data collection and analysis as well as for manuscript preparation. Dr. David S. Nobes and Dr. Sushanta K. Mitra were the supervisory authors and contributed to manuscript edits. Emulsion used in experiments was provided by Quadrise Canada Inc..

# Acknowledgements

I would like to thank my supervisor, Dr. David S. Nobes for believing in me in 2011 and giving me an opportunity to be part of PhD program at the Mechanical Engineering department. I am also thankful for the productive discussions that we had along my program. He gave me a passion to have attention on small details and provided continuous support during my program. I would also like to thank my co-supervisor, Dr. Sushanta K. Mitra for the time that he spend with me over weekends and helped me to improve my writing and thinking skills. His guidance and support over the last three years provided me an opportunity to do up-to-date level research.

My thanks and appreciation to Roger Marchand, Andrew Campbell, Rick Bubenko and other shop technicians who have provided me technical and engineering support whenever I needed it. I would also thank Rick Conrad for his expertise when I was setting up experimental set-up for the first time.

I would also like to thank my friends and colleagues: Anil Stephen, Prashant Waghmare, Orest Shardt, Lalit Pant, Arnab Guha, Sheng Tian, Amrit Bhinder, Reza Sabbagh and many others with whom I spent last three years. They have supported my research and my recreation time whenever I needed.

In addition, I would like to acknowledge Dr. Patrick Brunelle from Quadrise Canada Inc. for his valuable inputs and providing emulsion for experiments. Financial assistance from NSERC CRD (Grant No. CRDPJ 399500-10) is acknowledged here.

A sincere thank you to my wife Alexandra Komrakova and my little daughter Olivia Baldygin for their support, love and patience. Finally, a greatest thank you to my parents for providing me support during my whole live and believing that one day, I could be a PhD.

# Contents

<b>1</b>	<b>Introduction</b>	<b>1</b>
1.1	Motivation . . . . .	1
1.2	Thesis objective . . . . .	7
<b>2</b>	<b>Oil recovery background</b>	<b>10</b>
2.1	Porosity of Sand Pack . . . . .	10
2.2	Permeability of Sand Pack . . . . .	11
2.3	Saturation . . . . .	15
2.4	The physical Process of Oil Recovery . . . . .	16
2.5	Mobility . . . . .	19
2.6	The Composition of the Fluids . . . . .	20
2.7	Production of the Emulsion . . . . .	21
2.8	Scaling Analysis . . . . .	24
<b>3</b>	<b>A new laboratory core flooding experimental system</b>	<b>26</b>
3.1	Introduction . . . . .	26
3.2	Traditional Core Flooding Systems . . . . .	27
3.3	Developed Core Flooding System . . . . .	30
3.3.1	Core Flooding System Flexibility . . . . .	38

3.3.2	Core Flooding System Limitations . . . . .	41
3.3.3	Remote Control . . . . .	41
3.4	Materials and Specifications . . . . .	44
3.5	Experimental Validation of the Core Flooding System . . . . .	48
3.5.1	Effluent Management System . . . . .	48
3.5.2	Core Flooding Experiments . . . . .	53
3.6	Conclusion . . . . .	55
<b>4</b>	<b>Water-Alternate-Emulsion (WAE): A new technique for enhanced oil recovery</b>	<b>57</b>
4.1	Introduction . . . . .	57
4.2	Materials and Methods . . . . .	59
4.3	Results and Discussion . . . . .	66
4.3.1	Qualitative analysis of WAE Flooding . . . . .	66
4.3.2	Quantitative Analysis of WAE Flooding . . . . .	68
4.3.3	Effluent Analysis . . . . .	72
4.3.4	Comparison of WAE with Traditional Flooding . . . . .	74
4.4	Conclusions . . . . .	76
<b>5</b>	<b>Experimental flow visualization and pressure mapping of emulsion flooding with horizontal and vertical wells</b>	<b>77</b>
5.1	Introduction . . . . .	77
5.2	Experimental Setup . . . . .	80
5.3	Materials and Methods . . . . .	88
5.4	Results and Discussion . . . . .	95

5.4.1	Visual Analysis . . . . .	95
5.4.2	Pressure Maps . . . . .	100
5.4.3	Effluent Analysis . . . . .	111
5.4.4	Quantitative Analysis . . . . .	113
5.5	Conclusion . . . . .	122
<b>6</b>	<b>Conclusion and Future Work</b>	<b>124</b>
6.1	Conclusion . . . . .	124
6.2	Future Work . . . . .	127
<b>References</b>		<b>155</b>
<b>Appendix</b>		<b>156</b>
A-1	1D and 2D core holder . . . . .	156
A-1.1	One dimensional core holder . . . . .	156
A-1.2	Two dimensional core holder . . . . .	159
A-2	Error analysis . . . . .	162
A-3	Consistency in results during 2D core flooding experiments . . . . .	164
A-4	Image processing source code . . . . .	168
A-5	Pressure data processing source code . . . . .	181
A-6	Set of drawings . . . . .	203
A-7	Software flowchart . . . . .	238
A-8	Software source code . . . . .	240

# List of Tables

3.1	Summary of existing core flooding systems used globally. . . . .	29
3.2	Properties of the sand packs . . . . .	46
4.1	Relevant parameters for unconsolidated sand pack samples used in flooding experiments. . . . .	64
4.2	The physical properties of the liquids shown in Figure 4.6. . . . .	74
5.1	The physical properties of the liquids. . . . .	90
5.2	Relevant parameters for unconsolidated sand pack samples used in flooding experiments. . . . .	94
A-1	Relevant parameters for unconsolidated sand pack samples used in flooding experiments. . . . .	164

# List of Figures

2.1	A schematic of the concept of a single pore with trapped oil (contact angle is less than 90°). . . . .	17
2.2	Oil drop is sitting on the throat of pore (following Nazzal et al. (Nazzal and Wiesner, 1996)). . . . .	18
3.1	Schematic of the core flooding experimental apparatus. . . . .	31
3.2	Exploded view of the core holder (1 - cap, 2 - end plug's body, 3 - body, 4 - internal surface, 5 - fitting 1/8 NPT to 3.175 mm (1/8 in.) tube). . . . .	33
3.3	End plugs of the biaxial core holder. (a) - isometric view of end plugs; (b) - end plug assembled; (c) - cross section view of single end plug (1 - sandblasted internal surface, 2 - stainless steel filter, 3 - 3D-printed plate, 4 - strain ring, 5 - end plug's body, 6 - core holder's body) . . . . .	34
3.4	Variation of geometric configuration for end plug (a) single entrance, flat surface; (b) single entrance, grooves for flow distribution; (c) single entrance, channels for redistribution. . . . .	35

3.5 Variation of sub-components for end plug (a) perforated plate, single hole; (b) perforated plate, four entrance holes; (c) 40 micron stainless steel filter made of 316L SS; (d) cap with 9 holes and channels. . . . .	36
3.6 The horizontal velocity component distribution in the axial cross-section of the core holder obtained with different configurations of end plugs. . . . .	37
3.7 Schematics of the further updates to the developed system. . . . .	40
3.8 A graphical user interface to perform automation for the core flooding system. . . . .	42
3.9 A graphical user interface to perform configuration for the core flooding system. . . . .	43
3.10 An example of density measurements at the effluent side during core flooding experiment. . . . .	49
3.11 A comparison of data obtained from mass flow meter and test tube fractionation during water flooding. The vertical axis - recovered mixture/oil recorded by mass flow meter, the horizontal axis - recovered mixture/oil measured with test tubes. . . . .	51
3.12 A comparison of data obtained from mass flow meter and test tube fractionation during emulsion flooding. The vertical axis - recovered mixture/oil recorded by mass flow meter, the horizontal axis - recovered mixture/oil measured with test tubes. . . . .	52

3.13 Recovery comparison for studied cases: Run #1 and Run #2 - water flooding, Run #3 - direct emulsion flooding and Run #4 - water flooding followed by emulsion flooding. . . . .	53
4.1 Pore size distribution of studied silica sand. . . . .	61
4.2 Cross-section images of the sand pack (a) after complete WAE flooding with 2:1 ratio followed by water flooding up to 5.6 PV; (b) after complete water flooding followed by approximately 0.3 PV of emulsion injection. Here, the direction of injection is from left to right. . . . .	67
4.3 Variation of pressure drop across the core holder and the oil recovery with respect to PV of injected fluids, 2:1 WAE. The horizontal dashed lines indicate the location of the pressure jumps. . . . .	69
4.4 Variation of pressure drop across the core holder and the oil recovery with respect to PV of injected fluids, 4:1 WAE. The horizontal dashed lines indicate the location of the pressure jumps. . . . .	71
4.5 Variation of pressure drop across the core holder and the oil recovery with respect to PV of injected fluids, 5:1 WAE. The horizontal dashed lines indicate the location of the pressure jumps. . . . .	72
4.6 A photograph of liquids injected and collected during complete WAE flooding. From left to right: water, paraffin oil, emulsion, recovered oil, produced water. . . . .	73
4.7 Cumulative recovery curves for WAE flooding and comparison with waterflooding, emulsion flooding, and waterflooding followed by emulsion flooding (presented in Chapter 3). . . . .	75

5.1	A photograph of experimental setup used for the core flooding experiments with 2D core holder. . . . .	81
5.2	Exploded view of the 2D core holder (1) main frame with profiled slot, (2) cast acrylic wall, (3) stainless steel wall with pressure ports, (4) top cap, (5) profiled cap, and (6) holder. . . . .	82
5.3	Pattern for hole perforation in wells (28 holes/in <sup>2</sup> ). . . . .	84
5.4	Reference images with coordinates for pressure sensors in (a) VI-VP; (b) VI-HP; (c) HI-HP configuration. . . . .	85
5.5	Comparison of pressure maps collected with different settings in <i>scatteredInterpolant</i> function. . . . .	87
5.6	Drop size distribution measured by Quadrise Canada Inc. . . . .	91
5.7	Microscopic picture of diluted oil-in-water emulsion in phosphate buffered saline (PBS), pH 7.4 (Magnification: 11.13x, Total magnification: 256.08x). The picture was taken using motorized fluorescence stereo zoom microscope (Axio Zoom.V16, Carl Zeiss AG). . . . .	91
5.8	Drop size distribution measured using two particle analyzers (qNano and qMicro, Izon Science Ltd.). . . . .	92
5.9	Pore size distribution of studied silica sands. . . . .	93
5.10	An example snapshot from the emulsion flooding process after water flooding. . . . .	97
5.11	Cross-section images of the sand pack for different configurations: (a) VI-VP; (b) VI-HP; (c) HI-HP. . . . .	98
5.12	Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration. . . . .	102

5.13 Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration. . . . .	103
5.14 Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration. . . . .	104
5.15 Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration. . . . .	105
5.16 Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration. . . . .	106
5.17 Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration. . . . .	107
5.18 Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration. . . . .	108
5.19 Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration. . . . .	109
5.20 Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration. . . . .	110
5.21 Ultimate oil recovery curves for water flooding followed by emul- sion flooding at different well configurations: (a) complete flooding process and (b) emulsion flooding process after water flooding. . . .	112
5.22 Left column shows sand pack prior to water flooding, central col- umn shows sand pack prior emulsion flooding, right column shows evolution of interface of emulsion injection in (a) VI-VP configura- tion; (b) VI-HP configuration; (c) HI-HP configuration. Here, the direction of injection is from left to right. . . . . . . . . . .	114

5.23 Emulsion front position versus time at three locations of a sand pack (a) top; (b) center; (c) bottom, as it is shown in reference Figure 5.10, for VI-VP configuration. . . . .	115
5.24 Emulsion front position versus time at three locations of a sand pack (a) top; (b) center; (c) bottom, as it is shown in reference Figure 5.10, for VI-HP configuration. . . . .	117
5.25 Emulsion front position versus time at three locations of a sand pack (a) top; (b) center; (c) bottom, as it is shown in reference Figure 5.10, for HI-HP configuration. . . . .	118
5.26 Emulsion flood front velocity at three locations of a sand pack (a) top; (b) center; (c) bottom, as it is shown in reference Figure 5.10 . .	120
A-1 Cast acrylic wall deformation at 300 psi. . . . .	160
A-2 Cast acrylic wall deformation at 400 psi. . . . .	160
A-3 Cast acrylic wall deformation at 500 psi. . . . .	161
A-4 Cross-section images of the sand pack for different configurations: (a) HI-HP; (b) HI-HP (failed). . . . .	166
A-5 Ultimate oil recovery curves for water flooding followed by emulsion flooding at different well configurations. . . . .	167
A-1 Software flowchart. . . . .	239

# Nomenclature

$A$  Cross section

$d$  Diameter in 1D cell

$h$  Sand pack height

$H_{in}$  Hydraulic head inlet

$H_{out}$  Hydraulic head outlet

$K$  Hydraulic conductivity

$k, k_a$  Absolute permeability

$k_e$  Effective permeability

$k_r$  Relative permeability

$L$  Length of cell

$M$  Mobility

$P_c$  Capillary pressure

$P_{crit}$  Critical pressure

$p_{in}$	Water pressure at the inlet
$P_m$	Mean absolute pressure
$p_{out}$	Water pressure at the outlet
$Q$	Discharge from porous media
$q$	Darcy flux
$Q_{cur}$	Current volume flow rate
$R$	Droplet radius
$r$	Pore throat radius
$r^*, R^*$	Radii
$S$	Fluid saturation
$t_{step}$	Single time step
$u_t$	Darcy velocity in linear displacement
$U_{\text{in}}$	Interstitial velocity
$U_o$	Superficial (or empty tube) velocity
$V$	Bulk volume
$v$	Velocity of the displacing fluid
$V_d$	Dead volume
$V_{eff}$	Effective pore volume

$V_p, V_{pv}$  Pore volume

$V_s$  Grain volume

$V_v$  Void space

$V_{j,rec}$  Fluid volume for a given phase

$V_{kv}$  Volume of water in water tank

$V_{rem}, V_{water,rec}$  Remaining volume of water in water tank

$w$  Sand pack width

$z_{in}$  Porous media elevation at the inlet

$z_{out}$  Porous media elevation at the outlet

### Greek Letters

$\dot{\gamma}$  Share rate

$\eta, \eta_1$  Viscosity of displacing fluid

$\gamma, \gamma_{12}$  Interfacial tension

$\lambda$  Mobility ratio

$\Theta$  Contact angle

$\mu$  Dynamic viscosity

$\phi$  Porosity

$\rho_g$  Grain density

$\rho_{record}$  Recorded fluid density

$\rho_{ref}$  Reference fluid density

### Subscript

$e$  Emulsion

$g$  Gas

$i$  Row number (used in Chapter 5)

$j$  Oil or water, based on readings; column number (used in Chapter 5)

$n$  Number for Run/Experiment

$o$  Oil

$o/w$  Oil and water

$r$  Relative

$w$  Water

### Dimensionless numbers

$$We = \frac{\eta_1 \dot{\gamma} R}{\gamma_{12}} \text{ Weber number}$$

### Abbreviations

1D One dimensional

2D Two dimensional

CAG Chemical-augmented WAG

CSS Cyclic steam simulation

DAQ Data acquisition

DG Double gap

DSA Drop shape analyzer

DSD Droplet size distribution

DSLR Digital single-lens reflex

EOR Enhanced oil recovery

GUI Graphical user interface

HI Horizontal injection

HP Horizontal production

ID Internal diameter

IOR Improved oil recovery

LDS Liquid dosage system

NDT Nondestructive testing

O/W Oil-in-water

OBIP Original bitumen in placeG

OD Outer diameter

OOIP Original oil in place

PA      Piston accumulator

PBS    Phosphate buffered saline

PC      Personal computer

PV      Pore volume

ROC    Reservoir-on-a-Chip

SAGD Steam assisted gravity drainage

SMTP Simple mail transfer protocol

sRGB Standard Red Green Blue color space

VI      Vertical injection

VP      Vertical production

W/O    Water-in-oil

WAE   Water-alternate-emulsion

WAG   Water-alternate-gas

# Chapter 1

## Introduction

### 1.1 Motivation

For at least the next decade, fossil fuels, such as gas and oil will remain the dominant energy source (Dresselhaus and Thomas, 2001; Omrpublic.iea.org, 2014). Gas and oil are typically trapped inside the naturally formed pores in a geological formation (referred to porous media). The process of oil recovery can be divided into three stages. The first stage is called primary recovery and the efficiency of oil recovery at this stage is controlled by the geological formation. The primary stage typically allows recovery of 5-15 % of original oil in place (OOIP) (Tzimas et al., 2005). The second stage of oil recovery which is usually a form of water flooding, provides an additional 30-35 % (Green and Willhite, 1998). The final stage is tertiary recovery which has potential for high oil recovery ( $\approx$  80 - 90 %). The last two stages require the application of pressure to the system.

Different research groups are working on the improvement of current tertiary methods that include thermal recovery, surfactant/polymer flooding, emulsion flooding, and CO<sub>2</sub> injection (Liu et al., 2007; Asghari and Nakutnyy, 2008; Shen et al., 2009; Alvarado and Manrique, 2010; Hart, 2013; Hein et al., 2013). These methods

allowed to achieve record levels of oil production (92 million barrels/day (mb/d)) ([Om-  
rpublic.iea.org](http://Om-<br/>rpublic.iea.org), 2014). Emulsion flooding is one of the improved oil recovery (IOR) and enhanced oil recovery (EOR) techniques used for oil recovery. Emulsion (oil-in-water or water-in-oil) produced *ex-situ* as a fuel source for industrial and commercial, utility, marine engines or boilers ([www.altpetrol.com](http://www.altpetrol.com), 2014) can be used either during the secondary stage coupled with water flooding or as independent flooding during the tertiary stage. Process of residual oil emulsification has established itself as an efficient method for enhanced oil recovery (Speight, 2006). It can be used for recovering heavy crude oil with gravity from 5° to 20° API (Speight, 2006).

Heavy oil reserves in Canada exceed a trillion barrels (Adams, 1982) and it was estimated that only 8 - 9 % of the OOIP were recoverable (Adams, 1982) with available technologies on the market in 1982. Improved technologies allowed increased production up to 15 - 20% (Hein et al., 2013; Larter and Head, 2014). Steam-assisted gravity drainage (SAGD) and cyclic steam stimulation are used to recover heavy oil from thin reservoirs (Hart, 2013; Arhuoma et al., 2009). However, most heavy oil is available in the northern territories of Canada. In the case of shallow oil, thermal recovery can damage the environment (Qiu and Mamora, 2010). There is a possibility for high-pressure steam escaping to the surface with resulted damage to the ambient environment. In opposite, emulsion flooding technologies can already be used in proximity to the permafrost without possibility damaging a surface with a steam (Qiu and Mamora, 2010). However, there is a potential effect on nature from possible spills and usage of fresh water during oil production. These effects must be considered before attempting field trials.

Emulsions are mixtures of oil and water which can be obtained through the application of energy through mixing or friction (Schramm, 2006, p. 138). The essential parameters of emulsions are its type, *i.e.* water-in-oil (W/O) or oil-in-water (O/W), droplet size distribution (DSD), rheology (Newtonian or non-Newtonian fluid), and apparent density ( $\rho$ ). It is of great importance to obtain these parameters during the production of the emulsion and keep them constant during its lifetime since they influence the efficiency of emulsion flooding (Wasan et al., 1978). The stability of the emulsion can be controlled by surfactant or by variation of DSD (Schramm, 2006, p. 138-139). Emulsion, which was used in this study, is a product of Quadrisse Canada Inc. under brand name E<sup>2</sup>GOR. Their technology allows to tailor parameters for any particular application, such as viscosity, hydrocarbon content, the drop size distribution, chemistry and stability.

Emulsions can be used to decrease mobility of the injected fluids (extrusive liquid) or to block highly permeable zones (McAuliffe, 1973; Mandal et al., 2010a). Core flooding experiments can be used to provide information on the emulsion flooding process (Samanta et al., 2012; Moradi et al., 2014). The surfactant added to the emulsion reduces the interfacial tension of the produced fluid when it interacts within the porous media with oil (Kumar et al., 2010). Oil will be recovered first from small pores in water-wet reservoirs where these small pores are connected to each other and will create a highly permeable zone through which water can flow (Schramm, 2006, p. 268). This can be compared to the emulsion produced from crude oil which consists of the high viscous drops. These drops require higher critical pressure to squeeze and move through and out from the pore head. With known size of the pores, a designed emulsion can be produced with known drop

size distribution which is sized to block zones of high permeability and to resist the pressure of the injected fluid. Hence, injected liquids are forced to flow through the low permeable zone and recover additional oil.

[Decker and Flock \(1988\)](#) carried out experiments and showed that emulsions are efficient in emulsion blockage mechanism. Also, emulsions have viscosities higher compared to water and allow higher capillary numbers to be generated. Higher capillary numbers describe the presence of higher viscous forces in pores that allow mobilization of the oil drops in the porous media ([Moradi et al., 2014](#)). [Mandal et al. \(2010a\)](#) concluded that emulsion flooding is more efficient as a displace fluid compared to traditional water flooding because of improved mobility ratio as a result of increase in viscosity of the displacing fluid (emulsion). However, [Cobos et al. \(2009\)](#) pointed out that understanding of this process requires further pore-scale studies.

To move from pore-scale to macro-scale to investigate and understand how the emulsion phase interacts within the porous structures of the reservoir and the efficiency of this process, laboratory core flooding experiments are required. Laboratory core flooding experiments include investigation of reservoir parameters. Every newly introduced method for oil recovery requires testing experiments with different flow patterns, well configurations and field parameters. For instance, one dimensional (1D) core holders allow the study of linear flow patterns and obtain initial parameters, such as porosity, permeability, efficiency for oil recovery and set effective flow rates and can provide initial understanding for oil recovery mechanism during emulsion flooding ([Hadia et al., 2007a](#)). Mechanisms involved in emulsion flooding, the increase of the mobility of injected fluids or the blockage

of highly permeable zones, can be investigated with 1D core flooding experiments. Based on parameters obtained during 1D studies, such as pressure drop, the amount of oil recovered after induction emulsion into the system, it would be possible to investigate the mechanism of the emulsion for EOR.

Understanding of emulsion flooding process at the tertiary stage, its interaction with oil saturated porous media in multi-dimensional experimental studies has also been considered as another part of the research. A two dimensional (2D) core holder allows investigation of how the front of the flooding agent spreads through the porous media. A 2D core holder represents a sectional cut of a real reservoir. It is thin enough to assume that the flow is distributed in two directions only and there is no influence (flow) in the third direction. A 2D core holder highlights the effects of well configurations (Santosh et al., 2007, 2008) and strata (Chaudhari et al., 2011a) providing data on emulsion distribution in two directions and its interaction with the porous media. Based on obtained data, the type of emulsion can be specified. There is a significant number of studies showing how to increase oil recovery during water flooding by configuring wells in appropriate orientations (Chaudhari et al., 2011a; Bagci and Gumrah, 1992; Hadia et al., 2007b). Consequently, it is essential to study the dependency of wells configuration during emulsion flooding to determine their effect on the efficiency of recovery. Taking pictures from one side of the 2D visualization cell provide a map for oil, water and emulsion saturations and velocity of emulsion flood front. Another side of the core holder can be equipped with pressure sensors to provide pressure mapping analysis for the *in-situ* processes.

Core flooding experiments with emulsion flooding experiments have been performed by different research groups (Qiu and Mamora, 2010; D'Elia-S and Ferrer-

G, 1973; Walstra, 1993; Mandal et al., 2010b; Guillen et al., 2012; Kumar et al., 2012). A dominant part of these research studies have focused on ultimate oil recovery with an emulsion formed *in-situ* (D'Elia-S and Ferrer-G, 1973; Walstra, 1993; Kumar et al., 2012). Flooding agents (e.g., surfactant (Samanta et al., 2012; Kumar et al., 2012; Bryan and Kantzias, 2009; Krumrine and J.S., 1983)) present in injected fluids emulsify trapped residual oil and form *in-situ* emulsion. Only a limited number of studies are available for *ex-situ* produced emulsion (Moradi et al., 2014; Mandal et al., 2010b; Guillen et al., 2012; Qiu, 2010; Nogueira et al., 2013). Experimental setups for both types of emulsion followed a traditional design for core flooding studies.

During emulsion flooding experiments, multi-phase flows are present in the system and the experimental setup design has a significant influence from this. The amounts of injected and produced liquids have to be analyzed, as well as the pressure along the system has to be recorded. Emulsion has physical properties close to oil and water and conventional techniques for real-time effluent analysis, such as segregation method (Qiu and Mamora, 2010), use of visual cells or use of an ultra-sound separators (Boye et al., 2008) are not feasible. This leads to complex post-experimental analysis, such as Dean-Stark analysis, mass balance calculations with liquid-liquid separation to obtain amount for each phase collected from the system. Qiu and Mamora (2010) recently used these calculations and showed that around an additional 20 % of OOIP was recovered during emulsion flooding. Similar results were obtained by Mandal et al. (2010a). They, also, showed that additional 20 % of OOIP was recovered during emulsion flooding. The obtained numbers highlight the potential for emulsion flooding; however, the slow and com-

plicated post-experimental analysis slows down the progress of these types of studies. Thus, it is necessary to develop a system with on-line volume measurements of each phase.

During the past twenty years, control and measurement technologies have stepped forward and brought a wide range of new devices to the market. Their usage allows the development of a system to provide an extended range of measured parameters and improve experimental control. This allows the development of a system for core flooding studies. In order to avoid routine post-experimental procedures it may be possible to develop analysis equipment for the downstream effluent. This equipment would analyze the flow and coupled with data from upstream and downstream mass flow meters gives the values for recent drainage. Online information would potentially lead to the exploration of new regimes of three-phase relative permeability curves relevant to a particular EOR technique. Developing experimental setup to study enhance oil recovery considers as a part of the study, to provide facility for understanding emulsions' potential in oil recovery process.

## **1.2 Thesis objective**

The main objective of this study is to contribute to the global understanding of emulsion flooding by studying the process of enhance oil recovery with emulsion as flooding agent. The aim is to investigate the technical feasibility of using emulsion as recovery agent and to develop efficient method for using in a field. Present study does not include an economical analysis of the emulsion flooding process and mainly focuses on efficiency. It is worth emphasizing that the results of this research can be used to develop theory for emulsion flooding using *ex-situ* produced

emulsion and to guide field engineers during field trials.

The reservoir is a region of porous medium with pores and capillaries. In order to efficiently recover the oil, it is necessary to understand what traps oil within the reservoir. Conditions of the reservoir after and during the first two recovery stages impact the parameters of tertiary oil stage. It is important to know these conditions and the physics behind them. The second chapter of this thesis focuses on understanding the conditions and the physics of emulsion flooding in porous media and provides required background.

A literature review of existing experimental systems and a review of current technologies is described in details in Chapter 3. Based on obtained results, a system has been designed, procured, constructed, commissioned, and initial experiments with emulsion flooding were carried out, details are available in Chapter 3. Also, as a result of performing routine experiments, the method for effluent analysis based on the data from a mass flow meter has been developed and tested. In addition, the traditional design of the biaxial core holder has been modified to reduce internal dead volumes during flooding and improve flow stability.

A hypothesis of alternative flooding technique efficiency is proposed and tested and compared to the the previously accomplished traditional floodings in Chapter 3. As a result of these experiments, water-alternate-emulsion (WAE) flooding technique has been established to enhance oil recovery. The optimal ratio for the emulsion and water slug during flooding has been outlined in Chapter 4. This chapter also outlines the internal interactions involved in emulsion flooding. The results and analysis from Chapter 3 and 4 have been published as two journal papers ([Baldygin et al., 2014a,b](#)). The initial concept of the experimental system

has been presented during conference in 2012 ([Baldygin et al., 2012](#)). Results from Chapter 4 has been also published as conference paper ([Baldygin et al., 2014c](#)).

The proposed hypothesis that efficiency of emulsion flooding from well configurations was studied using 2D core holder and resulted analysis presented in Chapter 5. It includes flood front analysis, the influence of well configurations, and pressure mapping during emulsion flooding for perforation of wells oriented either vertically or horizontally. For instance, vertical injection - vertical production (VI - VP), vertical injection - horizontal production (VI - HP), horizontal injection - horizontal production (HI - HP) well configuration are tested. The 2D core holder allowed flow visualization through a single transparent side of the holder and to collect pressure data using pressure ports on another side for future pressure mapping. Using inspectional analysis, results are interpreted for reservoirs, so that industry can estimate costs and prognoses effects from emulsion flooding on oil recovery.

Chapter 6 summaries the work that has been done in current research project and also provides recommendations for future studies that can be undertaken in a field of emulsion flooding.

Additional details about the 1D and 2D core holder design procedure are given in Appendix A-1. An error analysis for equipment involved during experiments and post-experimental procedures is included in Appendix A-2. A comparison between complete and incomplete 2D core flooding experiment is shown in Appendix A-3. Source codes which were used for image analysis and pressure mapping in Chapter 5 are given in Appendix A-4 and Appendix A-5, respectively. A complete set of drawings for core holders and software flow chart with source code are presented in Appendix A-6, Appendix A-7 and Appendix A-8, respectively.

# Chapter 2

## Oil recovery background

The physics of fluid flow through porous media has been studied for a long period of time. Porosity, permeability, relative permeability, capillary pressure, fluid saturations and mobility ratios need to be understood, as these parameters represent relevant rock properties (Darcy, 1856; Athy, 1930; Towler, 2002). Also, it is important to know the nature of oil and water content within the reservoir. In order to be consistent in the core flooding experiments with emulsions, understanding of physical properties and the type of emulsion in use should be considered. Parameters that influence the production of emulsions with distinct functional properties and experimental procedures that effect on results are discussed below.

### 2.1 Porosity of Sand Pack

Porosity ( $\phi$ ) of sand pack depends on a packing density. Total bulk volume ( $V$ ) of the pack is a sum of grain volume ( $V_s$ ) and pore volume ( $V_p$ ). Pore volume indicates the amount of void space of the rock. Porosity can then be defined as (Athy, 1930):

$$\phi = \frac{V - V_s}{V} = \frac{V_p}{V} \quad (2.1)$$

Porosity plays an important role in core flooding experiments, as OOIP occupies only the pore volume. Also, it is important to indicate effective pore volume ( $V_{eff}$ ), as void space ( $V_v$ ) that is connected to each other forming flow channels (Towler, 2002; Edward W. Washburn, 1921). In general for experimental work it is important to be consistent in packing of the core by using sand with the same grain density ( $\rho_g$ ) and grain size distribution from experiment to experiment in order to compare results. Once it is proved that output results are valid; sand can be replaced for future studies.

## 2.2 Permeability of Sand Pack

In 1859, Darcy performed experiments utilizing sand packs with different orientations (Dake, 1998, p. 100),(Darcy, 1856). The pressure loss was measured across the pack with known flow rate for the given fluid. Consider a general case when sand pack can be oriented either vertical or horizontal and pressure at the inlet and outlet is measured. Taking into account that sand pack can be offset from a reference ground level the following equations for hydraulic head can be written:

$$H_{in} = z_{in} + \frac{p_{in}}{\rho g} \quad (2.2)$$

$$H_{out} = z_{out} + \frac{p_{out}}{\rho g} \quad (2.3)$$

where  $H_{in}$  and  $H_{out}$  are hydraulic head at the inlet and outlet, respectively;  $z_{in}$  and  $z_{out}$  are elevations for porous media at the inlet and outlet, respectively;  $p_{in}$  and  $p_{out}$  water pressure measured by pressure sensors at the inlet and outlet, respectively.

Taking geometry and measured flow rates, Darcys equation is defined as:

$$Q = -K \frac{(H_2 - H_1)}{\Delta l} \cdot A \quad (2.4)$$

where  $K$  is the hydraulic conductivity, which depends on fluid and porous media,  $\Delta l$  is the length of porous media,  $A$  is the cross section of porous media and  $Q$  is discharge from the porous media. Dividing left and right parts of the equation by cross section area, the Darcy flux ( $q$ ) can be defined as:

$$q = -K \frac{dH}{dl} \quad (2.5)$$

Hydraulic conductivity can differ for different sand packs. Consider a homogeneous porous media, where the hydraulic conductivity is constant throughout the sand pack such that  $K(x, y, z) = C$ . Otherwise, it is required to introduce a matrix for hydraulic conductivity for three axis, as:

$$\mathbf{K} = \begin{pmatrix} K_{xx} & K_{xy} & K_{xz} \\ K_{yx} & K_{yy} & K_{yz} \\ K_{zx} & K_{zy} & K_{zz} \end{pmatrix} \quad (2.6)$$

Consequently, for three dimensional porous media equation for Darcy flux in general form would be:

$$\bar{q} = - \begin{pmatrix} K_{xx} & K_{xy} & K_{xz} \\ K_{yx} & K_{yy} & K_{yz} \\ K_{zx} & K_{zy} & K_{zz} \end{pmatrix} \begin{pmatrix} \frac{\delta H}{\delta x} \\ \frac{\delta H}{\delta y} \\ \frac{\delta H}{\delta z} \end{pmatrix} \quad (2.7)$$

In the current studies, two different sand packs are used. A 1D horizontal pack with the assumption that there is no effect from gravity forces and a 2D pack with

the absence of penetration in the third direction. Also, the following assumptions for Darcys law are made:

- the media is homogeneous
- the fluid is incompressible
- the flow is single phase
- the flow is happening in isotropic media

Darcys law can also be written for 1D in  $x$ -direction in the following way:

$$q = -\mathbf{K} \frac{dH}{dx} \quad (2.8)$$

or

$$q = -\frac{kA}{\mu} \frac{dp}{dx} \quad (2.9)$$

where  $k$  is absolute permeability for the porous media. For 2D, the third components for  $z$ -direction vanishes:

$$\bar{q} = -\mathbf{K} \begin{pmatrix} \frac{dH}{dx} \\ \frac{dH}{dy} \end{pmatrix} \quad (2.10)$$

The equations written above are valid for single phase flow only. However, it is possible to apply Darcys law to multiphase flow. To do this it is necessary to introduce a relative ( $k_r$ ), effective ( $k_e$ ) and phase permeabilities ( $k$ ) (absolute) (Towler, 2002; Buckley and Leverett, 1941). Absolute permeability should be measured on samples which were saturated with a single phase using Darcys law for single phase which is defined as:

$$k_a = -\frac{q\mu}{A} \frac{dx}{dp} \quad (2.11)$$

where  $\mu$  is the dynamic viscosity of the fluid. For instance, if the water occupies 100% of the pore volume, the measure permeability -  $k_{wa}$  is the absolute permeability to water. Same can be undertaken for other fluids, such as gas -  $k_{ga}$ , oil -  $k_{oa}$  or emulsion -  $k_{ea}$ .

An emulsion flooding experiment begins with a water saturated pack. Consequently, absolute permeability needs to be measured for pure water flooding through a water saturated sample. Once a new fluid is introduced to the system, effective permeabilities for each phase  $k_{we}$ ,  $k_{oe}$ ,  $k_{ee}$  would be designated. The values are going to be less than their absolute. The ratio of the effective permeability to the absolute permeability gives relative permeability, as follows:

$$k_{or} = \frac{k_{oe}}{k_{wa}}, \quad k_{er} = \frac{k_{ee}}{k_{wa}}, \quad \text{and} \quad k_{wr} = \frac{k_{we}}{k_{wa}} \quad (2.12)$$

For instance for two-phase oil/water flow the relative permeability can be written as ([Buckley and Leverett, 1941](#)):

$$k_{or} = \frac{\left[ \frac{q_o \mu_o}{A} \frac{dx}{dp} \right]_{S_w}}{\left[ \frac{q_o \mu_o}{A} \frac{dx}{dp} \right]_{S_w=0}} = \frac{(q_o)_{S_w}}{(q_o)_{S_w=0}} \quad (2.13)$$

The error in values of relative permeabilities depends on selected absolute permeability. When three phase (e.g. water, oil and emulsion) flooding takes place, three phase relative permeability is in use. Direct experimental investigation of three phase relative permeability properties requires measuring the fluid saturation distribution along the length of the core. Advanced technologies are required to un-

dertake this. Instead of completing three phase relative permeability experiments, two sets of two phase experiments can be carried out (Stone, 1970, 1973). Two sets refer to the use of oil-water and oil-gas systems for oil, water and gas three-phase flooding. For emulsion flooding, it is an oil-water and oil-emulsion set. Based on obtained relative permeabilities, oil to water,  $k_{row}$ , in water system and oil to emulsion,  $k_{roe}$ , in emulsion system, oil relative permeability is determined for three-phase system using rough prediction as:

$$k_{ro} = k_{row} \cdot k_{roe} \quad (2.14)$$

In the future, in case of successful development of effluent analysis equipment, the simultaneous three phase flow takes place and using the obtained numbers for saturations, ternary diagrams (Corey et al., 1956) can be plotted. Wyllies correlations (Wyllie, 1961) can be taken into account to obtain an accurate results. Wyllie proposed equations for relative permeabilities in case of wetting and non wetting phases (Wyllie, 1961). Equations for water-wet system in case of cemented sandstone, vugular rock, or oolitic limestone can be possibly used in emulsion flooding considering an emulsion as a gas phase in equations.

## 2.3 Saturation

Fluid saturation is a ratio of the fluid volume that occupies the pore volume by a particular phase (water, oil or emulsion). Water saturation,  $S_w$ , is defined as:

$$S_w = \frac{V_w}{V_p} \quad (2.15)$$

where  $V_w$  is the pore volume occupied with water. This is also an important parameter that effects EOR performance. The number of saturations parameters present in the systems depends on the number of fluids present in the porous media. Thus, saturation of water, oil and emulsions take place in emulsion flooding named as  $S_w$ ,  $S_o$ ,  $S_e$ , respectively for water, oil and emulsion. The sum of the three equals to one such that:

$$S_w + S_o + S_e = \frac{V_w}{V_p} + \frac{V_o}{V_p} + \frac{V_e}{V_p} = 1 \quad (2.16)$$

During core flooding experiments, there are also several other important parameters, such as irreducible water saturation and saturation for immobile oil, to be determined as:  $S_{wi}$ ,  $S_{or}$ . Irreducible water saturation is obtained during initial oil saturation process. It shows the amount of water that cannot be reduced further by displacing water with oil, displacing process. While, immobile oil shows the amount of oil that cannot be recovered from porous media at the end of oil recovery stages.

## 2.4 The physical Process of Oil Recovery

In order to understand the recovery process and why applied pressure is needed, consider single drop behavior in a pore as shown in Figure 2.1. The capillary force keeps oil inside the pores during secondary recovery. During secondary and tertiary recovery injected fluids are intended to overcome capillary pressure which is defined as using Young-Laplace equation:

$$P_c = \frac{2\gamma\cos\theta}{r_{pore}} \quad (2.17)$$

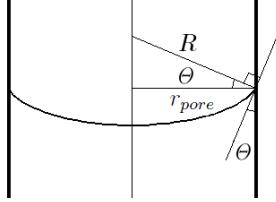


Figure 2.1: A schematic of the concept of a single pore with trapped oil (contact angle is less than 90°).

where  $\gamma$  - interfacial tension;  $\Theta$  - contact angle;  $r_{pore}$  - is the pore radius, as defined in Figure 2.1

In the case of two pores located above the same free water level, capillary pressure, contact angle and interfacial tension will be the same. This means that for water-wet pores the amount of oil in percentage to pore size relation will be greater for large pores than for small pores ([Schramm, 2006](#)). Consequently, oil will tend to recover from small pores first for water-wet ([Schramm, 2006](#), p. 269). The opposite situation is for oil-wet pores. Oil will tend to recover from large pores and the amount of oil is greater in small pores. A schematic of a single oil drop which is sitting on a pore is shown in Figure 2.2. In order to squeeze and move the drop through the pore (in other words recover the drop), pressure difference across the drop should be applied. ([Nazzal and Wiesner, 1996](#)) termed it as the critical pressure ( $P_{crit}$ ) at which drop starts moving. From the Young-Laplace equation (capillary force) ([Green and Willhite, 1998](#), p. 18), ([Nazzal and Wiesner, 1996](#); [Leverett, 1940](#)), they derived:

$$P_{crit} = \left( \frac{2\gamma_{o/w}}{r^*} \right) - \left( \frac{2\gamma_{o/w}}{R^*} \right) \quad (2.18)$$

where  $r^*$  and  $R^*$  are radii shown in Figure 2.2 and  $\gamma_{o/w}$  is the interfacial tension between two fluids, oil and water. Radius,  $r^*$  can be found from:

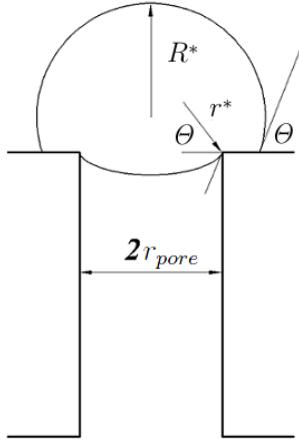


Figure 2.2: Oil drop is sitting on the throat of pore (following Nazzal et al. (Nazzal and Wiesner, 1996)).

$$r^* = r_{pore} / \cos \theta \quad (2.19)$$

An advantage of using emulsion as an extrusive liquid is that it contains surfactants which reduce the interfacial tension between the two fluids. Thus, the critical pressure required for oil recovery is reduced and the amount of recovered oil increases.

Another important parameter for oil recovery is the capillary number (Washburn, 1921) which describes the ratio of the viscous and interfacial forces in the form:

$$N_c = \frac{\eta v}{\gamma \phi} \quad (2.20)$$

where  $\eta$  is viscosity of displacing fluid;  $v$  is the velocity of the displacing fluid;  $\phi$  is the porosity; and  $\gamma$  is the interfacial tension. At the beginning of a water flooding process, the capillary number can be around  $10^{-6}$  (Schramm, 2006; Moore and Slobod, 2013). When residual oil mobilization begins the capillary number

would be around  $10^{-5}$ . Typical chemical flooding, *e.g.* presence of surfactant in flood front, regime would lie into the range from  $10^{-5}$  to  $10^{-3}$ . The end of oil recovery brings the capillary number to range from  $10^{-3}$  to  $10^{-2}$ . Consequently the capillary number changes as the remaining percentage of oil inside reservoir is lowered (Schramm, 2006; Foulser et al., 1991). Romero et al. (2011) developed a network model of flow of oil-water emulsion through porous media. It was shown that during the process of emulsion flooding capillary number ranges from  $10^{-6}$  to  $10^{-2}$ .

The process of emulsion flow through sand is similar to the process of oil recovery. Emulsion is a mixture of droplets of one fluid in another. Similar physics can be applied for an emulsion with assumption that emulsion is a single phase fluid.

## 2.5 Mobility

Mobility can be derived as a ratio of relative permeability of a fluid to viscosity of the same fluid. Using the term mobility, defined as (Homsy, 1987):

$$M_{ro} \text{ for oil phase} = \frac{k_{ro}}{\mu_o} \quad (2.21)$$

$$M_{rw} \text{ for water phase} = \frac{k_{rw}}{\mu_w} \quad (2.22)$$

$$M_{re} \text{ for emulsion phase} = \frac{k_{re}}{\mu_e} \quad (2.23)$$

The mobility ratio is another important parameter defined as a ratio of oil mobility to water mobility for water-oil system:

$$\lambda = \frac{M_{ro}}{M_{rw}} \quad (2.24)$$

or as a ratio of oil mobility to emulsion mobility for emulsion-oil system:

$$\lambda = \frac{M_{ro}}{M_{re}} \quad (2.25)$$

If it is less than or equal to one, the process of oil recovery is characterized as “stable displacement” (Homsy, 1987; Schowalter, 1965). For mobility ratio greater than one, the process of oil recovery suffers from unstable displacement and other processes such as fingering can occur (Homsy, 1987; Schowalter, 1965). Mobility control is a key component for effectiveness of oil recovery. French et al. (1986) demonstrated that temperature and water dilution resistant emulsion with appropriate size can be formed and used for blocking mechanism. It allows to modify permeability of the porous media and improved mobility control. Hence, the mobility of emulsion can have a wide range and be matched for a given sand pack (Speight, 2006).

## 2.6 The Composition of the Fluids

The ultimate goal for core flooding experiments is scaling to the real reservoir. Results obtained in experiments should correlate to oil recovery in a field. Thus, it is important to take into account for the composition of oil and water and other important species content.

Fluid composition also affects oil recovery and emulsion stability. The water present in sandstone reservoirs has major cations and anions, such as Na<sup>+</sup> and Cl<sup>-</sup> (Schmidt, 1973). Their content can vary with a depth with a rate of 30,000 mg/l Na<sup>+</sup> per 1,000 ft and 45,000 mg/l Cl<sup>-</sup> per 1,000 ft down to 3,000 ft (Schmidt, 1973). Bagci et al. (2001a; 2001b) reported the results of brine flooding tests using a core flooding system and showed that brine composition affects oil recovery. The

increased amount of salt reduces the amount of recovered oil from reservoir oil. Higher pH can be achieved with lower salinity for brine composition. The pH level was stabilized at 7.2, 7.4 and 6.8 for 2 wt %, 5 wt % and 10 wt % CaCl<sub>2</sub>, respectively after 1.0 pore volume of injection ([Bagci et al., 2001a](#)). [Yildiz et al. \(2013\)](#) identified that 16 % difference in an oil production can be as a result of using different brine compositions, e.g. Brine 1 (4 % NaCl + 0.5 % CaCl<sub>2</sub>) is more efficient than Brine 2 (2 % CaCl<sub>2</sub>). Also, in consolidated/unconsolidated limestone samples there may be a reduction in permeability when the critical salt concentration in brine is achieved ([Bagci et al., 2001a](#)).

The stability of emulsion also depends on fluid composition. [Moradi et al. \(2011\)](#) studied the stability of water-in-oil emulsion prepared with a crude oil and a synthetic reservoir water. It was shown that emulsion becomes unstable at higher salinity (1, 10 and 50 % water salinity values were examined). The base 100 % solution was a composition of NaCl, CaCl<sub>2</sub>, Na<sub>2</sub>SO<sub>4</sub>, MgSO<sub>4</sub> and TDS.

## 2.7 Production of the Emulsion

The process of emulsion production is termed emulsification and contains different physical processes. [Walstra \(1993\)](#) divided the process into three main categories: deformation coupled with possible break up; adsorption and transportation of surfactant to newly developed droplets; and bouncing and merging of drops. For the petroleum industry, there are two options to create emulsions *in-situ*, inside the reservoir, or *ex-situ*, outside in a process facility. Direct injection of alkali/surfactant (AS) solution after water flooding into porous media can result in emulsion formation ([Kumar et al., 2012](#)). Salt concentration and alkali concentration affect emul-

sion formation (Kumar et al., 2012; Perles et al., 2012). Another method is to use higher velocities and more efficient emulsifiers to increase shear stresses *in-situ* and form emulsion (Sarma et al., 1998).

Outside process facilities can also be used to prepare emulsion using oil, water and surfactants. Warmed heavy oil can be added to hot water premixed with surfactant and mixed using an industrial mixer. Another way would be circulating the fluid through a jet at a set volume rate with a centrifugal pump outside of reservoir (McAuliffe, 1973). Another procedure, the aqueous-phase solution and oil-phase solution can be prepared separately and stirred using a homogenizer (Son et al., 2014).

During production, the emulsion can be specified to be stable or unstable. Stable emulsions have a constant drop size distribution, while unstable emulsion forms larger droplets. In the critical case, the two liquids can segregate and form creaming and generate flocculation (Schramm, 2006). In the case of drop size around 10–100 nm, drops are stable (Windhab et al., 2005; Binks, 1998); however for larger sizes coalescence can occur. Surfactants can be added into the mixture to reduce surface tension between oil and water to avoid droplet break-up for sizes in the range of 0.5 to 100 micrometers (Binks, 1998). In addition, McAuliffe (1973) pointed out that mineral surfaces, reservoir water salinities, and water hardness can break droplets. Mandal et al. (2010a) observed the influence of stirring speed of a three-blade propeller and time of mixing on a stability of emulsion. In the present studies, the emulsion is prepared prior to experiment with known drop size distribution viscosity, stability and water/oil ratio (WOR).

It is important to know and control the emulsion parameters. During emulsion

production, the energy input can indicate different emulsion properties. In order to connect the energy input to properties of the liquids, such as viscosity of the continuous phase and interfacial tensions, the Weber (*We*) number can be used and is defined as (Schramm, 2006, p. 59):

$$We = \frac{\eta_1 \dot{\gamma} R}{\gamma_{12}} \quad (2.26)$$

where  $\eta_1$  the viscosity of the continuous phase;  $\dot{\gamma}$  shear rate;  $R$  droplet radius and  $\gamma_{12}$  the interfacial tension. Values of *We* in laminar and turbulent flows are discussed in detail in (Walstra, 1993) and can be used during emulsion production. Dependence of *We* versus ratio of dispersed phase velocity and continuous phase velocity is shown in (Schramm, 2006).

The production an emulsion is not part of this project. However, understanding of this process is necessary for future reference during experiments. Quadrise Canada Corporation, a collaborator in the project supplied an emulsion for this project. Their emulsions manufactured under brand name E<sup>2</sup>EOR are stable and flexible in parameters. Their technology allows to tailor parameters for any particular application, such as viscosity, hydrocarbon content, the drop size distribution, chemistry and stability. The drop size can be controlled within a few hundred nanometers to less than 10  $\mu\text{m}$ . The amount of available emulsion was limited due to the closing down of the company in earlier 2012 resulted in a reduced number of experiments being carried out to test the hypothesis.

## 2.8 Scaling Analysis

Carrying out the experiments in the field can be expensive and sometimes is even impossible due to lack of the information about reservoir conditions. Core flooding experiments simulate reservoirs porous media with assumptions stated by researchers (similar to Darcys law assumptions). Based on the obtained results, the number of assumptions can be reduced to make the porous media closer to the reservoir conditions. During core flooding experiments different core holders are in use. Core holders can be 1D, 2D or even 3D. The experiments are performed using pre-set physical parameters. The ones obtained from experimental results should be presented in a way that makes them applicable to the actual field reservoir. Thus, these parameters and dimensions of a core holder have to be scaled from typical reservoir where the method being developed will be used. The dynamic and physical characteristics of the experiment and reservoir are required to be scaled up.

For instance, pressure and temperature are the same in both cases. However, the dimensions of the cells and flow rates of injected liquids are parameters for scaling procedure. In order to set the flow rate for the 1D core holder, the Willhite's scaling coefficient is used ([Willhite, 1986](#)). Empirical correlation for water flooding to estimate the stabilizing criteria has been developed using the dimensional analysis by [Rapoport and Leas \(1953\)](#). According to [Bagci et al. \(2001b, p. 90\)](#), “displacement data for linear floods were independent of length, rate of injection, and viscosity of the injected water when the numerical value of the scaling coefficient,  $Lu_t\mu_w$ , exceeded a critical value”, which is given as

$$Lu_t\mu_w = 5.85 \times 10^{-9} N \quad (2.27)$$

where  $u_t$  - total Darcy velocity in linear displacement, m/D (ft/D);  $\mu_w$  - water-phase viscosity, Pa·s;  $L$  - length of cell, m. In reservoir engineering, it is a common practice to use ft/D as a unit for the velocity of flood front. After determining all the variables with fixable units, the following equation was obtained:

$$q = \frac{0.00351 \cdot A}{L \cdot \mu_w}, \text{cm}^3/\text{min} \quad (2.28)$$

where  $d$  - diameter in 1D cell, cm;  $A$  - cross sectional area for 1D cell,  $\text{cm}^2$ . It was found that applicable flow rates for 1D core holder are within a range of 0.1 to 1  $\text{cm}^3/\text{min}$ . For the 2D core holder it is within a range of 1 to 1.75  $\text{cm}^3/\text{min}$ .

# Chapter 3

## A new laboratory core flooding experimental system<sup>1</sup>

### 3.1 Introduction

The oil and gas industry heavily relied on laboratory core flooding experiments, where a core pack, often unconsolidated sand particles (Santosh et al., 2007; Hadia et al., 2007b; Mandal et al., 2010b; Hadia et al., 2008a) or in some cases consolidated cores (sandstone and carbonate outcrops) (Hadia et al., 2007a; D'Elia-S and Ferrer-G, 1973; Hadia et al., 2012, 2008b), mimicking the porous natural reservoir, is traditionally flooded with an injection fluid and resultant output in terms of oil recovery is measured. Existing core flooding systems use this concept, which was introduced for the first time in early 1930's (Wyckoff and Botset, 1936). When the industry is exploring new options for flooding the existing oil fields abandoned after the primary recovery process (Tzimas et al., 2005), there is a need to produce more robust, automated system to reduce time associated with experimental and post-experimental analysis.

A critical solution is provided to this pressing need for the oil and gas indus-

---

<sup>1</sup>A version of this chapter has been published. A. Baldygin, D. S. Nobes, and S. K. Mitra, "A new laboratory core flooding experimental system", *Industrial & Engineering Chemistry Research*, DOI: 10.1021/ie501866e, 2014

try by providing a robust, versatile, precise and automated core flooding platform which can be tested for various types of reservoir conditions using some of the advancements in fluid controls and data processing and automation. For validation purposes for the developed system, initially experiments are conducted with water and paraffin oil only, water flooding. To anticipate the future performance of the core flooding system for potential enhanced oil recovery (EOR) studies, applicability of the system for flooding complex fluids, such as an emulsion, is also demonstrated here.

## 3.2 Traditional Core Flooding Systems

The traditional core flooding system, as described in the existing literature ([Hadia et al., 2007a](#); [Mandal et al., 2010b](#)), has three main sections: the upstream, the core block, and the downstream. The upstream supplies relevant fluids (saturation and flooding agents) to the core block typically using syringe pumps and piston accumulators (PA) to provide a controlled flow rate. The core block contains the porous media and often simulates the reservoir conditions which could include overburden pressure and a thermal jacket to maintain reservoir temperature. The downstream collects the effluent from the core block by using fraction collectors ([Nasralla et al., 2011](#)) or two-/three-phase separators ([Boye et al., 2008](#); [Legowo and Pratomo, 1999](#)), the analysis of such data often leads to the estimation of the efficiency of tested oil recovery method.

Components of the system are connected to a data acquisition module through which the user can communicate, which is referred here as a control module. Such experimental techniques work well for single phase fluids (such as water or oil)

and certain restricted two-phase systems (oil and water mixture as effluent from the production wells).

Table. 3.1 provides a summary of existing core flooding systems, used for academic research and industrial applications for research in oil and gas industry. It can be noted that most of the systems use syringe pumps coupled with piston accumulators (Samanta et al., 2012; Hadia et al., 2007b; Legowo and Pratomo, 1999; Nobakht et al., 2007) which limits the type of liquids that can possibly be injected into the core as the inner surface of the piston-cylinder assembly of the syringe pump is susceptible to corrosion. The piston accumulator size limits the volume of fluid that can be continuously injected during flooding experiments and *a priori* calculations need to be performed to determine the size and specification of the piston accumulator to undertake a given core flooding study.

Table. 3.1 also suggests that a fraction collector was used for the downstream section in significant amount of the core flooding systems, which resulted in discrete estimation of oil and water effluents for the recovery curves (Samanta et al., 2012; Hadia et al., 2007b; Mandal et al., 2010b). Also, post experimental analysis is required to analyze the fraction of each effluent phase collected in each tube (Mandal et al., 2010a; Hadia et al., 2007b) of the fraction collector. In some cases, an ultrasound separator has been used for the effluent collection and analysis (Legowo and Pratomo, 1999). It is an effective method for experiments with three-phase effluent fractions, where phases are distinctly different from each other. As an example, experiments which involve water/oil/gas flooding has three components that can be separated in effectively inside the column of the three-phase separator using ultrasound and later can be quantified by volume.

Table 3.1: Summary of existing core flooding systems used globally.

Author	Year	Upstream	Downstream	Used fluids
Hornof and Morrow	1987	Metering pump	n/a	Isooctane, brine, water and oil
Chang and Grigg	1994	Syringe pumps with PA	Multiport rotary valve with vials	CO <sub>2</sub> , brine, oil and surfactant solution
Legowo and Pratomo	1999	Displacement pump "Quizix", with PA	Fraction collector and separator	Water, oil and different microbial cultures
Bagci et al.	2001	Syringe pump	Fraction collector	Water, oil and different microbial cultures
Sedaee and Fariborz	2004	Displacement pump with PA	Effluent condenser with collector	Steam, CH <sub>4</sub> and heavy oil
Nobakht et al.	2007	Syringe pump with PA	Oil sample collector with gas flow meter	Crude oil and CO <sub>2</sub>
Hadia et al.	2007	Dual piston syringe pump with PA	Fraction collector	Oil and water
Mandal et al.	2010	Syringe pump with PA	Fraction collector	Oil-in-water emulsion, oil and water
Samanta et al.	2012	Syringe pump with PA	Fraction collector	Oil, brine and chemical slug
Veerabhadrapa et al.	2013	Syringe pump with PA	Effluent sample collector	Oil, water and polymer
Ko et al.	2014	Syringe pump with PA	Fraction collector with centrifuge tubes	Brine, oil and surfactant

These traditional core flooding systems need to be modified in order to make it more versatile in terms of using a wide range of flooding fluids such as surfactants, polymers and emulsions. Often in such scenarios, to calculate the various fluid volume fractions in real-time is needed which requires the inclusion of modern fluid handling systems to increase the functionalities of traditional core flooding system.

### 3.3 Developed Core Flooding System

A core flooding apparatus has been designed and constructed by taking into account the potential challenges related to a traditional core flooding system and the availability of new technology. This is a further modification to the initial conceptual design reported earlier ([Baldygin et al., 2012](#)). A schematic of the system is shown in Figure 3.1. This schematic shows the layout for the core flooding system, which is divided into three sections: the upstream, the core block and the downstream. This schematic was developed using diagramming software (Microsoft Visio, Microsoft, Co.) with a set of standard diagram elements. The fluid lines, control and data transfer lines are shown to guide the reader through the fluid and data flow.

The upstream side of the system provides continuous injection of three different types of liquids. It consists of fluid holding containers (carboys), pumps, and mass flow meters. Three carboys (E-1,...,E-3) are directly connected to three dual piston pumps (Smartline 100, Wissenschaftliche Gerätebau Dr. Ing. Herbert KNAUER GmbH) through 6.35 mm (1/4 in.) stainless steel tubes. The precision and accuracy of the upstream pumps at 12 MPa and for flow rate of 1 ml/min are equal to < 0.5 % and < 1.0 %, respectively. These numbers are close to the flow accuracy of

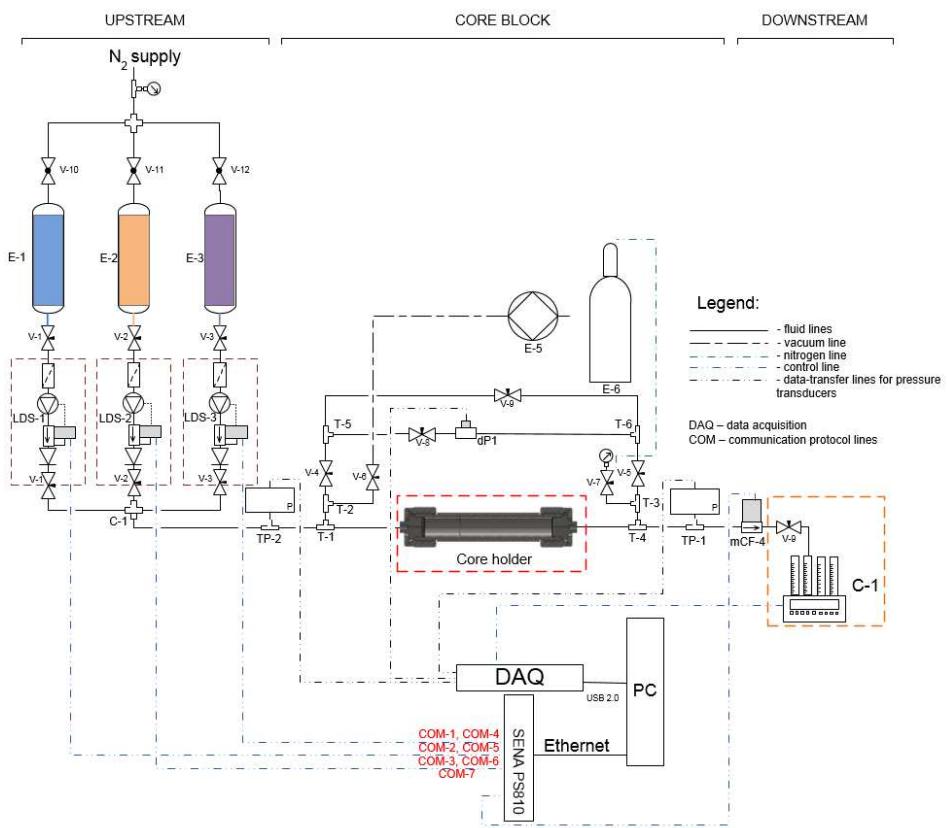


Figure 3.1: Schematic of the core flooding experimental apparatus.

a syringe pump. For example, 500D series pump (500D Teledyne Isco) has flow accuracy equal to 0.5 % of set point. In order to avoid cavitation at the inlet side of the pumps, the carboys are pressurized with nitrogen at 0.138 bar(g) (2 psig). Mass flow meters (M13, Bronkhorst Cori-Tech BV) are installed downstream of the pumps. Two of the mass flow meters are built of stainless steel, while one is made of Hastelloy to allow the use of salt (brine) water. According to the calibration certificates of the mass flow meters, the measurement error is  $\pm$  0.2% of the full-scale reading + 0.5 g/h. During the factory calibration procedure, density deviation was found to be 0.11 kg/m<sup>3</sup>, -0.16 kg/m<sup>3</sup>, -0.27 kg/m<sup>3</sup> and 0.01 kg/m<sup>3</sup> for water, oil, emulsion and downstream mass flow meter, respectively. The density measured using the three mass flow meters was compared with the one calculated using software (Bronkhorst High-Tech FLUIDAT<sup>®</sup>, Bronkhorst Cori-Tech BV) which defines physical properties of a fluid based on specific fluid temperature and pressure conditions with theoretical calculation methods. For example, with the water flow rate of 0.5 cm<sup>3</sup>/min for half hour (approximate time to fill a single test tube at the fraction collector) the error is  $\pm$  0.28 ml considering density of water at experimental conditions. Together with the pumps are coupled to check valves, they form the liquid dosage systems (LDS-1,...,LDS-3), which can keep constant mass/volume flow rate at a pre-set pressure.

There are three LDS in the current configuration to deliver water, oil and emulsion into the core block as needed. The LDS system can work simultaneously if it is needed for certain experimental conditions. In addition, the upstream has open access to refill the carboys to allow continuous injection of liquids for lengthy experimental runs. There is no need to stop an ongoing experimental run for refilling

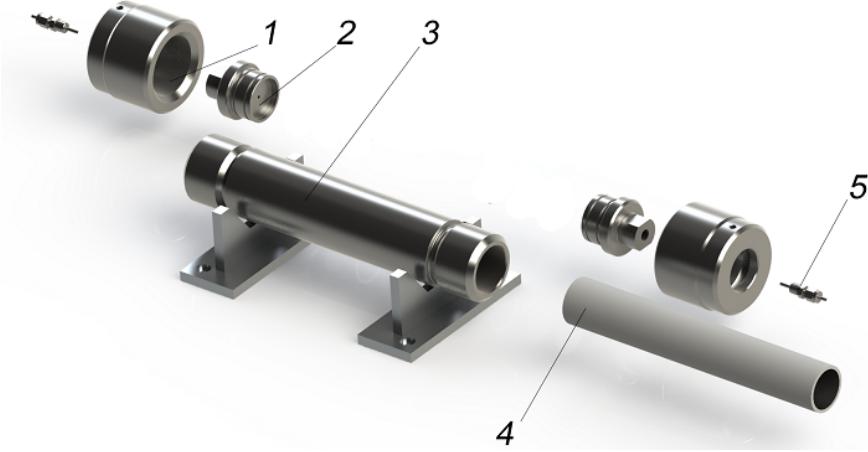


Figure 3.2: Exploded view of the core holder (1 - cap, 2 - end plug's body, 3 - body, 4 - internal surface, 5 - fitting 1/8 NPT to 3.175 mm (1/8 in.) tube).

purpose, which is a shortcoming in case of a traditional system with piston accumulators at the upstream side.

The core block consists of the core holder, in which the porous medium is usually packed which can be sand pack or samples, inline pressure sensors and differential pressure sensors. A biaxial horizontal core holder, shown in Figure 3.2, is used for containing and packing the medium. The core holder, shown here, is designed to perform one-dimensional core flooding experiments. However, any other two-dimensional ([Santosh et al., 2007](#)) or three-dimensional ([Hadia et al., 2007b, 2008a](#)) core holders, as and when available, can be plugged into the system through appropriate connections to 3.175 mm (1/8 in) stainless steel tube. The dimensions of the core holder used here as an example are: length: 284 mm (11.18 in) and diameter : 38.1 mm (1.5 in). This design incorporates minimal fluid leakage between the inner surface of the coreholder and the sand pack. At the same time, it also reduces the dead volumes at the inlet and outlet sides of the sand pack due to the modified entrance region, shown in Figure 3.3. The entrance region incorporates

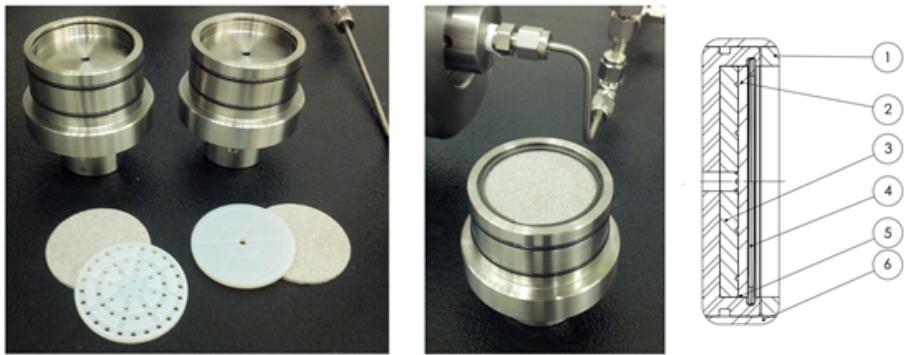


Figure 3.3: End plugs of the biaxial core holder. (a) - isometric view of end plugs; (b) - end plug assembled; (c) - cross section view of single end plug (1 - sandblasted internal surface, 2 - stainless steel filter, 3 - 3D-printed plate, 4 - strain ring, 5 - end plug's body, 6 - core holder's body)

modifications to the patents of [Stanley \(1984; 1985\)](#). It combines the geometrical configurations of both patents and thereby replaces/modifies the distribution plates as per current needs. A sand-blasted plastic tube is installed inside the core holder to prevent such fluid leakage. The distribution plugs, located at the two ends of the core holder, have built-in stainless steel media with mesh size of  $40 \mu\text{m}$  and 1.59 mm (1/16 in.) thickness and distribution plate printed using a 3D printing. This combination redistributes the liquid across the cross-section and reduces dead volumes.

The design for the distribution plates was optimized by performing separate simulation using commercial software (SolidWorks Simulations, Dassault Systemes SolidWorks, Corp.). In total, nine different configurations have been analyzed as a combination of three configurations for the end plug, which are shown in Figure 3.4, and four configurations for the distribution system, which are shown in Figure 3.5. Design of the end plugs shown in Figure 3.4 (b) and (c) bases on industry standard available in a core holders from two main manufactures (Core Laborato-

ries ([www.corelab.com](http://www.corelab.com), 2014a,b) and CORETEST Systems Inc. ([www.coretest.com](http://www.coretest.com), 2014)). Stainless steel filter, shown in Figure 3.5 (c), forms artificial porous media after perforated plate, shown in Figure 3.5, and helps additionally redistribute liquid before it goes into a sand pack. In addition, it provides sand control in a core holder. The cap with 9 holes, shown in Figure 3.5 (d) has internal thread and can be installed only on end plug with channels for flow redistribution. Thread allows to change orientation for holes with respect to the open channels and twist flow internally.

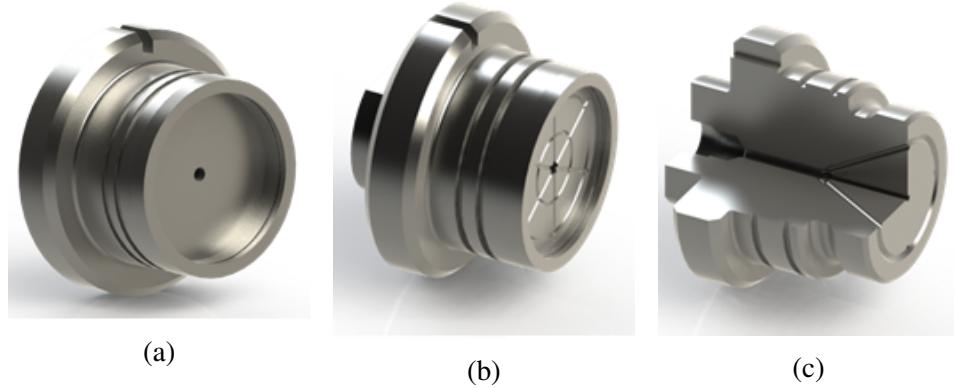


Figure 3.4: Variation of geometric configuration for end plug (a) single entrance, flat surface; (b) single entrance, grooves for flow distribution; (c) single entrance, channels for redistribution.

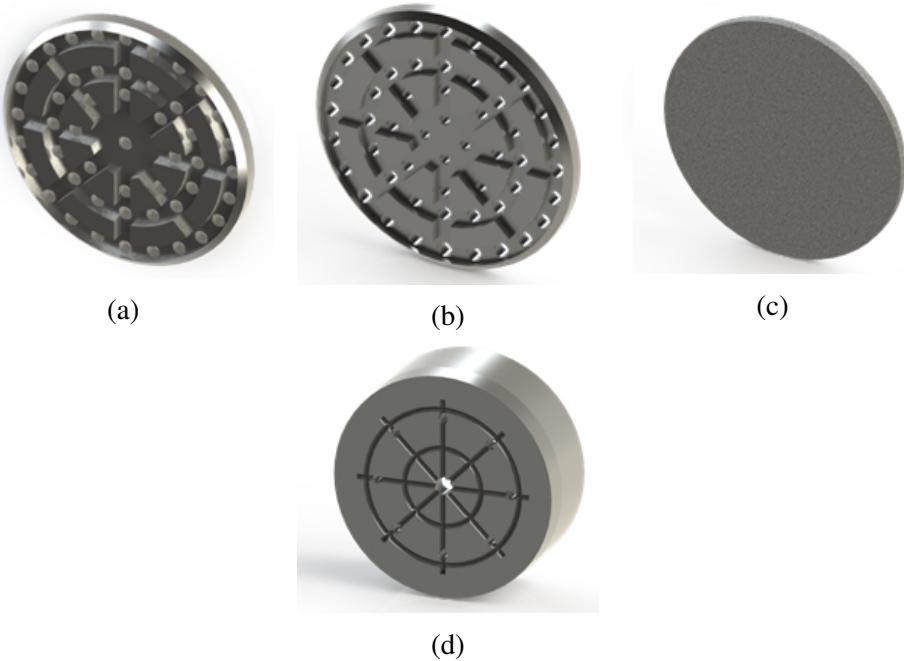


Figure 3.5: Variation of sub-components for end plug (a) perforated plate, single hole; (b) perforated plate, four entrance holes; (c) 40 micron stainless steel filter made of 316L SS; (d) cap with 9 holes and channels.

A comparison of the flow distribution between traditionally used and improved configuration is shown in Figure 3.6. The color map represents internal velocity through the cross section of the sand pack. Once the configuration was finalized particular attention was given to the size of the holes in the radial direction ([Stanley, 1984](#)). It was optimized to guarantee uniform flow distribution through the porous medium with known range of permeability and porosity.

For pressure monitoring, there are three pressure sensors (FP2000 series, Honeywell International Inc.), TP-2, TP-1 and dP-1, to measure the inlet pressure at the upstream, the outlet pressure at the downstream, and differential pressure across the porous media.

The downstream section has an effluent management system which allows it to quantify different fractions of effluents removed from the core block. The mass

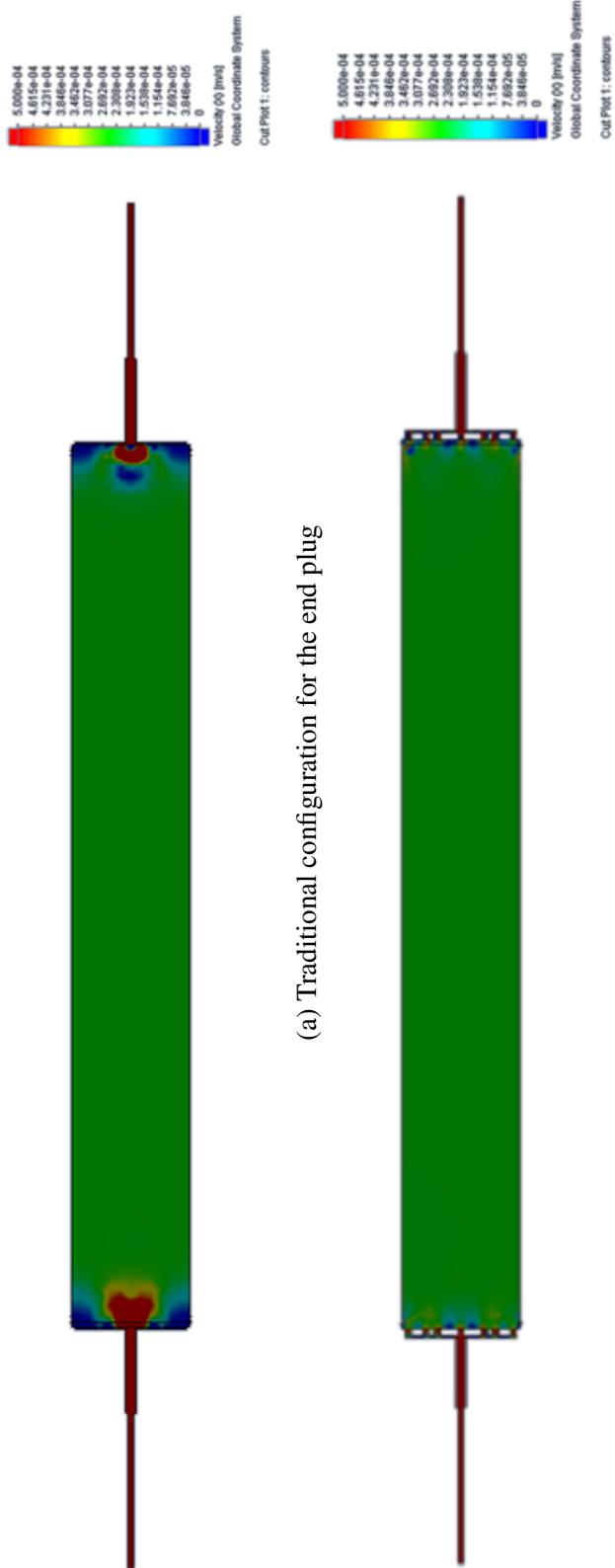


Figure 3.6: The horizontal velocity component distribution in the axial cross-section of the core holder obtained with different configurations of end plugs.

fraction of each component needed to be calculated to estimate the amount of oil recovered, which is often the ultimate goal for such core flooding system. The effluent management system has a mass flow meter and a fraction collector (CF-2, Spectrum Laboratories, Inc.). The fraction collector uses graded test tubes with 15 ml volume each. The error in a measuring volume of liquid collected in a test tube (430055, Cole-Parmer Canada Inc.), used for checking the effluent fraction data, is  $\pm 0.25$  ml. Since this error would be accumulated from sample to sample, the cumulative error in the oil production is around 6.5 ml (estimated based on expected number of test tubes in 1D experiments). The error bars incorporated for each data point in the recovery curves represent the error in measurements. Complete error analysis can be found in Appendix A-2. The mass flow meter (M13, Bronkhorst Cori-Tech BV) has the same specifications as that used for water flow, installed in LDS-1. The mass flow meter provides the flexibility to deal with effluents having different densities and it allows automatic evaluation of volumes of different effluent phases, the details of which are described later.

The experimental setup can be pressurized with nitrogen, E-6, and tested for leakage using soap-water, usually undertaken without the porous sand pack in place.

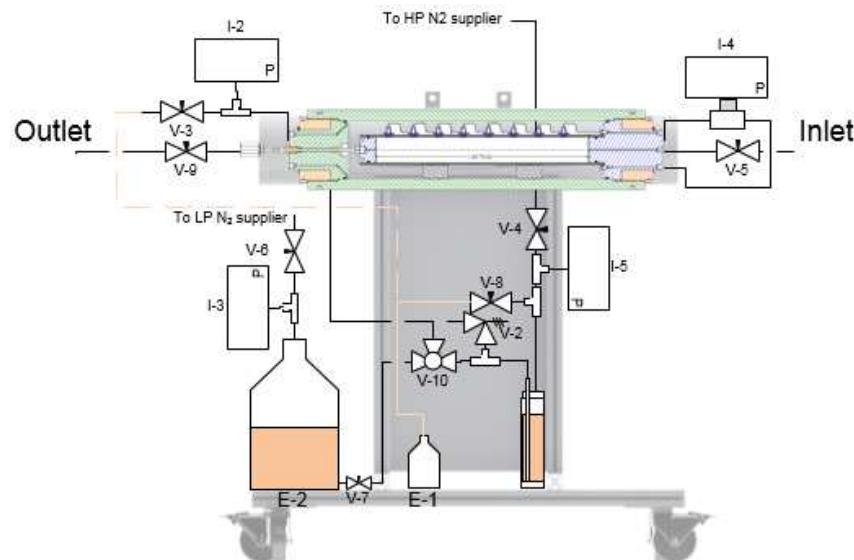
### 3.3.1 Core Flooding System Flexibility

The advantage of the developed system is that it is designed as a "plug-and-play" modular system. There is a possibility for further modification of the core block, which is only limited by the specification of the upstream pumps. The region highlighted with red dashed square in Figure 3.1 can be replaced with the sub-system, described in Figure 3.7(a), quite readily, or with a 2D core holder, used for experi-

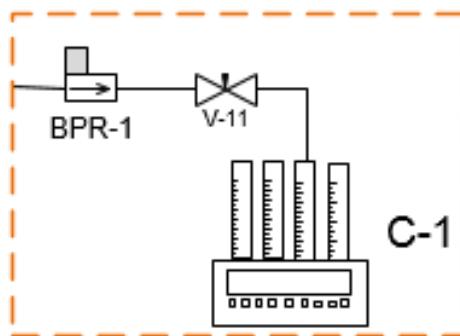
ments in Chapter 5.

Example of the subsystem, proposed in Figure 3.7(a), has a Hassler core holder ([www.corelab.com](http://www.corelab.com), 2014b) which allows the core to be maintained with a confining pressure up to 10,000 psi, to use actual cores previously extracted from reservoirs (outcrops) and to measure pressure drop across the core using eight tap-points. The confining pressure in the present configuration can be maintained using a high pressure N<sub>2</sub> line. This further can be replaced with either high pressure hand pump or a syringe pump. The temperature inside the core (or along its outer surface) can be measured using any of the eight tap-points of core's sleeve via thermocouples installed through the ports located on the end plug with appropriate pressure sealed feedthroughs (Series WF, Spectite Inc.). In order to maintain the temperature of the core block similar to reservoir conditions, the core holder can be placed inside an environmental chamber or an ultra-thin heat sheets can be mounted at the outer surface of the core holder covered with fiberglass pipe insulation. The chamber allows to maintain temperature up to 200 °C, whereas the heat sheets allow to maintain temperature up to 100 °C. The temperature can be controlled via programmable temperature PID controller with feedback from one or more thermocouples.

Similarly, the downstream section can be also modified to satisfy the requirements for the inline pressure. For example, a digital back pressure regulator (EL-PRESS P-712CV, Bronkhorst Cori-Tech BV) can be installed between downstream mass flow meter and fraction collector, as shown in Figure 3.7(b). It would allow to set the back pressure up to 103.4 bar(g) (1500 psig). These modifications to the core block and downstream section of the core flooding developed allow end-users to obtain the required parameters to mimic desired reservoir conditions.



(a) Core block



(b) Downstream section

Figure 3.7: Schematics of the further updates to the developed system.

### **3.3.2 Core Flooding System Limitations**

One of the limitations of the current system is that the produced water cannot be separated from the emulsion and re-injected back to the core block as a flooding fluid for further oil recovery. In order to utilize such produced water back into the flooding system, it would be required to install additional components at the downstream to separate emulsion, paraffin oil and water. Such separation of oil/water emulsion can be done using traditional membranes ([Chen et al., 2009](#)) or more recently through the use of microfluidics devices ([Fidalgo et al., 2008](#)).

### **3.3.3 Remote Control**

In order to minimize human intervention and have robust control on the experiment, software with a graphical user interface (GUI) was created for the entire system using a commercial environment (LabWindows CVI, National Instruments Inc.). This software allows user to control and track different components during the experiment, save data and analyze various experimental conditions. A commercial data acquisition (DAQ) system (cDAQ-9172, National Instruments Corp.) with onboard control modules for pressure sensors and fraction collector is used for data acquisition. In addition, the mass flow meters and pumps are connected to a universal eight port device server (PS 810, Sena Technologies, Inc.) which transfers and receives signals from personal computer (PC) through an ethernet network.

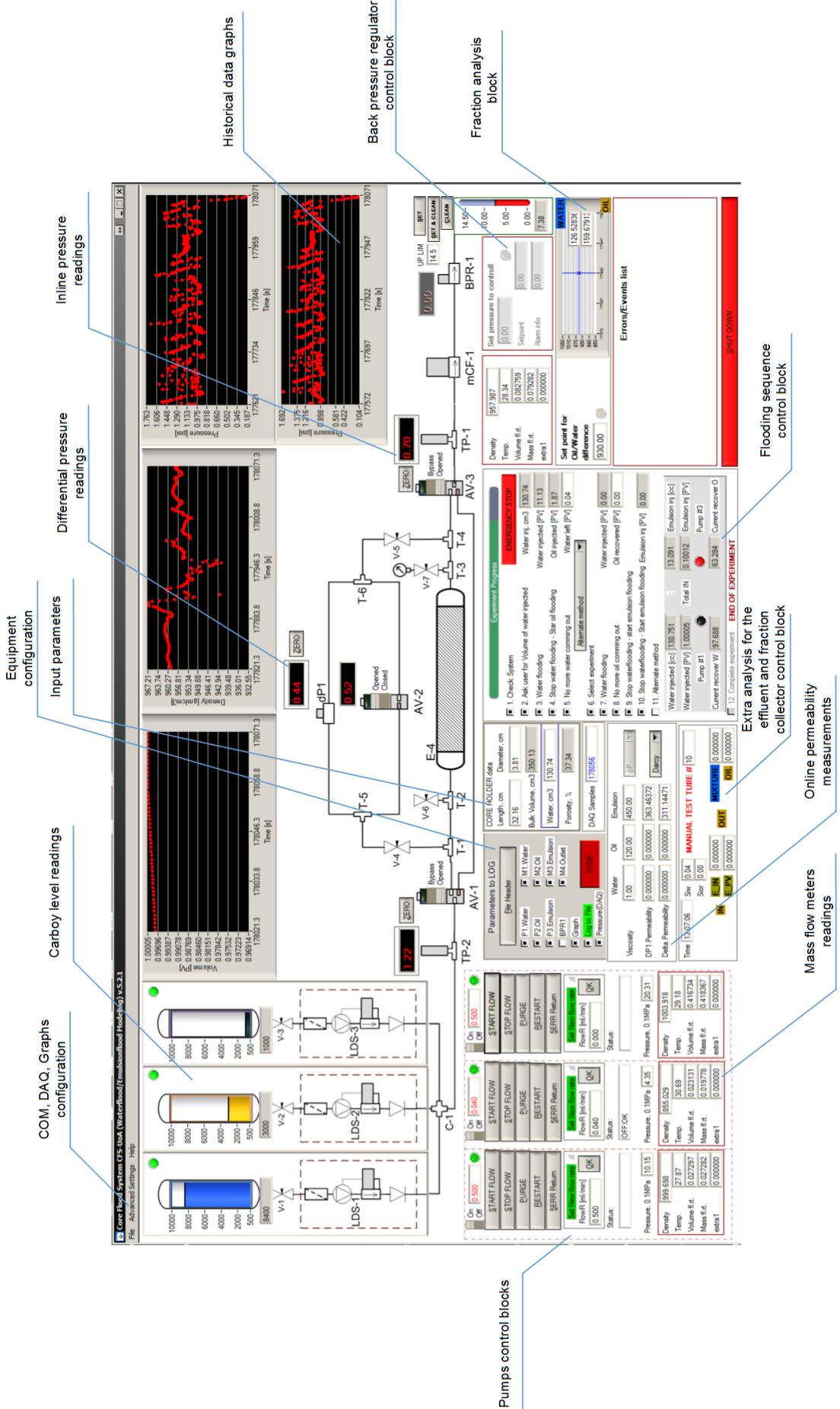


Figure 3.8: A graphical user interface to perform automation for the core flooding system.

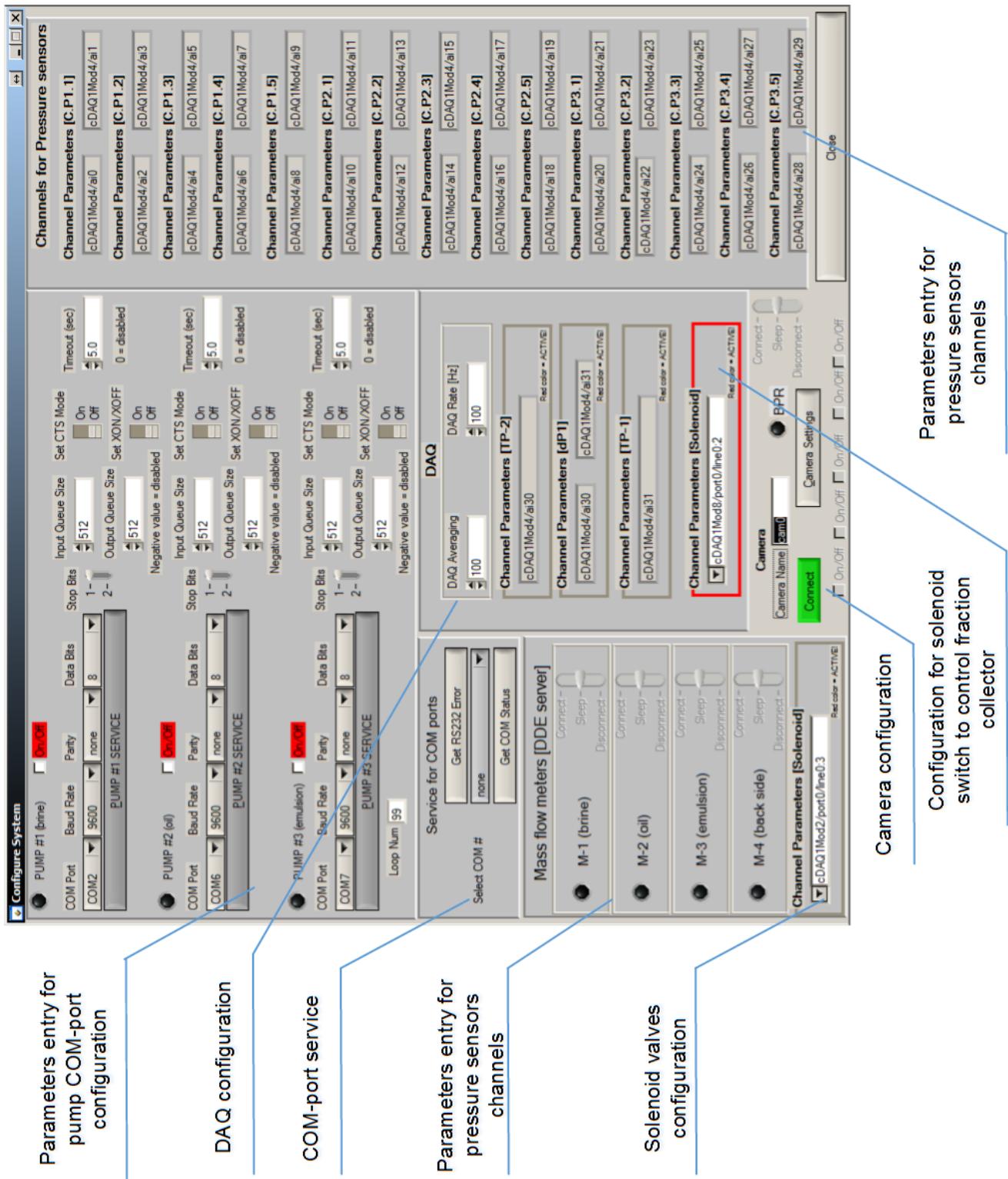


Figure 3.9: A graphical user interface to perform configuration for the core flooding system.

The developed GUI interface is shown in Figure 3.8. Similar to the experimental setup, it can be divided into three sub-sections: the upstream, the core block and the downstream. There are components for controlling different processes of experiment, load/save configuration parameters, saving data, monitor effluent properties, pressure and other parameters involved in each run. The developed software allows to monitor system in real time. There is a possibility to run experiments in “auto” operating mode using the developed logical structure. Figure 3.9 shows the GUI which was developed to configure individual components of the system.

### 3.4 Materials and Specifications

Using the developed core flooding system, both traditional core flooding using water as a flooding agent (secondary recovery process) and emulsion flooding using *ex-situ* produced emulsion (enhanced oil recovery) were performed. In this section, the details of different materials used during this experimental validation process for the core flooding system along with standard data extraction in the form of porosity and permeability of the core pack used for each flooding experiment are provided.

During 1D core flooding experiments, the injection rate was set at  $0.5 \text{ cm}^3/\text{min}$ . The core flooding temperature was at the room temperature of  $22^\circ\text{C}$  for all experiments. Distilled water (DI) produced from a water purification system (PURELAB Ultra, Elga Labwater, LLC) was used for the water flooding to obtain and to maintain initial water saturation. Paraffin oil (CAS Number 8012-95-1, Sigma-Aldrich Co. LLC) with viscosity of  $130 \text{ mPa}\cdot\text{s}$  at  $25^\circ\text{C}$  and density of  $868 \text{ kg/m}^3$ , measured by the mass flow meter (M13, Bronkhorst Cori-Tech BV), was used for oil saturation processes. The *ex-situ* emulsion used in this study was oil-in-water (70.75

wt% oil and 29.25 wt% water with average oil drop size of 2.46 micron. The stable emulsion was made of heavy-oil, which is distinctly different than the resident oil (paraffin oil) in the sand pack. Density and viscosity of the emulsion are 1014 kg/m<sup>3</sup> and 495 mPa·s at 100 s<sup>-1</sup> shear rate at 25°C ([Patrick Brunelle \(Quadrise Canada Corp.\), 2012](#)), respectively. Since the chosen emulsion is heavier than water and oil, it can be hypothesised that the downstream mass flow meter can detect each phase separately. By setting reference points for density of each phase in the developed software and using on-line measurements from the mass flow meter, fluid fraction-tracking software can be developed. Hence, the system can be further modified to eliminate the need for test tubes.

For each experiment, the sand (dry water-wet silica sand from Ottawa IL sand deposit with US sieve size# 10 (100-140), 53-251 µm) was weighted prior to the packing inside the core holder. The mass of the sand used for each pack was recorded to be 557 gm and was consistent from experiment to experiment with 1.5 % of deviation. The procedure for packing the core was as follows. The sand with a known mass was packed inside the void volume of the core holder (324 cm<sup>3</sup>) using a vibration table (VP-181, FMC Technologies) with the vibrator controller (Syntron Power Pulse AC, FMC Technologies) set at maximum level. The core holder with one opened end, containing the inner plastic tube, was placed vertically on the vibration table. The sand was poured inside the core holder continuously up to the top of the internal tube. The core holder was kept for 5 minutes on a powered table to let the sand settle and form a dense medium. A rod with diameter equal to the internal diameter of the plastic tube was used to compress the sand to produce a dense pack.

Table 3.2: Properties of the sand packs

Pack	Porosity, % by water/ by mass measurements	Pore volume , cm <sup>3</sup>	Absolute permeability, Darcy	Permeability with residual water, Darcy	Residual water saturation after oil saturation $S_{wi}$
Run #1	37/35	113.4	10.2	6.25	0.02
Run #2	36/36	116.0	19.8	11.2	0.18
Run #3	37/35.8	115.9	11.3	6.30	0.06
Run #4	35.8/33.4	108.1	11.3	7.90	0.06

Each pack was characterized for porosity and permeability, which were obtained prior to each flooding experiment. The obtained data are shown in Table 3.2. In order to obtain a porosity value (pore volume) for each pack, a vacuum pump (117, Labconco Corp.) was connected to the inlet side and a vacuum gage was connected to the outlet side of the core holder. The core holder was evacuated to 4 kPa absolute (28.74 in. mercury gauge or 1.18 in. mercury absolute) over half of an hour. Then the vacuum pump was disconnected and a tank filled with known volume of water,  $V_{kv}$ , was connected to the core holder and allowed to flow of water into the core holder. The remaining volume,  $V_{rem}$ , of water in the tank was recorded using a double metric scale glass cylinder (250 ml Brand 3025, Pyrex). From these measurements, the volume of water occupied by the pore space can be calculated using a modified Eq. 2.1, which provide the value of the porosity of the sand pack:

$$\phi = \frac{V_{kv} - V_{rem}}{V} \quad (3.1)$$

In addition, the porosity was calculated using the mass of packed sand, void volume inside the core holder and bulk density of silica sand ([Systems, 2014](#)) (2.65 gm/cm<sup>3</sup>). Pore volumes (PV), the volume of fluid within the packed core holder, were in the range from 113.4 to 120.0 cm<sup>3</sup>.

For each pack, the permeability was obtained using three different methods: with nitrogen, water and finally, with residual water saturation during oil flooding.

The absolute permeability was first found using nitrogen immediately after dry sand was packed in a core holder. The mass flow controller with built-in pressure sensor was connected to the inlet and a pressure sensor was installed at the outlet of the core holder. At different flow rates of nitrogen, the pressure difference was recorded. The absolute permeability was found using the Klinkenberg equation ([Klinkenberg, 1941](#)):

$$K_g = K_l \left( 1 + \frac{b}{P_m} \right) \quad (3.2)$$

where,  $K_g$  is the gas permeability, mD;  $K_l$  is the liquid permeability, mD;  $b$  is the Klinkenberg factor, Pa; and  $P_m$  is the mean absolute pressure, Pa.

The absolute permeability with water as the working fluid was calculated for water saturated pack using Eq. 2.11. Prior to obtaining permeability measurements with residual water saturation, the oil saturation process was carried out using paraffin oil. The oil was injected into the water saturated pack with a constant injection rate of  $0.5 \text{ cm}^3/\text{min}$  for 1 PV of injection; thereafter, the injection rate was increased to  $1.0 \text{ cm}^3/\text{min}$  for an extra 0.5 PV of injection, until the residual water saturation,  $S_{wi}$ , was reached (see Table 3.2). At the end of the process, the flow rate was reduced back to the  $0.5 \text{ cm}^3/\text{min}$  and the permeability was calculated using Eq. 2.11. The effluent stream was collected in batches in test tubes. The volume of water and oil collected were compared to the injected one and used to obtain values for residual water saturation, shown in Table 3.2. Porosity and permeability measurements showed that sand packing process was consistent for all one dimensional experiments experiments.

## 3.5 Experimental Validation of the Core Flooding System

### 3.5.1 Effluent Management System

The comparison of different flooding strategies in terms of oil recovery depends on the underlying physical processes in terms of the displacement of the resident oil phase by the invaded flooding agent. At the pore-level flooding strategies can be evaluated using a Reservoir-on-a-Chip (ROC) ([Gunda et al., 2011](#)) type system. However, on a macro-scale, where integrated cumulative measurements take place, it is important to estimate the volumes of respective phases through a reliable effluent management system. Thus, it is important to calibrate and ensure that the downstream stream is measuring both the volume of water and oil for the effluent streams in developed system. In developed core flooding system, two different approaches for the downstream analysis were utilized. The fractions collected into the test tubes with fraction collector were analyzed using mass flow meter data at first and later through visual inspection of test tubes.

In order to record the volume of each phases, the effluent flow through the mass flow meter was analyzed. A density reference point,  $\rho_{ref}$ , was set at  $935 \text{ kg/m}^3$  for measurements during the four runs, corresponding to different flooding experiments. This reference point was selected based on initial calibration runs with paraffin oil and DI water. As the liquid flows through the downstream mass flow meter during a single time step,  $t_{step}$  ( $\approx 1$  second), the density,  $\rho_{record}$  ( $\text{kg/m}^3$ ) and the current volume flow rate  $Q_{cur}$  ( $\text{cm}^3/\text{min}$ ) were recorded. Based on these quan-

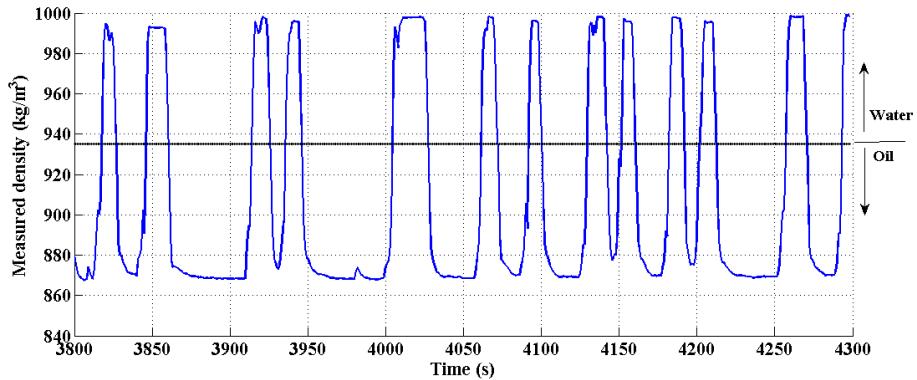


Figure 3.10: An example of density measurements at the effluent side during core flooding experiment.

tities, the fluid volume for a given phase,  $V_{j,rec}$  ( $\text{cm}^3$ ), was calculated as:

$$V_{j,rec} = \frac{Q_{cur} * t_{step}}{60}; \quad j = \text{oil or water} \quad (3.3)$$

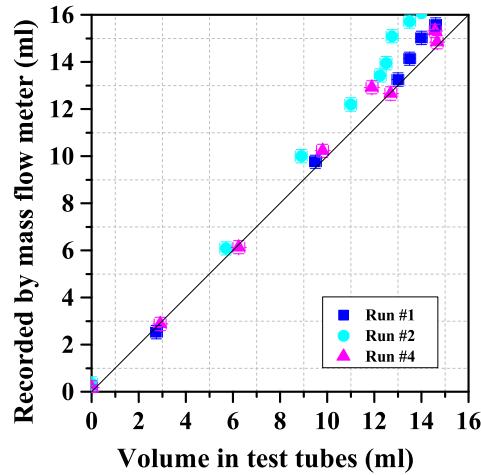
An example of density measurements at the effluent side is shown in Figure 3.10. If the density was larger than the reference level  $\rho_{ref}$ , the recorded volume (Eq. 3.3) was added to the water value  $V_{water,rec}$  and the oil value  $V_{oil,rec}$  was kept unchanged. Otherwise, it was vice versa. This approach was also used for emulsion flooding experiments, where the values above the reference level represented water and emulsion phases.

In total four runs - two water flooding experiments (Run #1 and Run #2), direct emulsion flooding (Run #3), and finally water flooding followed by emulsion emulsion flooding (Run #4) have been performed. For this purpose, the fractions of the effluent were collected into the test tubes and compared to the recorded volumes from the mass flow meter data and are shown in Figures 3.11 and 3.12. The error bars correspond to the error in mass flow meter and fraction measurements (the complete error analysis is available in Appendix A-2). The vertical axis here shows the total volume of each liquid recorded by the mass flow meter and the hor-

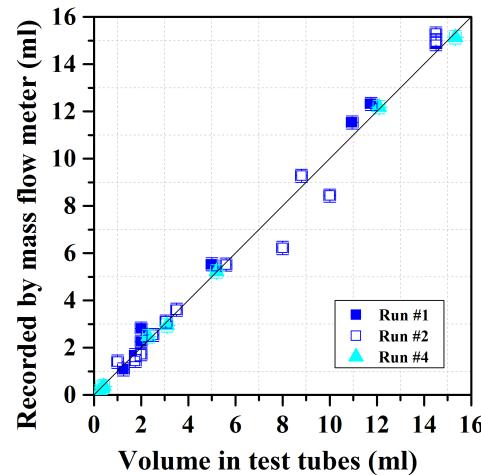
izontal axis represents the total volume collected in test tubes. Each test tube could be either filled with single liquid or can have multiple liquids, e.g. oil and water. Consequently, points on the graphs could be in a range from 0 to 15 ml. The diagonal line in these figures provides the measure of the data accuracy between two measurement techniques.

Figure 3.11 contains data points obtained during the process of water flooding for different runs, including one where the emulsion flooding was followed after the water flooding step (Run #4). Data points for produced water, shown in Figure 3.11 (a), follow the  $45^\circ$  line trend. Figure 3.11 (b) shows the similar trends for the recovered oil in the effluent stream. This highlights that measurements from the mass flow meter can be used for online determination of the effluent fraction.

Results obtained for the two emulsion flooding methods are presented in Figure 3.12. In Figure 3.12 (a) the results of produced mixture of emulsion and water are depicted and Figure 3.12 (b) shows the volume of recovered oil measured by the two techniques. Even though it can be observed a strong correlation between the two measurement techniques for certain measurement range, this is not true for the entire range of measured data, as was the case for Figure 3.11. In both cases, data correlation between the two measured techniques is not as strong compared to the water flooding results shown in Figure 3.11. This suggests further calibration for different regimes are required to increase the accuracy level(due to the limited amount of available emulsion, this has not been done in this research study). The worst deviation from the  $45^\circ$  line trend was found to be  $\pm 22\%$ .

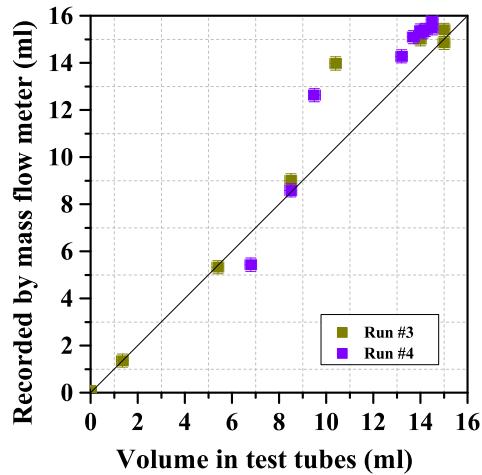


(a) Produced water

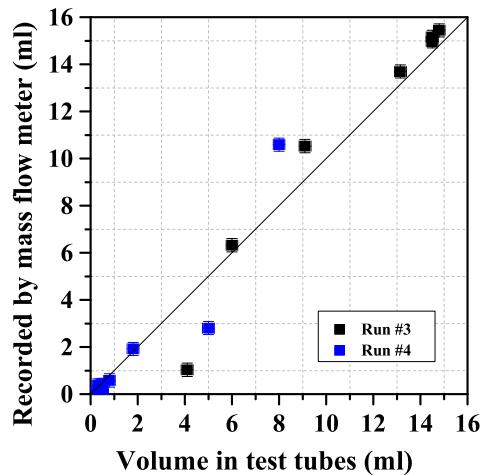


(b) Recovered oil

Figure 3.11: A comparison of data obtained from mass flow meter and test tube fractionation during water flooding. The vertical axis - recovered mixture/oil recorded by mass flow meter, the horizontal axis - recovered mixture/oil measured with test tubes.



(a) Produced mixture of emulsion and water/only water



(b) Recovered oil.

Figure 3.12: A comparison of data obtained from mass flow meter and test tube fractionation during emulsion flooding. The vertical axis - recovered mixture/oil recorded by mass flow meter, the horizontal axis - recovered mixture/oil measured with test tubes.

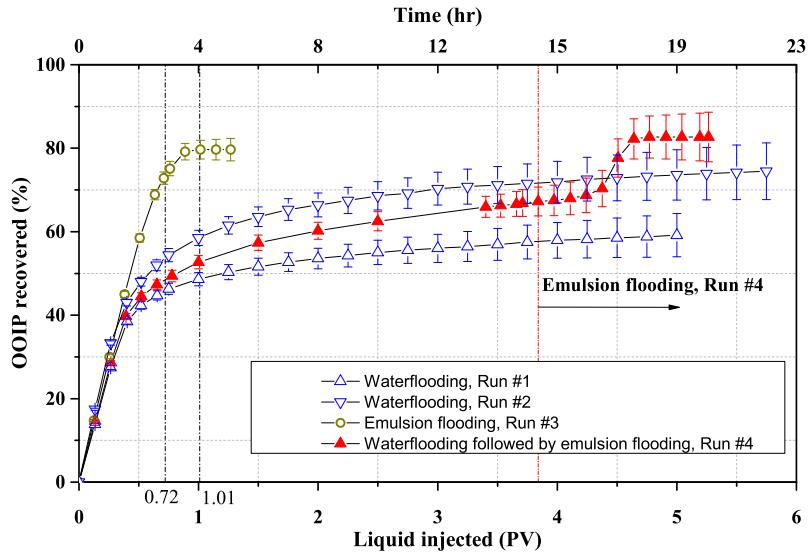


Figure 3.13: Recovery comparison for studied cases: Run #1 and Run #2 - water flooding, Run #3 - direct emulsion flooding and Run #4 - water flooding followed by emulsion flooding.

### 3.5.2 Core Flooding Experiments

Once the effluent management system is properly characterized and tested, the core flooding system was used to perform different flooding experiments. 19 to 22.5 hours are required to complete single experiment at a selected flow rate. Having reliable software with a graphical user interface allowed to run system overnight. The recovery curves for each set of flooding experiment is shown in Figure 3.13. Each recovery curve represents the cumulative oil production during single run/experiment. The presented data was obtained using determined volumes from test tube fractionation which were matched to the data collected from the effluent mass flow meter. Points used to plot recovery curves are collected from the test tubes analysis. The upstream and downstream mass flow meters supplemented mass balance calculations. It can be observed that the first two water flooding runs ended with recovery around 60% and 75% for Run #1 and Run #2, respectively. The water appeared at

the effluent side (breakthrough point) for Runs #1 and #2 occurred at 0.3 and 0.24 PV of injected displacement fluid, respectively. The obtained numbers were similar to the published data for unconsolidated sand packs with porosity around 30-40 % and permeability from 1.1 to 3.4 Darcy (Hadia et al., 2007b; Mandal et al., 2010b; Hadia et al., 2008a). It was observed that after 2 PV of injection of water, the ultimate recovery increased by only 6% and 8% for Run #1 and Run #2, respectively. Loose sand pack in Run #2 with higher absolute permeability compared to Run #1 resulted in higher oil recovery during water flooding. The data suggests that the pore volumes used in the experiments and the corresponding increase in the recovery are similar to the field applications (Dake, 1998, p.364). Alternate injection strategy must be incorporated to have economic recovery rate. Hence, instead of continuing with water flooding beyond a certain PV, emulsion was introduced to the system at 3.7 PV in Run # 4.

For Run #3, the emulsion was used as a primary flooding agent for the oil saturated porous media. As observed from Figure 3.13, the emulsion flooding alone produced larger oil recovery compared to water flooding for the same PV of injection. During the emulsion flooding almost 60% OOIP was recovered after injecting only 0.5 PV of emulsion. The total oil recovery was 79% OOIP at 1.25 PV of injection. From 1.01 PV of injection, additional oil recovery was not observed for Run #3. From the effluent analysis it was identified, that the breakthrough for this case happened at 0.72 PV of emulsion injection. Such a high efficiency of the emulsion flooding compared to the water flooding could be due to delayed breakthrough and having its viscosity similar to the viscosity of the paraffin oil. Emulsion saturated front moves steadily through porous media due to low viscous ratio between the

displaced and the displacing fluids (Doorwar and Mohanty, 2011).

For Run # 4, the complete water flooding experiment was carried out up to 3.7 PV of water injection. The recovery curve follows a similar trend to the Run #1 and Run #2, as is shown in Figure 3.13. At 3.7 PV of water injection, emulsion was introduced to the porous media as post water flooding process to enhance oil recovery. The total oil recovery was found to have increased. An additional 15 % of OOIP was recovered. The emulsion injection beyond 4.6 PV did not displace additional oil from the sand pack. Based on effluent collected into test tubes at the effluent side, similar to the Run #3, the emulsion saturated front moves steadily through a porous media. Complete understanding for the emulsion flooding process can be obtained by ceasing experiments and analyzing sand packs afterward. The residual oil saturation at the end of the Run #4 is around 18 %, which is similar to that in case of Run #3 with emulsion flooding only. It is to be noted that even though emulsion floodings (both Run #3 and Run #4) produced additional oil recovery ( $\sim 20\%$  OOIP), it required an amount of emulsion close to single pore volume to achieve such high recovery.

## 3.6 Conclusion

A core flooding experimental setup has been constructed to improve on the existing system which has been in use for several decades. The developed setup allows to test enhanced oil recovery techniques in more efficient time manner. The system was equipped with the up-to-date techniques and hardware available in fluid measurement systems. An automated effluent analysis incorporating properties (mass flow rate and density) measured by mass flow meters has been developed. This

allowed the replacement of the traditional fraction collector in the downstream section for online determination of effluent composition. The entire experimental setup is also monitored and controlled through a custom built software.

The core flooding experiments with unconsolidated sand packs as a medium has been performed for validation purpose. To understand the applicability of the system, emulsion (oil-in-water) used as a flooding agent, as an example of advanced technique for enhanced oil recovery. Here, two different strategies for emulsion flooding have been demonstrated - direct injection of emulsion (Run #3) and water flooding followed by emulsion flooding (Run #4). It has been shown that the engineered emulsion worked effectively as an independent flooding fluid and Run #3 produced 79% OOIP recovery at 1.2 PV of injection. Also, emulsion worked effectively as a substitute fluid after the water flooding in Run #4 and added an extra 15% OOIP to the total oil recovery at the cost of an additional 0.93 PV of emulsion injection. Comparison between these two runs suggests that, Run #3 was effective in terms of the time needed for the oil to be recovered from the porous media, while Run #4 was effective in terms of the emulsion used for the oil recovery process.

These core flooding experiments demonstrate that this newly developed core flooding system is capable of performing both the traditional water flooding and more advanced enhanced oil recovery process using *ex-situ* obtained emulsion as a flooding agent. This system can be used for academic research purpose using different types of core holders with various combinations of injection and production wells and at the same time can be adopted an industry bench mark to perform routine core studies and has a high potential of replacing the existing core flooding systems.

# **Chapter 4**

## **Water-Alternate-Emulsion (WAE): A new technique for enhanced oil recovery<sup>1</sup>**

### **4.1 Introduction**

Existing literature suggests, that the oil and gas industry has faced a challenge working with produced water for EOR, where the goal has been to minimize the overall water injection inside the oil reservoirs. Processes were formulated where water/steam and another immiscible fluid were injected simultaneously to reduce the overall water footprint for oil recovery. Good examples of such processes are cyclic steam simulation (CSS) and water-alternate-gas (WAG) flooding ([Alvarado and Manrique, 2010; Shah et al., 2010; Luo et al., 2013; Huang and Holm, 1988](#)). In the case of CSS, the cyclic process requires around a month to implement and involves three stages: steam injection, soaking of the steam into the heavy oil formations and oil production by natural flow or by artificial lift ([Shah et al., 2010; Scott, 2013](#)). This cycle can be repeated till the oil production rate becomes uneconomic.

---

<sup>1</sup>A version of this chapter has been published. A. Baldygin, D. S. Nobes, and S. K. Mitra, “Water-Alternate-Emulsion (WAE): A new technique for enhanced oil recovery”, *Journal of Petroleum Science and Engineering*, DOI:10.1016/j.petrol.2014.06.021, 2014

nomical (Shah et al., 2010). For WAG, different ratios for water to steam slugs for each cycle have been investigated, *e.g.* 2:1, 3:1, 4:1 and even 10:1 (Shah et al., 2010; Luo et al., 2013; Huang and Holm, 1988; Bagci and Tuzunoglu, 1998; Tüzenoglu and Bagci, 2000; Christensen et al., 2013). An increase in production was recorded up to 37% or even higher during cycling different slugs in a laboratory coreflooding system (Tortike, 1991). In order to further improve the WAG flooding technique an alternative technology was developed referred as chemical-augmented WAG (CAG), which replaced steam slugs with water-miscible chemical (alkali/surfactant/polymer) slugs (Luo et al., 2013).

All these mentioned techniques, *i.e.*, CSS, WAG, CAG, etc., are referred as enhanced oil recovery for processes. CSS can achieve 60 % higher recovery of original bitumen in place (OBIP) compared to the steam assisted gravity drainage (SAGD) in the Clearwater formation (Scott, 2013). CO<sub>2</sub> - CAG allows to recover 71.07 % OOIP compared to CO<sub>2</sub> - WAG with 54.25 % OOIP at the same experimental conditions (Luo et al., 2013). WAG field experience shows an increase in oil recovery from 0.7 to 37 % of OOIP (Christensen et al., 2013). However, replicating these enhanced oil recovery processes with emulsion and water slugs, particularly when such emulsion is produced *ex-situ* from hydrocarbon sources quite different from the *in-situ* resident oil phase within the pores, remains to be explored. Only one study has been reported on sequential emulsion flooding (Guillen et al., 2012), where the amount of emulsion (1.65 PV) and water used ( $\approx$ 22 PV) was economically ineffective in terms of recovered oil and the overall time required to complete the process (Guillen et al., 2012). Hence, in this work, the focus is on using emulsion slugs alternatively with the water slugs in a cyclic manner similar to earlier

strategies for enhanced oil recovery with water and steam (CSS,WAG) or water and chemicals (CAG). Experimental results in the previous Chapter also suggested finding an alternative injection strategy to improve emulsion flooding efficiency. In this study, the emulsion flooding technique is named as water-alternate-emulsion (WAE) process.

Like any other new method for oil recovery, the technology first needs to be tested in a laboratory core flooding system ([Santosh et al., 2007](#); [Hadia et al., 2007b](#); [Mandal et al., 2010b](#); [Hadia et al., 2008a, 2012](#)) before a field operation of the new process can be embarked. Hence, following similar trends, the WAE flooding technique was investigated in laboratory scale studies which are reported here. In this study, core flooding experiments with an unconsolidated sand pack as a model porous medium are conducted. For this purpose a biaxial core holder is used and three different water-emulsion flooding ratios, viz., 2:1, 4:1 and 5:1, are tested. The oil recovered using the WAE process is compared with the traditional flooding techniques such as water flooding, emulsion flooding, and water flooding followed by emulsion flooding, presented in previous Chapter 3. Based on the results obtained from this laboratory scale study, if the WAE method appears to be a promising option, further scale-up of this technique for field application can be readily executed ([Hadia et al., 2008b](#); [Islam and Farouq Ali, 1989, 1992](#); [Abou-Kassem and Farouq Ali, 1995](#); [Akin et al., 2000](#)).

## 4.2 Materials and Methods

The laboratory core flooding system used in this study is the one reported in previous Chapter 3. The injection flow rate of water-alternate-emulsion slugs was set

at 0.5 cm<sup>3</sup>/min for the entire flooding studies and temperature in the experimental facilities was maintained at room temperature (around 22°C).

The porous medium for the study is unconsolidated sand (dry water-wet silica sand from Ottawa IL sand deposit: US sieve size # 10 (100-140), 53-251μm), which was packed inside a biaxial core holder for each flooding experiment ([www.corelab.com](http://www.corelab.com), 2014a). The core holder has an internal diameter of 38.1 mm (1.50 in) and the internal length of 321.6 mm (12.66 in) and was oriented horizontally during the core flooding experiments. Parameters of the sand packs used for different flooding experiments are summarized in Table 4.1. Using values for porosity,  $\phi$ , cross section of the sand packs,  $A$ , and chosen flow rate,  $Q$ , the interstitial velocity,  $v$ , can be estimated for the studied porous media. This injection rate is equivalent to interstitial velocity of  $2.187 \cdot 10^{-5}$ m/s,  $2.071 \cdot 10^{-5}$ m/s,  $2.074 \cdot 10^{-5}$ m/s (6.20, 5.87, and 5.88 ft/day) for Run #5, Run #6 and Run #7, respectively. It can be defined by Tiab and Donaldson (2004):

$$v = \frac{Q}{\phi A} \quad (4.1)$$

With interstitial velocities of  $2.117 \cdot 10^{-5}$ m/s (6 ft/day), the saturation profiles would be independent of the capillary end effect (Tiab and Donaldson, 2004). In petroleum reservoirs with conventional multiphase flow the velocities are on the order of  $3.528 \cdot 10^{-6}$ m/s (1 ft/day) (Willhite, 1986, p. 21).

Values for residual water saturation,  $S_{wi}$ , absolute permeability, and porosity from Table 4.1 are consistent with available data in the literature for the core flooding experiments with unconsolidated sand packs (Kumar et al., 2010; Sarma et al., 1998; Hadia et al., 2008a; Luo et al., 2013). In addition to the presented parameters, the pore size distribution was measured using an automatic pore size ana-

lyzer (PoreMaster 33 , Quantachrome Instruments) using 1.0243 gm of sand sample with porosity of 38.9 %(loose pack). The total intruded volume was found to be 0.243183 cm<sup>3</sup>. The pore radius lies in a range from 0.003 to 109.71  $\mu\text{m}$  with an average value of 12.631  $\mu\text{m}$ , as it is shown on Figure 4.1. Using data from Table 4.1 with assumption that sand pack can be represented as the bundle of capillary tubes, the pore throat radius,  $r$ , can be found using the following equation Tiab and Donaldson (2004):

$$r = \left( \frac{\phi}{8k} \right)^{-0.5} \quad (4.2)$$

where,  $\phi$  is the porosity of sand pack in % and  $k$  is permeability of sand pack in Darcy. For Run #5, #6, and Run #7 it can be found that pore radius is equal to 13.09, 12.78 and 12.49  $\mu\text{m}$  with an above assumption, respectively. The obtained values lie within the same range as the once found using automatic pore size analyzer.

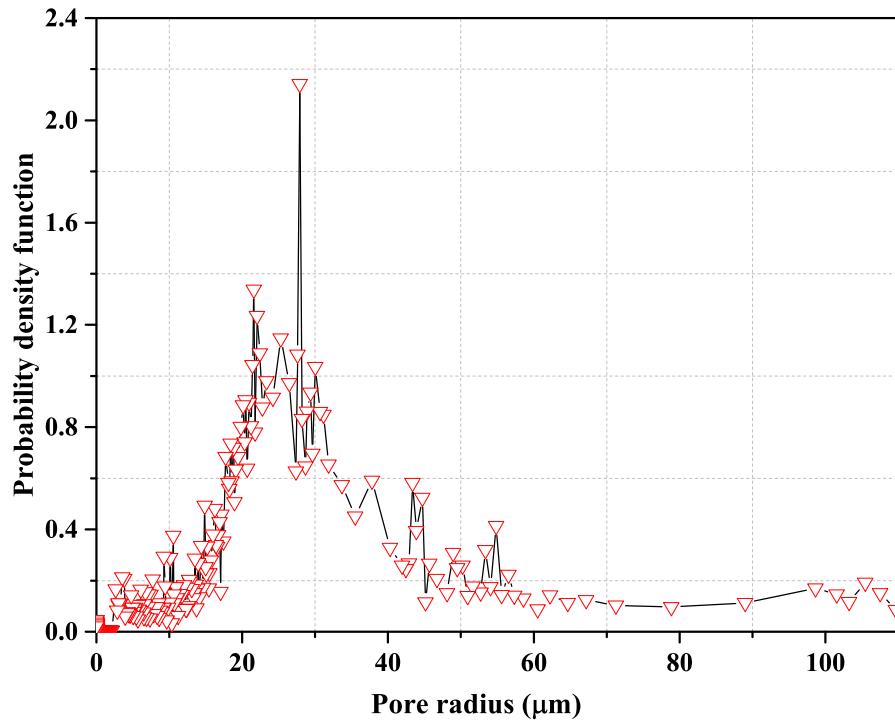


Figure 4.1: Pore size distribution of studied silica sand.

The packing process was followed the procedure discussed in previous Chapter 3. The residual water saturation was established using the following procedure. First, the sand was packed inside the core holder. The core holder was then evacuated using a vacuum pump (117, Labconco Corp.) to 4 kPa absolute (28.74 in. mercury gauge or 1.18 in. mercury absolute) over half of an hour. Graded tank was connected to the core holder and water was supplied by pressure difference to completely saturate the core. Once, the pressure of the effluent side of the core holder equals to atmospheric, the water supply was stopped and the recorded volume of water absorbed inside the core is used as the pore volume (PV),  $V_{pv}$ , for each pack. Once the absolute permeability was calculated, the paraffin oil was injected into the water saturated pack and effluent was collected into graded test tube. The injection rate was kept constant at 0.5 cm<sup>3</sup>/min for 1 PV of injection; thereafter, it was increased to 1.0 cm<sup>3</sup>/min for every 0.5 PV of injection till no water was observed at the effluent side. The amount of water recovered from the core holder,  $V_{water,rec}$ , was recorded. The residual water saturation,  $S_{wi}$ , was calculated with taking into account dead volumes of the system,  $V_d$ , such as supply lines, end plugs mass flow meter, etc. using:

$$S_{wi} = (V_{pv} - V_{water,rec} + V_d)/V_{pv} \quad (4.3)$$

The viscosity of the injected and produced fluids was measured using a rotational viscometer (Rheolab QC, Anton Paar USA Inc.) with a pre-installed double gap measuring system (DG42, Anton Paar USA Inc.). The density of the injected and produced fluids was measured by a mass flow meter (M13, Bronkhorst Cori-Tech BV) at the inlet and exit of the core holder. Surface tension of the injected and produced fluids was measured using the drop shape analyze (DSA 100, Krüs

GmbH) by the pendant drop technique (Waghmare and Mitra, 2010). The shear rate ( $100 \text{ s}^{-1}$ ) was selected as standard shear rate used in the literature (Cobos et al., 2009; Sorbie and Huang, 1991; Maia et al., 2009; Castro Dantas et al., 2006), so that it can easily compare WAE technique with previously used flooding reagents.

The internal shear rate, caused by the given injection rates used in the experiment, can be found from the known injection flow rate, sand pack dimensions, porosity and the estimated pore size. Hence, the superficial (or empty tube) velocity,  $U_o$ , can be calculated as (Darby, 2001):

$$U_o = \frac{Q}{A} = \frac{Q}{\frac{\pi d^2}{4}} = 7.309 \cdot 10^{-6}, \text{ m/s} \quad (4.4)$$

Also, the velocity within the bed (i.e., interstitial velocity,  $U_{\text{in}}$ ) can be calculated using porosity and the superficial velocity (Darby, 2001):

$$U_{\text{in}} = \frac{U_o}{\phi_{\text{run,n}}} \quad (4.5)$$

For Run #5, ..., Run #7 it can be found that the superficial velocity using porosity values would be equal to  $2.188 \cdot 10^{-5} \text{ m/s}$ ,  $2.071 \cdot 10^{-5} \text{ m/s}$ , and  $2.007 \cdot 10^{-5} \text{ m/s}$ , respectively. Finally, the shear rate,  $\gamma$ , based on the given injection rate can be estimated using the formula for the shear rate at the inner wall of a Newtonian fluid flow inside a pipe of diameter  $d$  (or radius  $r$ ) (Darby, 2001):

$$\gamma = \frac{8U_{\text{run,n}}}{d} = \frac{4U_{\text{run,n}}}{2r} \quad (4.6)$$

For Run #5, ..., Run #7 it can be found that the shear rate with selected injection rate would be equal to  $6.687 \text{ s}^{-1}$ ,  $6.482 \text{ s}^{-1}$ , and  $6.653 \text{ s}^{-1}$ , respectively. Taking this into account, the viscosity presented in this Chapter of the paraffin oil, produced oil and emulsion has been measured at  $6 \text{ s}^{-1}$  in addition to  $100 \text{ s}^{-1}$ .

Table 4.1: Relevant parameters for unconsolidated sand pack samples used in flooding experiments.

Pack	WAE ratio	Porosity, %	Pore volume, cm <sup>3</sup>	Mass of sand pack, g	Absolute permeability, Darcy	Permeability with residual water, Darcy	$S_{wi}^{\ddagger}$
Run #5	2:1	33.4	117.01	617.5	7.0 .. 7.5	5.5 .. 5.8	0.096
Run #6	4:1	35.3	123.83	599.4	7.2 .. 7.4	6.4 .. 6.8	0.085
Run #7	5:1	35.2	123.37	600.7	6.9 .. 7.0	6.8	0.085

‡ - Residual water saturation after oil saturation.

Initial water saturation and water flooding were completed using distilled water (DI) produced from a water purification system (PURELAB<sup>©</sup> Ultra, Elga Labwater, LLC). DI water used for this study has a density of 1000 kg/m<sup>3</sup>(measured using mass flow meter (M13, Bronkhorst Cori-Tech BV)) and measured viscosity of 1.0 mPa·s at 500 s<sup>-1</sup> shear rate and surface tension of 72.40 mN/m. Oil saturation was executed using paraffin oil (CAS Number 8012-95-1, obtained from Sigma-Aldrich Co. LCC) with a viscosity of 122.7 mPa·s and 120.5 mPa·s at 6 s<sup>-1</sup> and 100 s<sup>-1</sup> shear rate , respectively. The density of the paraffin oil was 868 kg/m<sup>3</sup> and surface tension of 29.85 mN/m. Stable oil-in-water emulsion (70.75 wt% oil and 29.25 wt% water with average oil drop size of 2.46  $\mu$ m) was procured from a commercial provider (Quadrise Canada Corporation, Canada) ([Patrick Brunelle \(Quadrise Canada Corp.\), 2012](#)). It should be noted that the emulsion used for flooding was made from heavy oil which is noticeably different from the residual oil (paraffin oil). The emulsion had a viscosity of 1084.9 mPa·s at 6 s<sup>-1</sup> shear rate and 495 mPa·s at 100 s<sup>-1</sup> shear rate and density of 1014 kg/m<sup>3</sup>. It was difficult to measure the surface tension of this emulsion using pendant drop method as symmetric drop generation was not achievable for a fluid of such high viscosity.

Three different ratios of water to emulsion slugs, 2:1, 4:1 and 5:1 were tested. For these tested WAE slug ratios, the water amount was kept fixed at 0.5 pore

volume (PV). Hence, the emulsion PV was varied accordingly to maintain the ratios between the water to emulsion slugs. As an example, 4:1 WAE slug would mean water with 0.5 PV and emulsion with  $0.125 (= 0.5/4)$  PV. In the case of 2:1 slug (Run #5), the WAE method has been applied only for two cycles, which amounts to cumulative injection of 1 PV of water and 0.5 PV of emulsion. In the case of 4:1 (Run #6) and 5:1 (Run #7) slug ratios, the WAE method was applied for three cycles, which amounts to 1.5 PV of water and 0.375 PV of emulsion for 4:1 ratio and 1.5 PV of water and 0.3 PV of emulsion for 5:1 ratio, respectively. It should be noted that at the end of each cyclic WAE process, only water injection has been performed, the amount of PV injected for each run is different. In addition, the effluent analysis has been performed to compare the viscosity and surface tension between the injected and the produced fluids.

## **4.3 Results and Discussion**

The aim of this study was to demonstrate the efficiency of an enhanced oil recovery technique, viz., WAE flooding, using laboratory core flooding experiments. In this section, detailed results for WAE are provided and this technique is compared with traditional water flooding or with emulsion flooding alone. These provide a comparative indicator of the efficiency of the proposed WAE technique. First, a qualitative analysis was performed through actual visualization of the sand pack after the WAE flooding and later, quantitative data in terms of pressure profiles during water-alternate-emulsion injection and resultant oil recovered from the sand pack during WAE flooding was provided.

### **4.3.1 Qualitative analysis of WAE Flooding**

Figure 4.2(a) shows the cross-section image of the actual sand pack corresponding to Run #5 (i.e., WAE ratio 2:1), which was removed from the core holder at the end of Run #5. This includes two cycles of WAE followed by  $\approx 4.1$  PV of water flooding. Visual inspection of the core pack suggests that there is a large build-up of the heavy oil component of the emulsion at the inlet section of the core. The hypothesis is that after the first cycle of WAE, further water injection for the next cycle causes water to interact with the emulsion available within the pore space of the sand pack. This destabilizes the emulsion resulting in phase segregation and thereby more of the heavy oil fraction of the emulsion is accumulated at the inlet section and the water phase of the emulsion is transported to the downstream section of the core.



(a)



(b)

Figure 4.2: Cross-section images of the sand pack (a) after complete WAE flooding with 2:1 ratio followed by water flooding up to 5.6 PV; (b) after complete water flooding followed by approximately 0.3 PV of emulsion injection. Here, the direction of injection is from left to right.

In contrast, when first traditional water flooding ( $\approx 3.5$  PV of injection) followed by only emulsion injection ( $\approx 0.3$  PV of injection) was performed, it was noticed that there is a piston like displacement of the resident oil and water phases by the injected emulsion. This is evident by a clear vertical front movement of the emulsion, as observed in Figure 4.2(b). Such piston-like displacement has been reported earlier for emulsified solvent flooding (Sarma et al., 1998; Shah et al., 2010; Mahmood and Brigham, 1987).

The amount of emulsion used in WAE flooding was both 0.52 PV and 0.3 PV for water flooding followed by emulsion flooding. The emulsion front progressed through the sand pack up to 9 cm in both cases. It indicates that for the alternative flooding, the emulsion stays inside the pack and slowly builds up the emulsion front at the inlet region cycle after cycle.

### 4.3.2 Quantitative Analysis of WAE Flooding

Pressure drop was continuously monitored and measured by differential (dP1 in Figure 3.1) and two inline pressure sensors(TP-2 and TP-1 in Figure 3.1) (FP2000 series, Honeywell International Inc.) across the core holder for each WAE ratio. Figure 4.3, 4.4, and 4.5 shows the pressure profiles for different WAE ratios along with the corresponding oil recovery curve. The raw pressure data obtained from the measurement has been processed using B-spline interpolation using graphical and data analysis software (Origin 9.1, OriginLab, Co.) to remove noise and smooth data, and the obtained values are plotted here.

In Figure 4.3, there is the graph where the left vertical axis is a percentage of original oil in place recovered from a porous media, the right vertical axis is a

pressure drop measured across the core holder and the horizontal axis is a volume of liquid injected normalized by a pore volume. The horizontal dashed lines indicate the location of the pressure jumps. There are two inflection points in the pressure drop curve which correspond to emulsion injection during the cyclic WAE process. During the first cycle, the introduction of the emulsion phase resulted in a gradual increase of pressure inside the core till the end of the emulsion injection with a resultant in total differential pressure rise of 12 psi. This pressure rise data is also confirmed by the visual inspection of the sand pack (Figure 4.2(a)) where most of the emulsion is plugged inside the pore-space which may result in the increase in overall pressure drop. This process has also been observed by others and is often referred as a blockage process (Decker and Flock, 1988). Also, the effluent analysis for this cycle suggested that the oil recovered from the core pack corresponds to paraffin oil only without any traces of the heavy oil phase of the emulsion. This again emphasizes that most of the emulsion is trapped at the inlet of the core pack as observed through visual inspection.

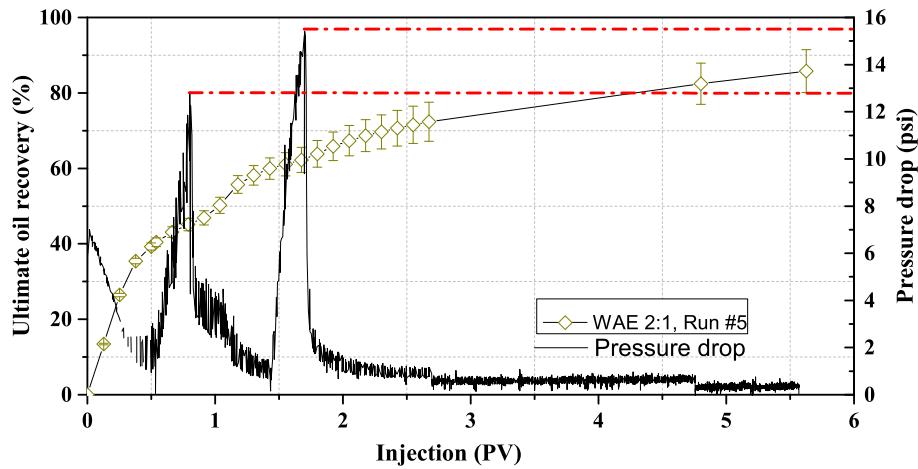


Figure 4.3: Variation of pressure drop across the core holder and the oil recovery with respect to PV of injected fluids, 2:1 WAE. The horizontal dashed lines indicate the location of the pressure jumps.

After the end of emulsion injection shown in Figure 4.3, water injection starts which is evident from the gradual drop in pressure across the core, allowing more oil to be recovered. This additional oil recovery is observed through the sudden change in the slope of the oil recovery curve during the start of the water injection. This pattern continues till the next WAE cycle, however the jump in the oil recovery is not as much as compared to the first cycle. The reason for comparatively higher recovery for the first cycle can be attributed to the much broaden pressure drop over 0.5 PV of water injection and higher oil availability compare to the following cycles. It confirms that the given emulsion blocks high permeable zones and redirects following water flooding to the oil saturated regions. Further water flooding breaks through the new regions and results in a pressure drop across the core holder after breakthrough. The oil recovery data shows that at the end of the second WAE cycle, the oil recovery from the core pack is around 60%. After the completion of the cyclic WAE process, water injection was always conducted to recover further resident oil. In this case, such water flooding eventually results in almost 86% recovery of the resident oil with only 0.5 PV of overall emulsion injection. The oil recovery for 2:1 WAE ratio can be compared with data presented in previous Chapter 3 involving direct emulsion flooding into a similar core holder (with slightly shorter internal length (284 mm (11.18 in))). It was found that this present technique produced higher oil recovery and more importantly using significantly less emulsion compared to direct emulsion injection of 1.01 PV used in previous experiment.

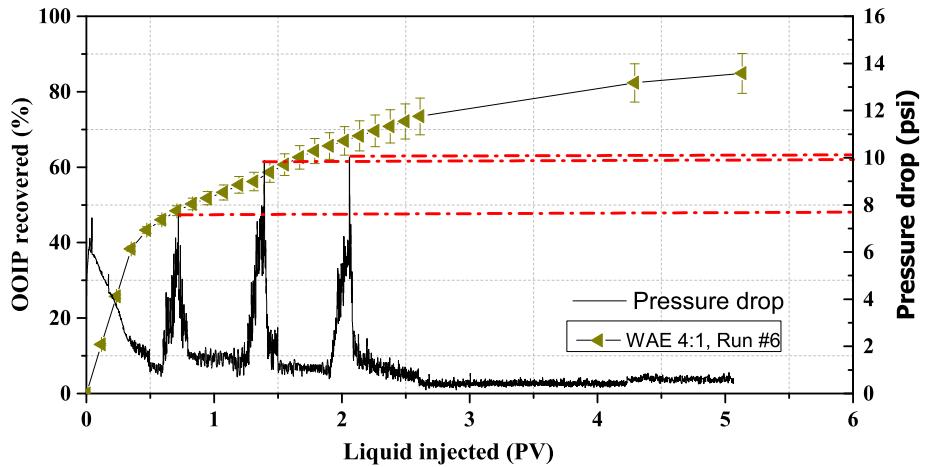


Figure 4.4: Variation of pressure drop across the core holder and the oil recovery with respect to PV of injected fluids, 4:1 WAE. The horizontal dashed lines indicate the location of the pressure jumps.

A similar trend in pressure drop was found for 4:1 WAE flooding, as shown in Figure 4.4. Since emulsion was injected three times during 4:1 WAE flooding, there are three inflection points which correspond to emulsion injection during the cyclic WAE process. During the first cycle, the introduction of the emulsion phase resulted in a gradual increase of pressure inside the core till the end of the emulsion injection with a resultant in total differential pressure rise of 8.3 psi. During both the second and the third cycle, the differential pressure across the core holder has increased to almost 10 psi which corresponds to the second and the third peaks in the pressure profile data. Also, in this case, no emulsion was observed at the effluent stream at the end of the first cycle which suggests the presence of a similar blockage process as observed for 2:1 WAE ratio has also occurred for this case. At the end of three cycle of WAE flooding, the recovered oil is  $\approx 65\%$  of OOIP and the final ultimate oil recovery equals to 85% of OOIP for overall 0.375 PV of emulsion injection.

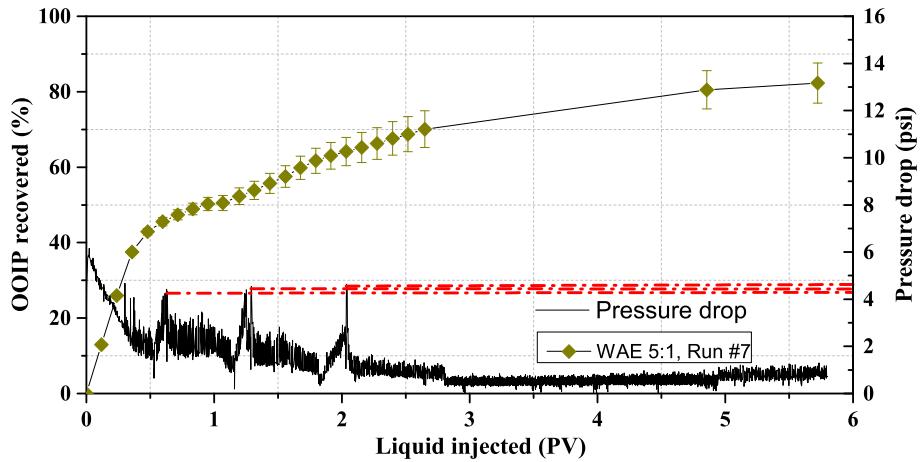


Figure 4.5: Variation of pressure drop across the core holder and the oil recovery with respect to PV of injected fluids, 5:1 WAE. The horizontal dashed lines indicate the location of the pressure jumps.

For the case of 5:1 WAE ratio, as observed for Figure 4.5, it was found that the pressure rise corresponding to each cyclic emulsion injection is almost three times lower than 2:1 WAE ratio. This can be attributed to the lower amount of emulsion injected in each cycle (0.1 PV). However, the overall oil recovery is similar to the other two ratios but with significantly less amount of injected emulsion ( $\approx 0.3$  PV). At the end of three cycles of WAE flooding, the recovered oil is  $\approx 62\%$  of OOIP and the final ultimate oil recovery equals to 82% of OOIP for overall 0.3 PV of emulsion injection.

### 4.3.3 Effluent Analysis<sup>2</sup>

Each effluent fraction, obtained from the different WAE flooding studies was analyzed to observe any change in density, viscosity and surface tension with respect to the original injected fluids. Here, the data for the 2:1 WAE flooding process is

---

<sup>2</sup>The photograph presented in this section has been published as conference paper. A. Baldygin, D. S. Nobes, and S. K. Mitra, “Oil recovery from porous media using emulsion”, *The ASME 2014 International Mechanical Engineering Congress & Exposition*, IMECE2014-37248, 2014

provided and summarized in Table 4.2. A photograph of liquids injected and collected during complete 2:1 WAE flooding is shown in Figure 4.6. Recovered emulsion is not present in a bottle, since it undergoes a separation process inside the porous media, as it was hypothesised in Section 4.3.1. It was found that the produced water, after the completion of two cyclic WAE flooding, is light brown in colour, which is quite similar to the emulsion colour. Recovered oil has dark yellow color, which is in between emulsion and produced water in a color scheme.



Figure 4.6: A photograph of liquids injected and collected during complete WAE flooding. From left to right: water, paraffin oil, emulsion, recovered oil, produced water.

The density of produced water is measured to be  $970 \text{ kg/m}^3$  and viscosity is  $1.2 \text{ mPa}\cdot\text{s}$  at  $500 \text{ s}^{-1}$  shear rate. Also, the surface tension of the produced water is  $40.50 \text{ mN/m}$ . It is observed that the density and the surface tension of the produced water are lower compare to the injected DI water, while its viscosity is higher. The measured density, viscosity, and surface tension of the recovered oil fraction at the effluent are  $865 \text{ kg/m}^3$ ,  $112.3 \text{ mPa}\cdot\text{s}$  at  $6 \text{ s}^{-1}$  shear rate,  $112.0 \text{ mPa}\cdot\text{s}$  at  $100 \text{ s}^{-1}$  shear

Table 4.2: The physical properties of the liquids shown in Figure 4.6.

Liquid	Density, kg/m <sup>3</sup>	Viscosity at 100 s <sup>-1</sup> , mPa·s	Viscosity, at 6 s <sup>-1</sup> , mPa·s	Surface tension, mN/m
Water	1000	1.0 <sup>‡</sup>	-	68.40
Produced water	970	1.2 <sup>‡</sup>	-	40.50
Paraffin oil	868	120.5	122.7	29.85
Recovered oil	865	112	112.3	29.85
Emulsion	1014	495	1085	n/d

<sup>‡</sup> - measured at 500 s<sup>-1</sup>.

rate, and 29.85 mN/m, respectively. It is found that the density and surface tension of the recovered oil is similar to the injected paraffin oil, while the viscosity is lower than the paraffin oil. These observations confirm that the emulsion blockage inside the sand pack and the surfactant present in the emulsion interacts with the injected DI water, thereby lowering its surface tension. The recovered oil has properties close to the the injected paraffin oil, which suggests that the heavy oil component of the emulsion remains trapped inside the core pack, with almost negligible amount being displaced out of the core holder.

The hypothesis stated in Section 4.3.1 is substantiated with effluent analysis, the water fraction recovered shows different surface tension and viscosity compared to the injected DI water. This may result in a change of the internal mobility ratio between the resident oil phase and the invading water phase, which may aid in recovering more oil from the core pack.

#### 4.3.4 Comparison of WAE with Traditional Flooding

Figure 4.7 shows the cumulative recovery curves for the three different WAE ratios used in this present study compared with Chapter 3 results for water flooding, direct

emulsion flooding and water flooding followed by emulsion flooding. It is found that at least 20% more recovery can be achieved compared to traditional methods, be it water flooding or only emulsion flooding. It is also found that for a given oil recovery with any of the methods illustrated in Figure 4.7, the proposed technique of water-alternate-emulsion always requires significantly less amount of emulsion injection. For the studied parameters, it is observed that the most economical way, in terms emulsion usage, to recover oil is with 5:1 WAE ratio. In such injection strategy, only 0.3 PV of emulsion injection is required to obtain 82% of OOIP. Hence, this laboratory scale study shows promising technology breakthrough in terms of the development of an enhanced oil recovery process, which further needs to be field tested.

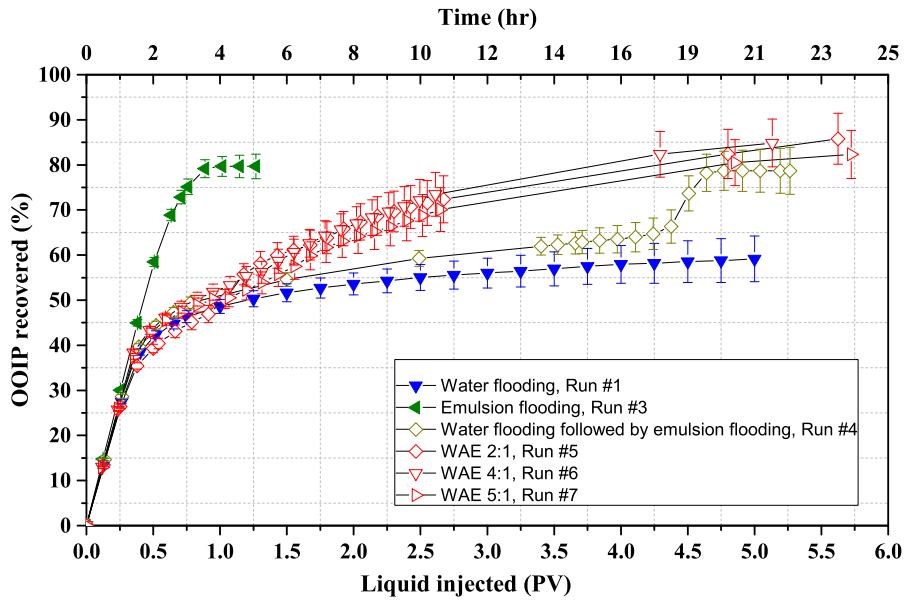


Figure 4.7: Cumulative recovery curves for WAE flooding and comparison with waterflooding, emulsion flooding, and waterflooding followed by emulsion flooding (presented in Chapter 3).

## **4.4 Conclusions**

The present study reports an efficient technique for enhanced oil recovery with utilization of emulsion (oil-in-water) produced *ex-situ*. The developed technique, water-alternate-emulsion (WAE), was tested using laboratory core flooding system. Three different slug ratios, 2:1, 4:1 and 5:1, were experimentally investigated. The qualitative analysis of the sand packs after the WAE floodings shows that emulsion has separated inside the porous media and the heavy oil fraction of the emulsion has been trapped near the entrance region of the core. In addition from the effluent analysis, it can be assumed that the surfactant present in the emulsion combines with the injected DI water which further assists in removing the resident oil phase from the pore spaces.

The quantitative data suggests that one can achieve 22 % - 26 % more recovery with WAE compared to the traditional flooding process. In summary, the WAE flooding technique appears to be a promising enhanced oil recovery process which utilizes minimum amount of emulsion and recovers a significant portion of the resident oil. Further steps are needed to test the efficiency of this process in field reservoirs, which may have been abandoned after water flooding.

# **Chapter 5**

## **Experimental flow visualization and pressure mapping of emulsion flooding with horizontal and vertical wells<sup>1</sup>**

### **5.1 Introduction**

The efficiency of emulsion flooding as a recovery agent (*ex-situ* produced oil-in-water emulsion) has been proved in previous Chapters 3 and 4. It was shown that emulsion flooding can potentially recover up to  $\approx 85\%$  of OOIP at 0.375 PV of total emulsion injection and  $\approx 4.5$  PV of total water injection using efficient method of injection - water-alternative-emulsion (WAE) (Guillen et al., 2012; Son et al., 2014; Ponce F. et al., 2014). Other methods for injection, such as direct emulsion flooding, presented in Chapter 3 and water flooding followed by emulsion (Qiu and Mamora, 2010; Willhite et al., 1980) or surfactant/polymer flooding (Samanta et al., 2012; Kumar et al., 2012; Bryan and Kantzias, 2009; Krumrine and J.S., 1983), also showed promising results. However, the time required to recovery the same

---

<sup>1</sup>A version of this chapter has been prepared for submission to the journal. A. Baldygin, D. S. Nobes, and S. K. Mitra, "Experimental flow visualization of emulsion flooding with horizontal and vertical wells", *Journal of Petroleum Science and Engineering*, 2014

amount of oil is significantly higher. Close to 97 % of resident oil at  $\approx 22$  PV of liquids injected can be recovered using emulsion made of a synthetic oil (Shell Tivela 460) (Guillen et al., 2012).

One of the important properties of the emulsion is the drop size distribution (DSD). The conventional methods which were previously used to get the drop size distribution reported presence of single particle group (Wasan et al., 1978; Moradi et al., 2014; Romero et al., 2011; Moradi et al., 2011; Romero et al., 2006). Compared to the previously used methods used for particle analysis, currently available particle analysers count particles individually (Anderson et al., 2013). They are able to distinct different sizes and to provide total number of particles (Anderson et al., 2013). It can be hypothesised that due to the availability of particle-by-particle analyzer the presence of two distinct groups of oil particles in emulsion can be now measured.

There are two ways for emulsion interaction within porous media. Either it can increase mobility of resident oil (Mandal et al., 2010a) or block high permeable regions (McAuliffe, 1973). In previous experiments, a biaxial (Chapter 3 and 4) and Hassler core holder (Qiu and Mamora, 2010; Ko et al., 2014) have been used to simulate reservoir conditions during emulsion flooding. Even after post-experimental analysis on collected sand packs in Chapter 4, the *in-situ* interactions during emulsion flooding process are still unclear. Understanding of the emulsion flooding process at the tertiary stage without ceasing experimental progress or changing experimental parameters (repacking), its interaction with oil saturated porous media, require nondestructive testing (NDT). It is limited in the core holders previously used in full-scale studies.

The way of studying interactions within porous media without causing damage to the porous media can be by using multi-dimensional experimental setups. At the micro-scale, the converging-diverging quartz capillary tube can be used to understand the physics of emulsion flow at the scale of the pore size (Cobos et al., 2009; Romero et al., 2011). At the macro-scale, reservoir on a chip (ROC) with glass beads (Guillen et al., 2012) or artificially constructed porous media (Mei et al., 2012) can be used to mimic porous media stricture, which is preset in the reservoir. Experimental data collected from these experiments allows the validation and development of fundamental theory about emulsion flooding. Thus, the efficiency of emulsion flooding at given reservoir conditions can be predicted. However, the pore volume utilized in these studies are about  $0.822 \text{ cm}^3$  (Mei et al., 2012) or  $2.980 \text{ cm}^3$  (Guillen et al., 2012) which is even less than in biaxial and Hassler core holder. A step further in terms of the experimental scale can be by utilizing a two dimensional (2D) core holder with the pore network 10 times larger than in conventional biaxial or Hassler core holders.

A two dimensional core holder shows how the front of the *in-situ* flow spreads through the porous media (Santosh et al., 2007; Doorwar and Mohanty, 2011; Robert et al., 2006; Chaudhari et al., 2011b; Naderi and Babadagli, 2011). The 2D core holder represents a sectional cut of a real reservoir with dimensions obtained from scaling parameters (Hadia et al., 2008b; Islam and Farouq Ali, 1989). The side wall of the 2D core holder can be transparent or solid piece with pressure/temperature ports (Butler and Chung, 1988; Li and Mamora, 2010). It is thin enough to assume that the flow is distributed in two directions only and there is no influence (flow) in the third direction. Another aspects, such as well configura-

tion, can be studied in addition to the flood front studies. Vertical injection - top or bottom horizontal production (VI-THP and VI-BHP), horizontal injection - vertical production (HI-VP), horizontal injection - horizontal production (HI-HP), vertical injection - vertical production (VI-VP) wells configurations can experimentally investigated (Santosh et al., 2007, 2008; Hadia et al., 2008a,b).

Flow visualization and pressure mapping of the emulsion flooding process can help to understand the internal dynamics happening inside the porous media. It also provides answers as to how well a configuration can affect on efficiency of emulsion flooding or how dynamics of emulsion flooding front through previously abandoned regions depends on well configuration and what is the increase in ultimate oil production. The previously utilized experimental setup has been modified accordingly to provide answers. In this Chapter, the results of water flooding followed by emulsion flooding experiments for three different configurations are presented. Details for the experimental setup components and materials and methods used to carry out experiments are provided. Results consist of visual image analysis, pressure data analysis, effluent analysis and internal flood front velocity analysis. Collected results provide one step further towards developing theory for the scale-up of emulsion flooding technique to the field application (Islam and Farouq Ali, 1989, 1992; Abou-Kassem and Farouq Ali, 1995; Akin et al., 2000).

## 5.2 Experimental Setup

A hydraulic schematic of the system developed for this study, previously described in Chapter 3, is a further modification of the concept of the core flooding system. The core block was modified compared to the previous configuration. The biax-

ial core holder has been replaced with a two dimensional (2D) core holder using the “plug-and-play” advantage of the developed system described earlier. A photograph of the final version of the experimental setup is shown in Figure 5.1. Final configuration of experimental setup prepared for the flow visualization and pressure mapping of emulsion flooding with horizontal and vertical wells is shown. It has an external light source to guarantee uniform light intensity on a core holder surface. Pressure demodulators are also added to process signals from 15 pressure sensors and to demodulate and amplify the input signals to a  $\pm 10$  Vdc full-scale output.

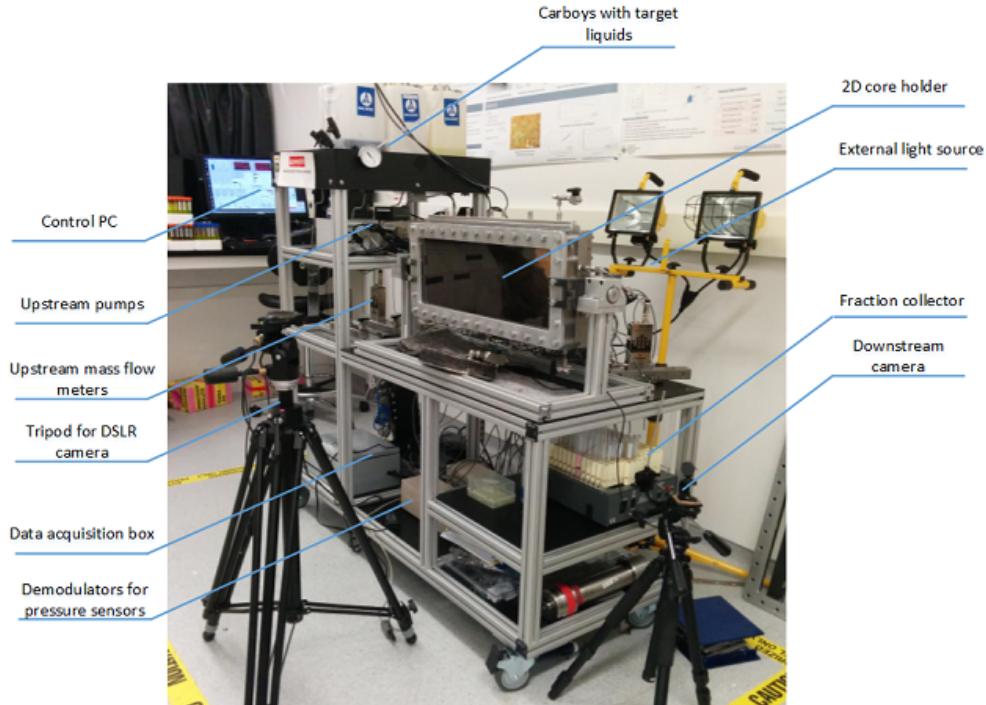


Figure 5.1: A photograph of experimental setup used for the core flooding experiments with 2D core holder.

The software with graphical user interface (GUI) used to control the system was developed based on the original version, previously discussed. Additional channels have been added to record data from extra pressure sensors installed on a two 2D core holder. Since the single experiment requires more than three days con-

tinuous running, it is crucial to provide sustained monitoring. The software was modified compared to previously released version used in previous Chapter 3 and 4 to have remote visual monitoring via a web-camera (Lifecam Studio Webcam, Microsoft, Corp.) and system monitoring via email reporting of important system parameters. The command line simple mail transfer protocol SMTP email client (sendEmail ([Zehm, 2009](#)), Brandon Zehm) was integrated into software and used for notifications. Email notifications and camera allows to monitor and to control the system 24 hours a day.

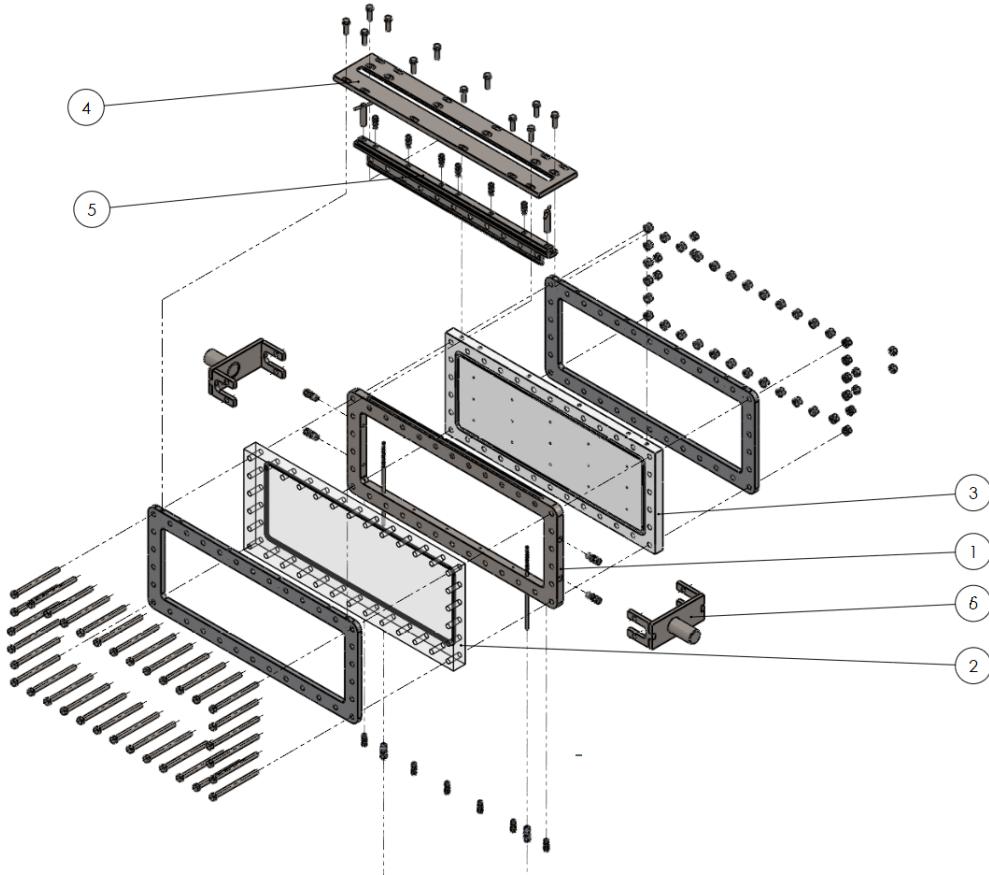


Figure 5.2: Exploded view of the 2D core holder (1) main frame with profiled slot, (2) cast acrylic wall, (3) stainless steel wall with pressure ports, (4) top cap, (5) profiled cap, and (6) holder.

The exploded view of the 2D core holder, shown in Figure 5.2, has an internal

void space of 600 x 200 x 20 mm. The main components, such as the main frame with profiled slot, cast acrylic wall, stainless steel wall with pressure ports, top cap, profiled cap, and holder are numbered. Compared to others Chaudhari et al. (2011a); Veerabhadrappa et al. (2013b), the current design has a modified configuration for the packing of sand. It has a main frame with profiled slot at the top for pouring sand inside the void space. Once the core holder is fully packed, the profiled cap closes the core holder and the top cap places on top of it. By tightening bolts, an additional compression allows to achieve a denser pack. The holder is mounted into a horizontal base (Part No. 8020-5930, 80/20 Inc.). It allows to fix at any angle and to rotate 360 degrees around horizontal axis. Well configurations can be reconfigured using multiple ports on side walls, two at the top, at the left and at the right side.

In order to recover oil from a reservoir, injection and production wells must be drilled into a reservoir. Wells used in the current study are designed in agreement with industrial requirements written for reservoirs with expected conditions close to the unconsolidated sand packs (King, 2009). Stainless steel tubes of 6.35 mm (1/4 in) outer diameter (OD) with perforations of 1.59 mm (1/16 in) were used during the core flooding experiments. The hole pattern, shown on Figure 5.3, was designed using existing recommendations (Cosad, 1992; Parrott and Walton, 2001). During the flooding process, wells were held in place with bored-through male connector (6.35 mm (1/4 in) tube OD x 1/4 in male NPT, SS-400-1-4BT, Swagelok, Co.) and were wrapped with stainless steel wire cloth (wire diameter 53.34  $\mu\text{m}$  (0.0021 in.), opening size 73.66  $\mu\text{m}$  (0.0029 in.), mesh size 200 x 200) (Article No. 54058, G. Bopp USA, Inc.) to provide sand control (Voll et al., 1998).

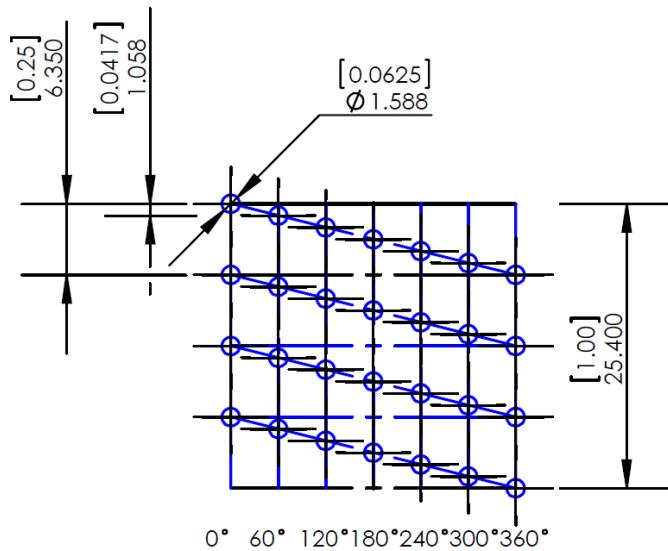


Figure 5.3: Pattern for hole perforation in wells (28 holes/in<sup>2</sup>).

A cast acrylic sheet was installed on one side of the core holder to allow visualization of emulsion flooding with horizontal and vertical wells. A digital single-lens reflex (DSLR) camera (D7100, Nikon Canada, Inc.) with 18-105mm lens (Nikon Canada, Inc.) is mounted on a tripod (Part# 028B, Manfrotto Co.) with a professional head (Part# 229, Manfrotto Co.) to capture the process of emulsion flooding and record any changes which may occur inside porous media. The images collected during flooding process have 6000 x 4000 resolution with 24 bit depth and sRGB color representation. The back plate of the 2D core holder has 15 pressure ports for monitoring the 2D pressure in the sand pack. Differential pressure sensors with replaceable membrane (DP15, Validyne Engineering Corp.) were chosen with an open end to the atmosphere. Pressure maps were generated using collected data from pressure sensors. These maps accompany data from the image analysis and provide better understanding of emulsion flooding process. Pressure sensors are named as  $CP_{i,j}$ , where  $i$  is the row and  $j$  is the column. Reference images with

coordinates for pressure sensors are shown in Figure 5.4. These configurations, vertical injection - vertical production (VI-VP), vertical injection - horizontal production (VI-HP), horizontal injection - horizontal production (HI-HP), were chosen as a continuation of existing experimental results with well configurations using 2D core holder for water flooding Santosh et al. (2007). It allows a comparison of results for the water flooding and benchmarking of the developed system.

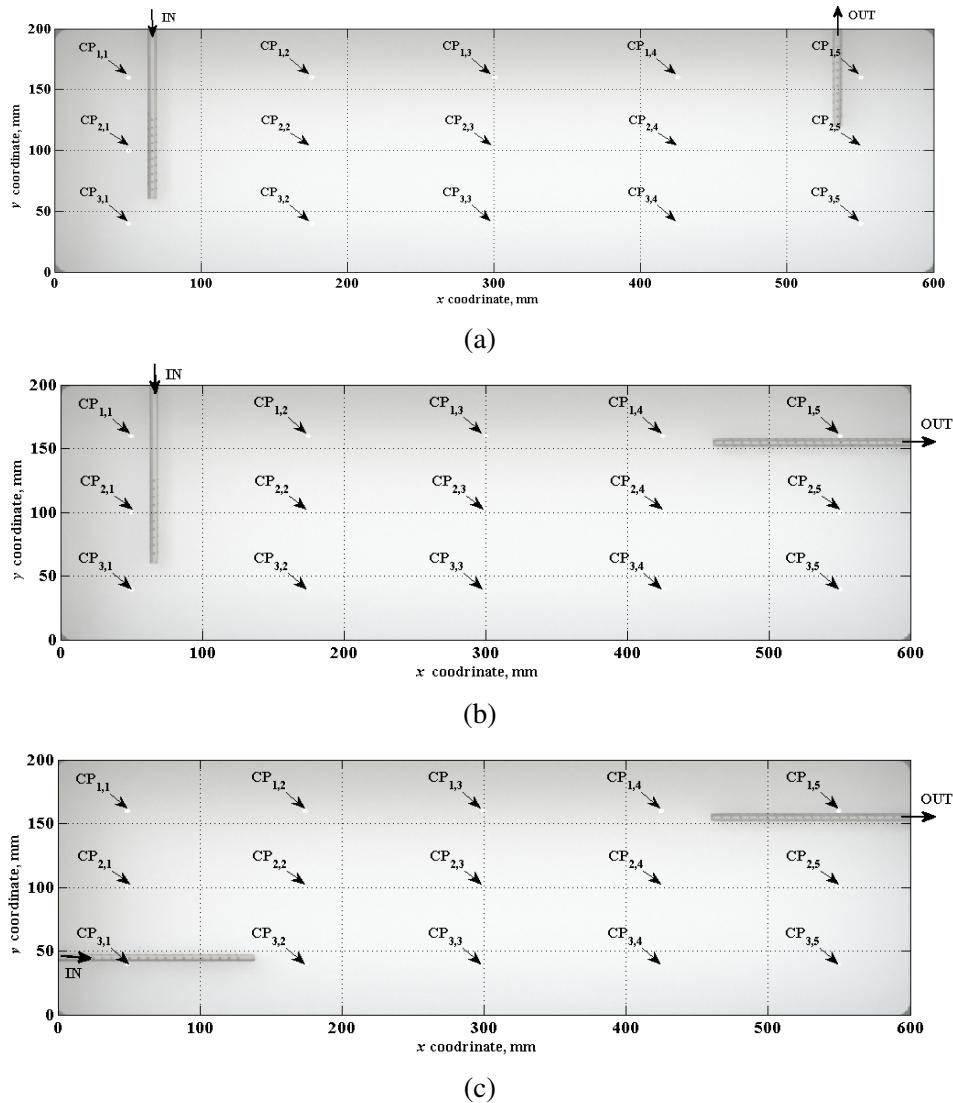


Figure 5.4: Reference images with coordinates for pressure sensors in (a) VI-VP; (b) VI-HP; (c) HI-HP configuration.

The processing code for image analysis was developed using commercial multi-paradigm numerical computing environment (MATLAB R2014a, MathWorks). This code provides data for the velocity of the flood front at three vertical locations for each well configuration. The locations can be obtained by individual bases for each run, based on image resolution. The code follows the same processing steps for each run: cuts three slices for each individual image, reads out the red-channel of the image, converts the image to the binary image based on threshold, detects emulsion edge using the Prewitt method ([Pre](#)), calculates the location for the end in horizontal direction, and scales it to the actual coordinate in millimeters. Finally, it loads the obtained data and fits and plots a cubic polynomial function with robust fitting options and centers and scales (normalize) for displacement versus time. The order of a cubic polynomial function was adjusted manually from case to case to reduce numerical error. In order to obtain velocity, it finds the first derivative of the polynomial function and scales from mm/min to m/s and plots.

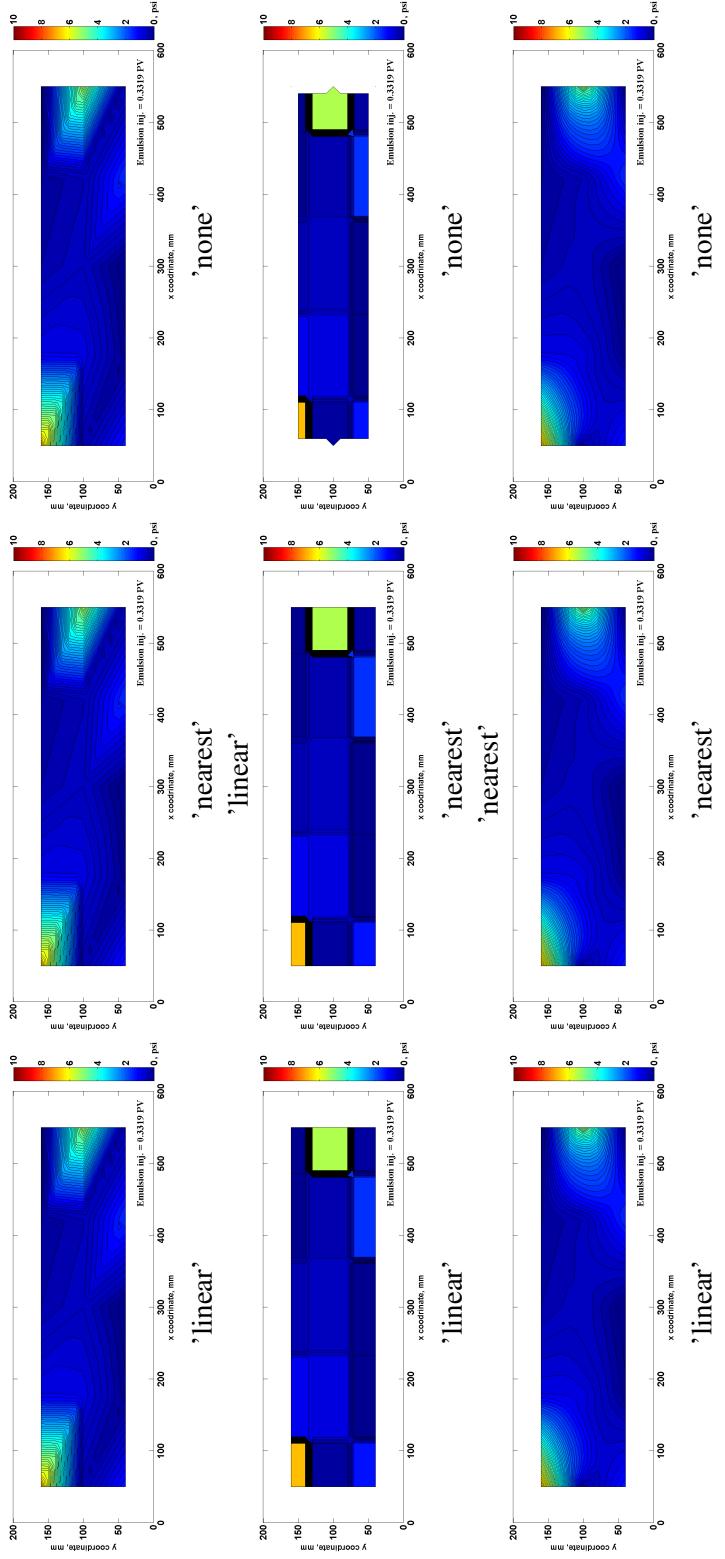


Figure 5.5: Comparison of pressure maps collected with different settings in *scatteredInterpolant* function.

Another code was developed to analyze data from pressure sensors collected during emulsion flooding. Collected data from pressure sensors along with coordinates was prepared for plotting as filled contour plot using `scatteredInterpolant` function. This function allows to perform interpolation on a 2-D scattered data set.

All nine configurations for `ScatteredInterpolant` function were investigated and are compared in Figure 5.5 to identify optimal configuration with a representation close to reality. There are three interpolation methods: linear, nearest and natural. Nearest method showed coarse results compared to two others and showed lack of representative information about *in-situ* processes. Natural neighbor interpolation re-distributes pressure equally in radial direction compared to linear interpolation with axial distribution. It is also expected that pressure follows fluid fronts. Considering images collected over different runs and presented later in this Chapter, the 'nearest' option was selected for interpolation method and 'linear' option for extrapolation method.

### 5.3 Materials and Methods

In this section, the details of materials and methods used to prepare and carry out experiments are provided along with a standard characterization for core flooding experiments. This data includes physical properties of utilized liquids, porosity, permeability and residual oil saturation.

The suppliers for liquids, water, oil and emulsion, were chosen the same as in previous Chapters. In order to have visible difference between liquids compared to previously reported data, the distilled water (DI) was dyed with liquid concentrate of yellow/green dye (Part # 106001, Bright Dyes, Division of Kingscote Chemicals

Inc.). Concentration was chosen as 1 ml per 1 L of DI water. The paraffin oil was dyed with liquid concentrate of red dye (Part # 506250-RF4, Bright Dyes, Division of Kingscote Chemicals Inc.). Concentration was chose as 10 ml per 5.5 L of oil. Emulsion was not dyed because of its natural high contrast compared to oil and water.

Viscosity, density and surface tension of dyed liquid were measured and compared with pure liquids to ensure that the introduced dye does not critically effect physical properties of the liquids. A rotational viscometer (Rheolab QC, Anton Paar USA Inc.) coupled with double gap measuring system (DG42, Anton Paar USA Inc.) was used to measure viscosity. A mass flow meter (M13, Bronkhorst Cori-Tech BV) was used to measure density. A drop shape analyzer (DSA 100, Krus GmbH) was used to measure the surface tension of dyed liquids using the pendant drop technique ([Waghmare and Mitra, 2010](#)). The physical properties of liquids are summarized in Table 5.1. Physical properties of dyed and pure paraffin oil have 0.67 % and 0.83 % deviation for surface tension and viscosity, respectively. Dyed water has 5.6 % deviation for surface tension. Considering difficulties associated with measuring surface tension of water, it is an acceptable deviation. Hence, both liquids can be used for the experiments without significant effect on results due to presence of dye.

The emulsion used for experiments was produced *ex-situ*. It is stable and oil-in-water type with composition of 70.75 wt % oil and 29.25 wt % water ([Corp., 2012](#)). Quadrise Canada Inc. provided the drop size distribution which is shown in Figure 5.6. It shows normalized a Gaussian curve, which is available in the literature as was discussed earlier. A microscopic image of diluted emulsion in phos-

Table 5.1: The physical properties of the liquids.

Liquid	Density, kg/m <sup>3</sup>	Viscosity, mPa·s	Surface tension, mN/m
Water†	1000	1.0 at 100 s <sup>-1</sup>	72.40
Dyed Water	1000.4	1.0 at 500 s <sup>-1</sup>	68.33
Paraffin oil†	868	120.5 at 100 s <sup>-1</sup>	29.85
Dyed Paraffin oil	867	119.5 at 100 s <sup>-1</sup>	29.65
Emulsion†	1014	495 at 100 s <sup>-1</sup>	n/d

† - Properties for clear liquids are taken from results reported in previous Chapters

phate buffered saline pH 7.4 (PBS) solution and stabilized with surfactant (Tween 20, CAS Number 9005-64-5, obtained from Sigma-Aldrich Co. LCC) is shown in Figure 5.7. The optimal concentration was found to be 2  $\mu\text{L}$  of emulsion in 49  $\mu\text{L}$  of PBS with 1  $\mu\text{L}$  of surfactant. Two dimensional groups can be identified from this image. First group shows the size of the drops close to 2  $\mu\text{m}$ , while second group stays in a range of 10  $\mu\text{m}$ . It is an evidence that the current emulsion has bimodal structure, namely two groups of particles. In order to prove the hypothesis for presence of bi-dispersal structure, emulsion has been tested using two particle analyzers (qNano and qMicro, Izon Science Ltd.). These particle analyzers use different membranes to count particles individually and provide total count per volume of liquid. Emulsion was diluted in 25 % PBS. Obtained results are presented in Figure 5.8. It provides evidence that emulsion consists of two distinct group of particles around 1.5  $\mu\text{m}$  and 9  $\mu\text{m}$ . The obtained curve is different compared to the supplied. Previously reported data in the literature does not provide such evidence either ([Wasan et al., 1978](#); [Romero et al., 2011](#); [Moradi et al., 2011](#); [Romero et al., 2006](#)). DSD is an important parameter in fundamental theory of emulsion flooding. Having data different from existing in the literature leads to the reviewing existing

models which covers emulsion flooding process with the presence of single group of oil particles. However, it does not consider as part of the field of study in the current research project.

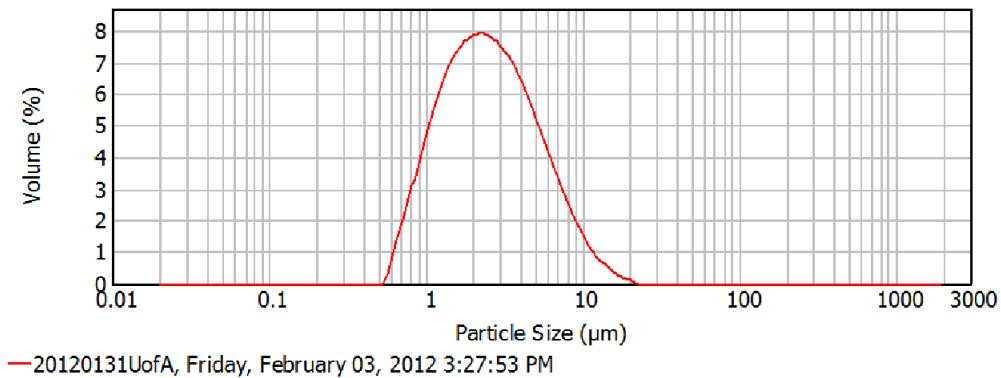


Figure 5.6: Drop size distribution measured by Quadrise Canada Inc.

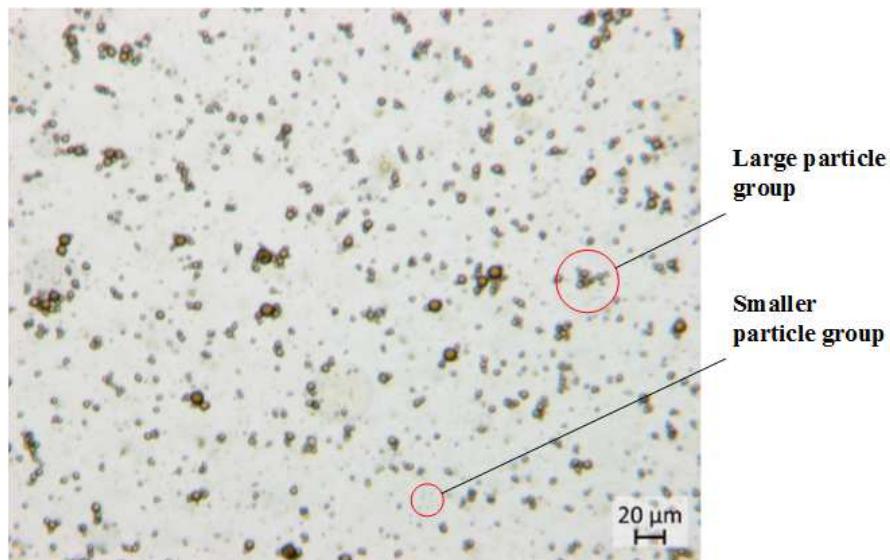


Figure 5.7: Microscopic picture of diluted oil-in-water emulsion in phosphate buffered saline (PBS), pH 7.4 (Magnification: 11.13x, Total magnification: 256.08x). The picture was taken using motorized fluorescence stereo zoom microscope (Axio Zoom.V16, Carl Zeiss AG).

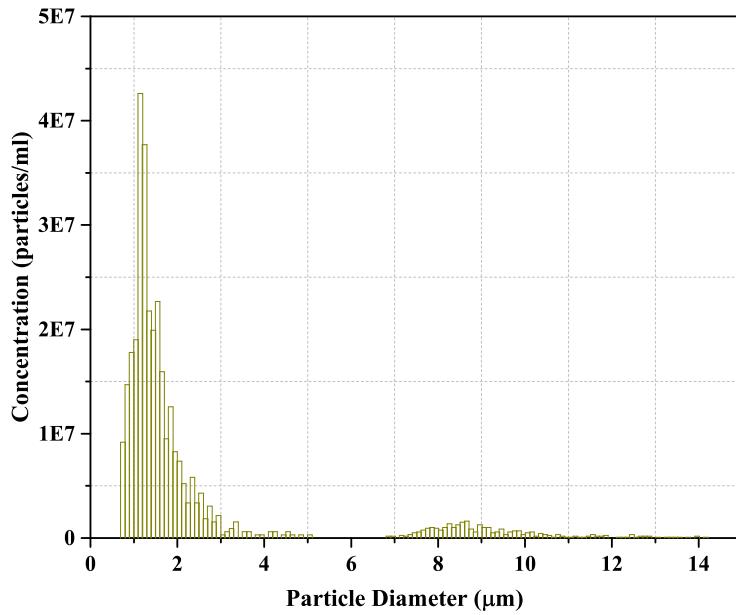


Figure 5.8: Drop size distribution measured using two particle analyzers (qNano and qMicro, Izon Science Ltd.).

The 2D core holder has been packed with unconsolidated sand from two batches. For Run #8 and Run #9, dry water-wet silica sand (Ottawa IL sand deposit, US sieve size #10 (100-140), particle size 53-251  $\mu\text{m}$ ) was used and for Run #10, dry water-wet testing silica sand (AGSCO Part #SSS000080-B5MBNK, US sieve size #10 (100-140), particle size 53-251  $\mu\text{m}$ ) was used. In order to prove that these sands can form similar porous media structure, an automatic pore size analyses (PoreMaster 33, Quantachrome Instruments) was used to measure the pore size distribution. Identical distributions were found for two batches, as it is shown in Figure 5.9. The pore size has distribution from 0.003  $\mu\text{m}$  to 109.71  $\mu\text{m}$  and 0.003  $\mu\text{m}$  to 107.51  $\mu\text{m}$  with an average 12.631  $\mu\text{m}$  and 17.27  $\mu\text{m}$  for silica sand and testing silica sand, respectively. Thus, sand packs would have similar pore size distributions and wetting properties.

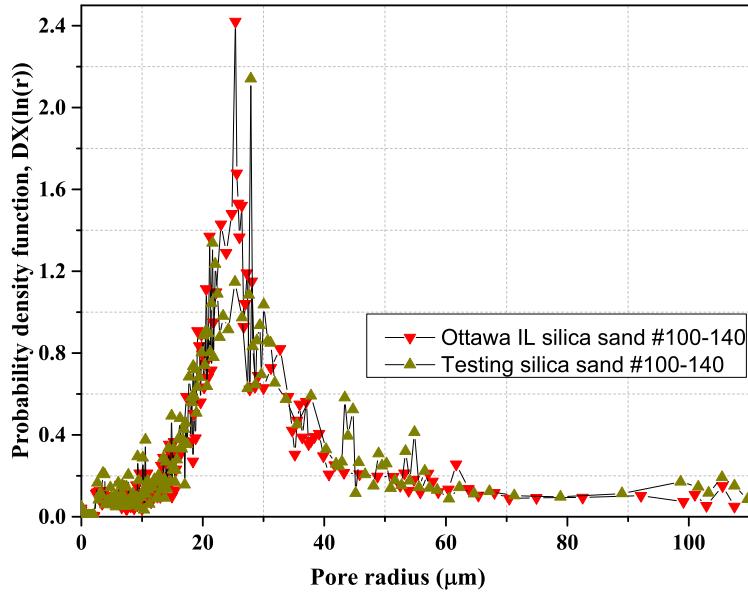


Figure 5.9: Pore size distribution of studied silica sands.

The sand packing process was different compared to previously described for biaxial core holders. The core holder was oriented vertically and fixed into the base. Dry sand with known mass was poured into the 2D core holder through the slot located at the top of the main frame. A concrete vibrator were applied on a stainless steel side of core holder for 15 minutes to create dense pack. Additional sand was added during this process, if required. At the end of this process, the slot was covered with profiled cap and compressed with top cap using bolts.

In order to saturate the core holder with water and estimate the pore volume, one side was connected to the vacuum pump (117, Labconco Corp.) and another one to a vacuum gauge. The vacuum pump was turned on for 60 minutes to guarantee vacuum level at 4 kPa absolute (28 in. mercury gauge). Once the desired vacuum level was reached, the vacuum pump was disconnected and a reservoir with a known volume of water was connected. The mass of the reservoir was measured before and

Table 5.2: Relevant parameters for unconsolidated sand pack samples used in flooding experiments.

Pack	Well configuration	Porosity, %	Pore volume, cm <sup>3</sup>	Mass of sand pack, g	Absolute permeability, Darcy	Permeability with residual water, Darcy	$S_{wi}^{\ddagger}$
Run #8	VI-VP	35.4	847.1	4107.5	$0.973 \pm 0.063$	$0.497 \pm 0.088$	0.114
Run #9	VI-HP	34.6	827.7	4159.0	$0.630 \pm 0.083$	$0.248 \pm 0.006$	0.022
Run #10	HI-HP	34.3	820.1	4179.2	$0.468 \pm 0.074$	$0.379 \pm 0.053$	0.057

‡ - Residual water saturation after oil saturation.

after connection using portable balance (SPE6001, OHAUS Canada, Co.). Taking into account the density of water and the difference in volume before and after and internal dead volumes for fittings and the core holder, the pore volume was recorded.

The procedures for absolute permeability, permeability with residual water saturation and residual water saturation after oil saturation are identical to the previously discussed for biaxial core holders. The only difference in flow rates, the flow rate for oil saturation was kept at 1.75 cm<sup>3</sup>/min and was changed to 2.00 cm<sup>3</sup>/min at the end of oil saturation process. Relevant parameters for unconsolidated sand pack samples are summarised in Table 5.2.

## 5.4 Results and Discussion

The main objective of this study was to understand the behavior of emulsion flooding process in a 2D and identify the effect from well configuration on ultimate oil recovery and *in-situ* velocity profiles. The modified system has been used to carry out experiments. In this section, detailed results for visualization experiments with three well configurations, vertical injection - vertical production (VI-VP), vertical injection - horizontal production (VI-HP) and horizontal injection - horizontal production (HI-HP) have been provided along with *in-situ* the pressure mapping analysis. Since the data for the water flooding has been reported before (Santosh et al., 2007), this work focuses mainly on post water flooding process - emulsion flooding. The water flooding at  $1.75 \text{ cm}^3/\text{min}$  was performed up to 2.05 PV, 2.54 PV and 2.12 PV of water injection for VI-VP, VI-HP and HI-HP, respectively, and continued with emulsion flooding at  $1.00 \text{ cm}^3/\text{min}$ .

Image analysis was performed to compare collected photographs at different stages of experiment and understand the *in-situ* interactions. A pressure mapping analysis was used to provide support to the image analysis. Also, the effluent collected into test tubes was analyzed and effect from the configuration. The quantitative analysis is given from analysis of velocity profiles which has been compiled using processing code.

### 5.4.1 Visual Analysis

An example snapshot from the emulsion flooding process after water flooding is shown in Figure 5.10. The direction for the liquid flow is from the left to the right, and injection and production well was installed on the left and right side, respec-

tively. The emulsion flood front can be identified due to high contrast between emulsion, oil and water. Trapped oil is an oil saturated region which is surrounded with low permeable zones. The region preferably saturated with water is named as water saturation region. A morphologically unstable interface between emulsion and oil/water present in a porous media forms a pattern, emulsion channeling (Blackwell et al., 1959). Locations for velocity measurements and wells and over all dimensions are also shown in Figure 5.10. The dark colour represents emulsion, yellow color represents water and red color represents oil saturated regions. During sand packing process different sand patterns can be formed, as it is shown in Figure 5.10.

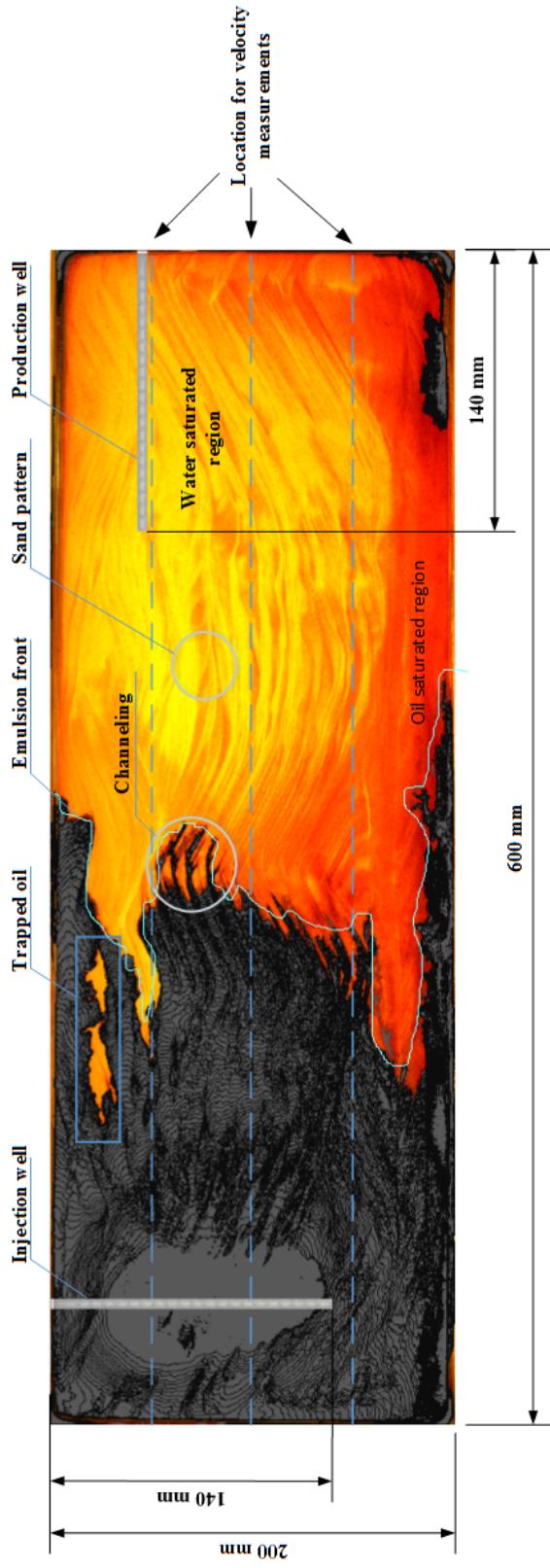


Figure 5.10: An example snapshot from the emulsion flooding process after water flooding.

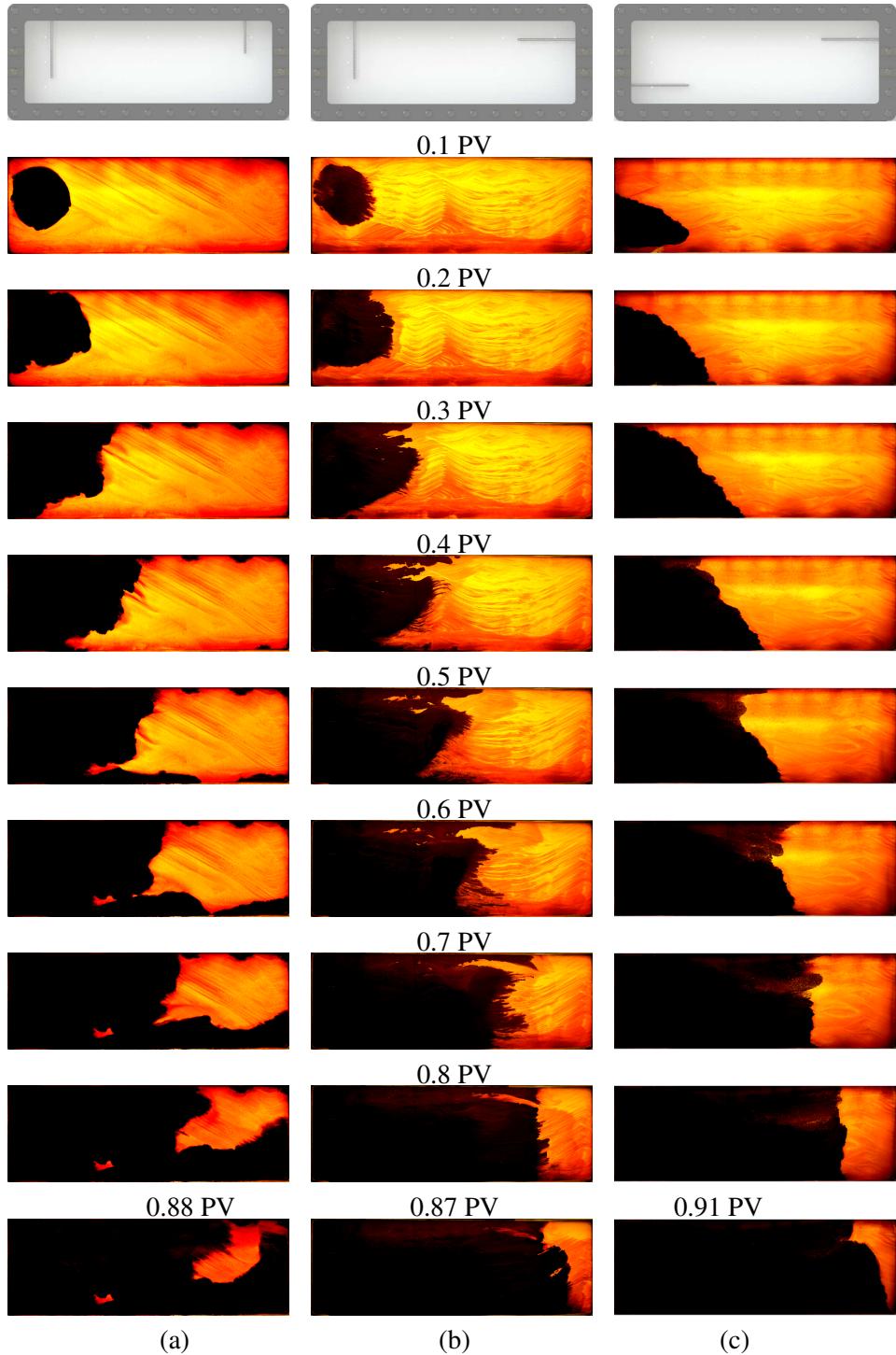


Figure 5.11: Cross-section images of the sand pack for different configurations: (a) VI-VP; (b) VI-HP; (c) HI-HP.

The photographs in Figure 5.11 (a)-(c) show snapshots of the 2D core holder at different pore volumes of emulsion injection for the studied configurations. Well configuration for each column is shown in the first image. Injection wells were half-perforated for vertical injection configurations and fully perforated for others with previously discussed perforation pattern.

In general, the pattern for the emulsion has similarities for VI-VP, VI-HP and HI-HP at the beginning of injection process, as it is shown in Figure 5.11 for 0.1, 0.2, and 0.3 PV of emulsion injection. The emulsion fills a region close to the left boundary first and then progresses towards the production well. For VI-VP, emulsion uses boundaries at first, due to slippage along the wall formed after water flooding process. It caused oil to be trapped inside the reservoir for VI-VP and VI-HP, as it is shown on last images in Figure 5.11. Emulsion pushes oil through the sand pack and forms a new oil saturated front. It can be observed compare images for 0.2 and 0.3 PV of emulsion injection.

An emulsion can block high permeable zones first during flooding process and re-direct post-flooding into high oil saturated regions. There is evidence of emulsion channeling in VI-VP and VI-HP configurations, as it is shown in Figure 5.11 (a) and (b). During water flooding water saturated channels inside the sand pattern are formed. The *in-situ* process at the scale of pore can be described as, oil drops present in the emulsion start to coalesce when the emulsion interacts with porous structure full of water and surfactant concentration drops down to a critical level. The result of this process is a significant local viscosity reduction for the emulsion. Taking into account that injection flow rate remains the same, local pressure reduction can occur in accordance with Poiseuille equation. This process can cause local

instabilities (Blackwell et al., 1959; Weitz et al., 1987) for the flow and the interface between two liquids cannot be predicted easily and channeling can form. Collected images support this hypothesis.

While HI-HP showed least oil production during water flooding, shown in Figure 5.11 (c), less high permeable zones were formed. As a results, the emulsion front has piston-like behaviour (Sarma et al., 1998; Shah et al., 2010; Mahmood and Brigham, 1987) and no channeling can be observed. Similar results were obtained during analysis of extracted sand packs from biaxial core holder in Chapter 3.

Flow visualization shows that VI-VP has a higher recovery during the water flooding process. However, emulsion flooding was not effective and caused oil to be trapped behind the emulsion front. At the same time, HI-HP was the most stable method for the emulsion injection after water flooding process.

### 5.4.2 Pressure Maps

Data collected from 15 pressure sensors was analyzed and plotted as filled contour plot. The filled contour plots represent the pressure map inside the 2D core holder, as it is shown in Figures 5.12 - 5.20, at given amounts of emulsion injected into porous media. From analysis of the data it was found that the maximum pressure gained during emulsion flooding inside the core holder is different from configuration to configuration. The maximum pressure drop across the core holder was found to be 9.5 psi, 59.4 psi and 114.4 psi for Run #8, Run #9 and Run #10, respectively. The color bars on the contour plots are set for three ranges 0 to 10 psi, 0 to 60 psi and 0 to 115 psi, respectively to the maximum pressure for each configuration. The difference in pressure drop scale from experiment to experiment is due to initial

conditions of porous media prior emulsion flooding. In Run #8 with VI-VP configuration, most of the oil was washed out during water flooding, even close to the boundaries. It allowed emulsion to penetrate through porous media without resistance, slipped along boundary and resulted in 10 psi pressure rise. While for Run #9 with VI-HP configuration, sand pack was still highly oil saturated, as it is shown in Figure 5.11 (b), after water flooding, emulsion at first blocked high permeable zones and proceeded with a piston-line flood front pattern. It resulted in a continuous pressure rise up to 59.4 psi at the end of emulsion flooding process. Similar was to Run #9 was found for Run #10 with even higher rise up to 114.4 psi.

The pressure during VI-VP rises after the initiation of the injection process and reaches a maximum around 0.4 PV of emulsion injection, as it is shown in Figure 5.15. After this point, pressure returns to the initial point. Comparing the pressure map with cross-section images for VI-VP, it can be seen that the emulsion slips across the boundary after 0.4 PV of emulsion injection and the drop in pressure values happened at the same time. Hence, there is *in-situ* bypassing process during VI-VP configuration.

For other configurations, VI-HP and HI-HP, pressure raises from the start of the emulsion flooding process and continues to a maximum by the end of injection, as it is shown in Figure 5.20. The direction of pressure contours has similarities with the emulsion front shown in the cross-section images. For HI-HP configuration in Figures 5.17 and 5.18, the front of emulsion goes with the same angle to the horizontal plane. Similar contours are found in the pressure maps. However, there are still differences in the data. A low pressure gap in the pressure data is observed for all configuration compared to the image data with continuous emulsion slug along

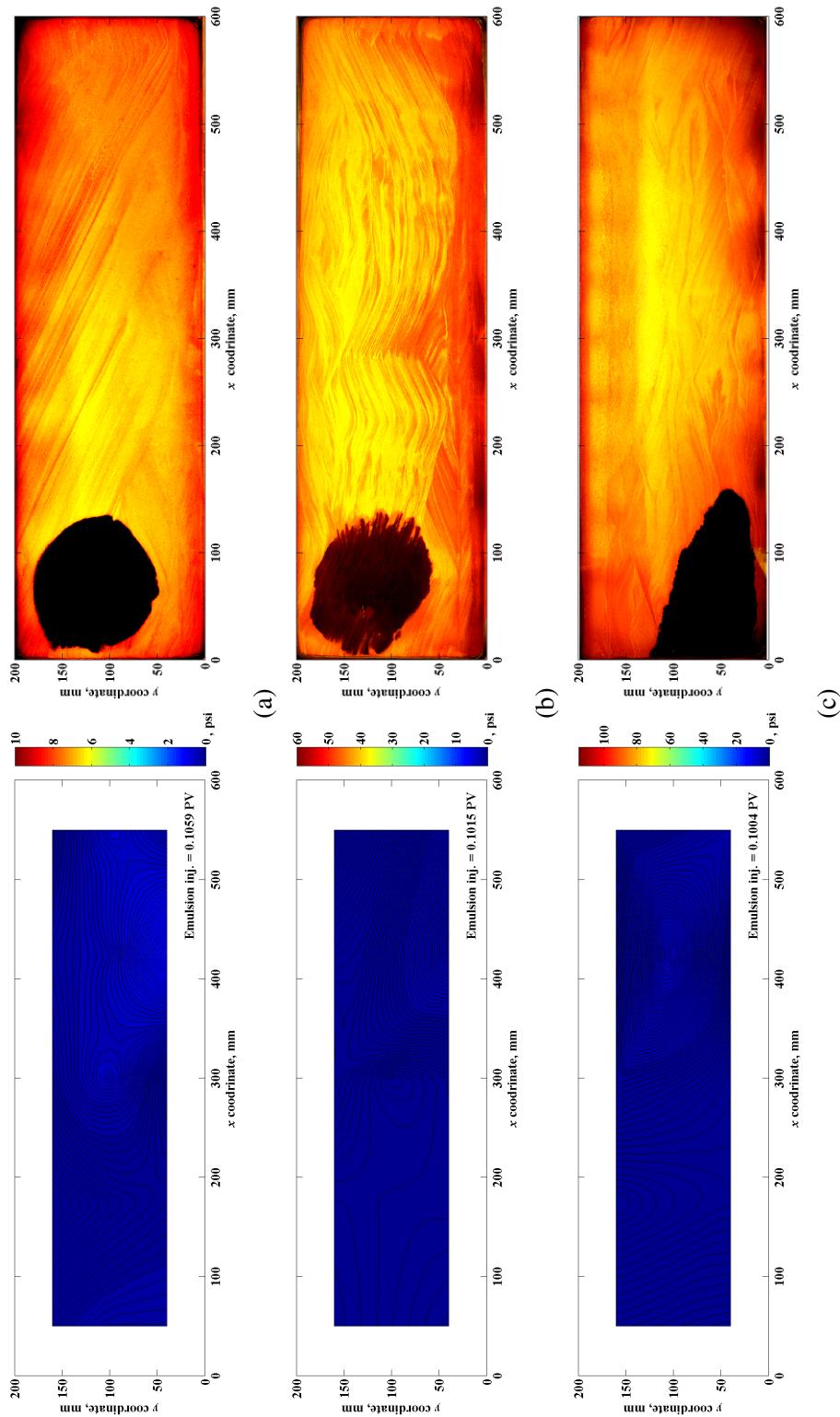


Figure 5.12: Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration.

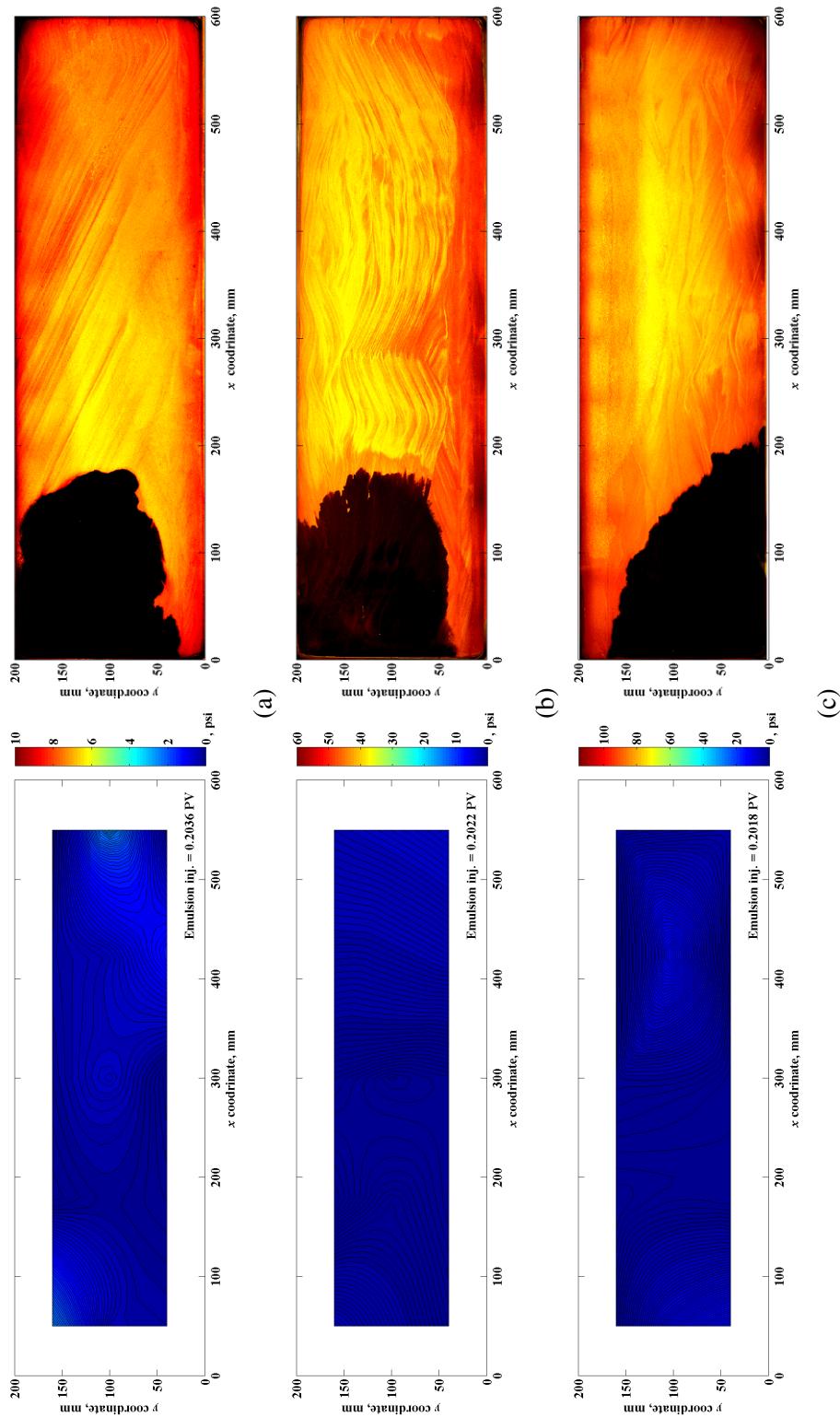


Figure 5.13: Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration.

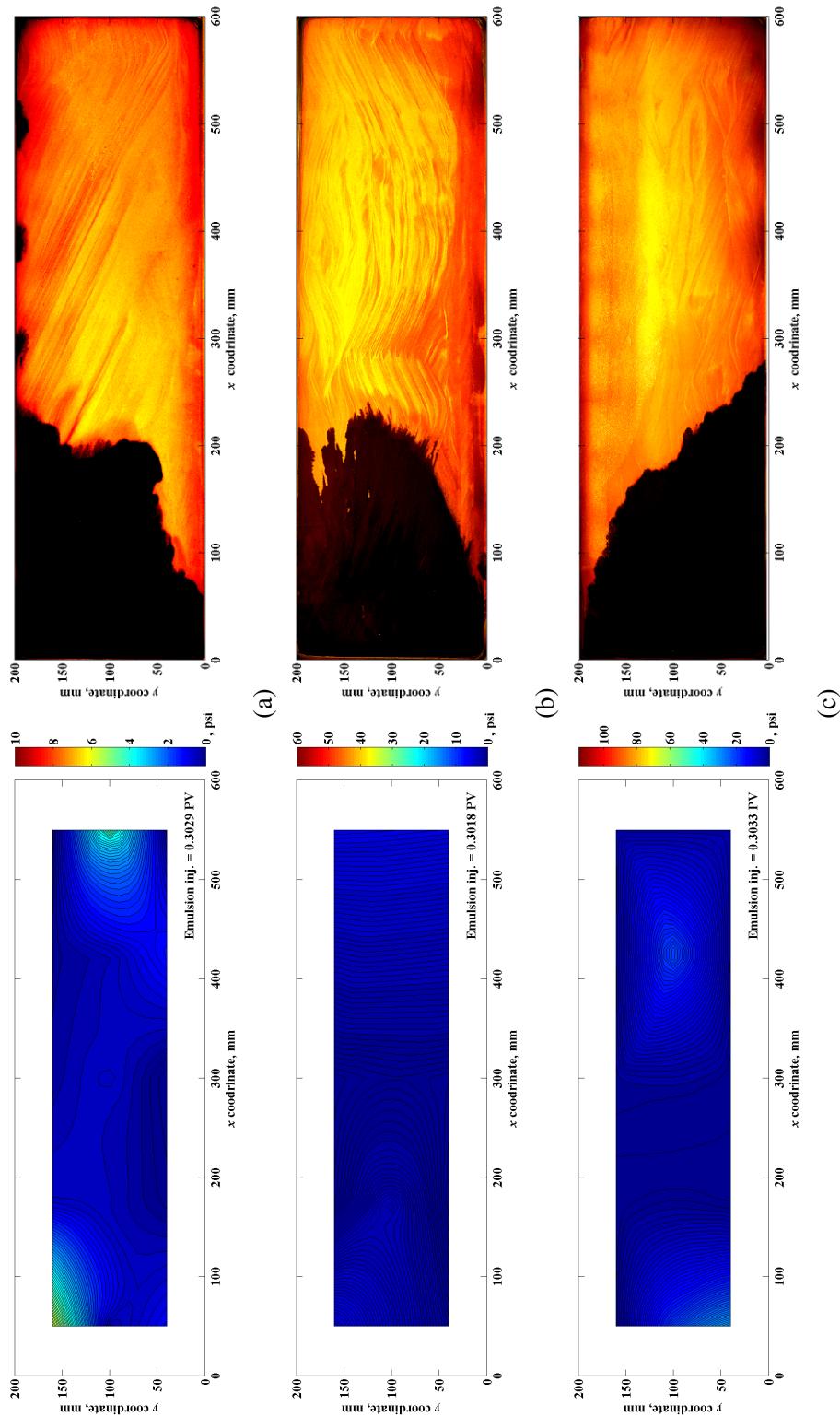


Figure 5.14: Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration.

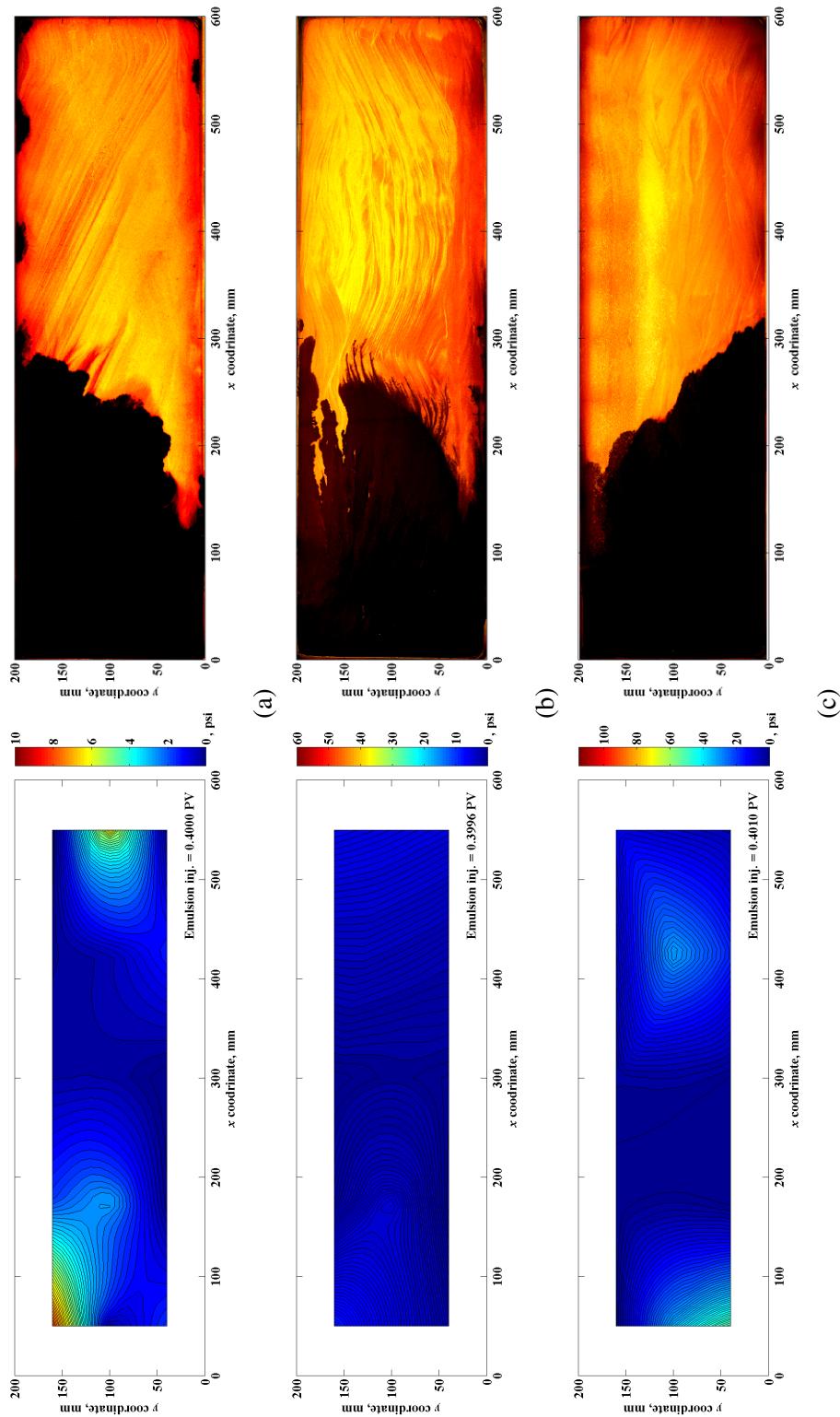


Figure 5.15: Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration.

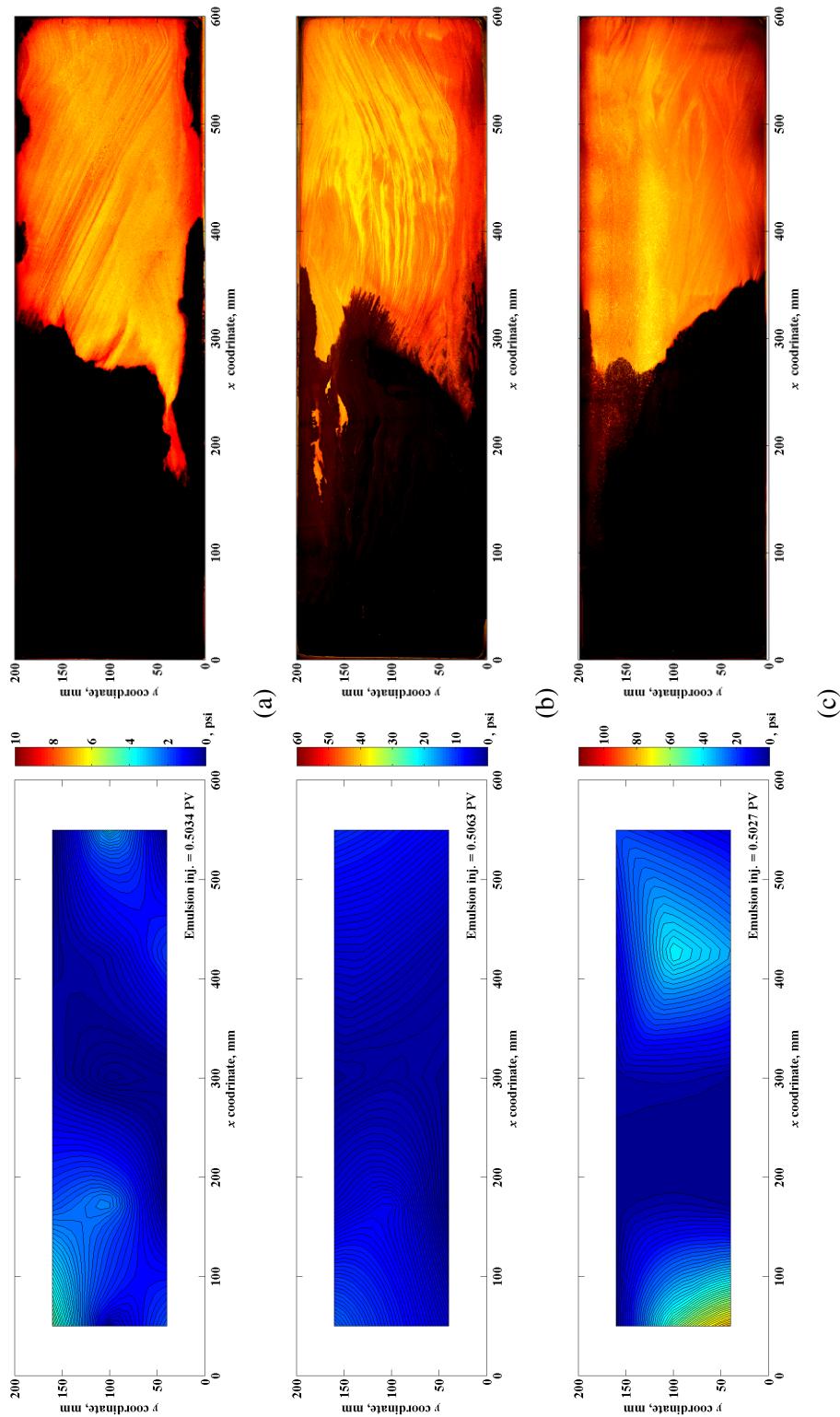


Figure 5.16: Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration.

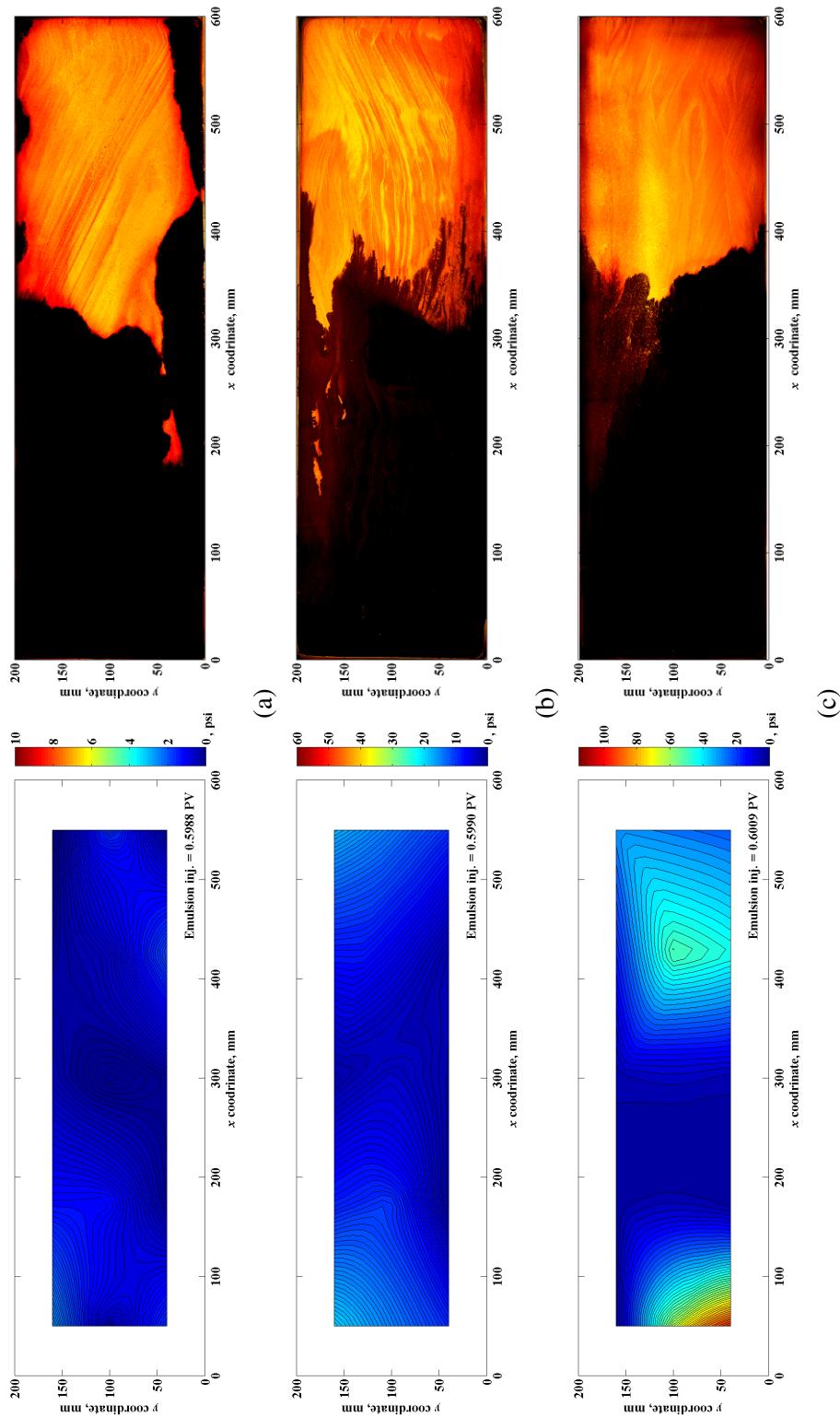


Figure 5.17: Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration.

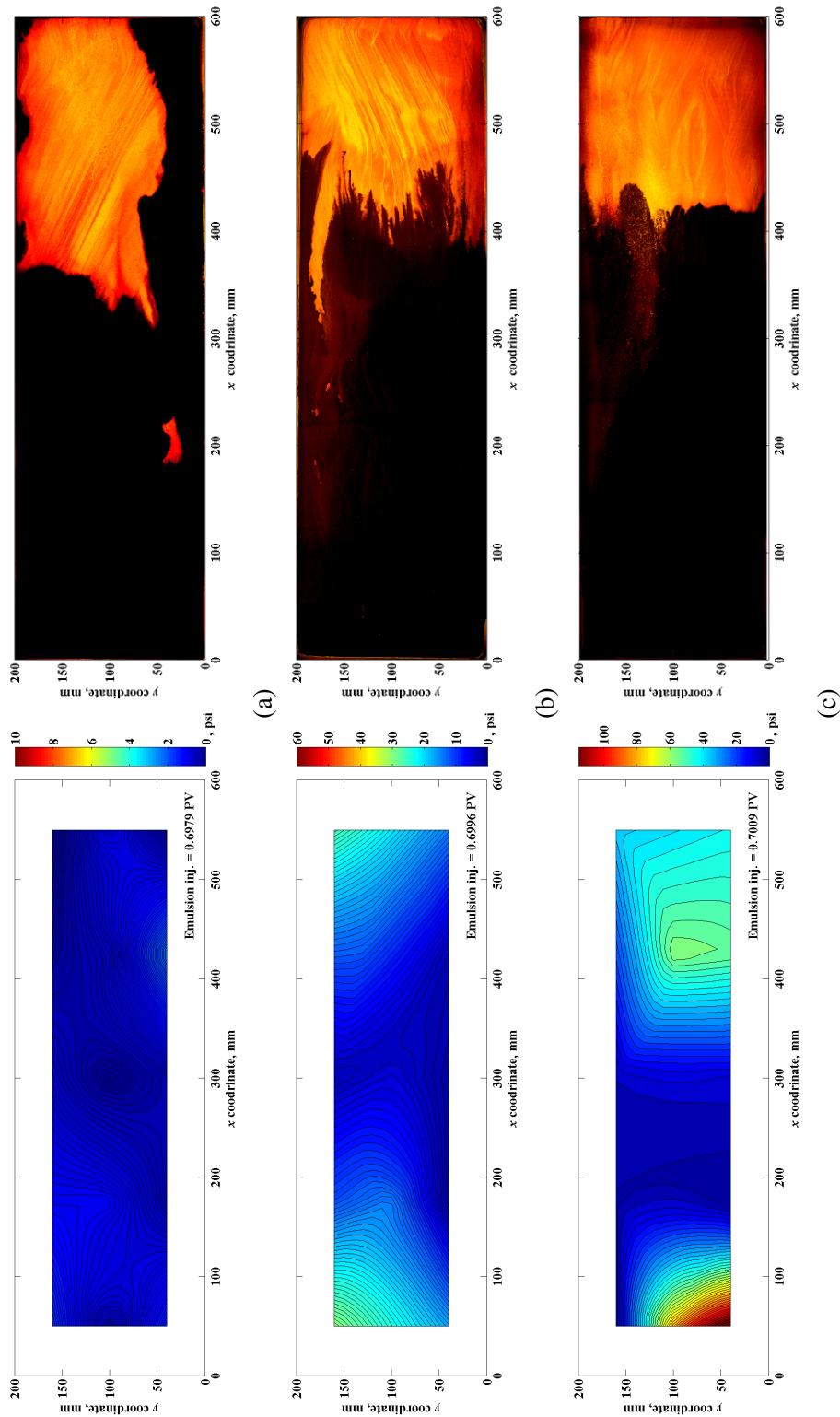


Figure 5.18: Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration.

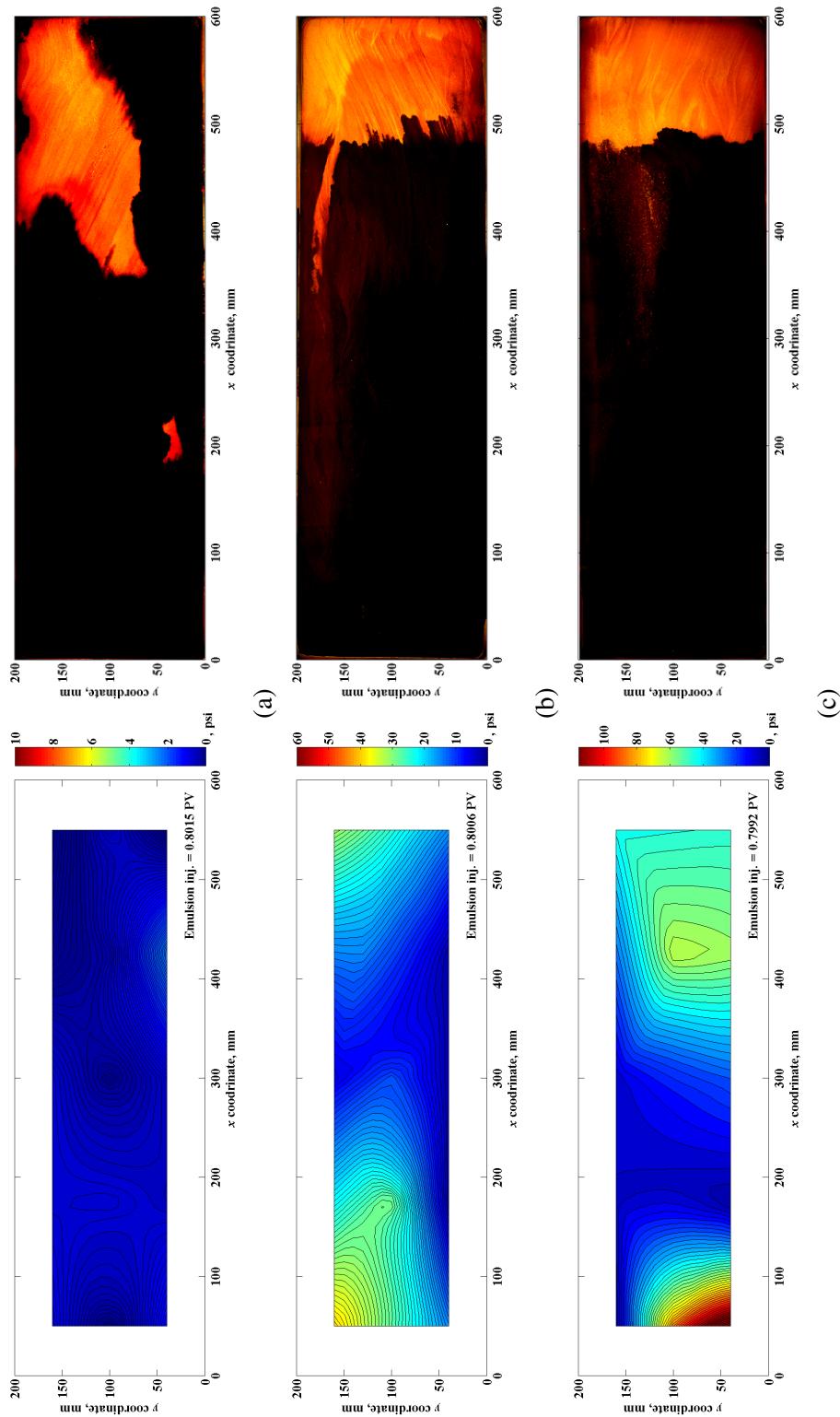


Figure 5.19: Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration.

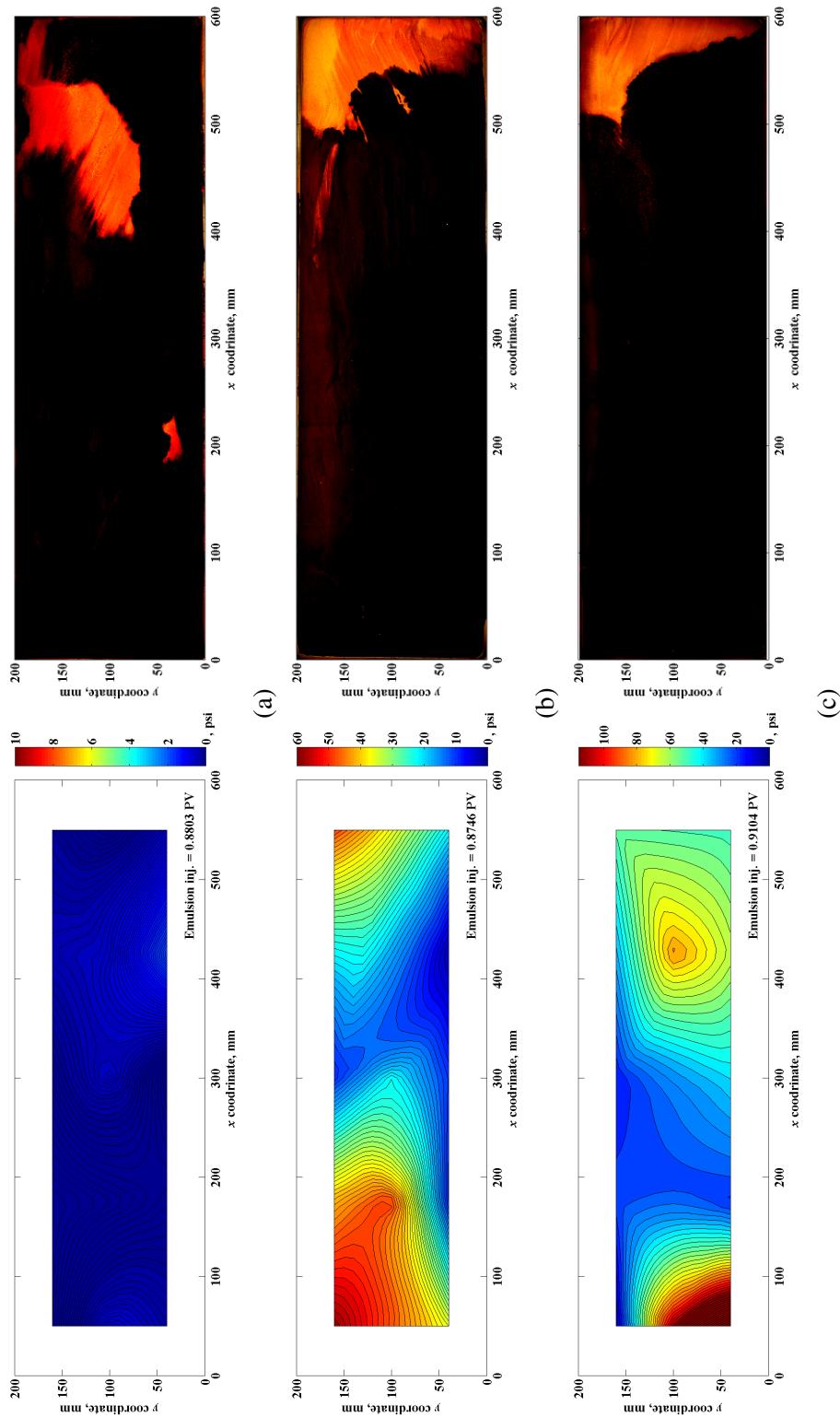


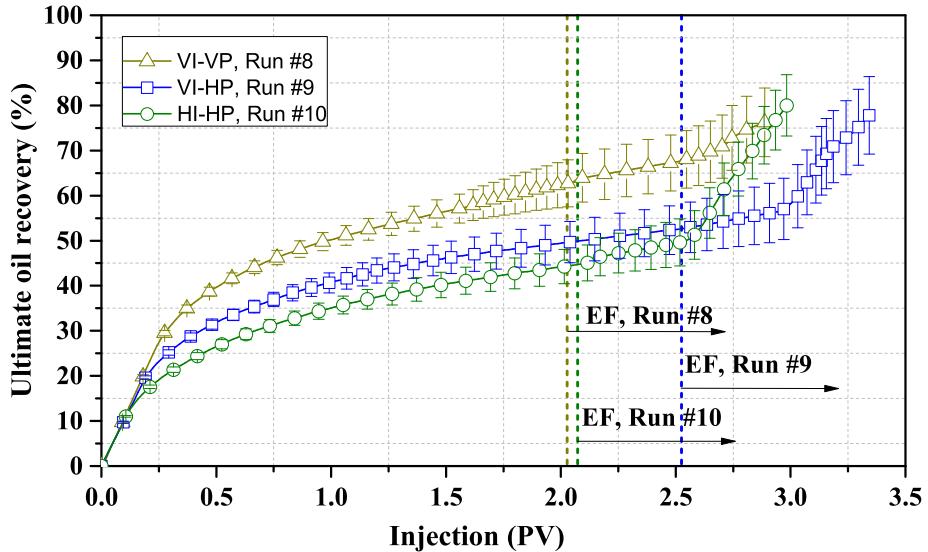
Figure 5.20: Comparison of pressure maps and cross-sectional images of sand packs in: (a) VI-VP; (b) VI-HP; (c) HI-HP configuration.

the flow direction. This can be due to the lack of data close to the boundaries where emulsion is possibly trying to slip through and builds up internal pressure. Due to the the lack of data points between pressure sensors and close to the boundaries, clear answer cannot be outlined.

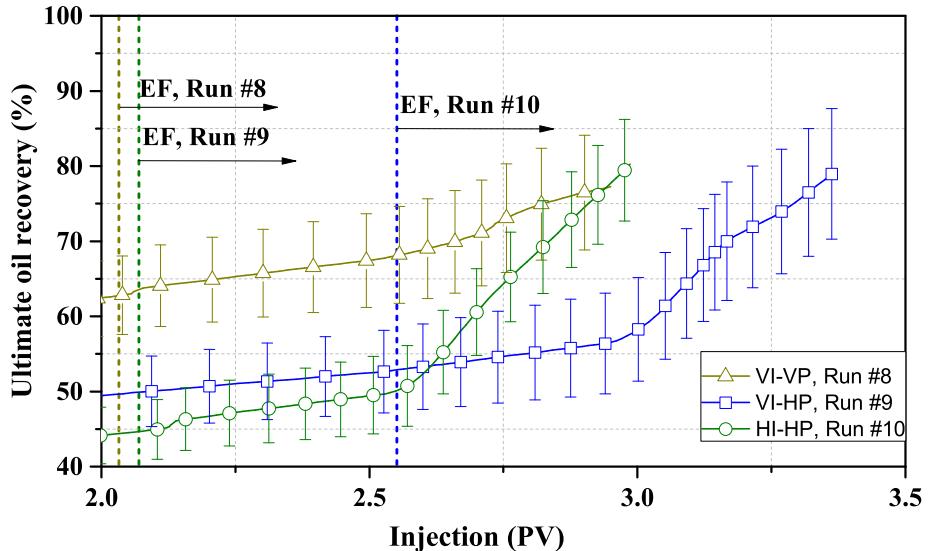
### **5.4.3 Effluent Analysis**

Compared to the previous effluent analysis undertaken in previous experiments with 1D core holder, for the 2D core holder, the process of gravity segregation was stimulated using a centrifuge (Part #EW-17414-21, Cole-Parmer Canada, Inc.). The test tubes collected with fraction collector were centrifuged at 4000 rpm for one minute. The configuration with one minute and 4000 rpm was found experimentally as the most time-efficient.

Figure 5.21 (a) shows the ultimate oil recovery curves for the three different well configurations used in a 2D core holder. The data for recovery curves was collected from the test tubes after centrifuge. In order to compare data from different experiments, the injected volume was normalized using respected pore volume (PV). In terms of oil recovery during water flooding, it was found that VI-VP is the most efficient configuration. At least 19 % more can be recovered compare to others at 2 PV of water injection. This result mainly can be due to a delayed break through point and significantly larger distance between wells surfaces in horizontal direction.



(a)



(b)

Figure 5.21: Ultimate oil recovery curves for water flooding followed by emulsion flooding at different well configurations: (a) complete flooding process and (b) emulsion flooding process after water flooding.

Figure 5.21 (b) shows a zoomed view of the recovery trends. VI-VP configuration is not as efficient for the emulsion flooding as for the water flooding, only 14 % can be recovered at 0.9 PV emulsion injection. For the studied parameters, it is observed that the most efficient configuration for the emulsion flooding is HI-HP, almost 34.75 % of OOIP can be additionally recovered from reservoir. The ultimate oil recovery for VI-VP, VI-HP and HI-HP are 77.2 %, 78.9 % and 80.2 %, respectively. Emulsion injection was ceased for each run, once it appeared at the effluent side. There is a delay in oil recovery after the emulsion is introduced to the porous media. Oil and water require time to form new fronts inside the porous media and initially only water is present in the effluent.

Similar observations were made from image analysis and pressure mapping analysis. The lowest pressure drop across the core holder measured during emulsion flooding was found in VI-VP configuration, where emulsion flooding was found to be ineffective process in terms of oil recovery. While the pressure drop across the core holder gradually increases in VI-HP and HI-HP configurations up to 59.4 psi and 114.4 psi, respectively, and caused higher production rates. Hence, the *in-situ* pressure rise has connection to the efficiency of emulsion flooding process.

#### 5.4.4 Quantitative Analysis

In order to estimate the behavior of emulsion flooding and provide a reasonable explanation for the velocity profiles, reference photographs are taken after oil saturation was completion and after water flooding completion at different configurations. These are shown in Figure 5.22. In addition, the last column shows evolution of the fractal interface of emulsion injection collected using commercial image analysis

software (Image-Pro Premier 9.1, Media Cybernetics, Inc.). The interface shows the boundaries of emulsion filled regions collected from each image. The background for the interface is post water flooding condition. The denser region means slower progress for the interface over single time step.

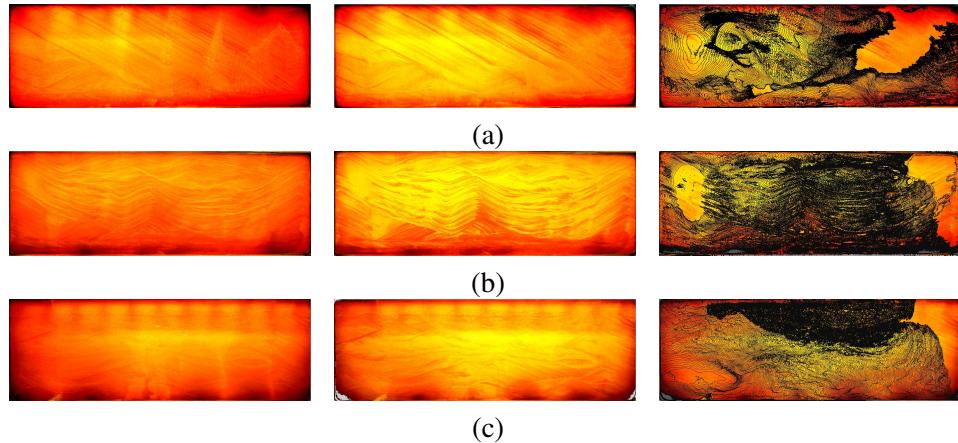


Figure 5.22: Left column shows sand pack prior to water flooding, central column shows sand pack prior emulsion flooding, right column shows evolution of interface of emulsion injection in (a) VI-VP configuration; (b) VI-HP configuration; (c) HI-HP configuration. Here, the direction of injection is from left to right.

After water flooding, most of the oil was washed out from central part of the core holder as represented by the yellow dyed water presented in Figure 5.22 (b). The least amount was for HI-HP, the most was for VI-VP, as it can be noticed on Figure 5.22 (a) and Figure 5.22 (c) and was previously confirmed with effluent analysis.

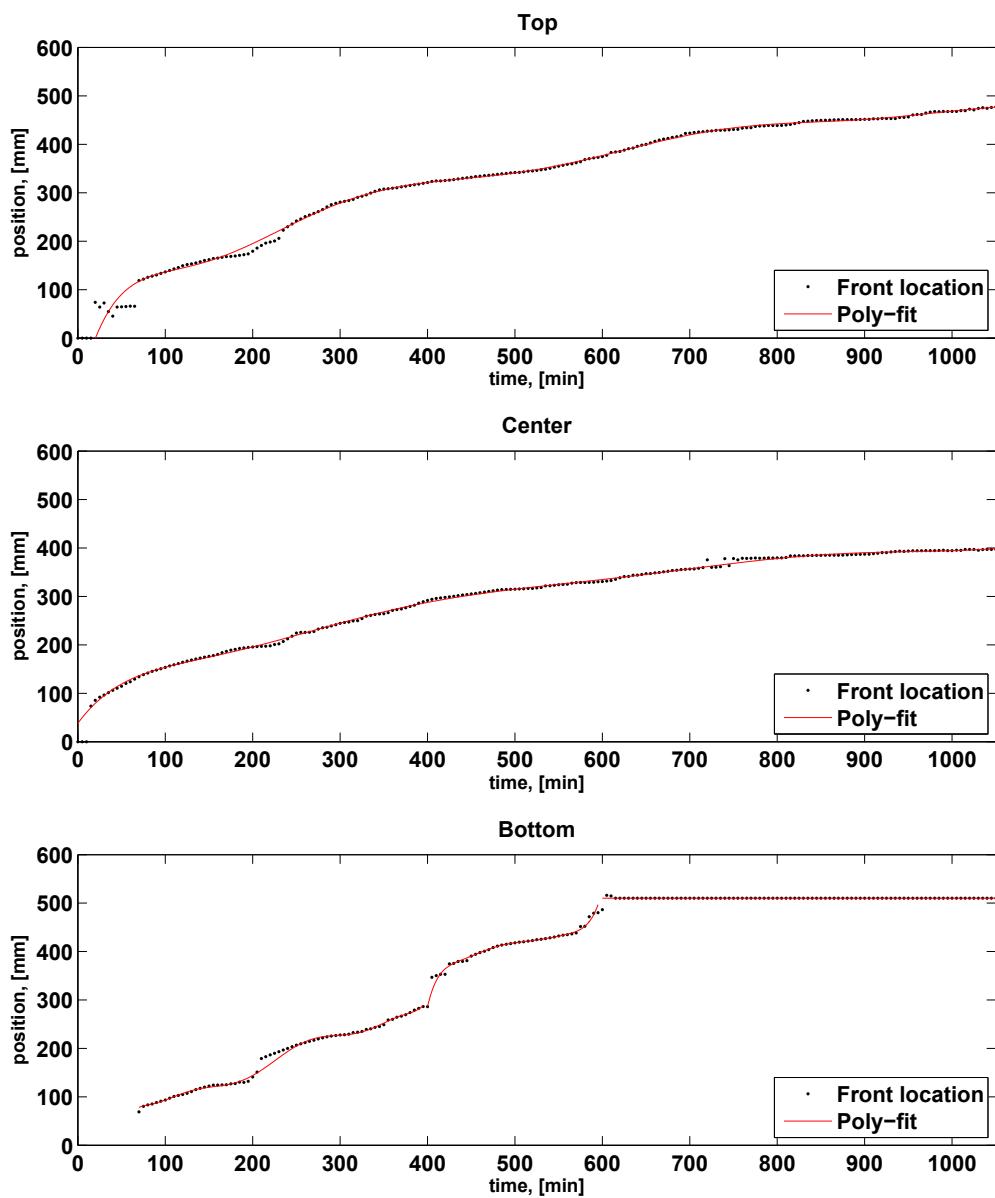


Figure 5.23: Emulsion front position versus time at three locations of a sand pack (a) top; (b) center; (c) bottom, as it is shown in reference Figure 5.10, for VI-VP configuration.

The position of the front plotted over the time for VI-VP configuration is shown in Figure 5.23. The position for the flood front follows a smooth curve for top and center locations. It also remains constant for bottom location at the 600 min due to a reflected flow from the right boundary. The order of cubic polynomial function fit is nine for top and eight for center location. For the bottom, the curve was divided into three regions, from 0 to 480 min, from 480 to 600 min and from 600 to ongoing. The orders for cubic polynomial function fits are nine, eight and seven, respectively.

The position of the front plotted over time for VI-HP configuration is shown in Figure 5.24. The position for the flood front follows smooth curve for top and center locations. There are some offset point at the top. The order for cubic polynomial function fit is nine for top and seven for center location. For the bottom, the curve was divided into two regions, from 0 to 480 min, from 480 to ongoing. The orders for cubic polynomial function fits are six and seven, respectively.

The position of the front plotted over time for HI-HP configuration is shown in Figure 5.25. The position for the flood front follows smooth curve for all three locations. The order for cubic polynomial function fit is 9, 7 and 6 for top, center and bottom location, respectively.

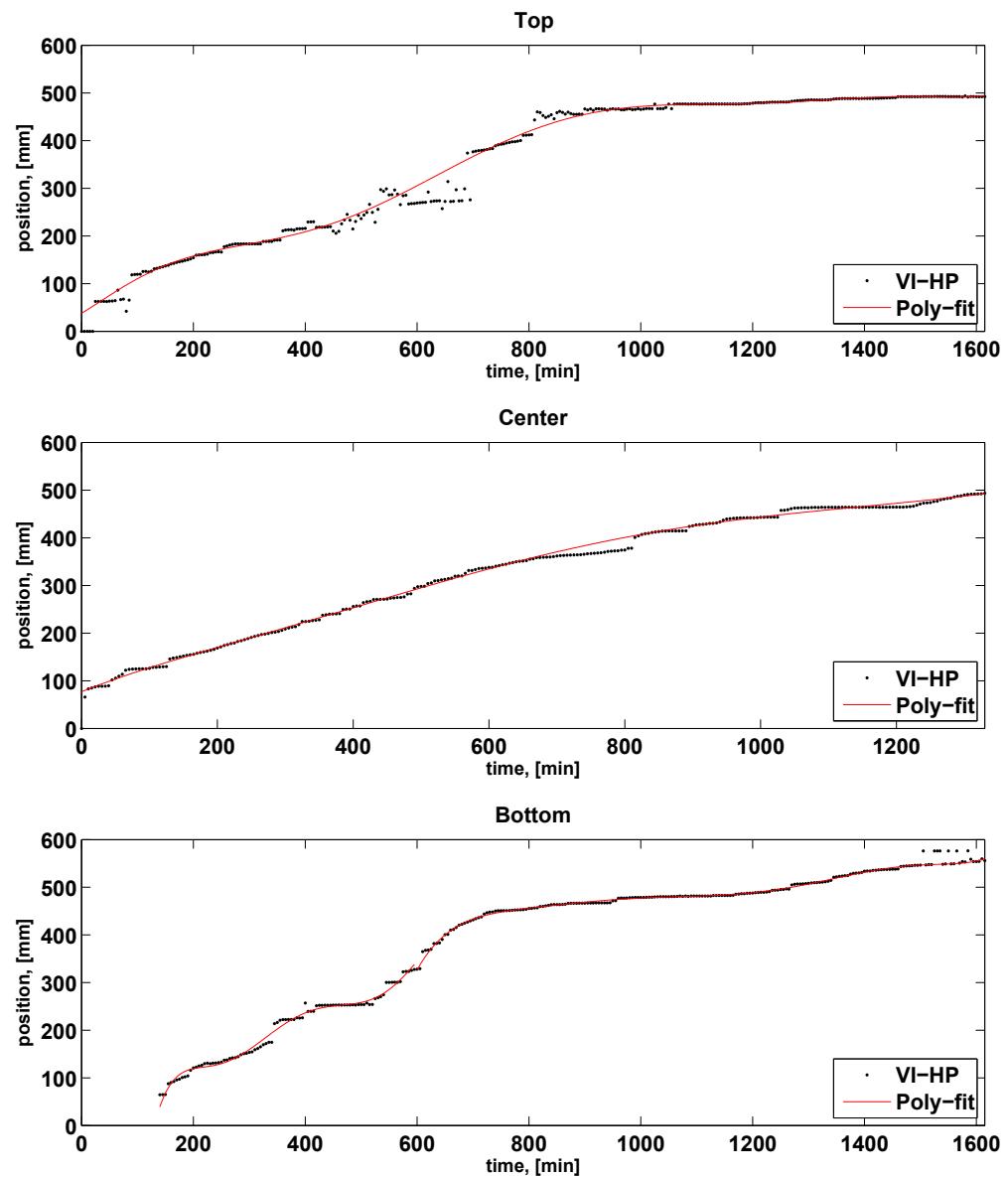


Figure 5.24: Emulsion front position versus time at three locations of a sand pack (a) top; (b) center; (c) bottom, as it is shown in reference Figure 5.10, for VI-HP configuration.

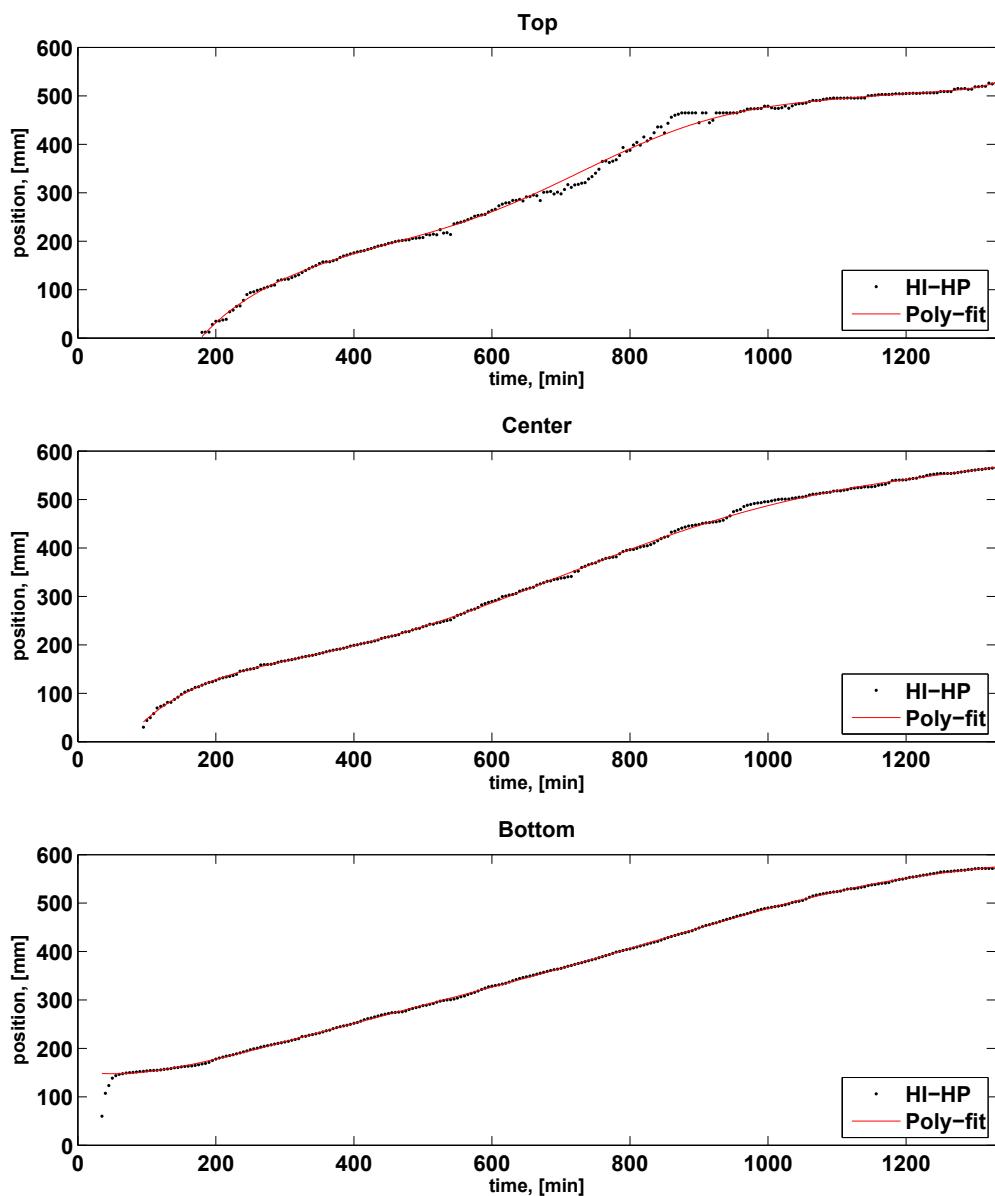


Figure 5.25: Emulsion front position versus time at three locations of a sand pack (a) top; (b) center; (c) bottom, as it is shown in reference Figure 5.10, for HI-HP configuration.

The derivatives of the collected cubic polynomial function fits were calculated to generate velocity profiles of the emulsion flood front. Figure 5.26 shows the velocity profiles versus volume of emulsion injected, collected at three locations, top, center and bottom, for each well configuration using custom developed code. The reference level for the velocity can be identified using parameters of sand packs from Table 5.2 and expected pore size distribution reported above. The superficial velocity,  $U_{\text{ref},n}$ , taking into account emulsion injection flow rate,  $Q$  (1.0 cm<sup>3</sup>/min), porosity,  $\phi_{\text{run},n}$ , and geometry of sand pack ( $h$  - height and  $w$  - width) can be written as (Darby, 2001):

$$U_{\text{ref},n} = \frac{Q}{h \cdot w \cdot \phi_{\text{run},n}} \quad (5.1)$$

For Run #8, Run #9 and Run #10 it can be found that superficial velocity can be estimated as  $1.177 \cdot 10^{-5}$  m/s,  $1.204 \cdot 10^{-5}$  m/s,  $1.215 \cdot 10^{-5}$  m/s, respectively for the emulsion flooding process. For the water flooding process with flow rate equal to 1.75 cm/m<sup>3</sup> during Run #8, Run #9 and Run #10 the superficial velocity can be estimated as  $2.06 \cdot 10^{-5}$  m/s,  $2.107 \cdot 10^{-5}$  m/s,  $2.126 \cdot 10^{-5}$  m/s, respectively. These numbers are close to the values reported earlier in previous Chapter. The superficial velocities are plotted along with emulsion front velocity for all configurations as a reference velocities.

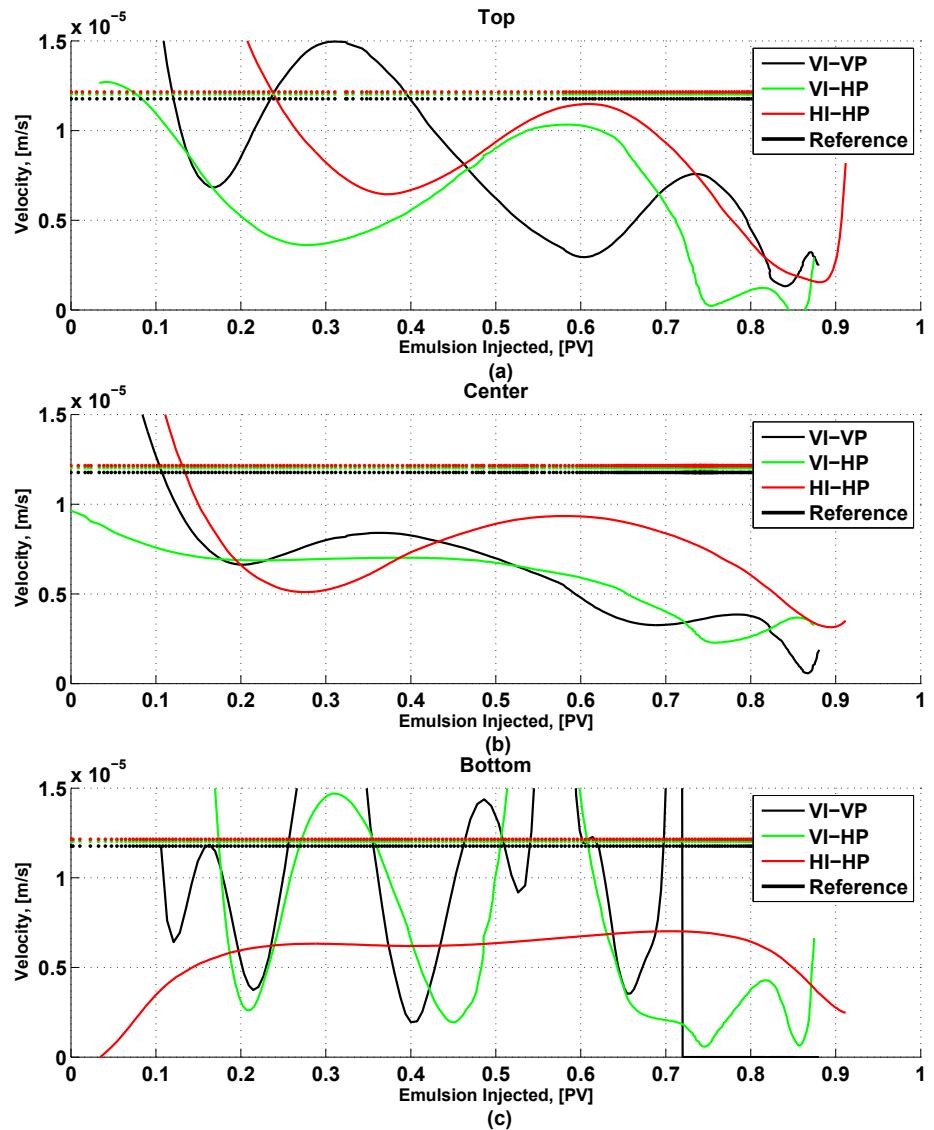


Figure 5.26: Emulsion flood front velocity at three locations of a sand pack (a) top; (b) center; (c) bottom, as it is shown in reference Figure 5.10

Velocity profiles, in Figure 5.26 (a), follow the same trend for all configurations. They fluctuated during the fronts movement across the core and slowly went down at the end of process as the front was getting closer to the production well. This can be due to presence of resident oil and its interactions with emulsion. It can be observed, that the profile was more stable for VI-HP configuration, as the least amount of oil can be observed in Figure 5.22.

Due to the presence of previously abandoned regions after water flooding at the center of the sand packs, as shown in Figure 5.22 central column, front velocity values are fluctuating close to the reference velocity level. The amplitude of fluctuations is smaller compared to the top profile, Figure 5.26 (b).

The most stable velocity profile was obtained for VI-HP configuration. Velocities for VI-VP and HI-HP follow similar trend with higher dispersion for HI-HP configuration. Compared to the top level, the velocities profiles behave more stable due to the presence of only a single liquid, water, in the porous media. By the end of emulsion flooding, front velocity stabilizes and all configurations end in the same region.

The most unstable trends for the velocity profiles were found at the bottom reference level for VI-VP and VI-HP configurations, where most of the resident oil was accumulated after water flooding, as shown in Figure 5.26 (c). However, HI-HP shows a smooth and stable curve with values close to the reference level. Horizontal injection for the emulsion allows the use of boundary conditions to guarantee improved stability for the front. From interface observation, Figure 5.22 the right column, it can be seen that emulsion progresses as piston like along the bottom surface without any instabilities. That observation can lead to the stable velocity

profile.

As it was found from the image analysis, pressure mapping and effluent analysis the most efficient and stable configuration for the water flooding followed by emulsion flooding is HI-HP. The stability of velocity profiles may also lead to the efficiency of enhanced oil recovery process, as it is also the most stable configuration.

## 5.5 Conclusion

The flow visualization and pressure mapping study has been carried out to investigate the effect from the well configuration on emulsion flooding after water flooding. Three different configurations for well orientation have been tested and analysed in terms of oil recovery and stability of the emulsion front. Visual analysis reports the pattern for the emulsion and shows *in-situ* processes happening inside porous media, such as oil trapping and channeling. Due to the presence of the red dye in oil, the region in front of emulsion turns into a red color during flow visualization. In a field test emulsion can be used to create regions with low permeability and the new well can be placed in front of the emulsion. It allows continue of oil recovery with traditional water flooding method.

Effluent analysis shows that vertical injection (VI) - vertical production (VP) is an efficient method for water flooding. However, emulsion flooding provides higher efficiency rate for the reservoirs with higher concentration for resident oil. It can be concluded that horizontal injection (HI) - horizontal production (HP) enhances oil recovery higher than any other configurations. The quantitative analysis suggests that stable velocity profile for an emulsion front can be achieved in HI-HP

configuration. While vertical injection (VI) - horizontal production (HP) and VI-VP has similar profiles to each other. It can be due to the same configuration for injection point. Obtained results can be used in future during field trials or in theory developments for the emulsion flooding.

# **Chapter 6**

## **Conclusion and Future Work**

### **6.1 Conclusion**

This study was aimed to investigate the efficiency of using emulsion flooding as a recovery agent. After reviewing the literature for physical processes inside oil reservoirs, important parameters for reservoir characterization were identified. It was also found that emulsion produced *ex-situ* and *in-situ* can be used as flooding agent. However, due to similarities in emulsion properties to the resident oil and water, extensive post-experimental analysis is required. As a result, the first priority was identified to be developing a core flooding system, which can be used in future core flooding experiments. Extensive literature review outlined the existence of traditional core flooding system and their limitations. An improved experimental apparatus was designed and constructed using up-to-date available technologies in the market. In addition, the main component of the system, core holder, was also modified. Established design for the end plugs of core holder was improved using available computational resources. It was also shown that developed apparatus can be further upgraded if it is required to study other flooding regimes. The software with graphical user interface and remote alarming system was developed to

guarantee continuous control in experiments.

Having highly controlled experimental apparatus allowed to perform benchmark experiments with oil and water and to understand the limitations of developed systems. As a result of routine core flooding experiments, an automated method for effluent analysis was developed using real time readings from the downstream mass flow meter. This method allows to automate process of core flooding experiments and collect effluent data in efficient time manner. Using this method, first experiments for enhanced oil recovery were conducted with emulsion. It was found that *ex-situ* produced emulsion has high recovery rate and it is a feasible method to recover oil from porous structure. Up to 80 % of resident oil can be recovered using direct injection or after water flooding. However, taking into account costs for emulsion production, as it was pointed out earlier, new technique for the emulsion flooding must be developed.

An alternative flooding technique for the emulsion flooding was proposed, developed and tested. This technique bases on a cyclic flooding of emulsion and water slugs through porous media with specified ratio, similar to water and steam (CSS, WAG) or water and chemicals (CAG) flooding techniques. The process was termed as water-alternate-emulsion (WAE). Collected data showed that at least an additional 20 % of a resident oil can be recovered from a reservoir compare to traditional flooding processes. It also allows the reduction of the required amount of emulsion three times compared to the direct injection. For instance, the final ultimate oil recovery was found to be 82 % of OOIP for overall 0.3 PV of emulsion injection. Sand packs were examined after experiments to provide additional understanding for the *in-situ* processes. However, it was limited due to the fact that once

pack recovered from the core holder it cannot be placed back. Thus, it was concluded that future studies with utilizing equipment for nondestructive testing, such as two dimensional (2D) core holder, of the *in-situ* process are required for more detailed understanding the interactions between different liquids inside the porous media and how the recovery curve formed during WAE strategy.

Finally, experimental flow visualization and pressure mapping analysis of emulsion flooding with horizontal and vertical wells was carried out as next step of this research project. During preparation to those experiments, it was discovered that the given emulsion has a bi-dispersal structure. A literature review showed that such structure was not previously reported in the literature. This finding leads to the reviewing existing theory about an emulsion, since it effects on *in-situ* processes happening at micro-scale, size of the pore. Testing three different configurations provided initial understanding for the emulsion flooding process at the scale of 2D core holder, which is eight times bigger compared to biaxial core holder. The velocity profiles of front floods, pressure maps and recovery curves of ultimate oil recovery were extracted and used along with collected images of the side wall. It was pointed out that the most efficient configuration for the emulsion flooding is horizontal injection - horizontal production (HII-HP). Field test trials can be now undertaken for similar reservoir conditions and geological formations. However, there is still a broad range of questions which should be answer to get the confidence that emulsion is an economically valuable process for oil recovery.

## 6.2 Future Work

Further studies can be done as a continuation of the current study and listed below:

- The biaxial holder can be replace with a modified version developed for acoustic measurement technique <sup>1</sup>. Acoustic measurements potentially can provide current saturation levels for each liquid and result in collecting data required for relative permeability curves.
- To be closer to the reservoir conditions, the core block can be modified as it is shown in Chapter 3. Sand packs will have different pore structure and might result in efficiency of emulsion flooding. Collected data can be further applied in field applications.
- In order to reproduce the real world scenario, when the reservoir has non homogeneous strata with residual oil saturation distributed within it, various configurations for strata need to be studied as well. Taking pictures from one side of the 2D visualization cell provide a map for oil, water and emulsion saturations.
- As it was shown in Chapter 5, during emulsion flooding resident oil forms a new front. Having the possibility to install new well during an experiment can be used to study the hypothesis of resuming to traditional water flooding.
- Water-alternate-emulsion (WAE) flooding technique proved to be an efficient method for oil recovery. However, it is still unclear what kind of interactions

---

<sup>1</sup>Paper in progress. M. Cassiede, A. Baldygin, A. Stephen, J. M. Shaw, D. S. Nobes, and S. K. Mitra, “Acoustic measurement technique in application to the bio-conversion of coal”, *Energy & Fuels*, 2014

present inside porous media. WAE flooding can be accomplished in 2D core holder to visualize *in-situ* process.

- Finally, the 3D core holder can be used to study complex porous media, with permeable and non-permeable zones, and complex well configurations, *e.g.* steering well.

# Bibliography

F. F. Nazzal and M. R. Wiesner. Microfiltration of emulsions. *Water*, 68(7):1187–1191, 1996.

M. S. Dresselhaus and I. L. Thomas. Alternative energy technologies. *Nature*, 414(6861):332–7, November 2001. ISSN 0028-0836. doi: 10.1038/35104599. URL <http://www.ncbi.nlm.nih.gov/pubmed/11713539>.

Omrpublic.iea.org. Oil market report, 2014. URL <http://omrpublic.iea.org/>.

E. Tzimas, A. Georgakaki, C. Garcia Cortes, and S.D. Peteves. Enhanced Oil Recovery using Carbon Dioxide in the European Energy System. Technical Report December, Institute for Energy, Petten, The Netherlands, 2005.

D. W. Green and G. P. Willhite. *Enhanced oil recovery*. Society of Petroleum Engineers, Richardson, TX USA, 1998.

Q. Liu, M. Dong, S. Ma, and Y. Tu. Surfactant enhanced alkaline flooding for Western Canadian heavy oil recovery. *Colloids and Surfaces A: Physicochemical and Engineering Aspects*, 293(1-3):63–71, February 2007. ISSN 09277757. doi: 10.1016/j.colsurfa.2006.07.013. URL <http://linkinghub.elsevier.com/retrieve/pii/S0927775706005231>.

K. Asghari and P. Nakutnyy. Experimental Results of Polymer Flooding of Heavy Oil Reservoirs. *Proceedings of Canadian International Petroleum Conference*, pages 1–7, June 2008. doi: 10.2118/2008-189. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=PETSOC-2008-189&soc=PETSOC>.

P. Shen, J. Wang, S. Yuan, T. Zhong, and X. Jia. Study of Enhanced-Oil-Recovery Mechanism of Alkali/Surfactant/Polymer Flooding in Porous Media From Experiments. *SPE Journal*, 14(2), June 2009. ISSN 1086-055X. doi: 10.2118/126128-PA. URL <http://www.spe.org/ejournals/jsp/journalapp.jsp?pageType=Preview&jid=ESJ&mid=SPE-126128-PA&pdfChronicleId=09014762801b994b>.

V. Alvarado and E. Manrique. Enhanced Oil Recovery: An Update Review. *Energies*, 3(9):1529–1575, August 2010. ISSN 1996-1073. doi: 10.3390/en3091529. URL <http://www.mdpi.com/1996-1073/3/9/1529/>.

A. Hart. The novel THAICAPRI technology and its comparison to other thermal methods for heavy oil recovery and upgrading. *Journal of Petroleum Exploration and Production Technology*, December 2013. ISSN 2190-0558. doi: 10.1007/s13202-013-0096-4. URL <http://link.springer.com/10.1007/s13202-013-0096-4>.

F. J. Hein, D. Leckie, S. Larter, and J. Suter. *Heavy-oil and Oil-sand Petroleum Systems in Alberta and Beyond: AAPG Studies in Geology* 64. Amer Assn of Petroleum Geologists, 1st edition, 2013. ISBN

0891810706. URL <http://books.google.com/books?hl=en&lr=&id=VbkuAgAAQBAJ&pgis=1>.

Www.altpetrol.com. Fuel oil emulsions, 2014. URL <http://www.altpetrol.com/en/2d-pd-foe.html>.

J. G. Speight. *The Chemistry and Technology of Petroleum*. CRC Press, 4 edition edition, 2006. ISBN 0849390672.

D. M. Adams. Experiences With Waterflooding Lloydminster Heavy-Oil Reservoirs. *Journal of Petroleum Technology*, 34(8), August 1982. ISSN 0149-2136. doi: 10.2118/10196-PA. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=00010196&soc=SPE>.

S. R. Larter and I. M. Head. Oil Sands and Heavy Oil: Origin and Exploitation. *Elements*, 10(4):277–283, August 2014. ISSN 1811-5209. doi: 10.2113/gselements.10.4.277. URL <http://elements.geoscienceworld.org/cgi/doi/10.2113/gselements.10.4.277>.

M. Arhuoma, D. Yang, M. Dong, H. Li, and R. Idem. Numerical Simulation of Displacement Mechanisms for Enhancing Heavy Oil Recovery during Alkaline Flooding. *Energy & Fuels*, 23(12):5995–6002, December 2009. ISSN 0887-0624. doi: 10.1021/ef900690y. URL <http://pubs.acs.org/doi/abs/10.1021/ef900690y>.

F. Qiu and D. Mamora. Experimental Study of Solvent-Based Emulsion Injection to Enhance Heavy Oil Recovery in Alaska North Slope Area. In *Proceedings of Canadian Unconventional Resources and In-*

*ternational Petroleum Conference*, pages 1–16. Society of Petroleum Engineers, October 2010. ISBN 9781555633127. doi: 10.2118/136758-MS. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=SPE-136758-MS&soc=SPE>.

L. Schramm. *Emulsions, Foams and Suspensions: Fundamentals and Applications*. WILEY-VCH, Weinheim, 2006. ISBN 3-527-30743-5. doi: 10.1002/cphc.200500530. URL <http://doi.wiley.com/10.1002/cphc.200500530>.

D. T. Wasan, S. M. Shah, N. Aderangi, M. S. Chan, and J. J. McNamara. Observations on the Coalescence Behavior of Oil Droplets and Emulsion Stability in Enhanced Oil Recovery. *Society of Petroleum Engineers Journal*, 18(6), December 1978. ISSN 0197-7520. doi: 10.2118/6846-PA. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=00006846&soc=SPE>.

C. McAuliffe. Crude-Oil-Water Emulsions to Improve Fluid Flow in an Oil Reservoir. *Journal of Petroleum Technology*, 25(6):721–726, June 1973. ISSN 0149-2136. doi: 10.2118/4370-PA. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=00004370&soc=SPE>.

A. Mandal, A. Samanta, A. Bera, and K. Ojha. Role of oil-water emulsion in enhanced oil recovery. In *2010 International Conference on Chemistry and Chemical Engineering*, number Iccce, pages 190–194. IEEE, August 2010a. ISBN 978-1-4244-7765-4. doi: 10.1109/ICCCENG.2010.

5560393. URL <http://ieeexplore.ieee.org/lpdocs/epic03/wrapper.htm?arnumber=5560393>.

A. Samanta, A. Bera, K. Ojha, and A. Mandal. Comparative studies on enhanced oil recovery by alkalisurfactant and polymer flooding. *Journal of Petroleum Exploration and Production Technology*, 2(2):67–74, June 2012. ISSN 2190-0558. doi: 10.1007/s13202-012-0021-2. URL <http://link.springer.com/10.1007/s13202-012-0021-2>.

M. Moradi, M. Kazempour, J. T. French, and V. Alvarado. Dynamic flow response of crude oil-in-water emulsion during flow through porous media. *Fuel*, 135:38–45, November 2014. ISSN 00162361. doi: 10.1016/j.fuel.2014.06.025. URL <http://linkinghub.elsevier.com/retrieve/pii/S0016236114005912>.

R. Kumar, E. Dao, and K. K. Mohanty. SPE 129914 Emulsion Flooding of Heavy Oil. In *SPE Journal*, number April, pages 24–28, 2010.

R. M. Decker and D. L. Flock. Thermal Stability And Application Of Emulsion Composed Blocking Agents For Steamflooding. *Journal of Canadian Petroleum Technology*, 27(4):69–78, 1988. ISSN 0021-9487. doi: 10.2118/88-04-05. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=PETSOC-88-04-05&soc=PETSOC>.

S. Cobos, M. S. Carvalho, and V. Alvarado. Flow of oil - water emulsions through a constricted capillary. *International Journal of Multiphase Flow*, 35(6):507–515, June 2009. ISSN 03019322. doi: 10.1016/j.ijmultiphaseflow.2009.

02.018. URL <http://linkinghub.elsevier.com/retrieve/pii/S0301932209000366>.

N. J. Hadia, L. S. Chaudhari, A. Aggarwal, S. K. Mitra, M. Vinjamur, and R. Singh. Experimental and numerical investigation of one-dimensional waterflood in porous reservoir. *Experimental Thermal and Fluid Science*, 32(2):355–361, November 2007a. ISSN 08941777. doi: 10.1016/j.expthermflusci.2007.04.009. URL <http://linkinghub.elsevier.com/retrieve/pii/S0894177707000660>.

V. Santosh, S. K. Mitra, M. Vinjamur, and R. Singh. Experimental and Numerical Investigations of Waterflood Profiles with Different Well Configurations. *Energy & Fuels*, 21(6):3353–3359, November 2007. ISSN 0887-0624. doi: 10.1021/ef0700376. URL <http://pubs.acs.org/doi/abs/10.1021/ef0700376>.

V. Santosh, S. K. Mitra, M. Vinjamur, and M. S. Kumar. Flow Visualization of Waterflooding with Horizontal and Vertical Wells. *Petroleum Science and Technology*, 26(15):1835–1851, September 2008. ISSN 1091-6466. doi: 10.1080/10916460701296418. URL <http://www.informaworld.com/openurl?genre=article&doi=10.1080/10916460701296418&magic=crossref|ID404A21C5BB053405B1A640AFFD44AE3>.

L. S. Chaudhari, N. J. Hadia, S. K. Mitra, and M. Vinjamur. Flow Visualization of Two-Phase Flow through Layered Porous Media. *Energy Sources, Part A: Recovery, Utilization, and Environmental Effects*, 33(10):948–958,

January 2011a. ISSN 1556-7036. doi: 10.1080/15567030903330702.

URL <http://www.informaworld.com/openurl?genre=article&doi=10.1080/15567030903330702&magic=crossref|ID404A21C5BB053405B1A640AFFD44AE3>.

S. Bagci and F. Gumrah. An examination of steam-injection processes in horizontal and vertical wells for heavy-oil recovery. *Journal of Petroleum Science and Engineering*, 8(1):59–72, July 1992. ISSN 09204105. doi: 10.1016/0920-4105(92)90044-2. URL <http://linkinghub.elsevier.com/retrieve/pii/0920410592900442>.

N. J. Hadia, L. S. Chaudhari, S. K. Mitra, M. Vinjamur, and R. Singh. Experimental investigation of use of horizontal wells in waterflooding. *Journal of Petroleum Science and Engineering*, 56(4):303–310, April 2007b. ISSN 09204105. doi: 10.1016/j.petrol.2006.10.004. URL <http://linkinghub.elsevier.com/retrieve/pii/S0920410506002270>.

R. D'Elia-S and J. Ferrer-G. Emulsion Flooding of Viscous Oil Reservoirs. In *Proceedings of Fall Meeting of the Society of Petroleum Engineers of AIME*. Society of Petroleum Engineers, September 1973. ISBN 9781555637736. doi: 10.2118/4674-MS. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=00004674&soc=SPE>.

P. Walstra. Principles of emulsion formation. *Chemical Engineering Science*, 48(2):333–349, January 1993. ISSN 00092509. doi: 10.1016/0009-2509(93)80021-H. URL <http://linkinghub.elsevier.com/retrieve/pii/000925099380021H>.

- A. Mandal, A. Samanta, A. Bera, and K. Ojha. Characterization of Oil - Water Emulsion and Its Use in Enhanced Oil Recovery. *Industrial & Engineering Chemistry Research*, 49(24):12756–12761, December 2010b. ISSN 0888-5885. doi: 10.1021/ie101589x. URL <http://pubs.acs.org/doi/abs/10.1021/ie101589x>.
- V. R. Guillen, M. S. Carvalho, and V. Alvarado. Pore Scale and Macroscopic Displacement Mechanisms in Emulsion Flooding. *Transport in Porous Media*, 94(1):197–206, April 2012. ISSN 0169-3913. doi: 10.1007/s11242-012-9997-9. URL <http://www.springerlink.com/index/10.1007/s11242-012-9997-9>.
- R. Kumar, E. Dao, and K. Mohanty. Heavy-Oil Recovery by In-Situ Emulsion Formation. *SPE Journal*, (July 2011):24–28, 2012. ISSN 1086-055X. doi: 10.2118/129914-PA. URL <http://www.spe.org/ejournals/jsp/journalapp.jsp?pageType=Preview&jid=ESJ&mid=SPE-129914-PA&pdfChronicleId=090147628025afe0>.
- J. Bryan and A. Kantzas. Potential for Alkali-Surfactant Flooding in Heavy Oil Reservoirs Through Oil-in-Water Emulsification. *Journal of Canadian Petroleum Technology*, 48(2), February 2009. ISSN 0021-9487. doi: 10.2118/09-02-37. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=PETSOC-09-02-37&soc=PETSOC>.
- P. H. Krumrine and F. J.S. Surfactant, Polymer, and Alkali Interactions in Chemical Flooding Processes. *Proceedings of SPE Oilfield and Geothermal Chemistry Symposium*, June 1983. doi: 10.2118/

11778-MS. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=00011778&soc=SPE>.

F. Qiu. The Potential Applications in Heavy Oil EOR With the Nanoparticle and Surfactant Stabilized Solvent-Based Emulsion. In *Proceedings of Canadian Unconventional Resources and International Petroleum Conference*, pages 1–12. Society of Petroleum Engineers, October 2010. ISBN 9781555633127. doi: 10.2118/134613-MS. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=SPE-134613-MS&soc=SPE>.

G. L. Nogueira, M. S. Carvalho, and V. Alvarado. Dynamic Network Model of Mobility Control in Emulsion Flow Through Porous Media. *Transport in Porous Media*, March 2013. ISSN 0169-3913. doi: 10.1007/s11242-013-0151-0. URL <http://link.springer.com/10.1007/s11242-013-0151-0>.

E. Boye, P. Jr, A. Lohne, J. O. Helland, and G. Virnovsky. Relative permeabilities for two- and three- phase flow processes relevant to the depressurization of the Statfjord field. *The Society of Core Analysis*, pages 1–12, 2008.

A. Baldygin, D. S. Nobes, and S. K. Mitra. New Laboratory Core Flooding Experimental System. *Industrial & Engineering Chemistry Research*, 53(34): 13497–13505, August 2014a. ISSN 0888-5885. doi: 10.1021/ie501866e. URL <http://pubs.acs.org/doi/abs/10.1021/ie501866e>.

A. Baldygin, D. S. Nobes, and S. K. Mitra. Water-Alternate-Emulsion (WAE): A new technique for enhanced oil recovery. *Journal of Petroleum Science and Engineering*, 121:167–173, July 2014b. ISSN 09204105. doi: 10.1016/j.petrol.

2014.06.021. URL <http://linkinghub.elsevier.com/retrieve/pii/S0920410514001776>.

A. Baldygin, D. S. Nobes, and S. K. Mitra. Novel Technique for Core Flooding Experiments. In *The biennial CSME International Congress: Symposium on Advanced Energy Systems (CSME'12 - Symposium on AES)*, University of Manitoba, Canada, June 2012.

A. Baldygin, D. S. Nobes, and S. K. Mitra. IMECE2014-37248 Oil recovery from porous media using emulsion. In *Proceedings of the ASME 2014 International Mechanical Engineering Congress & Exposition*, page 6, Montreal, Quebec, Canada, 2014c. IMECE 2014.

H. Darcy. *Les fontaines publiques de la ville de Dijon*. Paris, 1856.

L F Athy. American association of petroleum geologists. 17(1):1–24, 1930.

B. F. Towler. *Fundamental principles of reservoir engineering. SPE TEXTBOOK SERIES Vol. 8*. 2002.

Edward W. Washburn. Note on a Method of Determining the Distribution of Pore Sizes in a Porous Material. *Proceedings of the National Academy of Sciences of the United States of America*, 7(4):115–116, 1921. URL [http://www.jstor.org/stable/84084?seq=1#page\\_scan\\_tab\\_contents](http://www.jstor.org/stable/84084?seq=1#page_scan_tab_contents).

L. P. Dake. *Fundamentals of reservoir engineering*. Elsevier Science B.V., Amsterdam, seventeenth edition, 1998.

S E Buckley and M C Leverett. Mechanism of Fluid Displacement in Sands. *Transactions of the AIME*, 146(1):107–116, 1941. doi: 10.2118/942107-G.

H.L. Stone. Probability Model for Estimating Three-Phase Relative Permeability. *Journal of Petroleum Technology*, 22(2), February 1970. ISSN 0149-2136. doi: 10.2118/2116-PA. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=00002116&soc=SPE>.

H.L. Stone. Estimation of Three-Phase Relative Permeability And Residual Oil Data. *Journal of Canadian Petroleum Technology*, (May), 1973. ISSN 0021-9487. doi: 10.2118/73-04-06. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=PETSOC-73-04-06&soc=PETSOC>.

A. T. Corey, C. H. Rathjens, J. H. Henderson, and M. R. J. Wyllie. Three-Phase Relative Permeability. *Journal of Petroleum Technology*, 8(11):63–65, November 1956. ISSN 0149-2136. doi: 10.2118/737-G. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=SPE-000737-G&soc=SPE>.

M.R.J. Wyllie. Interrelationship between wetting and nonwetting phase relative permeability. *Transactions of the AIME*, page 83, 1961.

M C Leverett. Capillary behavior in porous solids. *Trans. Am. Inst*, 1940.

Edward W. Washburn. The Dynamics of Capillary Flow. *Physical Review*, 17(3): 273–283, March 1921. ISSN 0031-899X. doi: 10.1103/PhysRev.17.273. URL <http://link.aps.org/doi/10.1103/PhysRev.17.273>.

T.F. Moore and R.L. Slobod. Displacement of Oil by Water-Effect of Wettability, Rate, and Viscosity on Recovery. In *Fall Meeting of the Petroleum Branch of*

*AIME*. Society of Petroleum Engineers, April 2013. doi: 10.2118/502-G. URL <http://www.onepetro.org/doi/10.2118/502-G>.

R W S Foulser, S G Goodyear, and R J Sims. New concepts in relative permeabilities at high capillary numbers for surfactant flooding. *Transport in Porous Media*, 6(3):223–240, June 1991. ISSN 0169-3913. doi: 10.1007/BF00208951. URL <http://link.springer.com/10.1007/BF00208951>.

M. I. Romero, M. S. Carvalho, and V. Alvarado. Experiments and network model of flow of oil-water emulsion in porous media. *Physical Review E*, 84(4):1–7, October 2011. ISSN 1539-3755. doi: 10.1103/PhysRevE.84.046305. URL <http://link.aps.org/doi/10.1103/PhysRevE.84.046305>.

G M Homsy. Viscous fingering in porous media. *Annual Review of Fluid Mechanics*, 19(1):271–311, 1987.

W. R. Schowalter. Stability criteria for miscible displacement of fluids from a porous medium. *AICHE Journal*, 11(1):99–105, January 1965. ISSN 0001-1541. doi: 10.1002/aic.690110122. URL <http://doi.wiley.com/10.1002/aic.690110122>.

T. R. French, J. S. Broz, P. B. Lorenz, and K. M. Bertus. Use of Emulsions for Mobility Control During Steamflooding. In *SPE California Regional Meeting*. Society of Petroleum Engineers, April 1986. ISBN 978-1-55563-615-9. doi: 10.2118/15052-MS. URL <https://www.onepetro.org/conference-paper/SPE-15052-MS?sort=&start=0&q=SPE+>

15052&from\_year=&peer\_reviewed=&published\_between= &fromSearchResults=true&to\_year=&rows=10#.

G. W. Schmidt. Interstitial Water Composition and Geochemistry of Deep Gulf Coast Shales and Sandstones. *AAPG Bulletin*, 57(2):321–337, 1973. ISSN 0149-1423. URL <http://archives.datapages.com/data/bulletns/1971-73/data/pg/0057/0002/0300/0321.htm>.

S. Bagci, M. V. Kok, and U. Turksoy. SPE 65394 Effect of Brine Composition and Alkaline Fluid on the Permeability Damage of Limestone Reservoirs. 2001a.

S. Bagci, M. V. Kok, and U. Turksoy. Effect of brine composition on oil recovery by waterflooding. *Petroleum Science and Technology*, 19(3-4):359–372, January 2001b. ISSN 1091-6466. doi: 10.1081/LFT-100000769. URL <http://www.informaworld.com/openurl?genre=article&doi=10.1081/LFT-100000769&magic=crossref|ID404A21C5BB053405B1A640AFFD44AE3>.

H. O. Yildiz, M. Valat, and N. R. Morrow. Effect of Brine Composition On Wettability And Oil Recovery of a Prudhoe Bay Crude Oil. *Journal of Canadian Petroleum Technology*, 38(01), April 2013. ISSN 0021-9487. doi: 10.2118/99-01-02. URL <https://www.onepetro.org/journal-paper/PETSOC-99-01-02>.

M. Moradi, V. Alvarado, and S. Huzurbazar. Effect of Salinity on Water-in-Crude Oil Emulsion: Evaluation through Drop-Size Distribution Proxy. *Energy & Fu-*

*els*, 25(1):260–268, January 2011. ISSN 0887-0624. doi: 10.1021/ef101236h.

URL <http://pubs.acs.org/doi/abs/10.1021/ef101236h>.

C. E. Perles, P. L. O. Volpe, and A. J. F. Bombard. Study of the Cation and Salinity Effect on Electrocoalescence of Water/Crude Oil Emulsions. *Energy & Fuels*, 26(11):121107122506002, November 2012. ISSN 0887-0624. doi: 10.1021/ef301433m. URL <http://dx.doi.org/10.1021/ef301433m>.

H. K. Sarma, B. B. Maini, and K. Jha. Evaluation of Emulsified Solvent Flooding For Heavy Oil Recovery. *Journal of Canadian Petroleum Technology*, 37(7):55–62, July 1998. ISSN 0021-9487. doi: 10.2118/98-07-06. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=PETSOC-98-07-06&soc=PETSOC>.

H. A. Son, K. Y. Yoon, G. J. Lee, J. W. Cho, S. K. Choi, J. W. Kim, K. C. Im, H. T. Kim, K. S. Lee, and W. M. Sung. The potential applications in oil recovery with silica nanoparticle and polyvinyl alcohol stabilized emulsion. *Journal of Petroleum Science and Engineering*, November 2014. ISSN 09204105. doi: 10.1016/j.petrol.2014.11.001. URL <http://www.sciencedirect.com/science/article/pii/S0920410514003593>.

E. J. Windhab, M. Dressler, K. Feigl, P. Fischer, and D. Megias-Alguacil. Emulsion processing from single-drop deformation to design of complex processes and products. *Chemical Engineering Science*, 60(8-9):2101–2113, April 2005. ISSN 00092509. doi: 10.1016/j.ces.2004.12.003. URL <http://linkinghub.elsevier.com/retrieve/pii/S000925090400884X>.

B. Binks. *Modern Aspects of Emulsion Science*. Royal Society of Chemistry, Cambridge, 1998. ISBN 978-0-85404-439-9. doi: 10.1039/9781847551474. URL <http://ebook.rsc.org/?DOI=10.1039/9781847551474>.

G. P. Willhite. *Waterflooding*. Society of Petroleum Engineers, Richardson, TX USA, 1986. ISBN 1-55563-005-7.

L. A. Rapoport and W. J. Leas. SPE-000213-G Properties of linear waterfloods. *Petroleum Transactions AMIE*, 198:139–148, 1953.

N. J. Hadia, L. S. Chaudhari, S. K. Mitra, M. Vinjamur, and R. Singh. Waterflood Profiles and Oil Recovery with Vertical and Horizontal Wells. *Energy Sources, Part A: Recovery, Utilization, and Environmental Effects*, 30(17):1604–1618, January 2008a. ISSN 1556-7036. doi: 10.1080/15567030701773806. URL <http://www.informaworld.com/openurl?genre=article&doi=10.1080/15567030701773806&magic=crossref|ID404A21C5BB053405B1A640AFFD44AE3>.

N. J. Hadia, S. K. Mitra, and M. Vinjamur. Estimation of permeability heterogeneity in limestone outcrop by pressure measurements: Experiments and numerical simulation. *Experimental Thermal and Fluid Science*, 40:177–184, March 2012. ISSN 08941777. doi: 10.1016/j.expthermflusci.2012.03.005. URL <http://linkinghub.elsevier.com/retrieve/pii/S0894177712000726>.

N. J. Hadia, L. S. Chaudhari, S. K. Mitra, M. Vinjamur, and R. Singh. Effect of Scaling Parameters on Waterflood Performance with Horizontal and Vertical

Wells. *Energy & Fuels*, 22(1):402–409, January 2008b. ISSN 0887-0624. doi: 10.1021/ef070097b. URL <http://pubs.acs.org/doi/abs/10.1021/ef070097b>.

R. D. Wyckoff and H. G. Botset. The Flow of Gas-Liquid Mixtures Through Unconsolidated Sands. *Physics*, 7(9):325, 1936. ISSN 01486349. doi: 10.1063/1.1745402. URL <http://scitation.aip.org/content/aip/journal/jap/7/9/10.1063/1.1745402>.

R. Nasralla, M. Alotaibi, and H. Nasr-El-Din. Efficiency of Oil Recovery by Low Salinity Water Flooding in Sandstone Reservoirs. In *Proceedings of SPE Western North American Region Meeting*, number 1967. Society of Petroleum Engineers, May 2011. ISBN 9781613991206. doi: 10.2118/144602-MS. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=SPE-144602-MS&soc=SPE>.

E. H. Legowo and S. W. Pratomo. Microbial Core Flooding Experiments Using Indigenous Microbes. In *Proceedings of SPE Asia Pacific Improved Oil Recovery Conference*, pages 1–11. Society of Petroleum Engineers, October 1999. doi: 10.2118/57306-MS. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=00057306&soc=SPE>.

V. Hornof and N. R. Morrow. Gravity Effects in the Displacement of Oil by Surfactant Solutions. *SPE Reservoir Engineering*, 2(4), November 1987. ISSN 0885-9248. doi: 10.2118/13573-PA. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=00013573&soc=SPE>.

S.-H. Chang and R. B. Grigg. Laboratory Flow Tests Used To Determine Reservoir Simulator Foam Parameters for EVGSAU CO<sub>2</sub> Foam Pilot. In *Proceedings of Permian Basin Oil and Gas Recovery Conference*, pages 483–492. Society of Petroleum Engineers, March 1994. ISBN 9781555634735. doi: 10.2118/27675-MS. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=00027675&soc=SPE>.

S. Sedaee and R. Fariborz. Experimental Investigation of Steam/Methane Flooding in a Heavy Oil Reservoir. In *Proceedings of SPE International Petroleum Conference in Mexico*, number 1987. Society of Petroleum Engineers, November 2004. ISBN 9781555639822. doi: 10.2118/91968-MS. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=00091968&soc=SPE>.

M. Nobakht, S. Moghadam, and Y. Gu. Effects of Viscous and Capillary Forces on CO<sub>2</sub> Enhanced Oil Recovery under Reservoir Conditions. *Energy & Fuels*, 21(6):3469–3476, November 2007. ISSN 0887-0624. doi: 10.1021/ef700388a. URL <http://pubs.acs.org/doi/abs/10.1021/ef700388a>.

S. K. Veerabhadrappa, A. Doda, J. J. Trivedi, and E. Kuru. On the Effect of Polymer Elasticity on Secondary and Tertiary Oil Recovery. *Industrial & Engineering Chemistry Research*, 52(51):18421–18428, December 2013a. ISSN 0888-5885. doi: 10.1021/ie4026456. URL <http://pubs.acs.org/doi/abs/10.1021/ie4026456>.

K. M. Ko, B. H. Chon, S. B. Jang, and H. Y. Jang. Surfactant flooding characteristics of dodecyl alkyl sulfate for enhanced oil recovery. *Journal of Industrial and*

*Engineering Chemistry*, 20(1):228–233, January 2014. ISSN 1226086X. doi: 10.1016/j.jiec.2013.03.043. URL <http://linkinghub.elsevier.com/retrieve/pii/S1226086X13001494>.

C. J. Stanley. Perforated end plug plate for testing core samples, 1984.

C. J. Stanley. Porous end plug disk for testing core samples, 1985.

Www.corelab.com. Standard Core Holder - HCH Series, 2014a.  
URL <http://www.corelab.com/cli/core-holders/standard-core-holder-hch-series>.

Www.corelab.com. Core Laboratories: Hassler Type Core Holder - RCH Series, 2014b. URL <http://www.corelab.com/cli/core-holders/hassler-type-core-holders-rch-series>.

Www.coretest.com. CHG Series Coreholders, 2014. URL [http://www.coretest.com/product\\_detail.php?p\\_id=58](http://www.coretest.com/product_detail.php?p_id=58).

W. Chen, J. Peng, Y. Su, L. Zheng, L. Wang, and Z. Jiang. Separation of oil/water emulsion using Pluronic F127 modified polyethersulfone ultrafiltration membranes. *Separation and Purification Technology*, 66(3): 591–597, May 2009. ISSN 13835866. doi: 10.1016/j.seppur.2009.01.009. URL <http://linkinghub.elsevier.com/retrieve/pii/S1383586609000148>.

L. M. Fidalgo, G. Whyte, D. Bratton, C. F. Kaminski, C. Abell, and W. T. S. Huck. From microdroplets to microfluidics: selective emulsion separation in microfluidic devices. *Angewandte Chemie (International ed. in English)*, 47(11):

2042–5, January 2008. ISSN 1521-3773. doi: 10.1002/anie.200704903. URL <http://www.ncbi.nlm.nih.gov/pubmed/18264960>.

Patrick Brunelle (Quadrise Canada Corp.). Data sheet: UofA E2 Concentrate. *Personal communication*, 2012.

Manus Abrasive Systems. Bulk density chart, 2014. URL <http://www.manusabrasive.com/bulk-density-chart/>.

L. J. Klinkenberg. The permeability of porous media to liquids and gases. *American Petroleum Institute*, (02):57–73, 1941. ISSN 22186867. doi: 10.5510/OGP20120200114. URL [http://www.socar.az/ogpi/files/uploaders/57-73\\_Klinker.pdf](http://www.socar.az/ogpi/files/uploaders/57-73_Klinker.pdf).

N. S. K. Gunda, B. Bera, N. K. Karadimitriou, S. K. Mitra, and S. M. Hasanzadeh. Reservoir-on-a-chip (ROC): a new paradigm in reservoir engineering. *Lab on a chip*, 11(22):3785–92, November 2011. ISSN 1473-0189. doi: 10.1039/c1lc20556k. URL <http://www.ncbi.nlm.nih.gov/pubmed/22011687>.

S. Doorwar and K. Mohanty. Viscous Fingering during Non-Thermal Heavy Oil Recovery. In *Proceedings of SPE Annual Technical Conference and Exhibition*, number November. Society of Petroleum Engineers, October 2011. ISBN 9781613991473. doi: 10.2118/146841-MS. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=SPE-146841-MS&soc=SPE>.

A. Shah, R. Fishwick, J. Wood, G. Leeke, S. Rigby, and M. Greaves. A re-

view of novel techniques for heavy oil and bitumen extraction and upgrading. *Energy & Environmental Science*, 3(6):700, 2010. ISSN 1754-5692. doi: 10.1039/b918960b. URL <http://xlink.rsc.org/?DOI=b918960b>.

P. Luo, Y. Zhang, and S. Huang. A promising chemical-augmented WAG process for enhanced heavy oil recovery. *Fuel*, 104:333–341, February 2013. ISSN 00162361. doi: 10.1016/j.fuel.2012.09.070. URL <http://linkinghub.elsevier.com/retrieve/pii/S0016236112007831>.

E. T. S. Huang and L. W. Holm. Effect of WAG Injection and Rock Wettability on Oil Recovery During CO<sub>2</sub> Flooding. *SPE Reservoir Engineering*, 3(1):119–129, February 1988. ISSN 0885-9248. doi: 10.2118/15491-PA. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=00015491&soc=SPE>.

G. R. Scott. Comparison of CSS and SAGD Performance in the Clearwater Formation at Cold Lake. In *SPE International Thermal Operations and Heavy Oil Symposium and International Horizontal Well Technology Conference*. Society of Petroleum Engineers, April 2013. doi: 10.2118/79020-MS. URL <http://www.onepetro.org/doi/10.2118/79020-MS>.

S. Bagci and E. Tuzunoglu. 3D Model Studies of the Immiscible CO<sub>2</sub> Process Using Horizontal Wells For Heavy Oil Recovery. In *Annual Technical Meeting*, page 12. Petroleum Society of Canada, April 1998. ISBN 9781613991022. doi: 10.2118/98-74. URL <https://www.onepetro.org/conference-paper/PETSOC-98-74http://www.onepetro.org/doi/10.2118/98-74>.

E. Tüzünoglu and S. Bagci. Scaled 3-D model studies of immiscible CO<sub>2</sub> flooding using horizontal wells. *Journal of Petroleum Science and Engineering*, 26(1-4):67–81, May 2000. ISSN 09204105. doi: 10.1016/S0920-4105(00)00022-X. URL <http://linkinghub.elsevier.com/retrieve/pii/S092041050000022X>.

J. R. Christensen, E. H. Stenby, and A. Skauge. Review of WAG Field Experience. *SPE Reservoir Evaluation & Engineering*, 4(02):97–106, April 2013. ISSN 1094-6470. doi: 10.2118/71203-PA. URL <http://www.onepetro.org/doi/10.2118/71203-PA>.

W. S. Tortike. A Numerical Study Of Pressure Cycling Athabasca Oil Sand With Steam And Carbon Dioxide. In *Proceedings of Annual Technical Meeting*, pages 1–14. Society of Petroleum Engineers, April 1991. ISBN 9781555634827. doi: 10.2118/91-11. URL <https://www.onepetro.org/conference-paper/PETSOC-91-11>.

M. R. Islam and S. M. Farouq Ali. New Scaling Criteria For Polymer, Emulsion And Foam Flooding Experiments. *Journal of Canadian Petroleum Technology*, 28(4):79–87, 1989. ISSN 0021-9487. doi: 10.2118/89-04-05. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=PETSOC-89-04-05&soc=PETSOC>.

M. R. Islam and S. M. Farouq Ali. New scaling criteria for in-situ combustion experiments. *Journal of Petroleum Science and Engineering*, 6(4):367–379, January 1992. ISSN 09204105. doi: 10.1016/0920-4105(92)

90063-7. URL <http://linkinghub.elsevier.com/retrieve/pii/0920410592900637>.

J. H. Abou-Kassem and S. M. Farouq Ali. Modelling of Emulsion Flow In Porous Media. *Journal of Canadian Petroleum Technology*, 34(6):30–38, June 1995. ISSN 0021-9487. doi: 10.2118/95-06-02. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=PETSOC-95-06-02&soc=PETSOC>.

S. Akin, S. Bagci, and M. V. Kok. Dry Forward Combustion with Diverse Well Configurations. *Proceedings of SPE/AAPG Western Regional Meeting*, June 2000. doi: 10.2523/62551-MS. URL <http://www.spe.org/elibrary/servlet/spepreview?id=00062551>.

D. Tiab and E. C. Donaldson. *Petrophysics*. Gulf Professional Publishing, 3 edition, 2004. ISBN 9780750677110. doi: 10.1016/B978-075067711-0/50005-0. URL <http://www.sciencedirect.com/science/article/pii/B9780750677110500050>.

P. R. Waghmare and S. K. Mitra. Contact angle hysteresis of microbead suspensions. *Langmuir : the ACS journal of surfaces and colloids*, 26(22):17082–9, November 2010. ISSN 1520-5827. doi: 10.1021/la1025526. URL <http://www.ncbi.nlm.nih.gov/pubmed/20886898>.

K. S. Sorbie and Y. Huang. Rheological and transport effects in the flow of low-concentration xanthan solution through porous media. *Journal of Colloid and Interface Science*, 145(1):74–89, August 1991. ISSN 00219797. doi: 10.1016/

0021-9797(91)90100-M. URL <http://linkinghub.elsevier.com/retrieve/pii/002197979190100M>.

A. M. S. Maia, R. Borsali, and R. C. Balaban. Comparison between a polyacrylamide and a hydrophobically modified polyacrylamide flood in a sandstone core. *Materials Science and Engineering: C*, 29(2):505–509, March 2009. ISSN 09284931. doi: 10.1016/j.msec.2008.09.018. URL <http://linkinghub.elsevier.com/retrieve/pii/S0928493108002324>.

T. N. Castro Dantas, V. C. Santanna, A. A. Dantas Neto, F. D. S. Curbelo, and A. I. C. Garnica. Methodology to break test for surfactant-based fracturing gel. *Journal of Petroleum Science and Engineering*, 50(3-4):293–298, March 2006. ISSN 09204105. doi: 10.1016/j.petrol.2005.12.001. URL <http://linkinghub.elsevier.com/retrieve/pii/S0920410505001865>.

R. Darby. *Chemical Engineering Fluid Mechanics*. Marcel Dekker, Inc., second edi edition, 2001.

S. M. Mahmood and W. E. Brigham. Two dimensional displacement of oil by gas and surfactant solution under foaming conditions. Technical report, United States Department of Energy, 1987.

R. V. Ponce F., M. S. Carvalho, and V. Alvarado. Oil recovery modeling of macro-emulsion flooding at low capillary number. *Journal of Petroleum Science and Engineering*, 119:112–122, July 2014. ISSN 09204105. doi: 10.1016/j.petrol.

2014.04.020. URL <http://linkinghub.elsevier.com/retrieve/pii/S0920410514001089>.

G. P. Willhite, D. W. Green, D. M. Okoye, and M. D. Looney. A Study of Oil Displacement by Microemulsion Systems Mechanisms and Phase Behavior. *Society of Petroleum Engineers Journal*, 20(6), December 1980. ISSN 0197-7520. doi: 10.2118/7580-PA. URL <https://www.onepetro.org/journal-paper/SPE-7580-PA>.

C. Romero, B. Bazin, A. Zaitoun, and F. Leal Calderon. Behavior of a Scale Inhibitor Water-in-Oil Emulsion in Porous Media. In *Proceedings of International Symposium and Exhibition on Formation Damage Control*. Society of Petroleum Engineers, February 2006. ISBN 9781555632397. doi: 10.2118/98275-MS. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=SPE-98275-MS&soc=SPE>.

W. Anderson, D. Kozak, V. a Coleman, Å. K Jämting, and M. Trau. A comparative study of submicron particle sizing platforms: accuracy, precision and resolution analysis of polydisperse particle size distributions. *Journal of colloid and interface science*, 405:322–30, September 2013. ISSN 1095-7103. doi: 10.1016/j.jcis.2013.02.030. URL <http://www.ncbi.nlm.nih.gov/pubmed/23759321>.

S. Mei, J. Bryan, and A. Kantzas. Experimental Study of the Mechanisms in Heavy Oil Waterflooding Using Etched Glass Micromodel. *Proceedings of SPE Heavy Oil Conference Canada*, June 2012. doi: 10.2118/

157998-MS. URL <http://www.onepetro.org/mslib/servlet/onepetropreview?id=SPE-157998-MS&soc=SPE>.

T. Robert, R. Martel, S. H. Conrad, R. Lefebvre, and U. Gabriel. Visualization of TCE recovery mechanisms using surfactant-polymer solutions in a two-dimensional heterogeneous sand model. *Journal of contaminant hydrology*, 86(1-2):3–31, June 2006. ISSN 0169-7722. doi: 10.1016/j.jconhyd.2006.02.013. URL <http://www.ncbi.nlm.nih.gov/pubmed/16624443>.

L. S. Chaudhari, N. J. Hadia, S. K. Mitra, and M. Vinjamur. Flow Visualization of Two-Phase Flow through Layered Porous Media. *Energy Sources, Part A: Recovery, Utilization, and Environmental Effects*, 33(10):948–958, March 2011b. ISSN 1556-7036. doi: 10.1080/15567030903330702. URL <http://www.tandfonline.com/doi/abs/10.1080/15567030903330702>.

K. Naderi and T. Babadagli. Visual analysis of immiscible displacement processes in porous media under ultrasound effect. *Physical Review E*, 83(5):056323, May 2011. ISSN 1539-3755. doi: 10.1103/PhysRevE.83.056323. URL <http://link.aps.org/doi/10.1103/PhysRevE.83.056323>.

R. M. Butler and K. H. Chung. Goemetrical effect of steam injection on the formation of emulsions in the steam-assisted gravity drainage process. *The journal of Canadian Petroleum*, 1988.

W. Li and D. D. Mamora. SPE 133277 Experimental Investigation of Solvent Co-Injection in Vapor and Liquid Phase to Enhance SAGD Performance. *North*, i: 1–14, 2010.

B. Zehm. Software :: SendEmail - Send email with this free command line email client, 2009. URL <http://caspian.dotconf.net/menu/Software/SendEmail/>.

S. K. Veerabhadrappa, J. J. Trivedi, and E. Kuru. Visual Confirmation of the Elasticity Dependence of Unstable Secondary Polymer Floods. *Industrial & Engineering Chemistry Research*, 52(18):6234–6241, May 2013b. ISSN 0888-5885. doi: 10.1021/ie303241b. URL <http://pubs.acs.org/doi/abs/10.1021/ie303241b>.

G. E. King. Perforating Basics. How the perforating processes work. Technical report, 2009.

C. Cosad. Choosing a Perforation Strategy. *Oilfield Review*, 4(4):54–69, 1992.

R. A. Parrott and I. C. Walton. Perforating technology: well perforating solutions redefine sand management strategies. *Trade Publication*, 61(7):74, 2001.

B. A. Voll, B. M. Richard, A. D. Gabrysch, R. Kingwood, and A. Dale. Wire mesh filter, 1998. URL <http://www.google.com/patents/US5849188>.

Edge Detection. URL <http://www.mathworks.com/help/vision/ref/edgedetection.html>.

Patrick Brunelle (Quadrise Canada Corp.). UofA E2 Concentrate. *Personal communication*, page 5, 2012.

R J Blackwell, J R Rayne, and W M Terry. Factors Influencing the Efficiency of Miscible Displacement. *Society of Petroleum Engineers*, 1959.

D. Weitz, J. Stokes, R. Ball, and A. Kushnick. Dynamic Capillary Pressure in Porous Media: Origin of the Viscous-Fingering Length Scale. *Physical Review Letters*, 59(26):2967–2970, December 1987. ISSN 0031-9007. doi: 10.1103/PhysRevLett.59.2967. URL <http://link.aps.org/doi/10.1103/PhysRevLett.59.2967>.

# **Appendix**

## **A-1 1D and 2D core holder**

To ensure safe operation for the core holder when the system is pressurized, the components passed strength analysis for safe operation.

### **A-1.1 One dimensional core holder**

#### **Thread**

The strength analysis on 2.500 x 4 UNC thread was performed to determine the safety factor at working conditions. Based on available information, the following conservative assumptions were made:

- The material's mechanical properties are homogeneous and isotropic throughout the cross-section;
- The mechanical properties of the material are of equal magnitude in tension and compression;
- Cross-sections remain plane under loading conditions;
- The materials have ductile characteristics;
- Simple axial/shear loading results in uniform axial/shear stress distribution across a uniform crosssection;
- Materials obey Hooke's Laws of elasticity;
- The minimum yield strength at 0.2 % offset strain, rather than typical (average) yield strength of a material, is the basis by which stress at yield is defined;

- Shear strength is 50 % to 60 % of the minimum yield strength. Two existing theories are the distortion energy theory ( $0.577 * Y_s$ ) and the maximum shear stress theory ( $0.5 * Y_s$ );
- The selected material will not be used in an environment that will adversely affect its mechanical or physical properties;
- Calculated stresses are based on static loading conditions if appropriate to the application;
- Material for body is 630 SS,  $E = 196 \text{ GPa}$ .

The tensile strength area of screw thread can be calculated using the following formula:

$$A_t = 0.7854 \cdot \left( D - \frac{0.974}{n} \right)^2 \cdot \text{in}^2 = 4.0, \text{ in}^2 \quad (\text{A-1})$$

where  $D$  - basic major diameter,  $n$  - number of thread per inch, and  $A_t$  - tensile strength area of screw thread.

Pressure on a thread is a result of pressure applied on end plug (1,500 psi) with outside diameter equal to 1.5 in. Resulted force on a thread is  $2.651 \times 10^3 \text{ lbf}$ , and shear stress on thread can be found as:

$$\tau_{cut} = \frac{Q}{A_t} = \frac{2.651 \cdot 10^4 \text{ lbf}}{4.0 \text{ in}^2} = 662.9, \text{ psi} \quad (\text{A-2})$$

so that safety factor is:

$$sf = \frac{0.577 \cdot Y_s}{\tau_{cut}} = \frac{9.791 \cdot 10^4 \text{ psi}}{662.9 \text{ psi}} = 147.7 \quad (\text{A-3})$$

Obtained number for safety factor can guarantee safe operation at 1,500 psi.

## Wall thickness

The strength analysis on a wall thickness was performed to determine the safety factor at working conditions. In order to estimate safety factor for body's wall, the ASME B31.3 standard has been used. The input parameters are:

- Outside diameter (D), 3.346 in.
- Inside diameter (ID), 2.550 in.
- Wall thickness (t), 0.398 in.
- Wall thickness in weakest point (next to thread) ( $t_{low}$ ), 0.280 in.
- Stress value for material for Grad 316; 304; 321 (S), 20,000 psi
- Quality factor (E), 1
- Coefficient (function of material and temperature) (Y), 0.4
- Internal gauge pressure (P)

Formula from maximum allowed pressure from ASME B31.3 standard is:

$$P = \frac{2tSE}{D - 2tY} = 5258.3, \text{ psi} \quad (\text{A-4})$$

or for the thinnest point:

$$P_{low} = \frac{2t_{low}SE}{D - 2t_{low}Y} = 3587.4, \text{ psi} \quad (\text{A-5})$$

Taking into account working pressure,  $P_w$ , as 1,500 psi, safety factor is:

$$sf = \frac{P}{P_w} = 3.5 \quad (\text{A-6})$$

or for weakest point:

$$sf = \frac{P_{low}}{P_w} = 2.4 \quad (\text{A-7})$$

Both safety factors are above 2; thus, current dimensions for the core holder can safely be used up to 1,500 psi.

### A-1.2 Two dimensional core holder

#### Wall thickness and deformation

The required thickness for the cast acrylic wall was estimated using commercial software to guarantee least deformation at the center of the sand pack at 300, 400 and 500 psi. The following boundary conditions have been chosen for model in SolidWorks Simulations:

- No penetration between parts;
- Holes for brackets were fixed;
- Pressure was applied on internal surfaces;
- “Counterbore with Nut” condition with head diameter (0.625 in), nominal shank diameter (0.4375 in) and axial load 100 lbf. for nut and bolt connections at front panel
- “Counterbore Screw” condition with head diameter (0.5 in), nominal shank diameter (0.3125 in) and axial load 80 lbf. for screws used to tight top cap.

For 1.5 in. wall thickness the deformations are 0.109, 0.145 and 0.181 in, respectively, as it is shown in Figures A-1 - A-3.

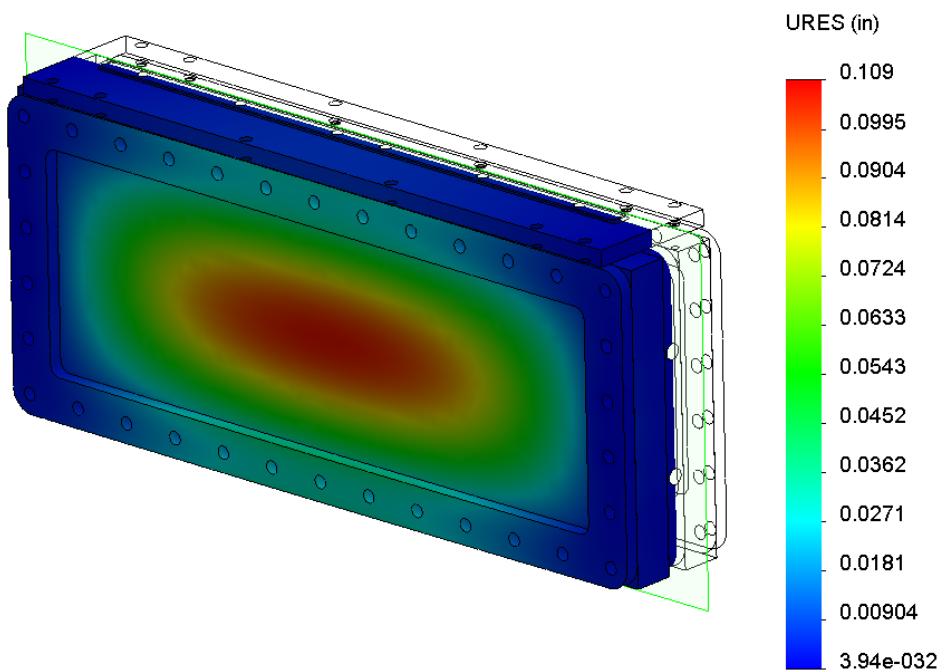


Figure A-1: Cast acrylic wall deformation at 300 psi.

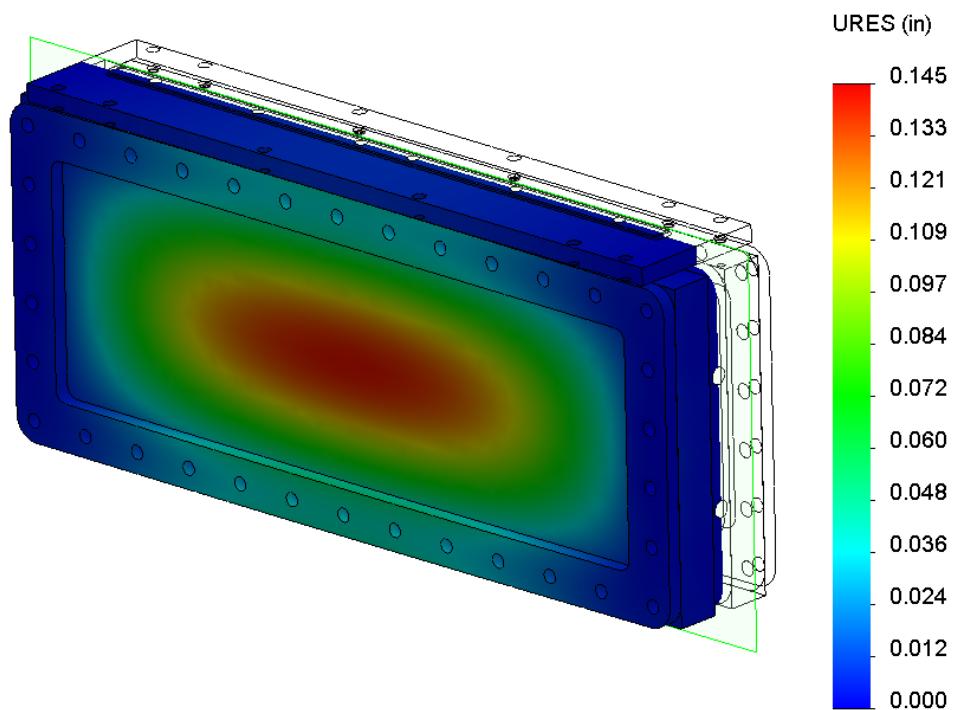


Figure A-2: Cast acrylic wall deformation at 400 psi.

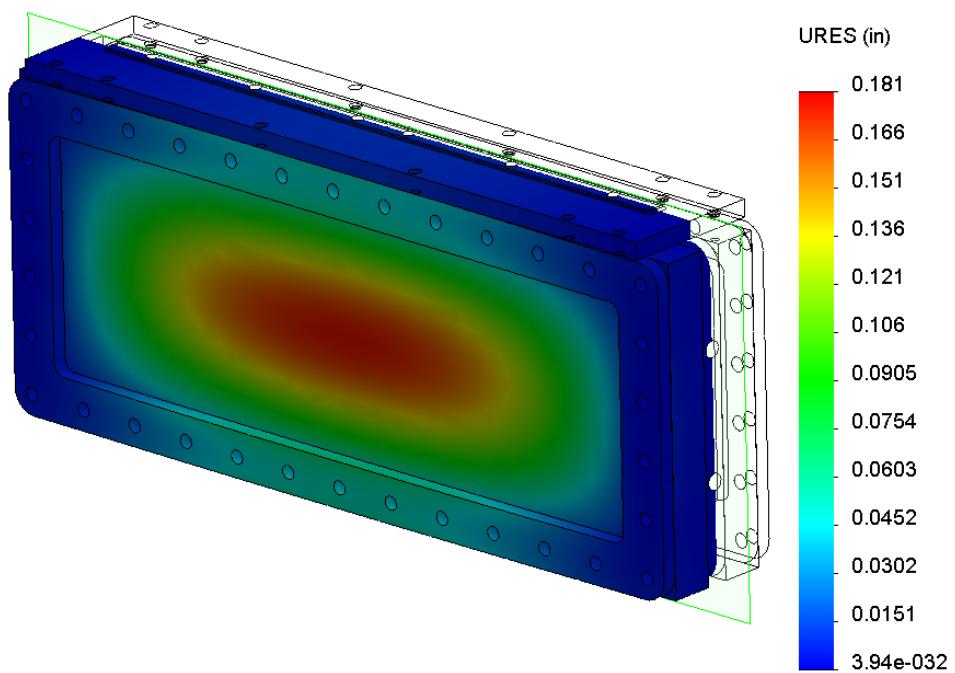


Figure A-3: Cast acrylic wall deformation at 500 psi.

## A-2 Error analysis<sup>2</sup>

Here, the error analysis for the components of the system used to carry out experiments and obtained data is provided.

The pore volume and residual water saturation, provided in Chapters 3, 4 and 5, were obtained using the 250 ml graduated glass cylinder (70022-250, Cole-Parmer Canada Inc.) with least count of 2.0 ml. The tolerance specified by the supplier is  $\pm 2.0$  ml.

The ultimate oil recovery was measured using 15 ml test tubes (430055, Cole-Parmer Canada Inc.) with least count of 0.5 ml. As a result, it introduced the error  $\pm 0.25$  ml in measuring recovered fluid, which was accumulated during each experiment. The corresponding error bars are shown on Figures in Chapter 3, 4 and 5.

The upstream consists of dual-piston pumps coupled with mass flow meters. The flow accuracy and flow precision at 1 ml/min and 12 MPa are equal to  $< 1.0\%$  and  $< 0.5\%$ , respectively. The mass flow meters have the measurements error equal to  $\pm 0.2\%$  of the full scale reading  $+ 0.5$  g/h, according to calibration certificates. The calibration has been performed by Bronkhorst Cori-Tech BV. Since, the flow rate was set at  $0.5 \text{ cm}^3/\text{min}$ , for half hour the accumulated error would be equal to  $\pm 0.28$  ml.

The densities of injected and produced liquids, provided in Chapter 3, 4 and 5, were measured using a mass flow meter (M13, Bronkhorst Cori-Tech BV). As per obtained data, the uncertainty in measurements of density for water, paraffin oil,

---

<sup>2</sup>A version of this appendix has been published as conference paper. A. Baldygin, D. S. Nobes, and S. K. Mitra, "Oil recovery from porous media using emulsion", *Proceedings of the ASME 2014 International Mechanical Engineering Congress & Exposition*, 2014

emulsion, recovered oil and produced water were  $\pm 2.7 \text{ kg/m}^3$ ,  $\pm 0.4 \text{ kg/m}^3$ ,  $\pm 7.4 \text{ kg/m}^3$ ,  $\pm 4.1 \text{ kg/m}^3$ ,  $\pm 9.6 \text{ kg/m}^3$ , respectively.

The viscosity of injected and produced liquids, provided in Chapter 3, 4 and 5, was measured using a rotational viscometer (Rheolab QC, Anton Paar USA Inc.) which has torque resolution of  $< 0.1 \mu\text{Nm}$ . Hence, it would introduce an error into final value of viscosity in a range of  $< 1.85 \cdot 10^{-3}\%$  without taking into account the variation of the geometry of double gap cell. As per collected data, the uncertainty in measurements of viscosity for water, paraffin oil, emulsion, recovered oil, produced water, dyed oil and dyed water were  $\pm 0 \text{ Pa}\cdot\text{s}$ ,  $\pm 0.024 \text{ Pa}\cdot\text{s}$ ,  $\pm 16.70 \text{ Pa}\cdot\text{s}$ ,  $\pm 2.4 \text{ Pa}\cdot\text{s}$ ,  $\pm 0 \text{ Pa}\cdot\text{s}$ ,  $\pm 0.00018 \text{ Pa}\cdot\text{s}$  and  $\pm 0 \text{ Pa}\cdot\text{s}$ , respectively. The viscosity of water and produced water was measured near the top limits of the double gap cell, as a result the uncertainty equals to zero.

The surface tension, provided in Chapter 4 and 5, was measured using a drop shape analyzer(DSA 100, Krüs GmbH). As per obtained data, the uncertainty in measurements of surface tension for water, paraffin oil, recovered oil, produced water, dyed oil and dyed water were  $\pm 1.8 \text{ mN/m}$ ,  $\pm 0.04 \text{ mN/m}$ ,  $\pm 0.09 \text{ mN/m}$ ,  $\pm 0.32 \text{ mN/m}$ ,  $\pm 0.11 \text{ mN/m}$  and  $\pm 0.58 \text{ mN/m}$ , respectively.

### A-3 Consistency in results during 2D core flooding experiments

Here, the comparison of data from complete and incomplete 2D core flooding experiment with horizontal injection - horizontal production (HI-HP) is provided. During incomplete 2D experiment, crashing of the computer operating system has happened during process of emulsion flooding. It caused data lost for an amount of liquid injected into the system and effluent was not collected into the test tubes after 0.35 PV of emulsion injected. The main focus is in understanding the consistency in results from pack to pack for the same well configuration using visual analysis and available test tubes with collected effluent. Relevant parameters for unconsolidated sand pack samples are summarized in Table A-1.

Table A-1: Relevant parameters for unconsolidated sand pack samples used in flooding experiments.

Pack	Well configuration	Porosity, %	Pore volume, cm <sup>3</sup>	Mass of sand pack, g	Absolute permeability, Darcy	Permeability with residual water, Darcy	$S_{wi}^{\ddagger}$
Run #10	HI-HP	34.3	820.1	4179.2	$0.468 \pm 0.074$	$0.379 \pm 0.053$	0.057
Run #11	HI-HP*	34.2	818.6	4183.1	$0.607 \pm 0.064$	$0.521 \pm 0.032$	0.03

‡ - Residual water saturation after oil saturation.

\* - Failed experiment

The photographs in Figure A-4 (a)-(b) show snapshots of the 2D core holder at different pore volumes of emulsion injection for HI-HP configuration. Injection wells are fully perforate with previously discussed perforation pattern. The flood front pattern has similarities in both experiments. The emulsion fills a region close to the left boundary first and then progresses towards the production well. Starting from 0.6 PV of emulsion injection, channeling is observed in Figure A-4 (b). Also, there is a flow across bottom boundary which allows to lift up oil and redirect towards production well. Overall, these images show repeatability and consistency in

experiments from pack to pack for same well configuration.

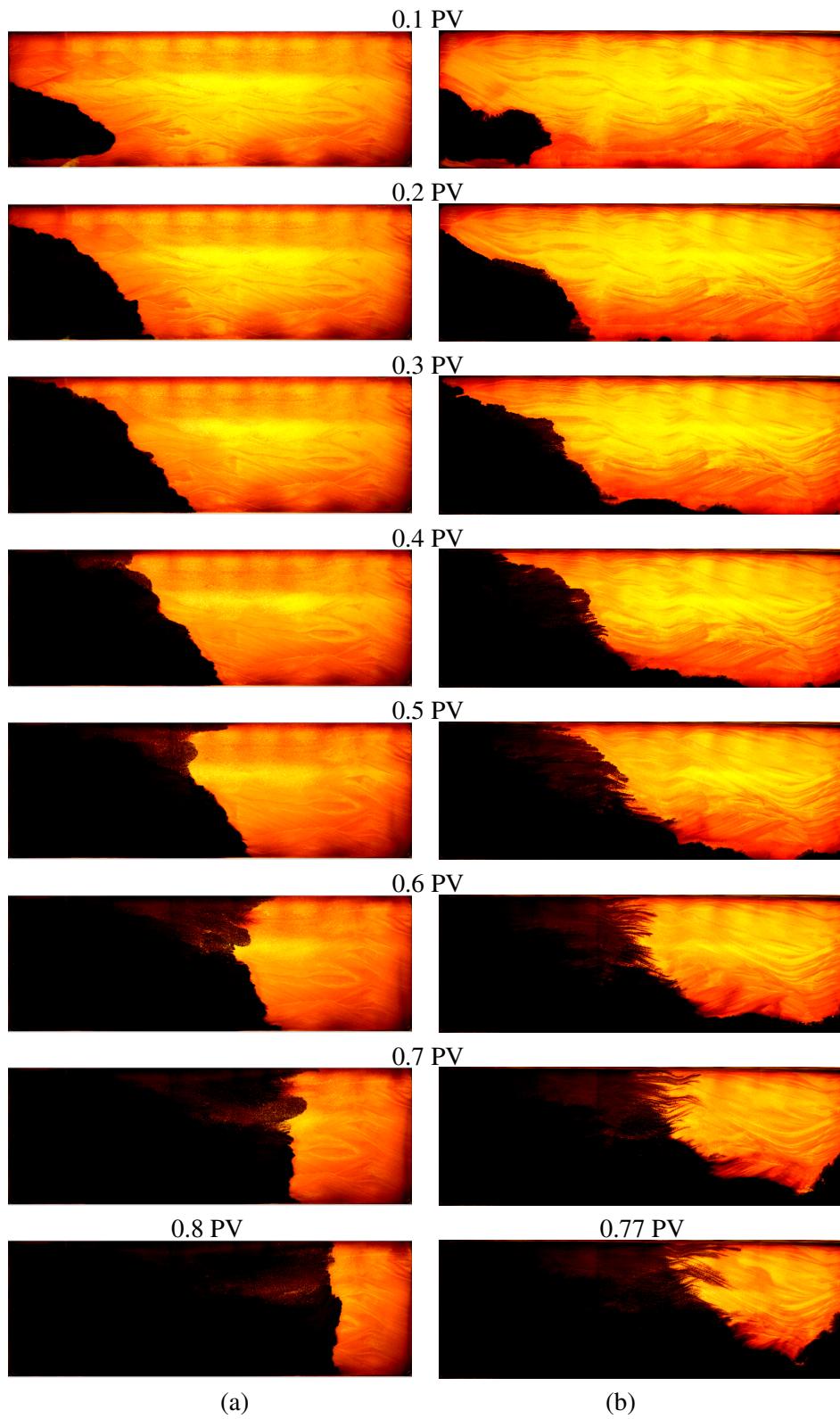


Figure A-4: Cross-section images of the sand pack for different configurations: (a) HI-HP; (b) HI-HP (failed).

Additional Run #11 was added to previously shown Figure 5.21 (a). Figure A-5 shows the ultimate oil recovery curves for three well configurations used in a 2D core holder. The recovery curve for incomplete flooding experiment follows the recovery curve for complete experiment with HI-HP well configuration. It proves repeatability and consistency in experiments from pack to pack for same well configuration.

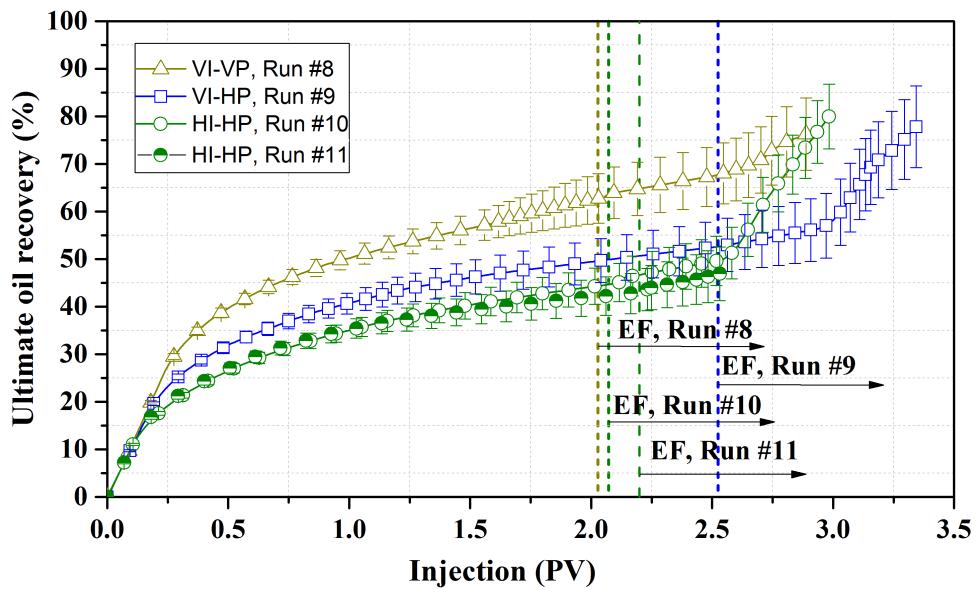


Figure A-5: Ultimate oil recovery curves for water flooding followed by emulsion flooding at different well configurations.

## **A-4 Image processing source code**

The following code was developed using commercial multi-paradigm numerical computing environment (MATLAB R2014a, MathWorks). In order to reduce number of lines in code, due to similar procedures for each section of the core holder, the function to find profile was written into separate file, profilefinder.m. Main file, mainprogram new ref.m, recalls it for every location. Each file has detailed comments.

```
%% Finding Emulsion profile for set of images
%% Quadrise project. 2D core holder experiments
%% Aleksey Baldygin, baldygin@ualberta.ca
%% September 26, 2014
```

```
clear
clc
% File path for Run#1
image_r1 = 'Run1_complete_set/%03d.JPG';
% File path for Run#2
image_r2 = 'Run2_complete_set/%03d.JPG';
% File path for Run#3
image_r3 = 'Run3_complete_set/%03d.JPG';
%% Input parameters
%total number of images
r_r1 = 211;
r_r2 = 324;
r_r3 = 267;
    % Image resolution:
    % Run 1:
    % 3968 x 1360
    % Run 2:
    % 4884 x 1686
    % Run 3:
    % 5336 x 1792
% length for image
l_r1 = 3968;
l_r2 = 4884;
l_r3 = 5336;
% width for image
w_r1 = 1360;
w_r2 = 1686;
w_r3 = 1792;
%(pix/mm) scale 600 - 60 cm - 600 mm
cal_r1 = 600/l_r1;
cal_r2 = 600/l_r2;
cal_r3 = 600/l_r3;
% Reference image for pore volume calculations
A_r1 = imread(sprintf(image_r1,1));
A_r2 = imread(sprintf(image_r2,1));
A_r3 = imread(sprintf(image_r3,1));
% Total area for image
area_r1 = l_r1 * w_r1;
area_r2 = l_r2 * w_r2;
area_r3 = l_r3 * w_r3;

q = 0; % how big is the slice
crop_y=100; %crop top and bottom (for removing artefacts)

crop_yb_r1 = 550;
crop_yb_r2 = 100;
```

```

crop_yb_r3 = 250;

%% Recall function to anylize data
%Run #1
[H_Z1_1,H_Z2_1,H_Z3_1,PV_1] = profilefinder(r_r1,image_r1,l_r1,w_r1,cal_r1,crop_y,↖
crop_yb_r1,q,A_r1,area_r1);
% Run #2
[H_Z1_2,H_Z2_2,H_Z3_2,PV_2] = profilefinder(r_r2,image_r2,l_r2,w_r2,cal_r2,crop_y,↖
crop_yb_r2,q,A_r2,area_r2);
% Run #3
[H_Z1_3,H_Z2_3,H_Z3_3,PV_3] = profilefinder(r_r3,image_r3,l_r3,w_r3,cal_r3,crop_y,↖
crop_yb_r3,q,A_r3,area_r3);

%% Plot, Fit and Velocity profile

fpm=1/5; % 1 image in 5 minutes
%set-up required time for complete experiment
t_r1=[0:r_r1-1]/fpm;
t_r2=[0:r_r2-1]/fpm;
t_r3=[0:r_r3-1]/fpm;

%% Run #1 // get through the data
%Re-crop matrix for future use.
% _c stands for crop
crop_H_Z1_1 = find(H_Z1_1 > 0, 1);
crop_H_Z2_1 = find(H_Z2_1 > 0, 1);
crop_H_Z3_1 = find(H_Z3_1 > 0, 1);

PV_1_1_c = PV_1 (crop_H_Z1_1:end);
PV_2_1_c = PV_1 (crop_H_Z2_1:end);
PV_3_1_c = PV_1 (crop_H_Z3_1:end);

% crop zeros at the begining
H_Z1_1_c = H_Z1_1(crop_H_Z1_1:end);
t_Z1_1_c = t_r1(crop_H_Z1_1:end);

H_Z2_1_c = H_Z2_1(crop_H_Z2_1:end);
t_Z2_1_c = t_r1(crop_H_Z2_1:end);

H_Z3_1_c = H_Z3_1(crop_H_Z3_1:end);
%t_Z3_1_c = t_r1(crop_H_Z3_1:end);
% Split Bottom data in three, based on obtained results.
H_Z3_1_c_1_3 = H_Z3_1(crop_H_Z3_1:80); % crop zeros at the begining
t_Z3_1_c_1_3 = t_r1(crop_H_Z3_1:80);
H_Z3_1_c_2_3 = H_Z3_1(81:120); % crop zeros at the begining
t_Z3_1_c_2_3 = t_r1(81:120);
H_Z3_1_c_3_3 = H_Z3_1(121:end); % crop zeros at the begining
t_Z3_1_c_3_3 = t_r1(121:end);

f_Z1_1=fit(t_Z1_1_c',H_Z1_1_c','poly9','Normalize','on','Robust','LAR');
f_Z2_1=fit(t_Z2_1_c',H_Z2_1_c','poly8','Normalize','on','Robust','Bisquare');

```

```
%f_Z3_1=fit(t_Z3_1_c',H_Z3_1_c','poly7','Normalize','on','Robust','Bisquare');
% Split for three curves
f_Z3_1_1_3=fit(t_Z3_1_c_1_3',H_Z3_1_c_1_3','poly9','Normalize','on','Robust','Bisquare');
f_Z3_1_2_3=fit(t_Z3_1_c_2_3',H_Z3_1_c_2_3','poly7','Normalize','on','Robust','LAR');
f_Z3_1_3_3=fit(t_Z3_1_c_3_3',H_Z3_1_c_3_3','poly7','Normalize','on','Robust','LAR');

[d1_Z1_1,d2_Z1_1] = differentiate(f_Z1_1,t_Z1_1_c); % differentiate plot
[d1_Z2_1,d2_Z2_1] = differentiate(f_Z2_1,t_Z2_1_c);
%[d1_Z3_1,d2_Z3_1] = differentiate(f_Z3_1,t_Z3_1_c);
% Split for three curves
[d1_Z3_1_1_3,d2_Z3_1_1_3] = differentiate(f_Z3_1_1_3,t_Z3_1_c_1_3);
[d1_Z3_1_2_3,d2_Z3_1_2_3] = differentiate(f_Z3_1_2_3,t_Z3_1_c_2_3);
[d1_Z3_1_3_3,d2_Z3_1_3_3] = differentiate(f_Z3_1_3_3,t_Z3_1_c_3_3);

d1_Z1_1_m_s= d1_Z1_1 * 1.66666667*10^(-5); % convert into m/s from mm/min
d1_Z2_1_m_s= d1_Z2_1 * 1.66666667*10^(-5);
% d1_Z3_1_m_s= d1_Z3_1 * 1.66666667*10^(-5);

% Split for 3 curves
d1_Z3_1_m_s_1_3= d1_Z3_1_1_3 * 1.66666667*10^(-5);
d1_Z3_1_m_s_2_3= d1_Z3_1_2_3 * 1.66666667*10^(-5);
d1_Z3_1_m_s_3_3= d1_Z3_1_3_3 * 1.66666667*10^(-5);
% combine back
d1_Z3_1_m_s= cat(1, d1_Z3_1_m_s_1_3, d1_Z3_1_m_s_2_3, d1_Z3_1_m_s_3_3);
t_Z3_1_c = cat (2, t_Z3_1_c_1_3, t_Z3_1_c_2_3, t_Z3_1_c_3_3);

%% Run #2 // get through the data
%Re-crop matrix for future use.
% _c stands for crop
crop_H_Z1_2 = find(H_Z1_2 > 0, 1);
% crop_H_Z2_2 = find(H_Z2_2 > 0, 1);
crop_H_Z3_2 = find(H_Z3_2 > 0, 1);

PV_1_2_c = PV_2 (crop_H_Z1_2:end);
%PV_2_2_c = PV_2 (crop_H_Z2_2:end);
PV_3_2_c = PV_2 (crop_H_Z3_2:end);

H_Z1_2_c = H_Z1_2(crop_H_Z1_2:end); % crop zeros at the begining
t_Z1_2_c = t_r2(crop_H_Z1_2:end);

%H_Z3_2_c = H_Z3_2(crop_H_Z3_2:end); % crop zeros at the begining
%t_Z3_2_c = t_r2(crop_H_Z3_2:end);

% Split Bottom data in two, based on obtained results.
H_Z3_2_c_1_2 = H_Z3_2(crop_H_Z3_2:120); % crop zeros at the begining
t_Z3_2_c_1_2 = t_r2(crop_H_Z3_2:120);
H_Z3_2_c_2_2 = H_Z3_2(121:end); % crop zeros at the begining
t_Z3_2_c_2_2 = t_r2(121:end);
```

```

f_Z1_2=fit(t_Z1_2_c',H_Z1_2_c','poly9','Normalize','on','Robust','Bisquare');
f_Z2_2=fit(t_r2',H_Z2_2','poly7','Normalize','on','Robust','Bisquare');

% f_Z3_2=fit(t_Z3_2_c',H_Z3_2_c','poly8','Normalize','on','Robust','Bisquare');
% Split for two curves
f_Z3_2_1_2=fit(t_Z3_2_c_1_2',H_Z3_2_c_1_2','poly6','Normalize','on','Robust','Bisquare');
f_Z3_2_2_2=fit(t_Z3_2_c_2_2',H_Z3_2_c_2_2','poly7','Normalize','on','Robust','Bisquare');

[d1_Z1_2,d2_Z1_2] = differentiate(f_Z1_2,t_Z1_2_c); % differentiate plot
[d1_Z2_2,d2_Z2_2] = differentiate(f_Z2_2,t_r2);
%[d1_Z3_2,d2_Z3_2] = differentiate(f_Z3_2,t_r2);
% Split for two curves
[d1_Z3_2_1_2,d2_Z3_2_1_2] = differentiate(f_Z3_2_1_2,t_Z3_2_c_1_2);
[d1_Z3_2_2_2,d2_Z3_2_2_2] = differentiate(f_Z3_2_2_2,t_Z3_2_c_2_2);

d1_Z1_2_m_s= d1_Z1_2 * 1.66666667*10^(-5); % convert into m/s from mm/min
d1_Z2_2_m_s= d1_Z2_2 * 1.66666667*10^(-5);
%d1_Z3_2_m_s= d1_Z3_2 * 1.66666667*10^(-5);
% Split for 2 curves
d1_Z3_2_m_s_1_2= d1_Z3_2_1_2 * 1.66666667*10^(-5);
d1_Z3_2_m_s_2_2= d1_Z3_2_2_2 * 1.66666667*10^(-5);
% combine back
d1_Z3_2_m_s_com = cat(1, d1_Z3_2_m_s_1_2, d1_Z3_2_m_s_2_2);
t_Z3_2_c_com = cat (2, t_Z3_2_c_1_2, t_Z3_2_c_2_2);

%% Run #3 // get through the data
%Re-crop matrix for future use.
% _c stands for crop
crop_H_Z1_3 = find(H_Z1_3 > 0, 1);
crop_H_Z2_3 = find(H_Z2_3 > 0, 1);
crop_H_Z3_3 = find(H_Z3_3 > 0, 1);

PV_1_3_c = PV_3 (crop_H_Z1_3:end);
PV_2_3_c = PV_3 (crop_H_Z2_3:end);
PV_3_3_c = PV_3 (crop_H_Z3_3:end);

H_Z1_3_c = H_Z1_3(crop_H_Z1_3:end); % crop zeros at the begining
t_Z1_3_c = t_r3(crop_H_Z1_3:end);

H_Z2_3_c = H_Z2_3(crop_H_Z2_3:end); % crop zeros at the begining
t_Z2_3_c = t_r3(crop_H_Z2_3:end);

H_Z3_3_c = H_Z3_3(crop_H_Z3_3:end); % crop zeros at the begining
t_Z3_3_c = t_r3(crop_H_Z3_3:end);

f_Z1_3=fit(t_Z1_3_c',H_Z1_3_c','poly9','Normalize','on','Robust','Bisquare');
f_Z2_3=fit(t_Z2_3_c',H_Z2_3_c','poly7','Normalize','on','Robust','Bisquare');
f_Z3_3=fit(t_Z3_3_c',H_Z3_3_c','poly6','Normalize','on','Robust','Bisquare');

```

```
[d1_Z1_3,d2_Z1_3] = differentiate(f_Z1_3,t_Z1_3_c); % differentiate plot
[d1_Z2_3,d2_Z2_3] = differentiate(f_Z2_3,t_Z2_3_c);
[d1_Z3_3,d2_Z3_3] = differentiate(f_Z3_3,t_Z3_3_c);

d1_Z1_3_m_s= d1_Z1_3 * 1.66666667*10^(-5); % convert into m/s from mm/min
d1_Z2_3_m_s= d1_Z2_3 * 1.66666667*10^(-5);
d1_Z3_3_m_s= d1_Z3_3 * 1.66666667*10^(-5);

%% Plot Run %1
scrsz = get(0,'ScreenSize'); % get screen size
figure('Position',[0 scrsz(4)/4 1000 500])
% figure('Position', [x y width height])
plot(t_Z1_1_c,d1_Z1_1_m_s,'r',t_Z2_1_c,d1_Z2_1_m_s,'g',t_Z3_1_c,d1_Z3_1_m_s,'c',t_r1,%
7.309*10^(-6),'b') % double plot method
title('Velocity')
axis([0,max(t_r1),0,1.3*10^(-5)])
%axis normal
set(gca,'YTick',[10^(-6),2*10^(-6),4*10^(-6),6*10^(-6),8*10^(-6),1*10^(-5),1.25*10^(-5)])
xlabel('time, [min]')
ylabel('speed, [m/s]')
grid on
hleg1 = legend('top','center','bottom','reference');

fig1 = figure('Position',[1000 0 1000 1500])
subplot(3,1,1)
plot(f_Z1_1, t_r1, H_Z1_1,'k.')
title('Top','FontWeight','bold','FontSize',14,'FontName','Arial')
hleg_sp1 = legend('Front location','Poly-fit','Location','SouthEast');
ylabel('position, [mm]','FontWeight','bold','FontSize',12, ...
'FontName','Arial');
xlabel('time, [min]','FontWeight','bold','FontSize',12, ...
'FontName','Arial');
axis([0,max(t_r1),0,600])
set(gca,'color','w','FontWeight','bold','FontSize',14,'FontName','Arial');
subplot(3,1,2)
plot(f_Z2_1, t_r1, H_Z2_1,'k.')
title('Center','FontWeight','bold','FontSize',14,'FontName','Arial')
hleg_sp2 = legend('Front location','Poly-fit','Location','SouthEast');
ylabel('position, [mm]','FontWeight','bold','FontSize',12, ...
'FontName','Arial');
xlabel('time, [min]','FontWeight','bold','FontSize',12, ...
'FontName','Arial');
axis([0,max(t_r1),0,600])
set(gca,'color','w','FontWeight','bold','FontSize',14,'FontName','Arial');
subplot(3,1,3)
hold on
box on
plot (f_Z3_1_1_3, t_Z3_1_c_1_3', H_Z3_1_c_1_3', 'k.')
plot (f_Z3_1_2_3, t_Z3_1_c_2_3', H_Z3_1_c_2_3', 'k.')
plot (f_Z3_1_3_3, t_Z3_1_c_3_3', H_Z3_1_c_3_3', 'k.')


```

```
% plot(f_Z3_1, t_r1', H_Z3_1')
title('Bottom','FontWeight','bold','FontSize',14,'FontName','Arial')
hleg_sp3 = legend('Front location','Poly-fit','Location','SouthEast');
ylabel('position, [mm]','FontWeight','bold','FontSize',12,... ...
'FontName','Arial');
xlabel('time, [min]','FontWeight','bold','FontSize',12,... ...
'FontName','Arial');
axis([0,max(t_r1),0,600])
set(gca,'color','w','FontWeight','bold','FontSize',14,'FontName','Arial');
set(gcf,'PaperPositionMode','auto'); % freeze configuration for image, to save image as ↵
it is shown on the screen
print(fig1,'-dpng','VIVP');
print(fig1,'-depsc','VIVP');

%% Plot Run # 2
scrsz = get(0,'ScreenSize'); % get screen size
figure('Position',[0 scrsz(4)/4 1000 500])
% figure('Position', [x y width height])
hold on
plot(t_Z1_2_c,d1_Z1_2_m_s,'r',t_r2,d1_Z2_2_m_s,'g',t_Z3_2_c_1_2,d1_Z3_2_m_s_1_2,'c',t_r2, ↵
7.309*10^(-6),'b') % double plot method
plot(t_Z3_2_c_2_2,d1_Z3_2_m_s_2_2,'c')
title('Velocity')
axis([0,max(t_r2),0,2.5*10^(-5)])
%axis normal
set(gca,'YTick',[10^(-6),2*10^(-6),4*10^(-6),6*10^(-6),8*10^(-6),1*10^(-5),1.25*10^(-5)])
xlabel('time, [min]')
ylabel('speed, [m/s]')
grid on
hleg1 = legend('top','center','bottom','reference');

fig2 = figure('Position',[1000 0 1000 1500])
subplot(3,1,1)
plot(f_Z1_2, t_r2', H_Z1_2','k.')
title('Top','FontWeight','bold','FontSize',14,'FontName','Arial')
hleg_sp1 = legend('VI-HP','Poly-fit','Location','SouthEast');
ylabel('position, [mm]','FontWeight','bold','FontSize',12,... ...
'FontName','Arial');
xlabel('time, [min]','FontWeight','bold','FontSize',12,... ...
'FontName','Arial');
axis([0,max(t_r2),0,600]);
set(gca,'color','w','FontWeight','bold','FontSize',14,'FontName','Arial');
subplot(3,1,2)
plot(f_Z2_2, t_r2', H_Z2_2','k.')
title('Center','FontWeight','bold','FontSize',14,'FontName','Arial')
hleg_sp2 = legend('VI-HP','Poly-fit','Location','SouthEast');
ylabel('position, [mm]','FontWeight','bold','FontSize',12,... ...
'FontName','Arial');
```

```

xlabel('time, [min]', 'FontWeight', 'bold', 'FontSize', 12, ...
       'FontName', 'Arial');
axis([0, max(t_r3), 0, 600]);
set(gca, 'color', 'w', 'FontWeight', 'bold', 'FontSize', 14, 'FontName', 'Arial');
subplot(3,1,3)
hold on
box on
plot(f_Z3_2_1_2, t_Z3_2_c_1_2, H_Z3_2_c_1_2, 'k.')
plot(f_Z3_2_2_2, t_Z3_2_c_2_2, H_Z3_2_c_2_2, 'k.')
title('Bottom', 'FontWeight', 'bold', 'FontSize', 14, 'FontName', 'Arial')
hleg_sp3 = legend('VI-HP', 'Poly-fit', 'Location', 'SouthEast');
ylabel('position, [mm]', 'FontWeight', 'bold', 'FontSize', 12, ...
       'FontName', 'Arial');
xlabel('time, [min]', 'FontWeight', 'bold', 'FontSize', 12, ...
       'FontName', 'Arial');
axis([0, max(t_r2), 0, 600]);
set(gca, 'color', 'w', 'FontWeight', 'bold', 'FontSize', 14, 'FontName', 'Arial');
set(gcf, 'PaperPositionMode', 'auto'); % freeze configuration for image, to save image as ↵
it is shown on the screen
print(fig2, '-dpng', 'VIHP');
print(fig2, '-depsc', 'VIHP');

%% Plot Run # 3
scrsz = get(0, 'ScreenSize'); % get screen size
figure('Position', [0 scrsz(4)/4 1000 500])
% figure('Position', [x y width height])
plot(t_Z1_3_c, d1_Z1_3_m_s, 'r', t_Z2_3_c, d1_Z2_3_m_s, 'g', t_Z3_3_c, d1_Z3_3_m_s, 'c', t_r3, ↵
7.309*10^(-6), 'b') % double plot method
title('Velocity')
axis([0, max(t_r3), 0, 2.25*10^(-5)])
%axis normal
set(gca, 'YTick', [10^(-6), 2*10^(-6), 4*10^(-6), 6*10^(-6), 8*10^(-6), 1*10^(-5), 1.25*10^(-5)])
xlabel('time, [min]')
ylabel('speed, [m/s]')
grid on
hleg1 = legend('top', 'center', 'bottom', 'reference');

fig3 = figure('Position', [1000 0 1000 1500])
subplot(3,1,1)
plot(f_Z1_3, t_Z1_3_c, H_Z1_3_c, 'k.')
title('Top', 'FontWeight', 'bold', 'FontSize', 14, 'FontName', 'Arial')
hleg_sp1 = legend('HI-HP', 'Poly-fit', 'Location', 'SouthEast');
ylabel('position, [mm]', 'FontWeight', 'bold', 'FontSize', 12, ...
       'FontName', 'Arial');
xlabel('time, [min]', 'FontWeight', 'bold', 'FontSize', 12, ...
       'FontName', 'Arial');
axis([0, max(t_r3), 0, 600]);
set(gca, 'color', 'w', 'FontWeight', 'bold', 'FontSize', 14, 'FontName', 'Arial');
subplot(3,1,2)

```

```

plot(f_Z2_3, t_Z2_3_c, H_Z2_3_c,'k.')
title('Center','FontWeight','bold','FontSize',14,'FontName','Arial')
hleg_sp2 = legend('HI-HP','Poly-fit','Location','SouthEast');
ylabel('position, [mm]','FontWeight','bold','FontSize',12,...'FontName','Arial');
xlabel('time, [min]','FontWeight','bold','FontSize',12,...'FontName','Arial');
axis([0,max(t_r3),0,600])
set(gca,'color','w','FontWeight','bold','FontSize',14,'FontName','Arial');
subplot(3,1,3)
plot(f_Z3_3, t_Z3_3_c, H_Z3_3_c,'k.')
title('Bottom','FontWeight','bold','FontSize',14,'FontName','Arial')
hleg_sp3 = legend('HI-HP','Poly-fit','Location','SouthEast');
ylabel('position, [mm]','FontWeight','bold','FontSize',12,...'FontName','Arial');
xlabel('time, [min]','FontWeight','bold','FontSize',12,...'FontName','Arial');
axis([0,max(t_r3),0,600])
set(gca,'color','w','FontWeight','bold','FontSize',14,'FontName','Arial');
set(gcf,'PaperPositionMode','auto'); % freeze configuration for image, to save image as ↵
it is shown on the screen
print(fig3,'-dpng','HIHP');
print(fig3,'-depsc','HIHP');

%% Combined Runs into single plot vs Time % Final for paper
figure('Position',[1000 0 1000 1500])
subplot(3,1,1)
hold on
% Run #1
plot (t_Z1_1_c,d1_Z1_1_m_s,'k') % top
% Run #2
plot(t_Z1_2_c,d1_Z1_2_m_s,'g') % top
% Run #3
plot(t_Z1_3_c,d1_Z1_3_m_s,'r') % top
plot(t_r3,7.309*10^(-6),'b') % reference
title('Top')
hleg_sp1 = legend('VI-HP','HI-HP','Reference','Location','NorthEast');
ylabel('position, [mm]')
xlabel('time, [min]')
grid on
axis([0,max(t_r3),0,1.5*10^(-5)])
subplot(3,1,2)
hold on
% Run #1
plot(t_Z2_1_c,d1_Z2_1_m_s,'k') % Center
% Run #2
plot(t_r2,d1_Z2_2_m_s,'g') % Center
% Run #3
plot(t_Z2_3_c,d1_Z2_3_m_s,'r') % Center
plot(t_r3,7.309*10^(-6),'b') % reference
title('Center')

```

```

hleg_sp2 = legend('VI-HP','HI-HP','Reference','Location','NorthEast');
ylabel('position, [mm]')
xlabel('time, [min]')
grid on
axis([0,max(t_r3),0,1.5*10^(-5)])
subplot(3,1,3)
hold on
% Run #1
plot (t_Z3_1_c,d1_Z3_1_m_s,'k')
% Run #2
%h1_1_2= plot(t_Z3_2_c_1_2,d1_Z3_2_m_s_1_2,'g',t_Z3_2_c_2_2,d1_Z3_2_m_s_2_2,'g')
plot (t_Z3_2_c_com,d1_Z3_2_m_s_com,'g')
% Run #3
plot(t_Z3_3_c,d1_Z3_3_m_s,'r') % bottom
plot(t_r3,7.309*10^(-6),'b-') % reference
title('Bottom')
legend('VI-HP','HI-HP','Reference','Location','NorthEast');
ylabel('position, [mm]')
xlabel('time, [min]')
grid on
axis([0,max(t_r3),0,1.5*10^(-5)])

%% Combined Runs into single plot vs PV % Final for paper
fig4 = figure('Position',[1000 0 1000 1500])
subplot(3,1,1)
hold on
% Run #1
plot (PV_1_1_c,d1_Z1_1_m_s,'k','LineWidth',1.5) % top
% Run #2
plot (PV_1_2_c,d1_Z1_2_m_s,'g','LineWidth',1.5) % top
% Run #3
plot (PV_1_3_c,d1_Z1_3_m_s,'r','LineWidth',1.5) % top
plot(PV_1,1.177*10^(-5),'k','LineWidth',2.5) % reference
plot(PV_1,1.204*10^(-5),'g','LineWidth',2.5) % reference
plot(PV_1,1.215 *10^(-5),'r','LineWidth',2.5) % reference
title('Top','FontWeight','bold','FontSize',14,'FontName','Arial');
legend('VI-VP','VI-HP','HI-HP','Reference','Location','NorthEast');
ylabel('Velocity, [m/s]','FontWeight','bold','FontSize',12,...,
      'FontName','Arial');
xlabel('Emulsion Injected, [PV]','FontWeight','bold','FontSize',12,...,
      'FontName','Arial');
grid on
axis([0,1,0,1.5*10^(-5)]);
set(gca,'color','w','FontWeight','bold','FontSize',14,'FontName','Arial');
subplot(3,1,2)
hold on
% Run #1
plot (PV_2_1_c,d1_Z2_1_m_s,'k','LineWidth',1.5) % Center
% Run #2
plot (PV_2,d1_Z2_2_m_s,'g','LineWidth',1.5) % Center

```

```
% Run #3
plot (PV_2_3_c,d1_Z2_3_m_s,'r','LineWidth',1.5) % Center
plot(PV_2,1.177*10^(-5),'k','LineWidth',2.5) % reference
plot(PV_2,1.204*10^(-5),'g','LineWidth',2.5) % reference
plot(PV_2,1.215 *10^(-5),'r','LineWidth',2.5) % reference
title('Center','FontWeight','bold','FontSize',14,'FontName','Arial');
legend('VI-VP','VI-HP','HI-HP','Reference','Location','NorthEast');
ylabel('Velocity, [m/s]','FontWeight','bold','FontSize',12,...,
      'FontName','Arial');
xlabel('Emulsion Injected, [PV]','FontWeight','bold','FontSize',12,...,
      'FontName','Arial');
grid on
axis([0,1,0,1.5*10^(-5)]);
set(gca,'color','w','FontWeight','bold','FontSize',14,'FontName','Arial');
subplot(3,1,3)
hold on
% Run #1
plot (PV_3_1_c,d1_Z3_1_m_s,'k','LineWidth',1.5)
% Run #2
%h1_1_2= plot(t_Z3_2_c_1_2,d1_Z3_2_m_s_1_2,'g',t_Z3_2_c_2_2,d1_Z3_2_m_s_2_2,'g')
plot (PV_3_2_c,d1_Z3_2_m_s_com,'g','LineWidth',1.5)
% Run #3
plot (PV_3_3_c,d1_Z3_3_m_s,'r','LineWidth',1.5) % bottom
plot(PV_3,1.177*10^(-5),'k','LineWidth',2.5) % reference
plot(PV_3,1.204*10^(-5),'g','LineWidth',2.5) % reference
plot(PV_3,1.215 *10^(-5),'r','LineWidth',2.5) % reference
title('Bottom','FontWeight','bold','FontSize',14,'FontName','Arial');
legend('VI-VP','VI-HP','HI-HP','Reference','Location','NorthEast');
ylabel('Velocity, [m/s]','FontWeight','bold','FontSize',12,...,
      'FontName','Arial');
xlabel('Emulsion Injected, [PV]','FontWeight','bold','FontSize',12,...,
      'FontName','Arial');
grid on
axis([0,1,0,1.5*10^(-5)]);
set(gca,'color','w','FontWeight','bold','FontSize',14,'FontName','Arial');
set(gcf,'PaperPositionMode','auto'); % freeze configuration for image, to save image as ↵
it is shown on the screen
print(fig4,'-dpng','Figure10');
print(fig4,'-depSC','Figure10');
```

```

function [H_Z1,H_Z2,H_Z3,PV] = profilefinder(r,image,l,w,cal,crop_y,crop_yb,q,A_ref,ref)

%prepare space for data (front)
H_Z1=zeros(1,r);
H_Z2=zeros(1,r);
H_Z3=zeros(1,r);

%Set locations for speed profiles:
w_3=round(w/4); %bottom
w_2=2*w_3; %center
w_1=3*w_3; %top

for k=1:r

%Read nth image!
A = imread(sprintf(image,k)); %read out images
B = imrotate(A,270); %270 degrees, since 'edge'-function starts from the top of the ↴
image

% First position
Z1=B(crop_y:l-crop_yb,w_1-q:w_1+q,1,:);
Z1_bw=im2bw(Z1,100/255);
Z1_edge=edge(Z1_bw,'prewitt');
find_loc_Z1 = find(Z1_edge == 1);
if find_loc_Z1 > 0 % if emulsion was detected + correct location for crop value
location_corr_Z1 = find(Z1_edge == 1) + crop_y - 1;
else
location_corr_Z1 = 0;
end

y_Z1 = mean(location_corr_Z1); % Most frequent values in array
H_Z1(k) = y_Z1*cal; % TOP

% Second position
Z2=B(crop_y:l-crop_yb,w_2-q:w_2+q,1,:); %red channel
Z2_bw=im2bw(Z2,100/255);
Z2_edge=edge(Z2_bw,'prewitt');
find_loc_Z2 = find(Z2_edge == 1); % search for front location
if find_loc_Z2 > 0 % if emulsion was detected + correct location for crop value
location_corr_Z2 = find(Z2_edge == 1) + crop_y - 1;
else % if there is no emulsion, set to zero
location_corr_Z2 = 0;
end

y_Z2 = max(location_corr_Z2); % set location
H_Z2(k)=y_Z2*cal; % correct location with calibration (\approx number)

% Third position
Z3=B(crop_y:l-crop_yb,w_3-q:w_3+q,1,:);
Z3_bw=im2bw(Z3,100/255);
Z3_edge=edge(Z3_bw,'prewitt');
find_loc_Z3 = find(Z3_edge == 1);

```

```
if find_loc_Z3 > 0 % if emulsion was detected + correct location for crop value
location_corr_Z3 = find(Z3_edge == 1) + crop_y - 1;
elseif isempty(find_loc_Z3) && (k > 100) % if there is no emulsion, set to zero
    % do nothing
else % if there is no emulsion, set to zero
location_corr_Z3 = 0;
end

y_Z3 = max(location_corr_Z3);
H_Z3(k)=y_Z3*cal; % BOTTOM

%% Finding PV

A_an = imsubtract (A_ref, A);
A_an_RED = A_an(:,:,1,:);
A_an_RED_bw = im2bw(A_an_RED,40/255);
total = bwarea(A_an_RED_bw);
PV(k) = 1 - (ref - total) / ref;

end

return
```

## **A-5 Pressure data processing source code**

The following code was developed using commercial multi-paradigm numerical computing environment (MATLAB R2014a, MathWorks) to process data collected from 15 pressure sensors during 2D core flooding studies. Each file has detailed comments.



```

try
    result = regexp(rawData{row}, regexstr, 'names');
    numbers = result.numbers;

    % Detected commas in non-thousand locations.
    invalidThousandsSeparator = false;
    if any(numbers==',');
        thousandsRegExp = '^\d+?(\,\d{3})*\.\{0,1\}\d*$';
        if isempty(regexp(thousandsRegExp, ',', 'once'));
            numbers = NaN;
            invalidThousandsSeparator = true;
        end
    end
    % Convert numeric strings to numbers.
    if ~invalidThousandsSeparator;
        numbers = textscan(strrep(numbers, ',', ''), '%f');
        numericData(row, col) = numbers{1};
        raw{row, col} = numbers{1};
    end
    catch me
    end
end
%% Replace non-numeric cells with NaN
R = cellfun(@(x) ~isnumeric(x) && ~islogical(x), raw); % Find non-numeric cells
raw(R) = {NaN}; % Replace non-numeric cells

%% Allocate imported array to column variable names
Timeinmin = cell2mat(raw(:, 1));
PoreVolumePV = cell2mat(raw(:, 2));
Pressureinlet = cell2mat(raw(:, 3));
EMULSIONIN = cell2mat(raw(:, 4));
CP11 = cell2mat(raw(:, 5));
CP12 = cell2mat(raw(:, 6));
CP13 = cell2mat(raw(:, 7));
CP14 = cell2mat(raw(:, 8));
CP15 = cell2mat(raw(:, 9));
CP21 = cell2mat(raw(:, 10));
CP22 = cell2mat(raw(:, 11));
CP23 = cell2mat(raw(:, 12));
CP24 = cell2mat(raw(:, 13));
CP25 = cell2mat(raw(:, 14));
CP31 = cell2mat(raw(:, 15));
CP32 = cell2mat(raw(:, 16));
CP33 = cell2mat(raw(:, 17));
CP34 = cell2mat(raw(:, 18));
CP35 = cell2mat(raw(:, 19));

```

```
EMULSIONIN (1) = 0;
PoreVolumePV(1) = PoreVolumePV(2);
Pressureinlet(1) = Pressureinlet(2);
Timeinmin (1) = 0;

%% Clear temporary variables
clearvars filename delimiter formatSpec fileID dataArray ans raw col numericData rawData ↵
row regexstr result numbers invalidThousandsSeparator thousandsRegExp me R;

CP11_f = zeros (size(CP11,1),1);
CP12_f = zeros (size(CP12,1),1);
CP13_f = zeros (size(CP13,1),1);
CP14_f = zeros (size(CP14,1),1);
CP15_f = zeros (size(CP15,1),1);
CP21_f = zeros (size(CP21,1),1);
CP22_f = zeros (size(CP22,1),1);
CP23_f = zeros (size(CP23,1),1);
CP24_f = zeros (size(CP24,1),1);
CP25_f = zeros (size(CP25,1),1);
CP31_f = zeros (size(CP31,1),1);
CP32_f = zeros (size(CP32,1),1);
CP33_f = zeros (size(CP33,1),1);
CP34_f = zeros (size(CP34,1),1);
CP35_f = zeros (size(CP35,1),1);

CP11_f(:) = - CP11(:);
CP12_f(:) = - CP12(:);
CP13_f(:) = - CP13(:);
CP14_f(:) = CP14(:);
CP15_f(:) = CP15(:);
CP21_f(:) = CP21(:);
CP22_f(:) = - CP22(:);
CP23_f(:) = CP23(:);
CP24_f(:) = CP24(:);
CP25_f(:) = - CP25(:);
CP31_f(:) = - CP31(:);
CP32_f(:) = - CP32(:);
CP33_f(:) = - CP33(:);
CP34_f(:) = CP34(:);
CP35_f(:) = CP35(:);

clearvars CP11 CP12 CP13 CP14 CP15 CP21 CP22 CP23 CP24 CP25 CP31 CP32 CP33 CP34 CP35;

% load data from image analysis
load('PVandTime_from_images.mat');
clearvars PV_2 PV_3 t_r2 t_r3;

% temp time for double check
temp_time = zeros (size(t_r1,2),1);
```

```
%% set coordinates for surface plot
x_crd = zeros (15,1);
x_crd(1) = 50;
x_crd(2) = 175;
x_crd(3) = 300;
x_crd(4) = 425;
x_crd(5) = 550;

x_crd(6) = 50;
x_crd(7) = 175;
x_crd(8) = 300;
x_crd(9) = 425;
x_crd(10) = 550;

x_crd(11) = 50;
x_crd(12) = 175;
x_crd(13) = 300;
x_crd(14) = 425;
x_crd(15) = 550;

y_crd = zeros (15,1);
y_crd(1) = 160;
y_crd(2) = 160;
y_crd(3) = 160;
y_crd(4) = 160;
y_crd(5) = 160;

y_crd(6) = 100;
y_crd(7) = 100;
y_crd(8) = 100;
y_crd(9) = 100;
y_crd(10) = 100;

y_crd(11) = 40;
y_crd(12) = 40;
y_crd(13) = 40;
y_crd(14) = 40;
y_crd(15) = 40;

CP = zeros (15,size(t_r1,2));
%%
step_image = 2;
for step = 1 : size (Timeinmin,1)
    if (Timeinmin(step) >= t_r1(step_image))
        % save current time for further reference
        temp_time (step_image) = Timeinmin(step,1);

        %Set new step for pressure data
        step_p_min = step - 10;
        step_p_max = step + 10;
```

```

%Trim new data for plotting +/- 10 steps from given point
%1st row
CP11_f_temp = CP11_f (step_p_min:step_p_max);
CP (1,step_image) = mean2(CP11_f_temp);
CP12_f_temp = CP12_f (step_p_min:step_p_max);
CP (2,step_image) = mean2(CP12_f_temp);
CP13_f_temp = CP13_f (step_p_min:step_p_max);
CP (3,step_image) = mean2(CP13_f_temp);
CP14_f_temp = CP14_f (step_p_min:step_p_max);
CP (4,step_image) = mean2(CP14_f_temp);
CP15_f_temp = CP15_f (step_p_min:step_p_max);
CP (5,step_image) = mean2(CP15_f_temp);

%2nd row
CP21_f_temp = CP21_f (step_p_min:step_p_max);
CP (6,step_image) = mean2(CP21_f_temp);
CP22_f_temp = CP22_f (step_p_min:step_p_max);
CP (7,step_image) = mean2(CP22_f_temp);
CP23_f_temp = CP23_f (step_p_min:step_p_max);
CP (8,step_image) = mean2(CP23_f_temp);
CP24_f_temp = CP24_f (step_p_min:step_p_max);
CP (9,step_image) = mean2(CP24_f_temp);
CP25_f_temp = CP25_f (step_p_min:step_p_max);
CP (10,step_image) = mean2(CP25_f_temp);

%3rd row
CP31_f_temp = CP31_f (step_p_min:step_p_max);
CP (11,step_image) = mean2(CP31_f_temp);
CP32_f_temp = CP32_f (step_p_min:step_p_max);
CP (12,step_image) = mean2(CP32_f_temp);
CP33_f_temp = CP33_f (step_p_min:step_p_max);
CP (13,step_image) = mean2(CP33_f_temp);
CP34_f_temp = CP34_f (step_p_min:step_p_max);
CP (14,step_image) = mean2(CP34_f_temp);
CP35_f_temp = CP35_f (step_p_min:step_p_max);
CP (15,step_image) = mean2(CP35_f_temp);

% next point for time-data
step_image = step_image + 1;
if (step_image > size(t_r1,2))
    break;
end
end

% Load background image
img = imread('run1background.png');
min_x = 0;
max_x = 600;
min_y = 0;
max_y = 200;

```

```

fig1 = figure('Position',[500 100 1200 350], 'Color',[1 1 1]); %500 left coord. 100 bottom coord. 1200 width 400 height
winsize = get(fig1,'Position'); %set position, dimension of figure for future reference.
winsize(1:2) = [0 0]; %adjust windows size for recording
numframes=size(CP,2); %determines number of frames
set(fig1,'nextplot','replacechildren');
set(gcf,'Renderer','zbuffer');

image = 'Run1/Run1_%03d'; %set name for saving .png-files
pvinj = 'Emulsion inj. = %1.4f PV'; %set name for legends

writerObj = VideoWriter('run1.avi'); %prepares .avi-file for saving frames
open(writerObj); %opens .avi-file for saving

for i=1:numframes
    % Get current data for plot
    z_p=CP(:,i);
    Data = scatteredInterpolant(x_crd,y_crd,z_p); %converts data for suitable format
    x_n = 50:10:550;
    y_n = 40:10:160;
    [x_nn,y_nn] = meshgrid(x_n,y_n);
    z_nn = Data (x_nn,y_nn);
    hold off;
    imagesc([min_x max_x], [min_y max_y], flipud(img));
    hold on;
    contourf(x_nn,y_nn,z_nn,50); % plot counter plot

    %set(h,'EdgeColor','none');
    % grid on
    set(gca,'ydir','normal'); % restore normal axis after loading background

    % Settings for labes, colorbar, axis, title and legend:
    axis([0,600,0,200]) % set axis
    caxis([0, 10])
    set(gca,'color','w','FontWeight','bold','FontSize',14,'FontName','Arial');
    % Create xlabel
    xlabel('x coodrinate, mm','FontWeight','bold','FontSize',12,...)
    % Create ylabel
    ylabel('y coordinate, mm','FontWeight','bold','FontSize',12,...)
    % Create colorbar
    colorbar('FontWeight','bold','FontSize',14,'FontName','Arial');
    % Create title
    title('Pressure map','FontWeight','bold','FontSize',14,'FontName','Arial');
    legend(sprintf(pvinj ,PV_1(i)), 'Location','SouthEast');
    legend('boxoff');

    frame = getframe(fig1,winsize); %get window size
    writeVideo(writerObj,frame); %write figure in avi-file
    %saveas(fig1,sprintf(image,i),'fig') %save a matlab-fig file

```

```
set(gcf,'PaperPositionMode','auto') % freeze configuration for image, to save image ↵
as it is shown on the screen
print(fig1,'-dpng',sprintf(image,i))
end
close(writerObj);

% References:
% 1. Videowriter
% http://www.mathworks.com/help/matlab/ref/videowriter-class.html
% 2. Creating movies in MATLAB
% http://www.math.canterbury.ac.nz/~c.scarrott/MATLAB\_Movies/movies.html
% 3. Background image
% http://www.peteryu.ca/tutorials/matlab/plot\_over\_image\_background
% 4. Save image as png-file
% http://www.mathworks.com/help/matlab/ref/print.html?searchHighlight=print
```



```

% Detected commas in non-thousand locations.
invalidThousandsSeparator = false;
if any(numbers==',');
    thousandsRegExp = '^\\d+?(\\,\\d{3})*\\.\\{0,1}\\d*\\$';
    if isempty(regexp(thousandsRegExp, ',', 'once'));
        numbers = NaN;
        invalidThousandsSeparator = true;
    end
end
% Convert numeric strings to numbers.
if ~invalidThousandsSeparator;
    numbers = textscan(strrep(numbers, ',', ''), '%f');
    numericData(row, col) = numbers{1};
    raw{row, col} = numbers{1};
end
catch me
end
end

%% Replace non-numeric cells with NaN
R = cellfun(@(x) ~isnumeric(x) && ~islogical(x), raw); % Find non-numeric cells
raw(R) = {NaN}; % Replace non-numeric cells

%% Allocate imported array to column variable names
Timeinmin = cell2mat(raw(:, 1));
PoreVolumePV = cell2mat(raw(:, 2));
Pressureinlet = cell2mat(raw(:, 3));
EMULSIONIN = cell2mat(raw(:, 4));
CP11 = cell2mat(raw(:, 5));
CP12 = cell2mat(raw(:, 6));
CP13 = cell2mat(raw(:, 7));
CP14 = cell2mat(raw(:, 8));
CP15 = cell2mat(raw(:, 9));
CP21 = cell2mat(raw(:, 10));
CP22 = cell2mat(raw(:, 11));
CP23 = cell2mat(raw(:, 12));
CP24 = cell2mat(raw(:, 13));
CP25 = cell2mat(raw(:, 14));
CP31 = cell2mat(raw(:, 15));
CP32 = cell2mat(raw(:, 16));
CP33 = cell2mat(raw(:, 17));
CP34 = cell2mat(raw(:, 18));
CP35 = cell2mat(raw(:, 19));

%% Clear temporary variables
clearvars filename delimiter formatSpec fileID dataArray ans raw col numericData rawData
row regexstr result numbers invalidThousandsSeparator thousandsRegExp me R;

```

```
CP11_f = zeros (size(CP11,1),1);
CP12_f = zeros (size(CP12,1),1);
CP13_f = zeros (size(CP13,1),1);
CP14_f = zeros (size(CP14,1),1);
CP15_f = zeros (size(CP15,1),1);
CP21_f = zeros (size(CP21,1),1);
CP22_f = zeros (size(CP22,1),1);
CP23_f = zeros (size(CP23,1),1);
CP24_f = zeros (size(CP24,1),1);
CP25_f = zeros (size(CP25,1),1);
CP31_f = zeros (size(CP31,1),1);
CP32_f = zeros (size(CP32,1),1);
CP33_f = zeros (size(CP33,1),1);
CP34_f = zeros (size(CP34,1),1);
CP35_f = zeros (size(CP35,1),1);

CP11_f(:) = - CP11(:);
CP12_f(:) = - CP12(:);
CP13_f(:) = - CP13(:);
CP14_f(:) = - CP14(:);
CP15_f(:) = - CP15(:);
CP21_f(:) = - CP21(:);
CP22_f(:) = - CP22(:);
CP23_f(:) = - CP23(:);
CP24_f(:) = - CP24(:);
CP25_f(:) = - CP25(:);
CP31_f(:) = - CP31(:);
CP32_f(:) = - CP32(:);
CP33_f(:) = - CP33(:);
CP34_f(:) = - CP34(:);
CP35_f(:) = - CP35(:);

clearvars CP11 CP12 CP13 CP14 CP15 CP21 CP22 CP23 CP24 CP25 CP31 CP32 CP33 CP34 CP35;

% load data from image analysis
load('PVandTime_from_images.mat');

% temp time for double check
temp_time = zeros (size(t_r2,2),1);

%% set coordinates for surface plot
x_crd = zeros (10,1);
x_crd(1) = 50;
x_crd(2) = 175;
x_crd(3) = 300;
%x_crd(4) = 425;
%x_crd(5) = 550;

%x_crd(6) = 50;
x_crd(4) = 175;
x_crd(5) = 300;
```

```
%x_crd(9) = 425;
x_crd(6) = 550;

x_crd(7) = 50;
x_crd(8) = 175;
x_crd(9) = 300;
x_crd(10) = 425;
%x_crd(15) = 550;

y_crd = zeros (10,1);
y_crd(1) = 160;
y_crd(2) = 160;
y_crd(3) = 160;
%y_crd(4) = 160;
%y_crd(5) = 160;

%y_crd(6) = 100;
y_crd(4) = 100;
y_crd(5) = 100;
%y_crd(9) = 100;
y_crd(6) = 100;

y_crd(7) = 40;
y_crd(8) = 40;
y_crd(9) = 40;
y_crd(10) = 40;
%y_crd(15) = 40;

CP = zeros (10,size(t_r2,2));
%%
step_image = 2;
for step = 1 : size (Timeinmin,1)
    if (Timeinmin(step) >= t_r2(step_image))
        % save current time for further reference
        temp_time (step_image) = Timeinmin(step,1);

        %Set new step for pressure data
        step_p_min = step - 10;
        step_p_max = step + 10;

        %Trim new data for plotting +/- 10 steps from given point
        %1st row
        CP11_f_temp = CP11_f (step_p_min:step_p_max);
        CP (1,step_image) = mean2(CP11_f_temp);
        CP12_f_temp = CP12_f (step_p_min:step_p_max);
        CP (2,step_image) = mean2(CP12_f_temp);
        CP13_f_temp = CP13_f (step_p_min:step_p_max);
        CP (3,step_image) = mean2(CP13_f_temp);
        %CP14_f_temp = CP14_f (step_p_min:step_p_max);
        %CP (4,step_image) = mean2(CP14_f_temp);
        %CP15_f_temp = CP15_f (step_p_min:step_p_max);
```

```
%CP (5,step_image) = mean2(CP15_f_temp);

%2nd row
%CP21_f_temp = CP21_f (step_p_min:step_p_max);
%CP (6,step_image) = mean2(CP21_f_temp);
CP22_f_temp = CP22_f (step_p_min:step_p_max);
CP (4,step_image) = mean2(CP22_f_temp);
CP23_f_temp = CP23_f (step_p_min:step_p_max);
CP (5,step_image) = mean2(CP23_f_temp);
%CP24_f_temp = CP24_f (step_p_min:step_p_max);
%CP (9,step_image) = mean2(CP24_f_temp);
CP25_f_temp = CP25_f (step_p_min:step_p_max);
CP (6,step_image) = mean2(CP25_f_temp);

%3rd row
CP31_f_temp = CP31_f (step_p_min:step_p_max);
CP (7,step_image) = mean2(CP31_f_temp);
CP32_f_temp = CP32_f (step_p_min:step_p_max);
CP (8,step_image) = mean2(CP32_f_temp);
CP33_f_temp = CP33_f (step_p_min:step_p_max);
CP (9,step_image) = mean2(CP33_f_temp);
CP34_f_temp = CP34_f (step_p_min:step_p_max);
CP (10,step_image) = mean2(CP34_f_temp);
%CP35_f_temp = CP35_f (step_p_min:step_p_max);
%CP (15,step_image) = mean2(CP35_f_temp);

% next point for time-data
step_image = step_image + 1;
if (step_image > size(t_r2,2))
    break;
end
end

% Load background image
img = imread('run2background.png');
min_x = 0;
max_x = 600;
min_y = 0;
max_y = 200;

fig1 = figure('Position',[500 100 1200 350], 'Color',[1 1 1]); %500 left coord. 100 bottom
%coord. 1200 width 400 height
winsize = get(fig1,'Position'); %set position, dimension of figure for future reference.
winsize(1:2) = [0 0]; %adjust windows size for recording
numframes=size(CP,2); %determines number of frames
set(fig1,'nextplot','replacechildren');
set(gcf,'Renderer','zbuffer');

image = 'Run2/Run2_%03d'; %set name for saving .png-files
pvinj = 'Emulsion inj. = %1.4f PV'; %set name for legends
```

```
writerObj = VideoWriter('run2.avi'); %prepares .avi-file for saving frames
open(writerObj); %opens .avi-file for saving

for i=1:numframes
    % Get current data for plot
    z_p=CP(:,i);
    Data = scatteredInterpolant(x_crd,y_crd,z_p); %converts data for suitable format
    x_n = 50:10:550;
    y_n = 40:10:160;
    [x_nn,y_nn] = meshgrid(x_n,y_n);
    z_nn = Data (x_nn,y_nn);
    % hold off;
    % imagesc([min_x max_x], [min_y max_y], flipud(img));
    % hold on;
    contourf(x_nn,y_nn,z_nn,50); % plot counter plot

    %set(h,'EdgeColor','none');
    % grid on
    % set(gca,'ydir','normal'); % restore normal axis after loading background

    % Settings for labes, colorbar, axis, title and legend:
    axis([0,600,0,200]) % set axis
    caxis([0, 65])
    set(gca, 'color', 'w', 'FontWeight', 'bold', 'FontSize', 14, 'FontName', 'Arial');
    % Create xlabel
    xlabel('x coordinate, mm', 'FontWeight', 'bold', 'FontSize', 12, ...
    'FontName', 'Arial');
    % Create ylabel
    ylabel('y coordinate, mm', 'FontWeight', 'bold', 'FontSize', 12, ...
    'FontName', 'Arial');
    % Create colorbar
    colorbar('FontWeight', 'bold', 'FontSize', 14, 'FontName', 'Arial');
    % Create title
    title('Pressure map', 'FontWeight', 'bold', 'FontSize', 14, 'FontName', 'Arial');
    legend(sprintf(pvinj ,PV_2(i)), 'Location', 'SouthEast');
    legend('boxoff');

    frame = getframe(fig1,winsize); %get window size
    writeVideo(writerObj,frame); %write figure in avi-file
    %saveas(fig1,sprintf(image,i),'fig') %save a matlab-fig file
    set(gcf, 'PaperPositionMode', 'auto') % freeze configuration for image, to save image as it is shown on the screen
    print(fig1, '-dpng', sprintf(image,i))
end
close(writerObj);

figure
plot(Timeinmin,CP15_f)

% References:
```

```
% 1. Videowriter
% http://www.mathworks.com/help/matlab/ref/videowriter-class.html
% 2. Creating movies in MATLAB
% http://www.math.canterbury.ac.nz/~c.scarrott/MATLAB_Movies/movies.html
% 3. Background image
% http://www.peteryu.ca/tutorials/matlab/plot_over_image_background
% 4. Save image as png-file
% http://www.mathworks.com/help/matlab/ref/print.html?searchHighlight=print
```



```

try
    result = regexp(rawData{row}, regexstr, 'names');
    numbers = result.numbers;

    % Detected commas in non-thousand locations.
    invalidThousandsSeparator = false;
    if any(numbers==',');
        thousandsRegExp = '^\d+?(\,\d{3})*\.\{0,1\}\d*$';
        if isempty(regexp(thousandsRegExp, ',', 'once'));
            numbers = NaN;
            invalidThousandsSeparator = true;
        end
    end
    % Convert numeric strings to numbers.
    if ~invalidThousandsSeparator;
        numbers = textscan(strrep(numbers, ',', ''), '%f');
        numericData(row, col) = numbers{1};
        raw{row, col} = numbers{1};
    end
    catch me
    end
end
%% Replace non-numeric cells with NaN
R = cellfun(@(x) ~isnumeric(x) && ~islogical(x), raw); % Find non-numeric cells
raw(R) = {NaN}; % Replace non-numeric cells

%% Allocate imported array to column variable names
Timeinmin = cell2mat(raw(:, 1));
PoreVolumePV = cell2mat(raw(:, 2));
Pressureinlet = cell2mat(raw(:, 3));
EMULSIONIN = cell2mat(raw(:, 4));
CP11 = cell2mat(raw(:, 5));
CP12 = cell2mat(raw(:, 6));
CP13 = cell2mat(raw(:, 7));
CP14 = cell2mat(raw(:, 8));
CP15 = cell2mat(raw(:, 9));
CP21 = cell2mat(raw(:, 10));
CP22 = cell2mat(raw(:, 11));
CP23 = cell2mat(raw(:, 12));
CP24 = cell2mat(raw(:, 13));
CP25 = cell2mat(raw(:, 14));
CP31 = cell2mat(raw(:, 15));
CP32 = cell2mat(raw(:, 16));
CP33 = cell2mat(raw(:, 17));
CP34 = cell2mat(raw(:, 18));
CP35 = cell2mat(raw(:, 19));

```

```
EMULSIONIN (1) = 0;
PoreVolumePV(1) = PoreVolumePV(2);
Pressureinlet(1) = Pressureinlet(2);
Timeinmin (1) = 0;

%% Clear temporary variables
clearvars filename delimiter formatSpec fileID dataArray ans raw col numericData rawData ↵
row regexstr result numbers invalidThousandsSeparator thousandsRegExp me R;

CP11_f = zeros (size(CP11,1),1);
CP12_f = zeros (size(CP12,1),1);
CP13_f = zeros (size(CP13,1),1);
CP14_f = zeros (size(CP14,1),1);
CP15_f = zeros (size(CP15,1),1);
CP21_f = zeros (size(CP21,1),1);
CP22_f = zeros (size(CP22,1),1);
CP23_f = zeros (size(CP23,1),1);
CP24_f = zeros (size(CP24,1),1);
CP25_f = zeros (size(CP25,1),1);
CP31_f = zeros (size(CP31,1),1);
CP32_f = zeros (size(CP32,1),1);
CP33_f = zeros (size(CP33,1),1);
CP34_f = zeros (size(CP34,1),1);
CP35_f = zeros (size(CP35,1),1);

CP11_f(:) = - CP11(:);
CP12_f(:) = - CP12(:);
CP13_f(:) = - CP13(:);
CP14_f(:) = - CP14(:);
CP15_f(:) = - CP15(:);
CP21_f(:) = - CP21(:);
CP22_f(:) = - CP22(:);
CP23_f(:) = - CP23(:);
CP24_f(:) = - CP24(:);
CP25_f(:) = - CP25(:);
CP31_f(:) = - CP31(:);
CP32_f(:) = - CP32(:);
CP33_f(:) = - CP33(:);
CP34_f(:) = - CP34(:);
CP35_f(:) = - CP35(:);

clearvars CP11 CP12 CP13 CP14 CP15 CP21 CP22 CP23 CP24 CP25 CP31 CP32 CP33 CP34 CP35;

% load data from image analysis
load('PVandTime_from_images.mat');

clearvars PV_1 PV_2 t_r1 t_r2;

% temp time for double check
temp_time = zeros (size(t_r3,2),1);
```

```
%% set coordinates for surface plot
x_crd = zeros (10,1); %set to 10, since 5 pressure ports are out
x_crd(1) = 50;
x_crd(2) = 175;
x_crd(3) = 300;
%x_crd(3) = 425;
x_crd(4) = 550;

x_crd(5) = 50;
%x_crd(5) = 175;
%x_crd(8) = 300;
x_crd(6) = 425;
%x_crd(6) = 550;

%x_crd(7) = 50;
x_crd(7) = 175;
x_crd(8) = 300;
x_crd(9) = 425;
x_crd(10) = 550;

y_crd = zeros (10,1);
y_crd(1) = 160;
y_crd(2) = 160;
y_crd(3) = 160;
%y_crd(3) = 160;
y_crd(4) = 160;

y_crd(5) = 100;
%y_crd(5) = 100;
%y_crd(8) = 100;
y_crd(6) = 100;
%y_crd(6) = 100;

%y_crd(7) = 40;
y_crd(7) = 40;
y_crd(8) = 40;
y_crd(9) = 40;
y_crd(10) = 40;

CP = zeros (10,size(t_r3,2));
%%
step_image = 2;
for step = 1 : size (Timeinmin,1)
    if (Timeinmin(step) >= t_r3(step_image))
        % save current time for further reference
        temp_time (step_image) = Timeinmin(step,1);

        %Set new step for pressure data
        step_p_min = step - 10;
        step_p_max = step + 10;
```

```

%Trim new data for plotting +/- 10 steps from given point
%1st row
CP11_f_temp = CP11_f (step_p_min:step_p_max);
CP (1,step_image) = mean2(CP11_f_temp);
CP12_f_temp = CP12_f (step_p_min:step_p_max);
CP (2,step_image) = mean2(CP12_f_temp);
CP13_f_temp = CP13_f (step_p_min:step_p_max);
CP (3,step_image) = mean2(CP13_f_temp);
%CP14_f_temp = CP14_f (step_p_min:step_p_max);
%CP (3,step_image) = mean2(CP14_f_temp);
CP15_f_temp = CP15_f (step_p_min:step_p_max);
CP (4,step_image) = mean2(CP15_f_temp);

%2nd row
CP21_f_temp = CP21_f (step_p_min:step_p_max);
CP (5,step_image) = mean2(CP21_f_temp);
%CP22_f_temp = CP22_f (step_p_min:step_p_max);
%CP (5,step_image) = mean2(CP22_f_temp);
%CP23_f_temp = CP23_f (step_p_min:step_p_max);
%CP (8,step_image) = mean2(CP23_f_temp);
CP24_f_temp = CP24_f (step_p_min:step_p_max);
CP (6,step_image) = mean2(CP24_f_temp);
%CP25_f_temp = CP25_f (step_p_min:step_p_max);
%CP (6,step_image) = mean2(CP25_f_temp);

%3rd row
%CP31_f_temp = CP31_f (step_p_min:step_p_max);
%CP (7,step_image) = mean2(CP31_f_temp);
CP32_f_temp = CP32_f (step_p_min:step_p_max);
CP (7,step_image) = mean2(CP32_f_temp);
CP33_f_temp = CP33_f (step_p_min:step_p_max);
CP (8,step_image) = mean2(CP33_f_temp);
CP34_f_temp = CP34_f (step_p_min:step_p_max);
CP (9,step_image) = mean2(CP34_f_temp);
CP35_f_temp = CP35_f (step_p_min:step_p_max);
CP (10,step_image) = mean2(CP35_f_temp);

% next point for time-data
step_image = step_image + 1;
if (step_image > size(t_r3,2))
    break;
end
end

% Load background image
img = imread('run3background.png');
min_x = 0;
max_x = 600;
min_y = 0;
max_y = 200;

```

```

fig1 = figure('Position',[500 100 1200 350], 'Color',[1 1 1]); %500 left coord. 100 bottom coord. 1200 width 400 height
winsize = get(fig1,'Position'); %set position, dimension of figure for future reference.
winsize(1:2) = [0 0]; %adjust windows size for recording
numframes=size(CP,2); %determines number of frames
set(fig1,'nextplot','replacechildren');
set(gcf,'Renderer','zbuffer');

image = 'Run3/Run3_%03d'; %set name for saving .png-files
pvinj = 'Emulsion inj. = %1.4f PV'; %set name for legends

writerObj = VideoWriter('run3.avi'); %prepares .avi-file for saving frames
open(writerObj); %opens .avi-file for saving

for i=1:numframes
    % Get current data for plot
    z_p=CP(:,i);
    Data = scatteredInterpolant(x_crd,y_crd,z_p); %converts data for suitable format
    x_n = 50:10:550;
    y_n = 40:10:160;
    [x_nn,y_nn] = meshgrid(x_n,y_n);
    z_nn = Data (x_nn,y_nn);
    hold off;
    imagesc([min_x max_x], [min_y max_y], flipud(img));
    hold on;
    contourf(x_nn,y_nn,z_nn,50); % plot counter plot

    %set(h,'EdgeColor','none');
    % grid on
    set(gca,'ydir','normal'); % restore normal axis after loading background

    % Settings for labes, colorbar, axis, title and legend:
    axis([0,600,0,200]) % set axis
    caxis([0, 115])
    set(gca,'color','w','FontWeight','bold','FontSize',14,'FontName','Arial');
    % Create xlabel
    xlabel('x coodrinate, mm','FontWeight','bold','FontSize',12,...)
    % Create ylabel
    ylabel('y coordinate, mm','FontWeight','bold','FontSize',12,...)
    % Create colorbar
    colorbar('FontWeight','bold','FontSize',14,'FontName','Arial');
    % Create title
    title('Pressure map','FontWeight','bold','FontSize',14,'FontName','Arial');
    legend(sprintf(pvinj ,PV_3(i)), 'Location','SouthEast');
    legend('boxoff');

    frame = getframe(fig1,winsize); %get window size
    writeVideo(writerObj,frame); %write figure in avi-file
    %saveas(fig1,sprintf(image,i),'fig') %save a matlab-fig file

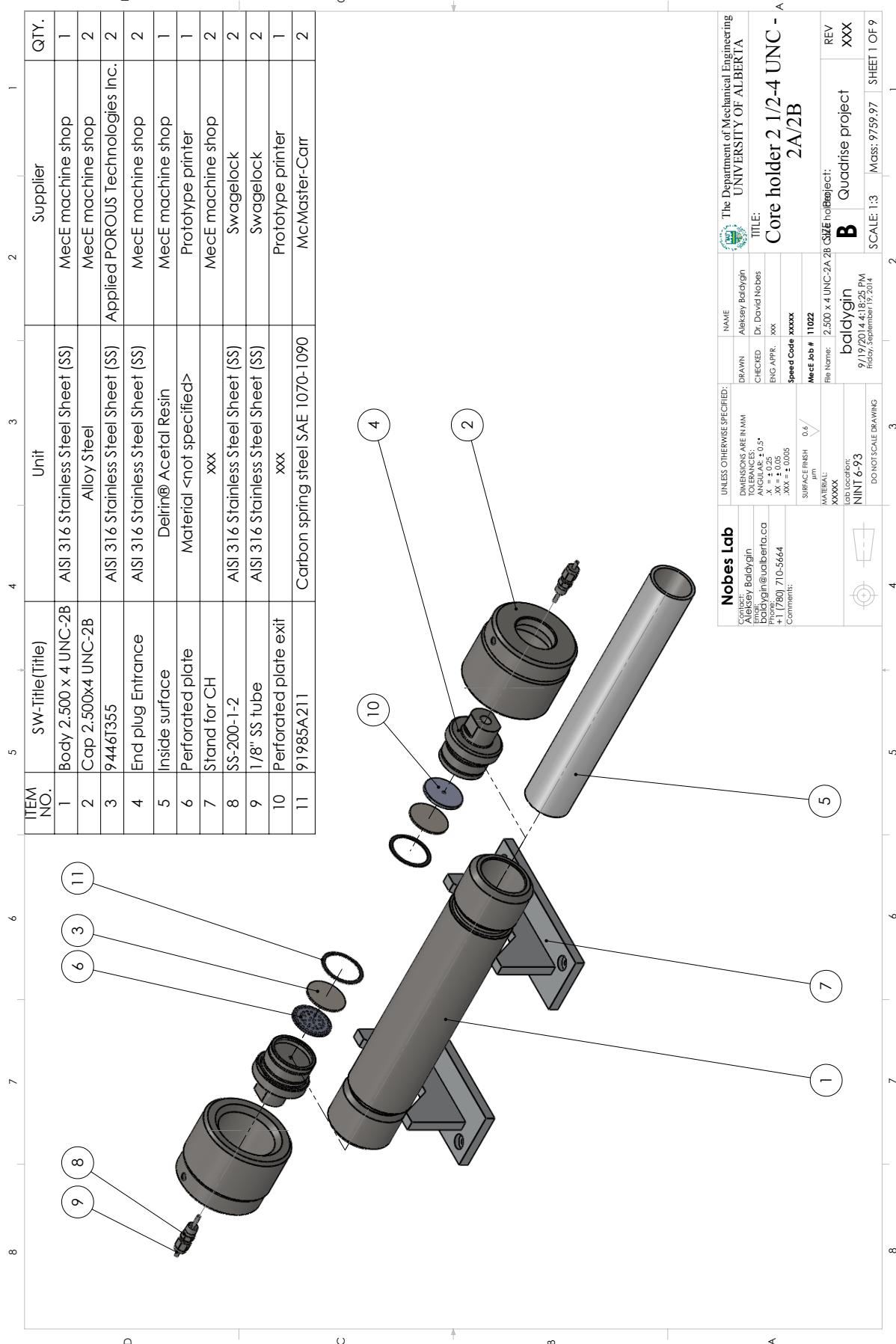
```

```
set(gcf,'PaperPositionMode','auto') % freeze configuration for image, to save image ↵
as it is shown on the screen
print(fig1,'-dpng',sprintf(image,i))
end
close(writerObj);

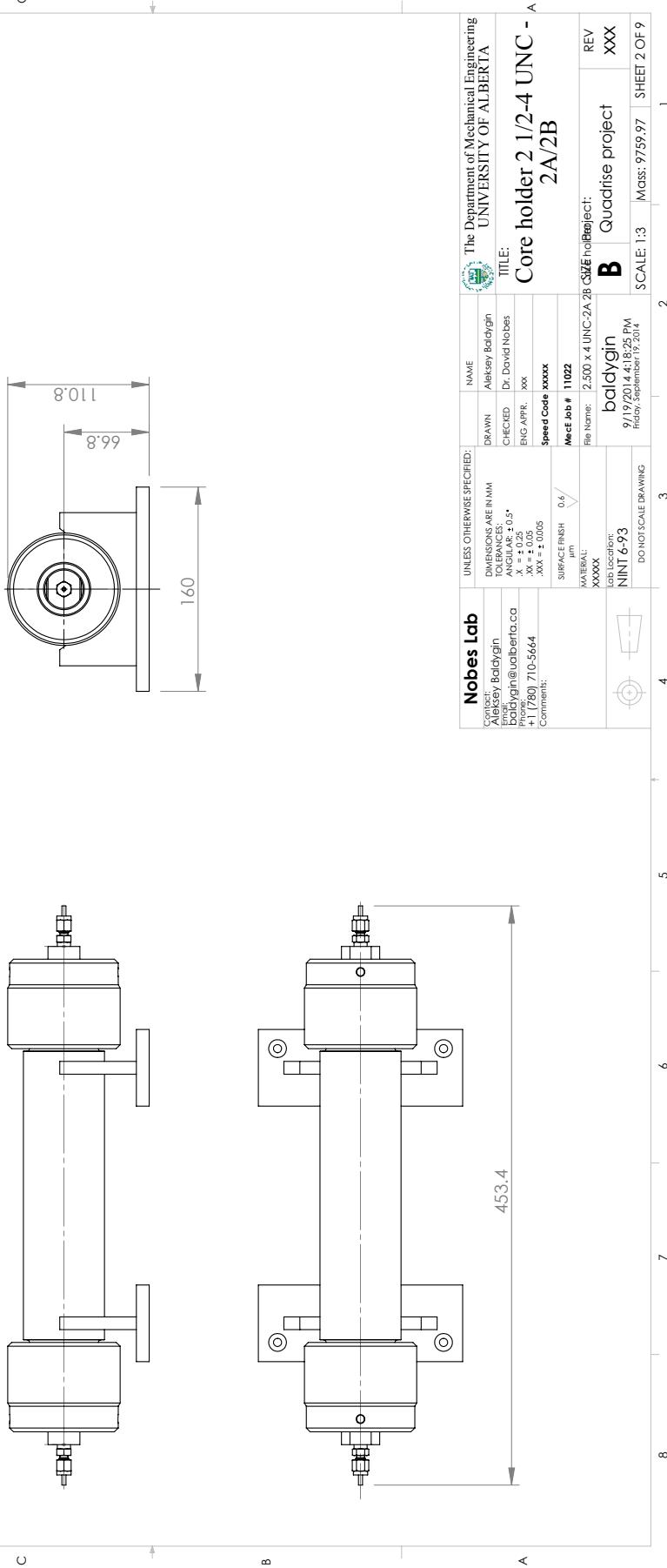
% References:
% 1. Videowriter
% http://www.mathworks.com/help/matlab/ref/videowriter-class.html
% 2. Creating movies in MATLAB
% http://www.math.canterbury.ac.nz/~c.scarrott/MATLAB\_Movies/movies.html
% 3. Background image
% http://www.peteryu.ca/tutorials/matlab/plot\_over\_image\_background
% 4. Save image as png-file
% http://www.mathworks.com/help/matlab/ref/print.html?searchHighlight=print
```

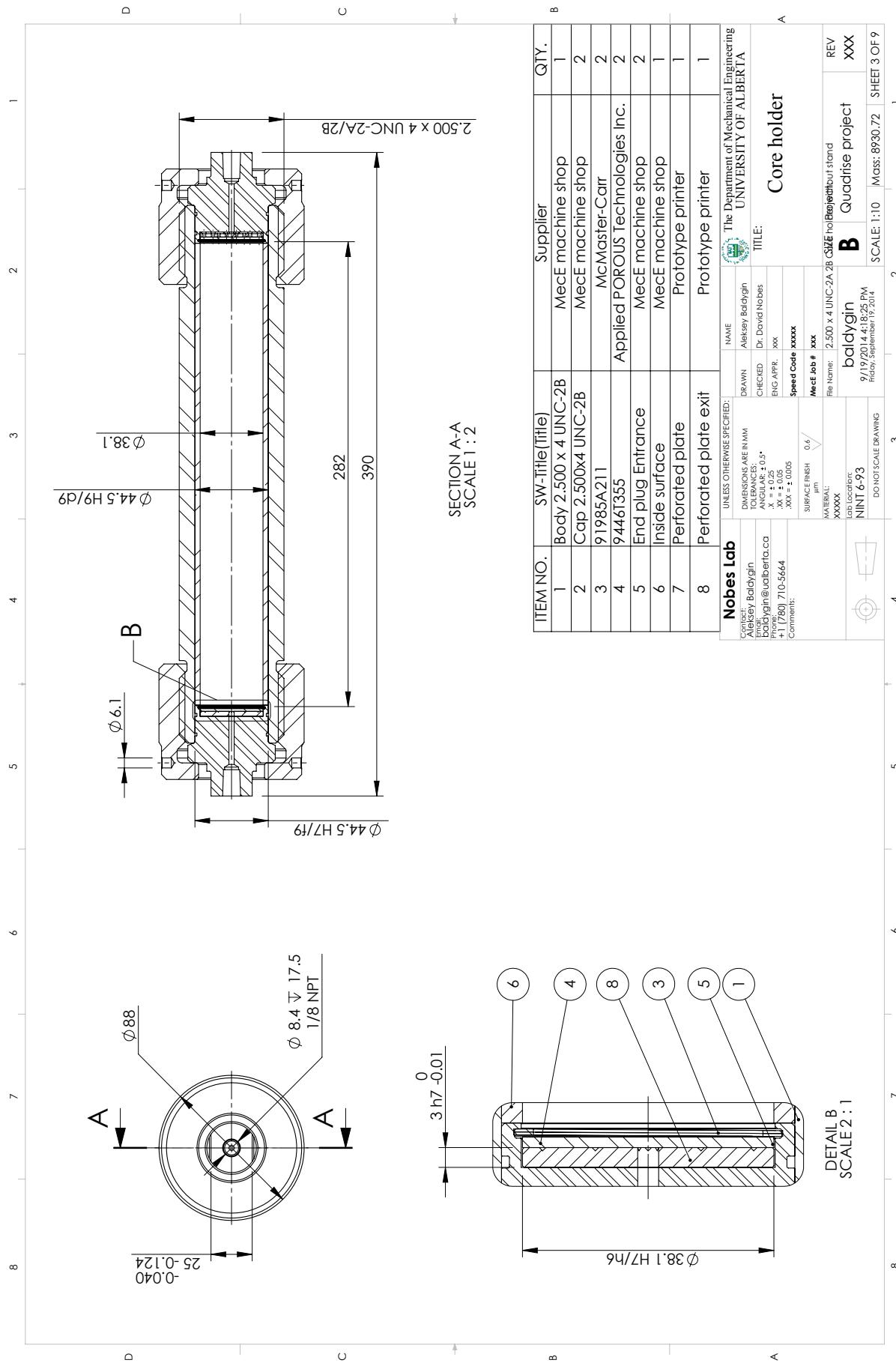
## **A-6 Set of drawings**

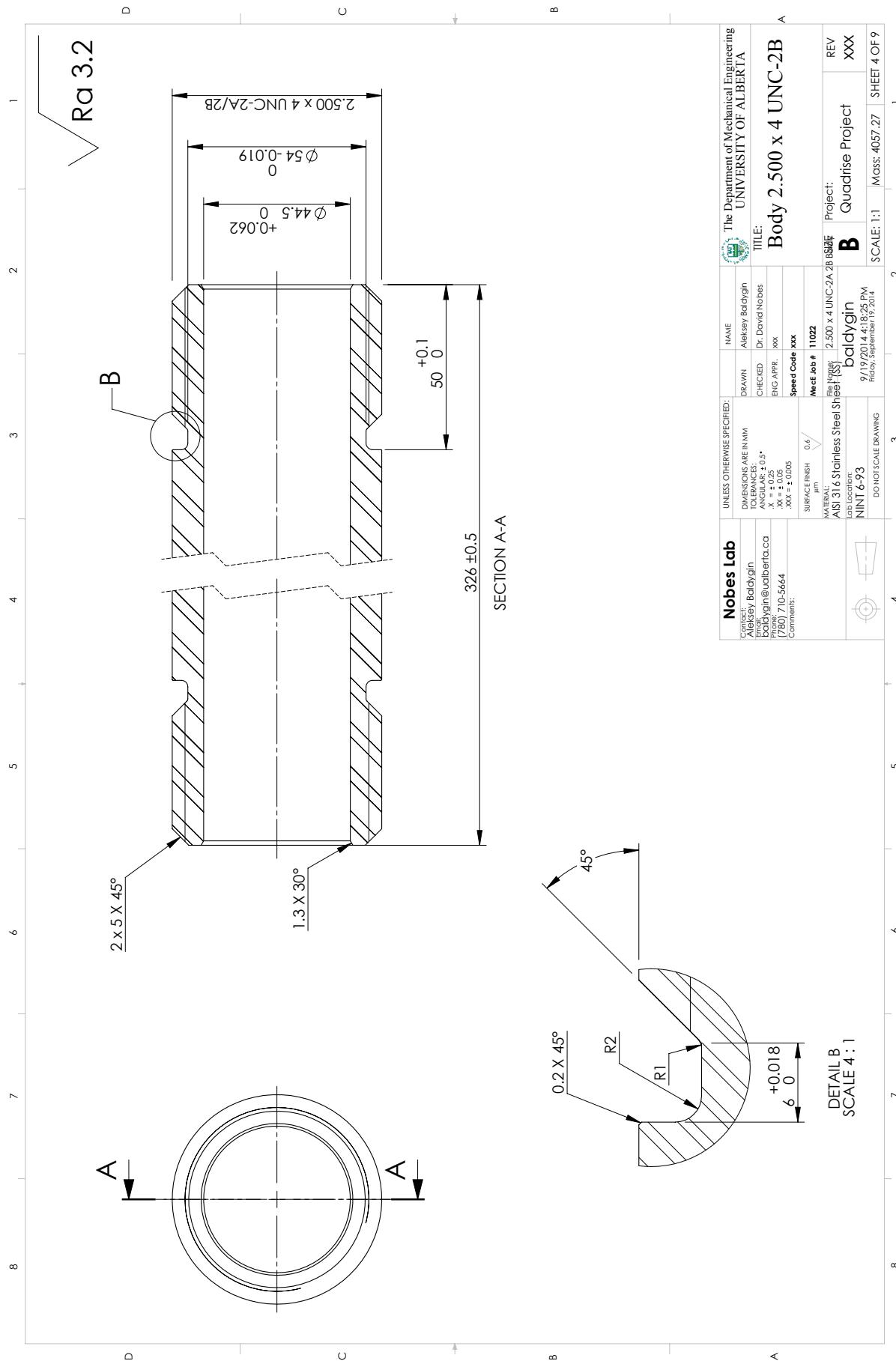
The following set of drawings was prepared using computer-aided design software (CAD) (SolidWorks 2011-2014, Dassault Systèmes SolidWorks Corp.).

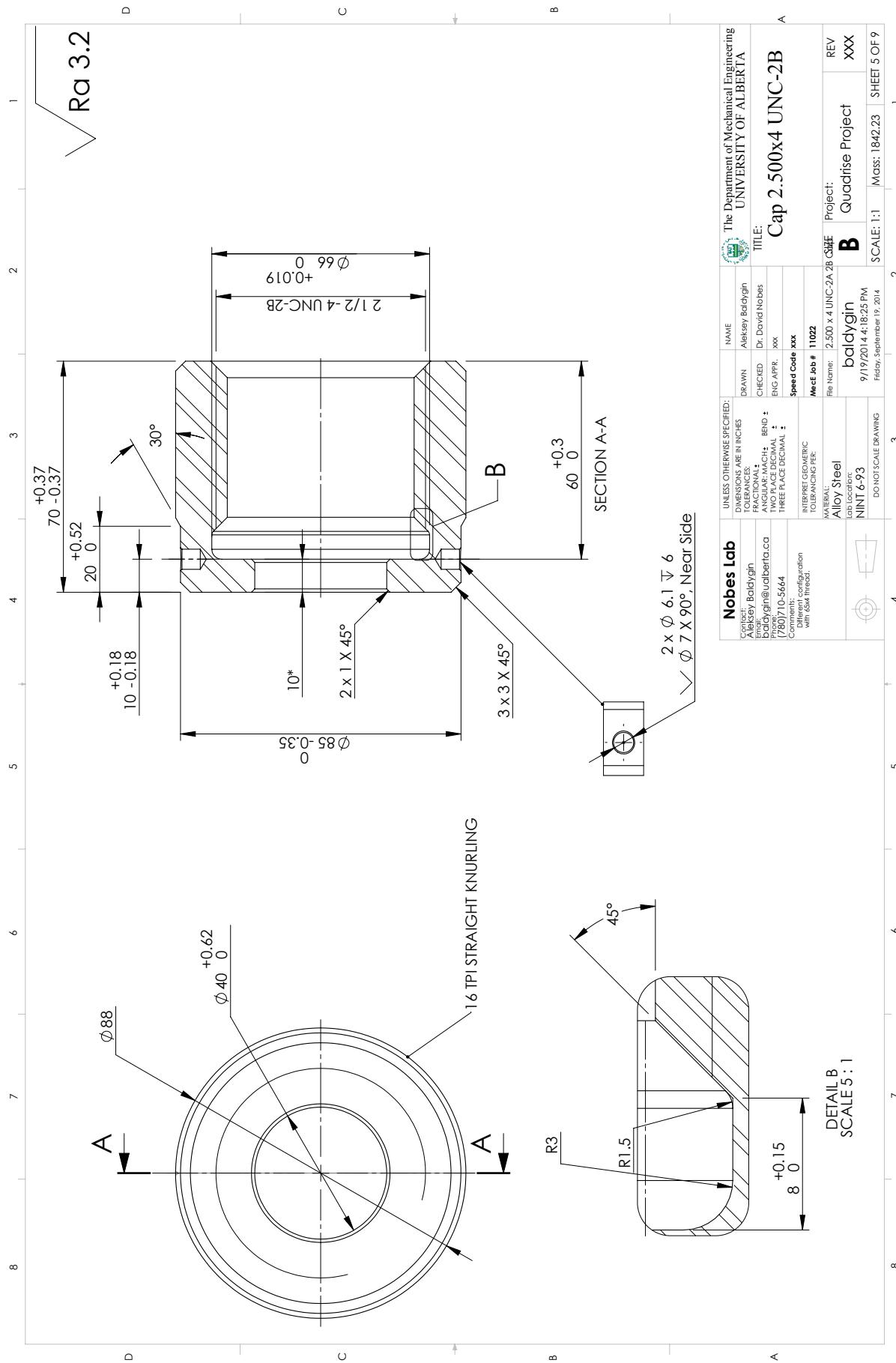


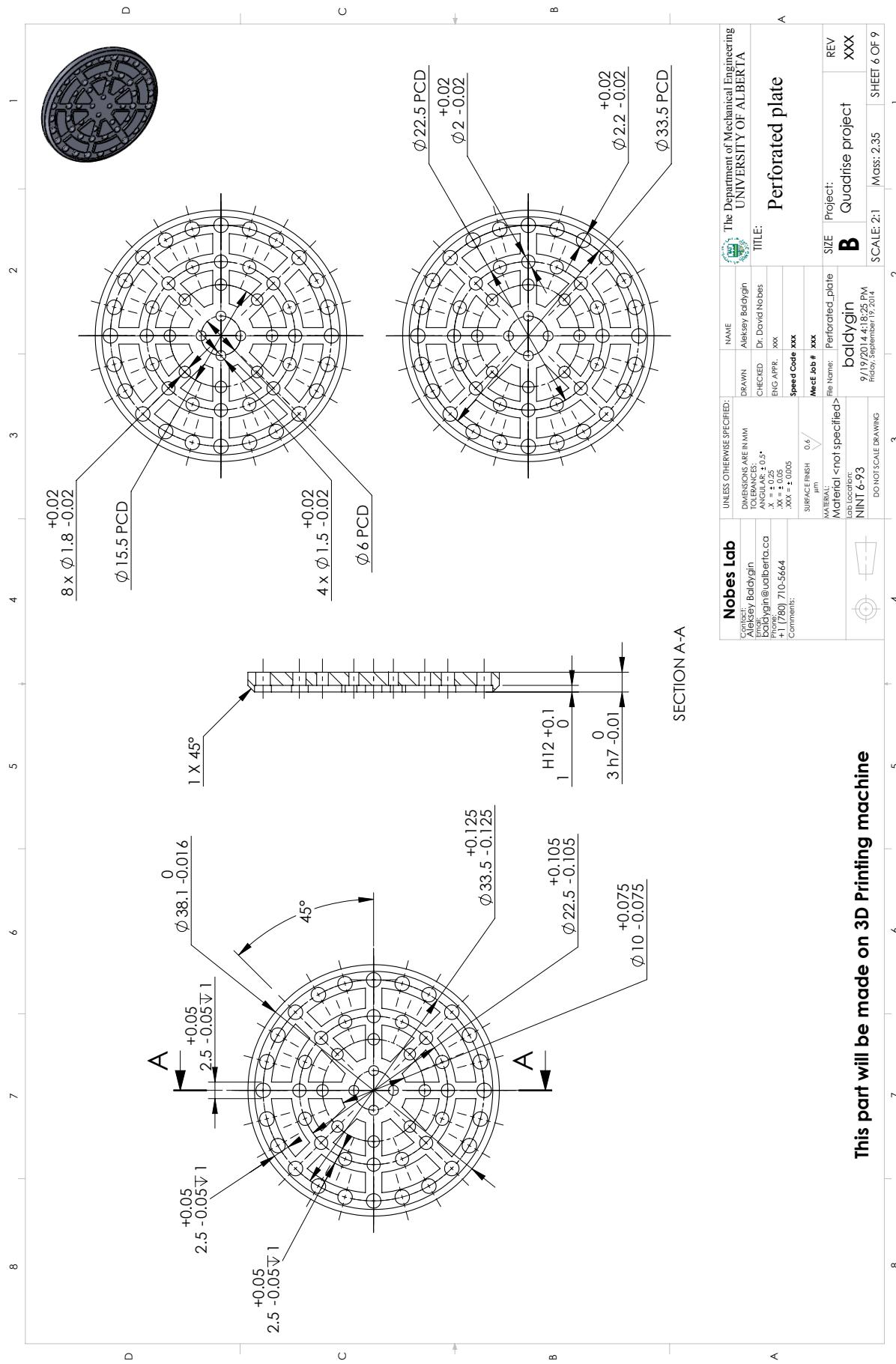
ITEM NO.	SW-Title(title)	Supplier	QTY.
1	91985A211	McMaster-Carr	2
2	94467355	Applied POROUS Technologies Inc.	2
3	End plug Entrance	MecE machine shop	2
4	Inside surface	MecE machine shop	1
5	Perforated plate	Prototype printer	1
6	Stand for CH	MecE machine shop	2
7	SS-200-12	Swagelock	2
8	1/8" SS tube	Swagelock	2
9	Perforated plate exit	Prototype printer	1
10	Body 2.500 x 4 UNC-2B	MecE machine shop	1
11	Cap 2.500x4 UNC-2B	MecE machine shop	2

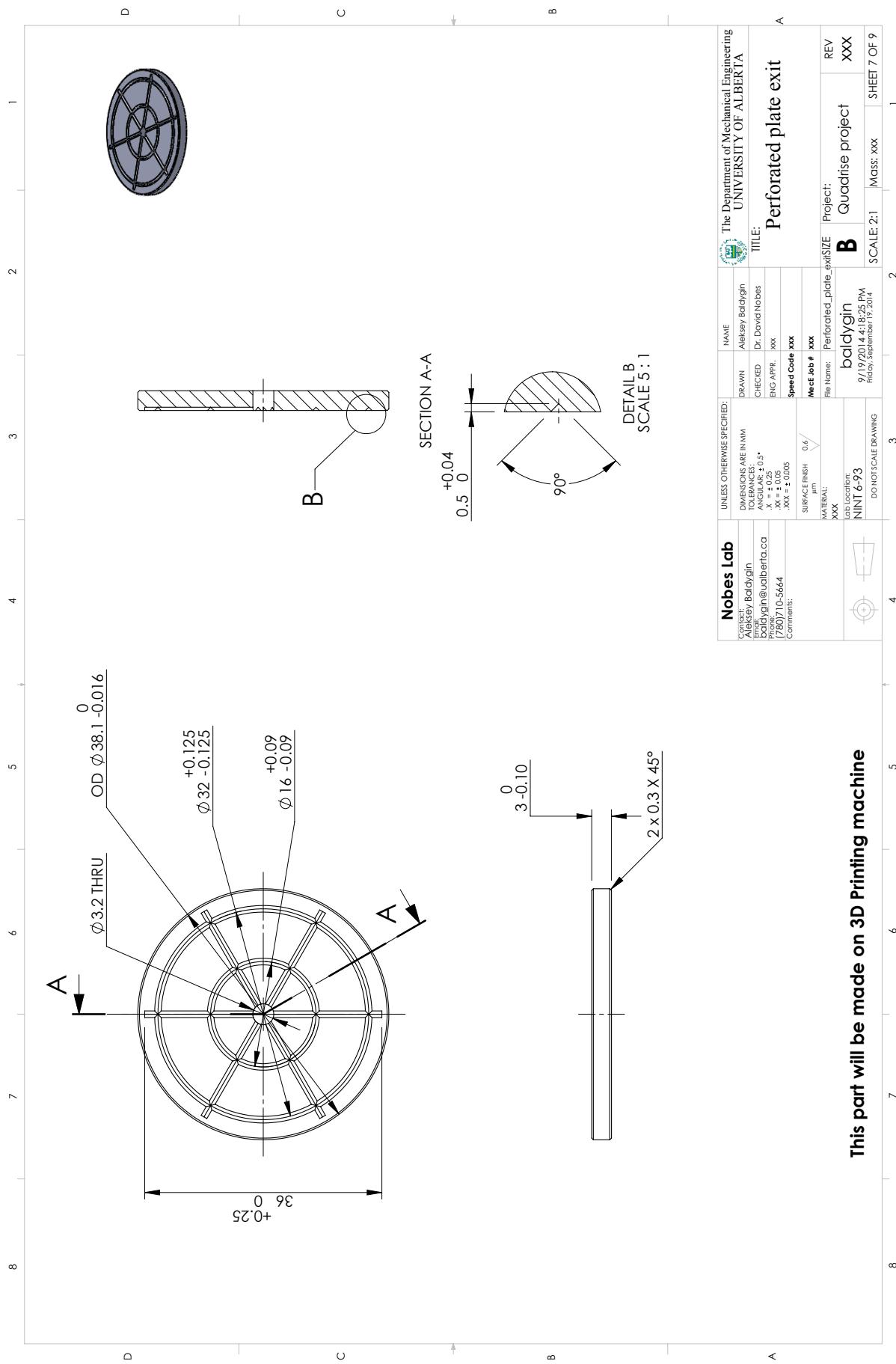




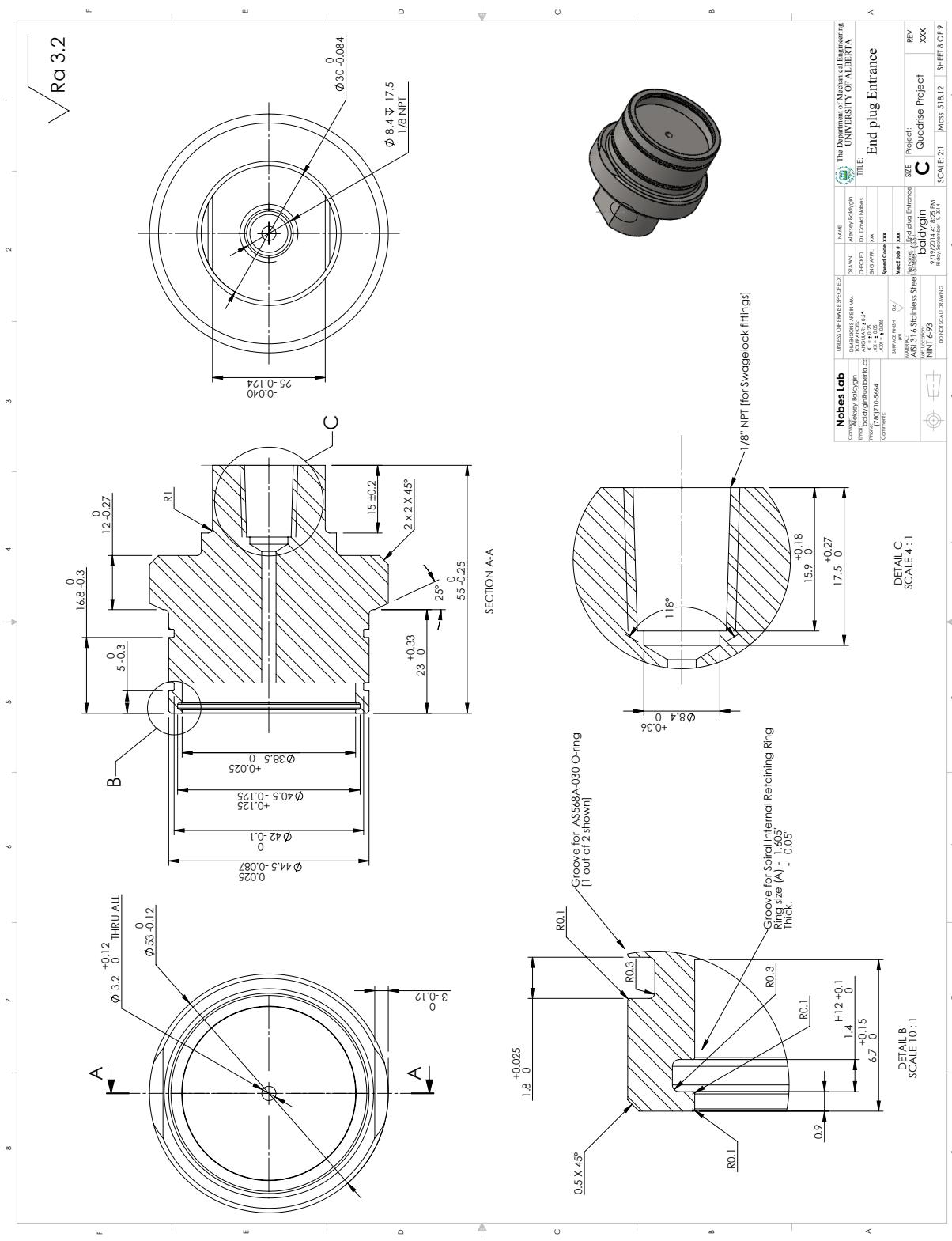


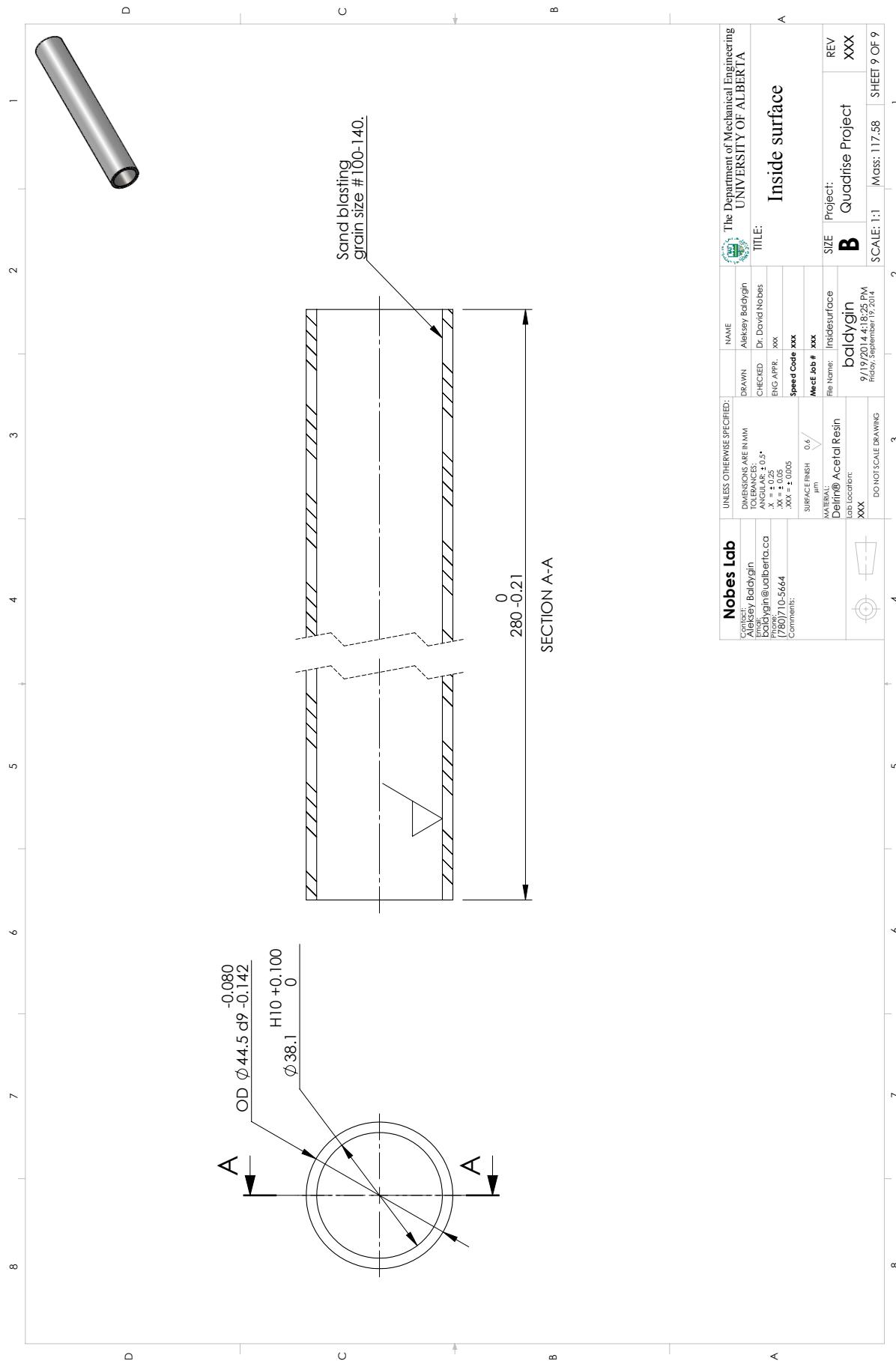


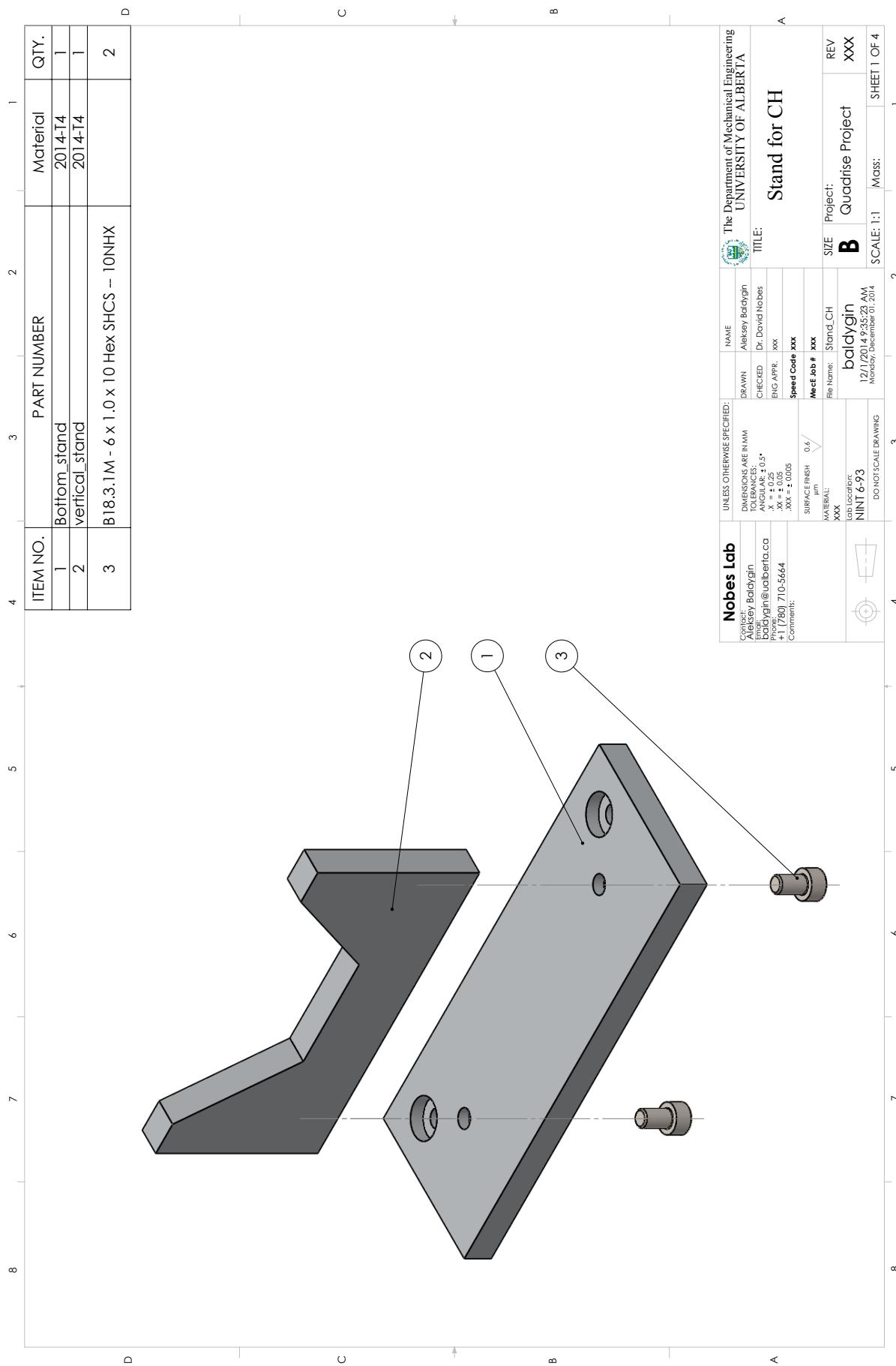


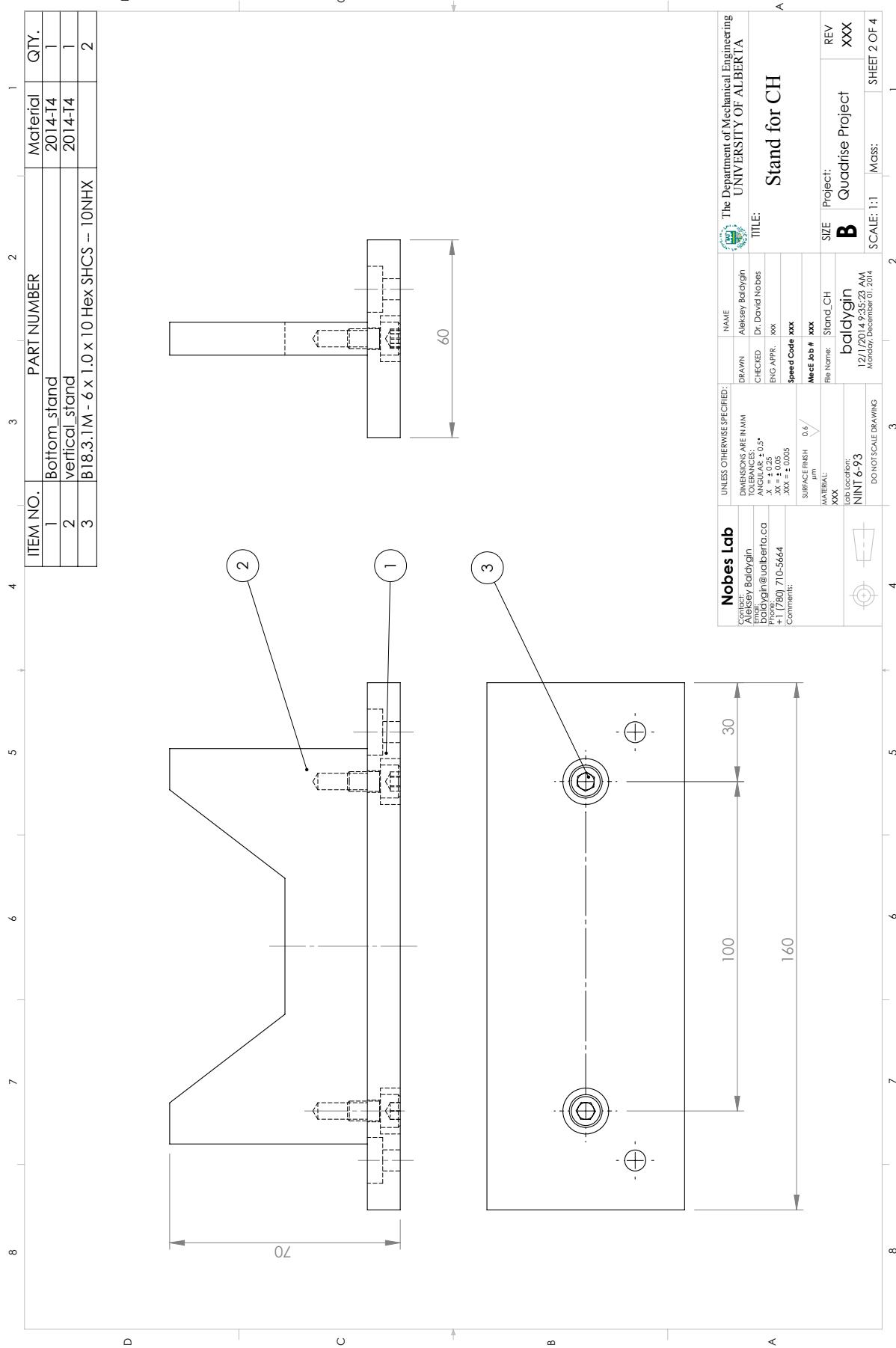


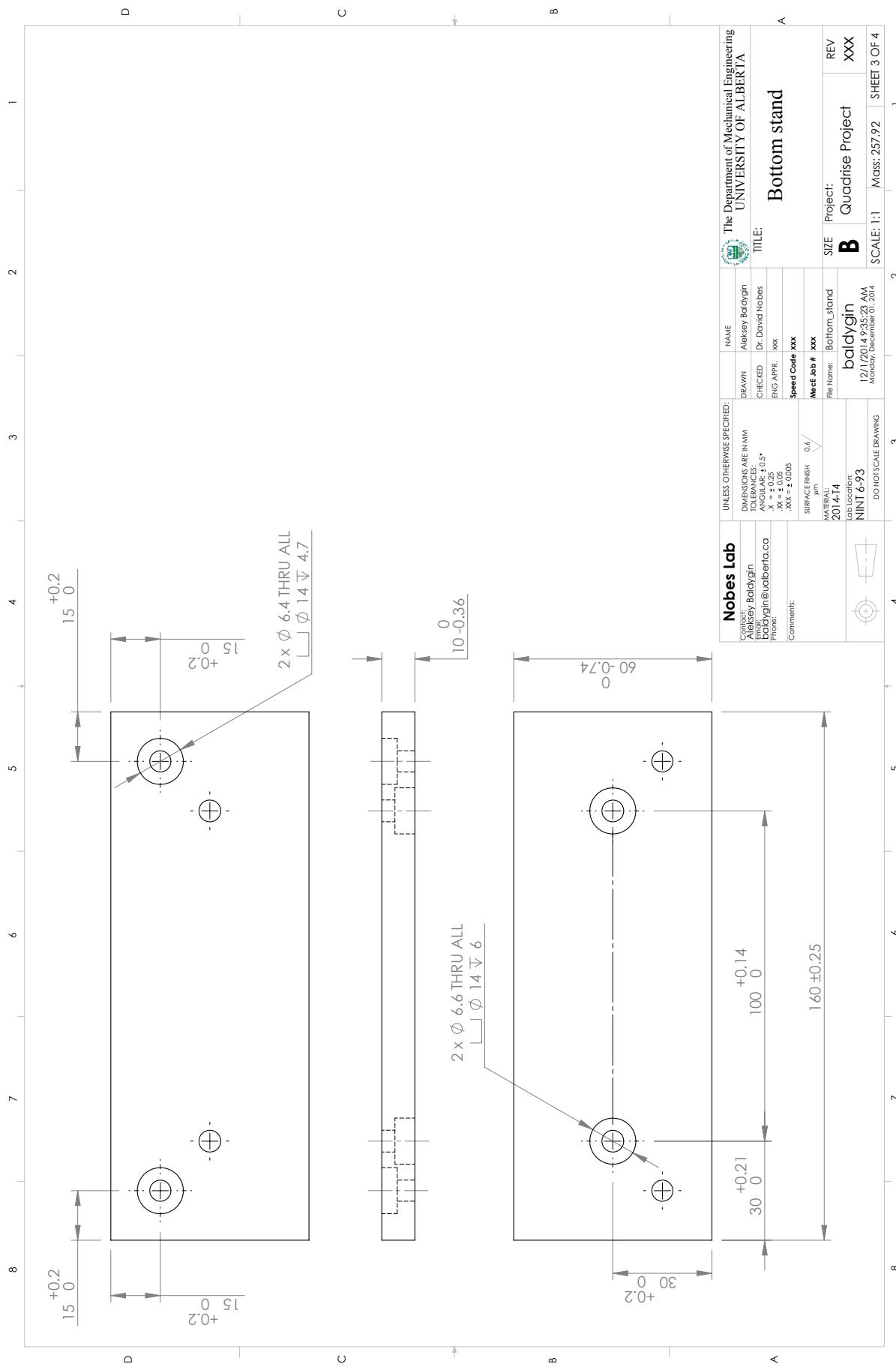
<b>Nobes Lab</b>		UNLESS OTHERWISE SPECIFIED: DIMENSIONS ARE IN MM TOLERANCES: $\pm 0.05$ X = $\pm 0.05$ $XX = 0.005$ $XXX = 0.0005$	NAME: DRAWN: Alexey Baldygin CHECKED: Dr. Dovile Norkus ENG APPR.: XXX Speed Code XXX	FILE: Title: Perforated plate exit
Object:	Alexey Baldygin Email: baldygin@uoberta.ca Phone: 780710-5664 Comments:	SURFACE FINISH: $0.6 \mu\text{m}$	Sheet Code XXX	
Material:	XXX	Matl Job # XXX	File Name: Perforated_plate_exit	Project: Nobes Lab
Lab Location:	NINI & 93	Lab Locat. NINI & 93 NOT TO SCALE DRAWING	REV: B	REV: XXX
9/19/2014 4:18:25 PM Friday, September 19, 2014	SCALE: 2:1	Mass: XXX	DETAIL B	SECTION A-A
		2	3	1
		4	5	6
		7	8	9

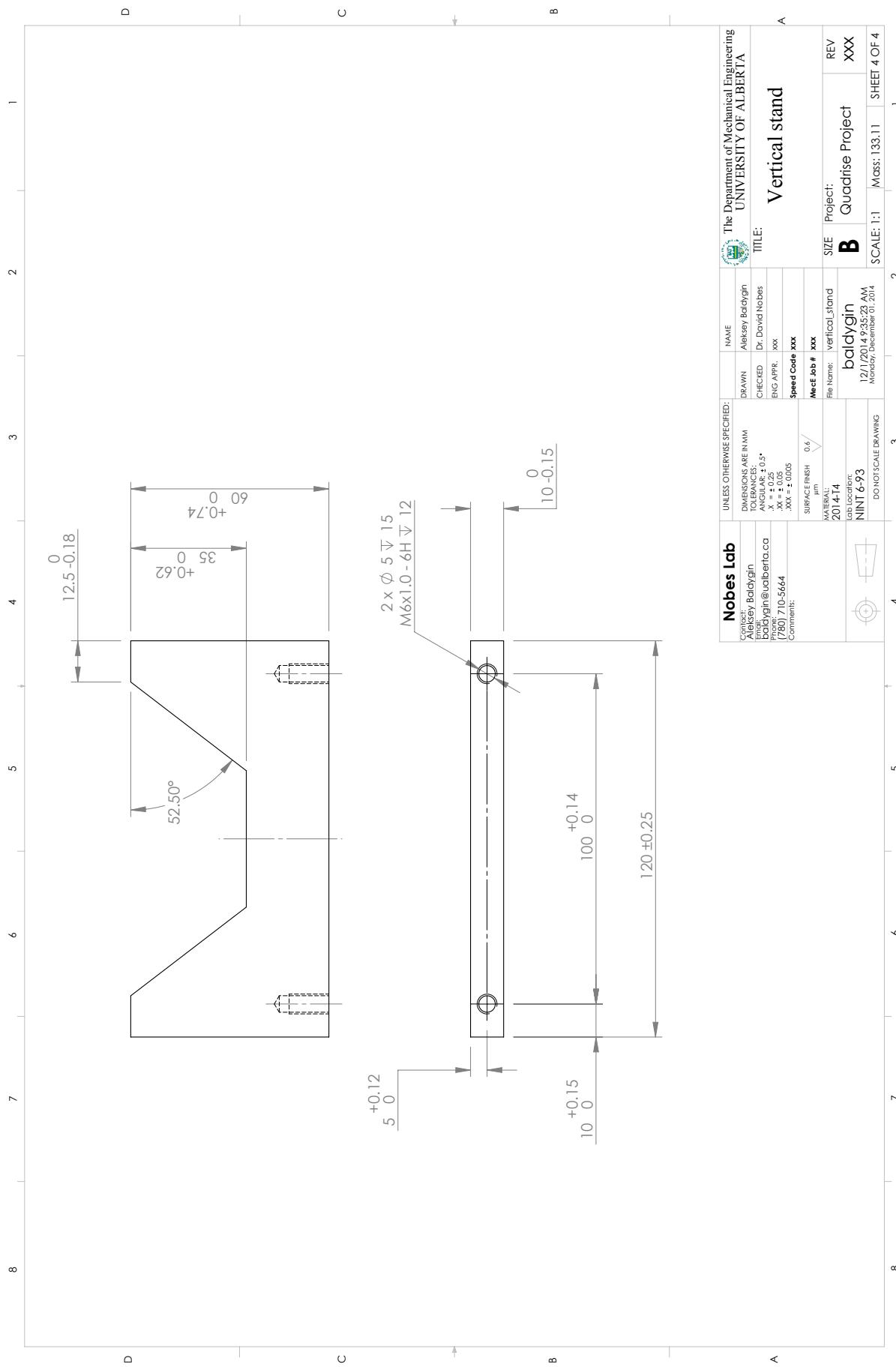




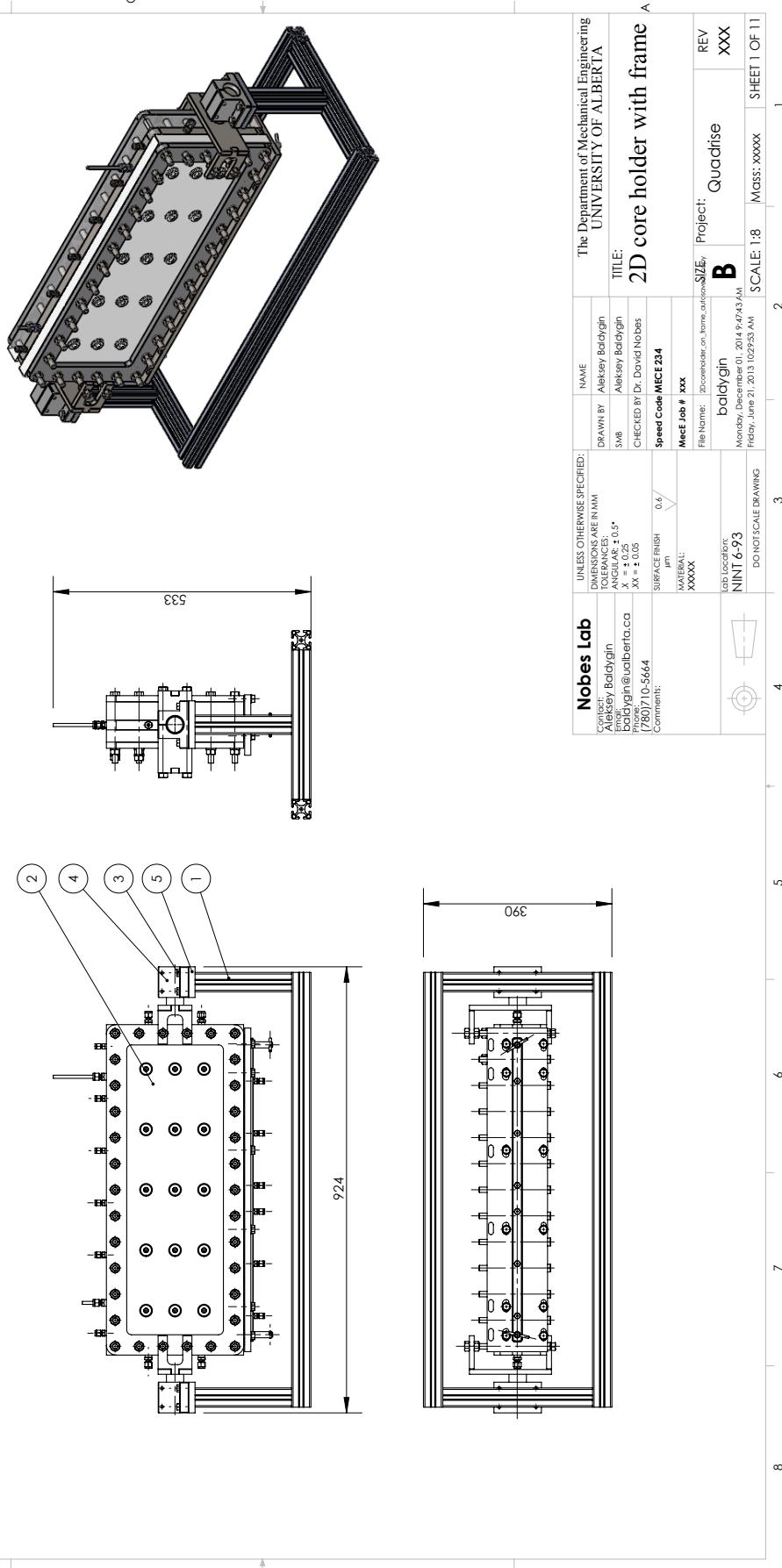


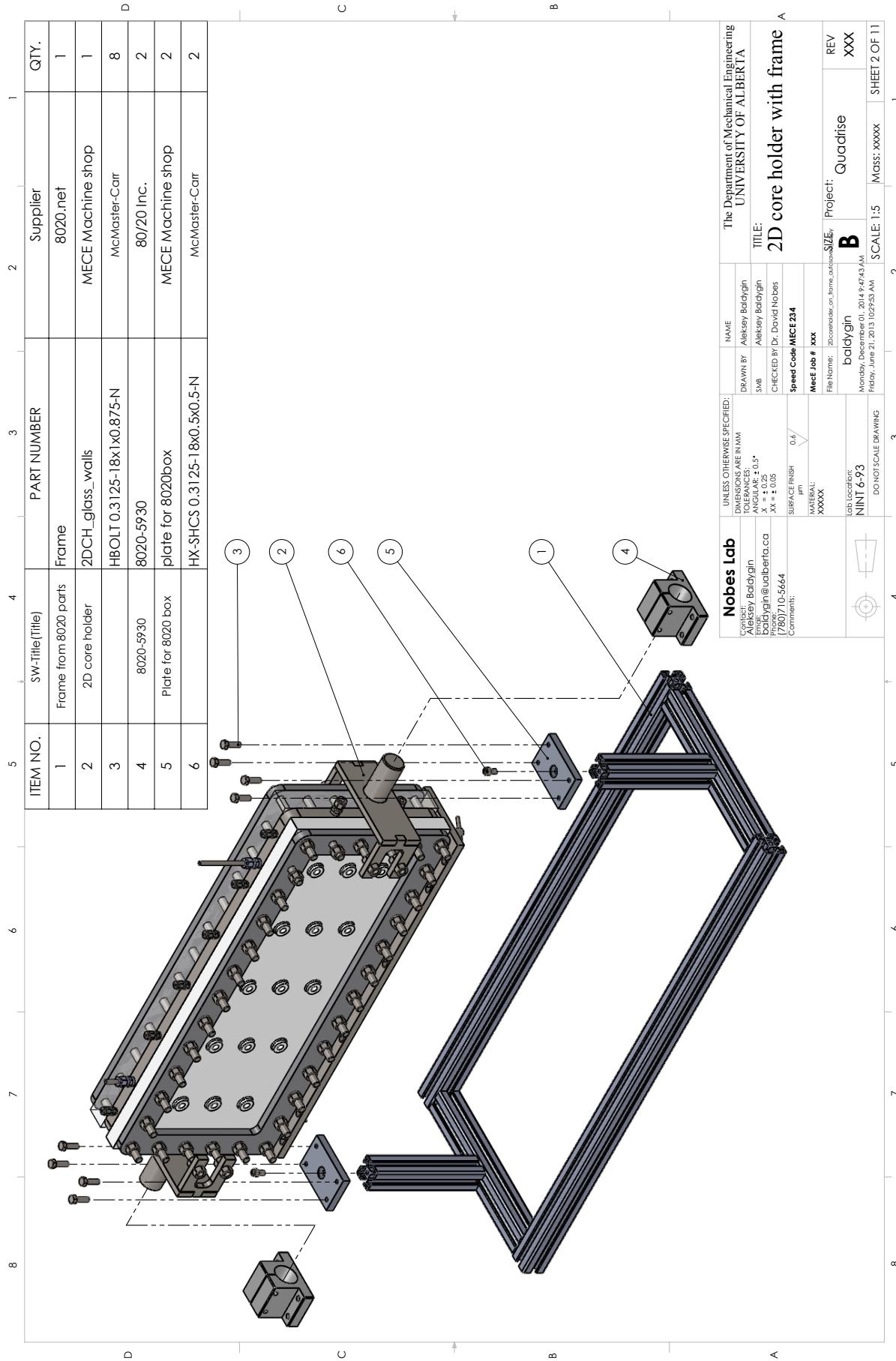


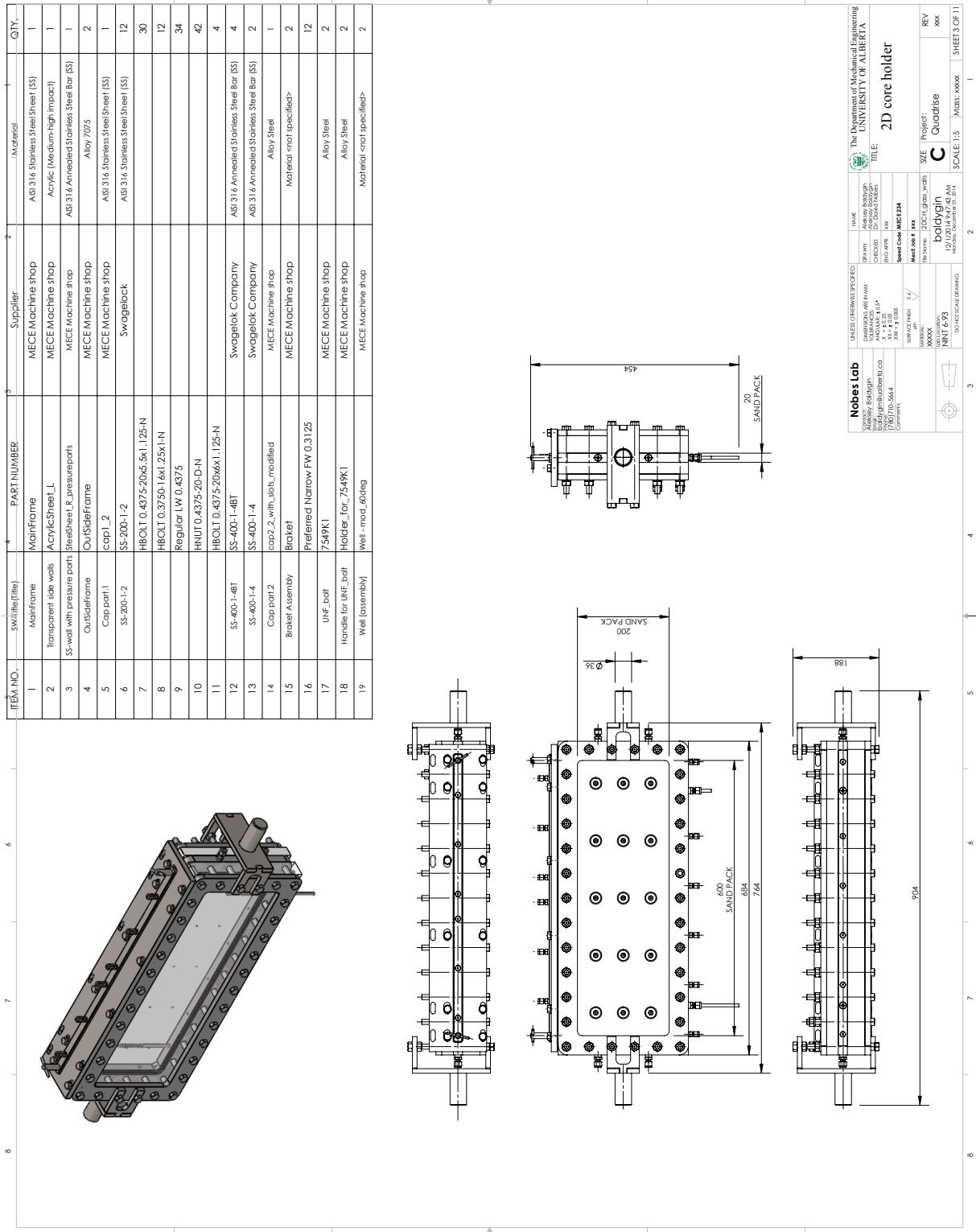


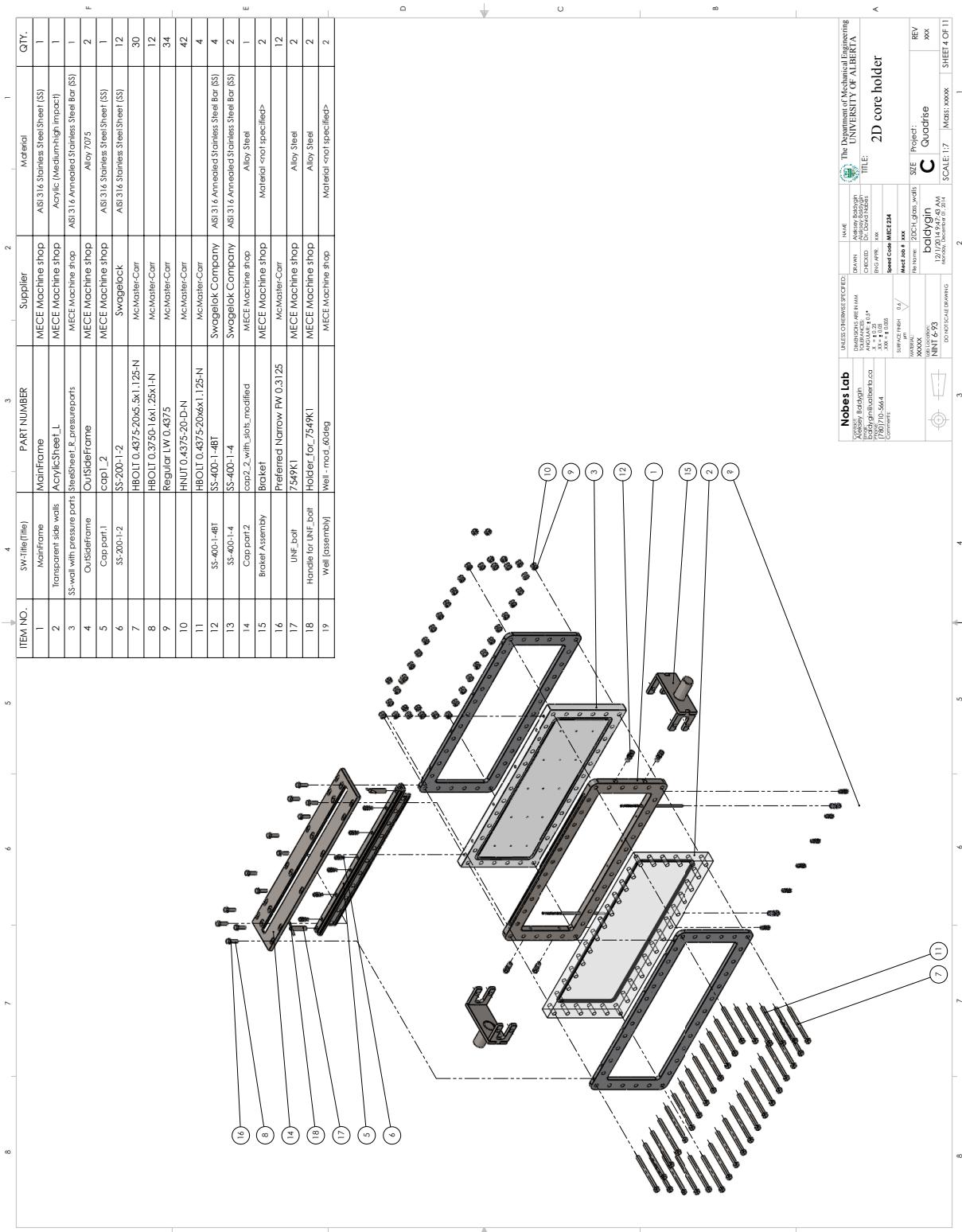


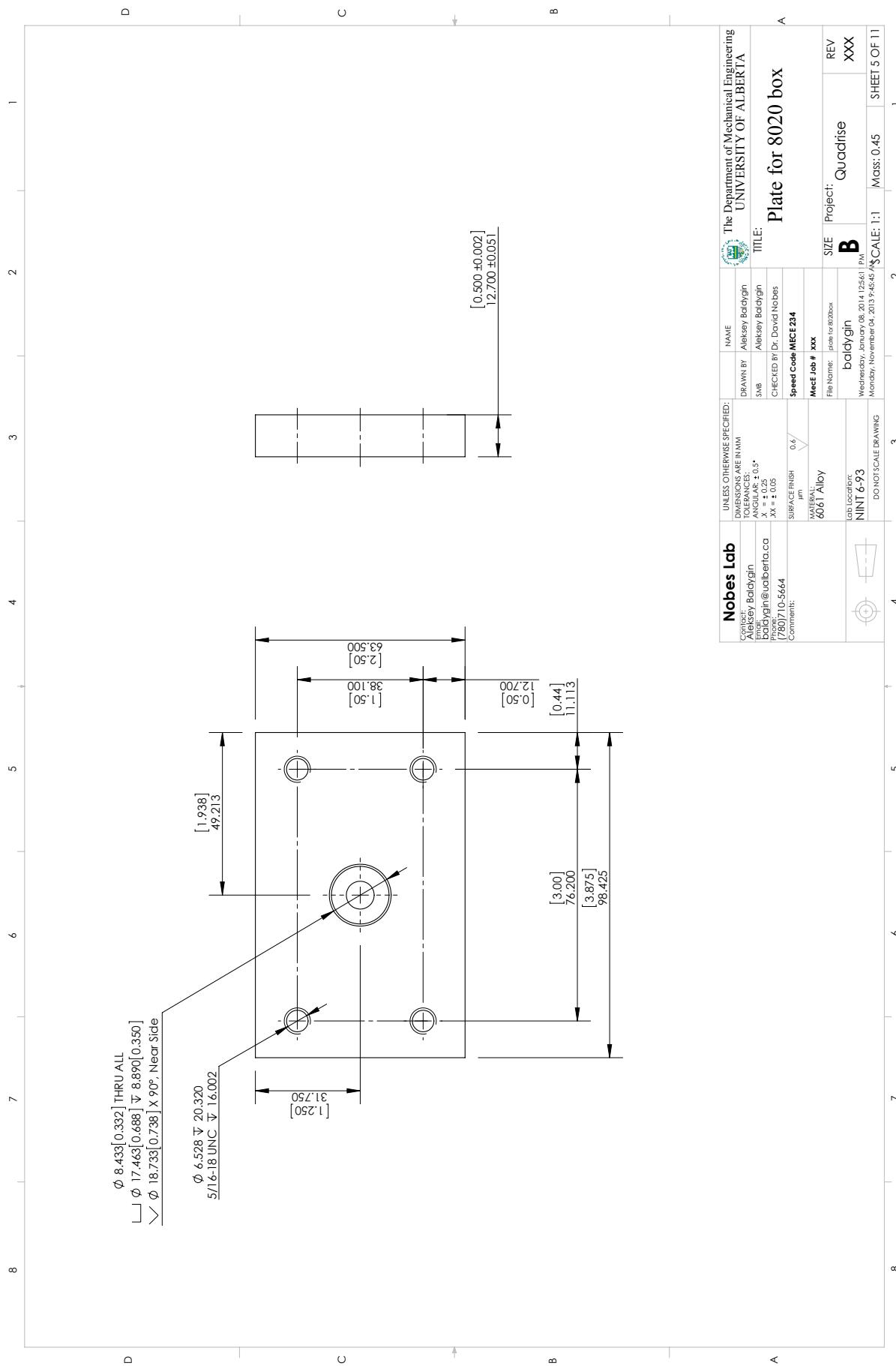
ITEM NO.	SW-Title[Title]	PART NUMBER	Supplier	QTY.
1	Frame from 8020 parts	Frame	8020.net	1
2	2D core holder	2DCH glass walls	MECE Machine shop	1
3		HBUIT 0.3125-18x1x0.875-N	McMaster-Carr	8
4	8020-5930	8020-5930	8020 Inc.	2
5	Plate for 8020 box	plate for 8020box	MECE Machine shop	2

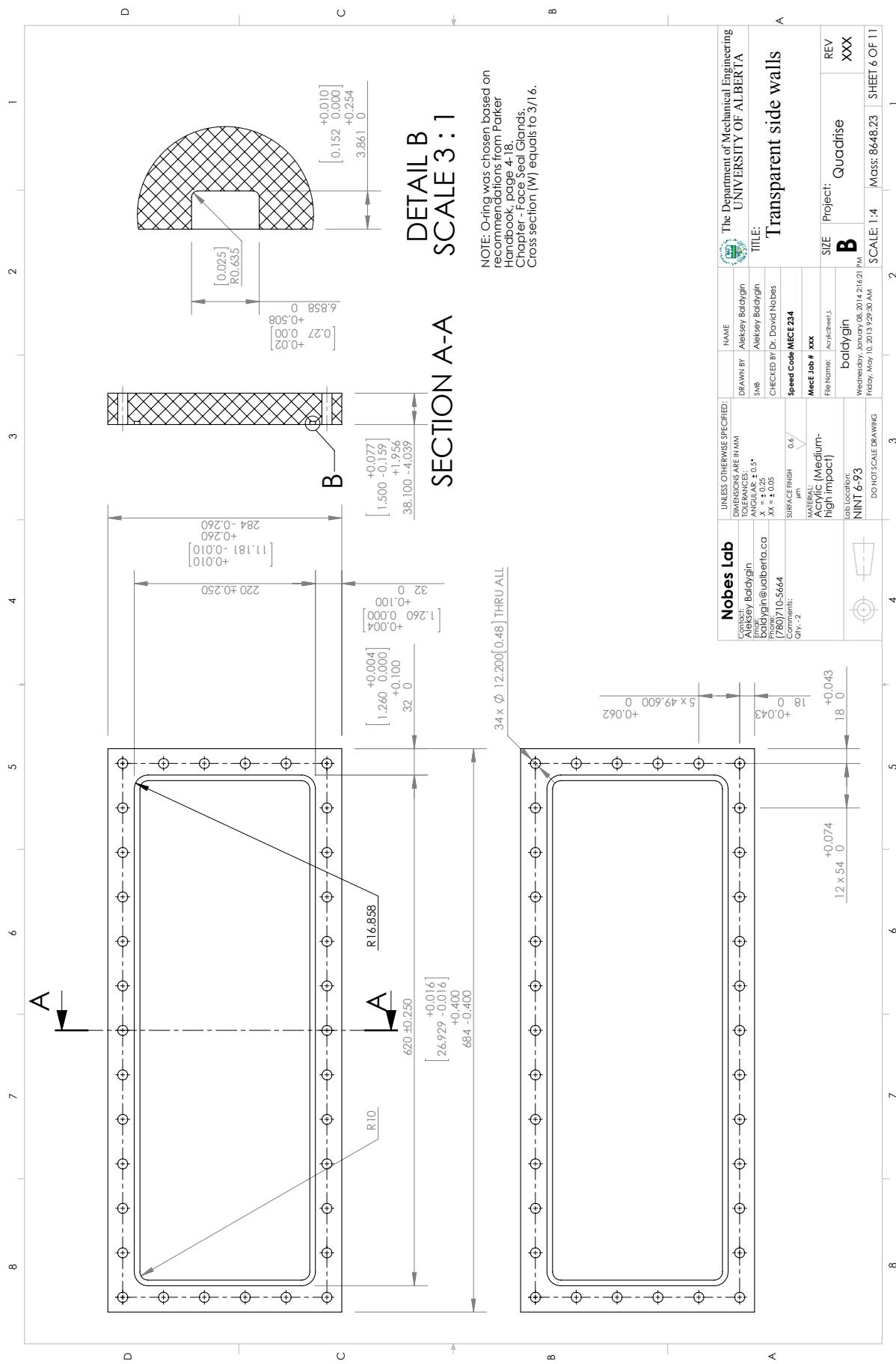


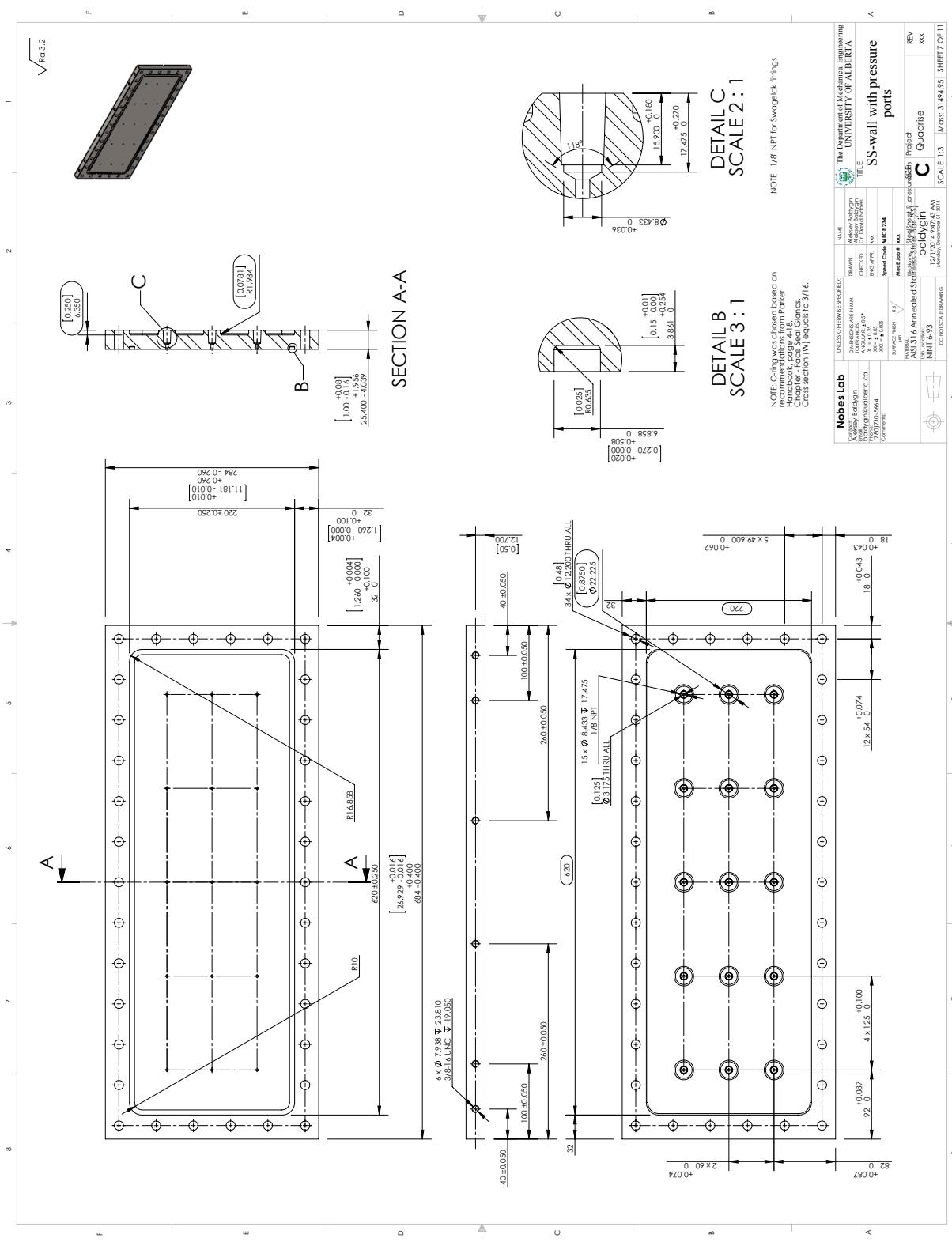


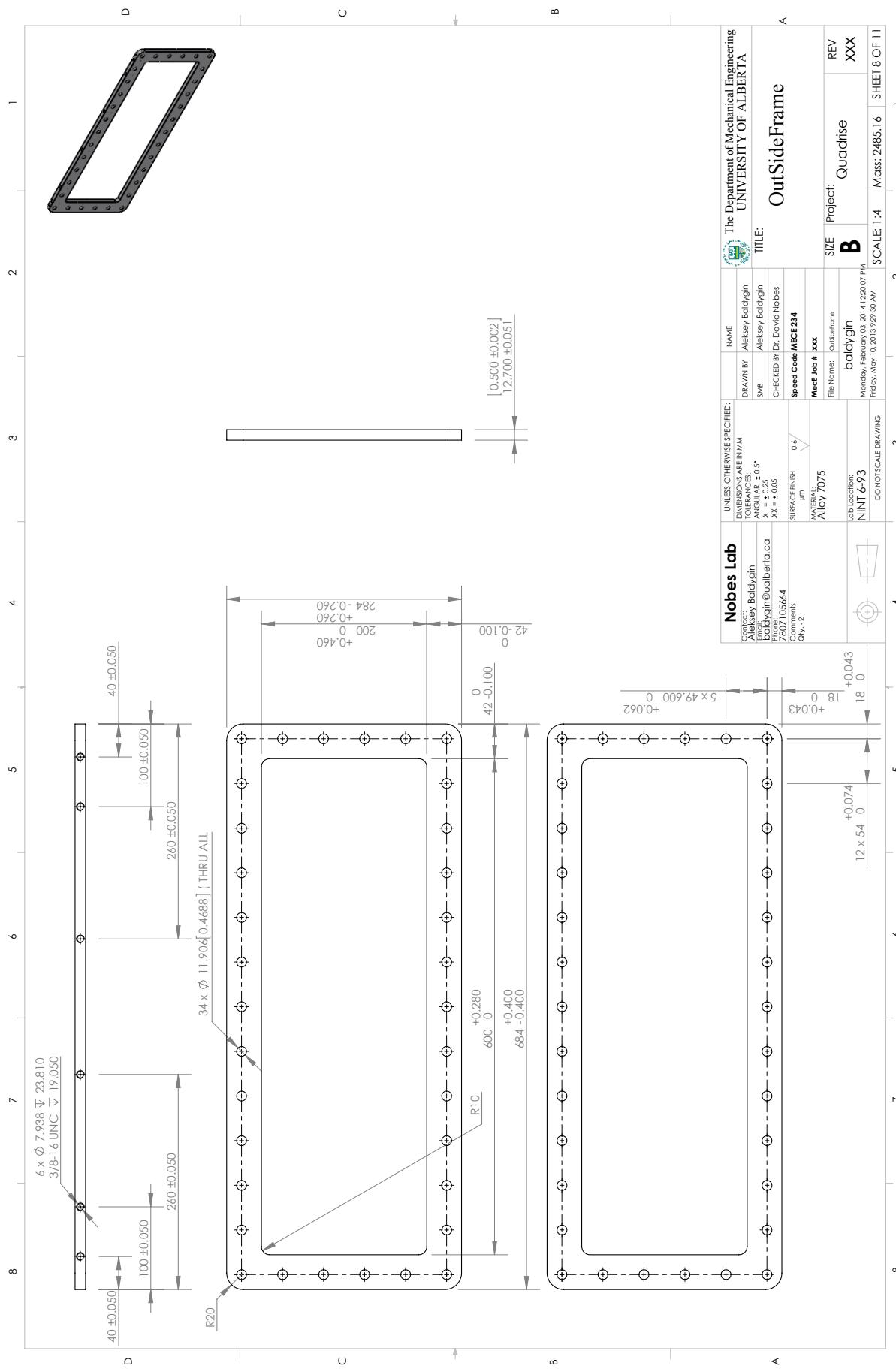


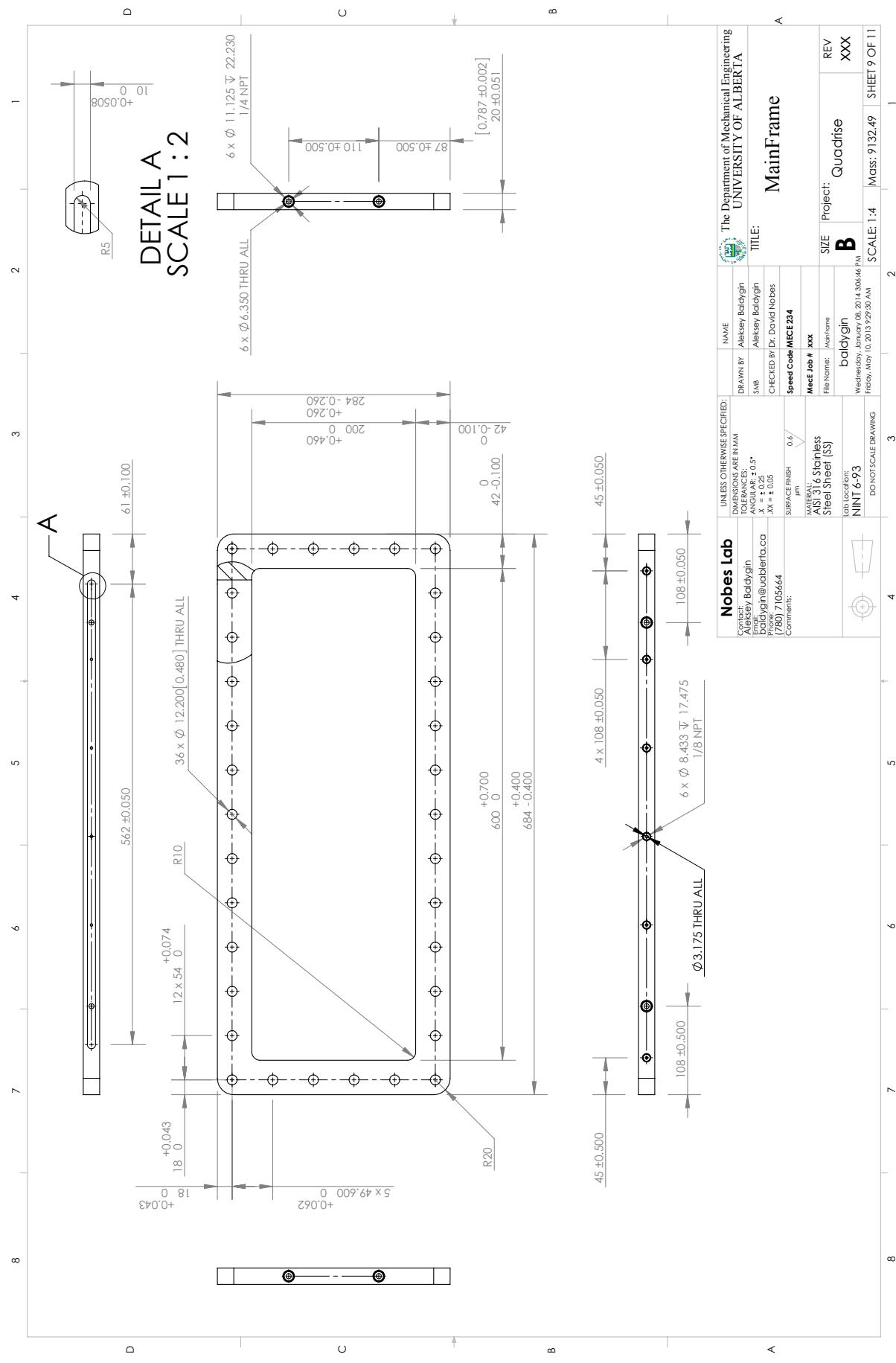


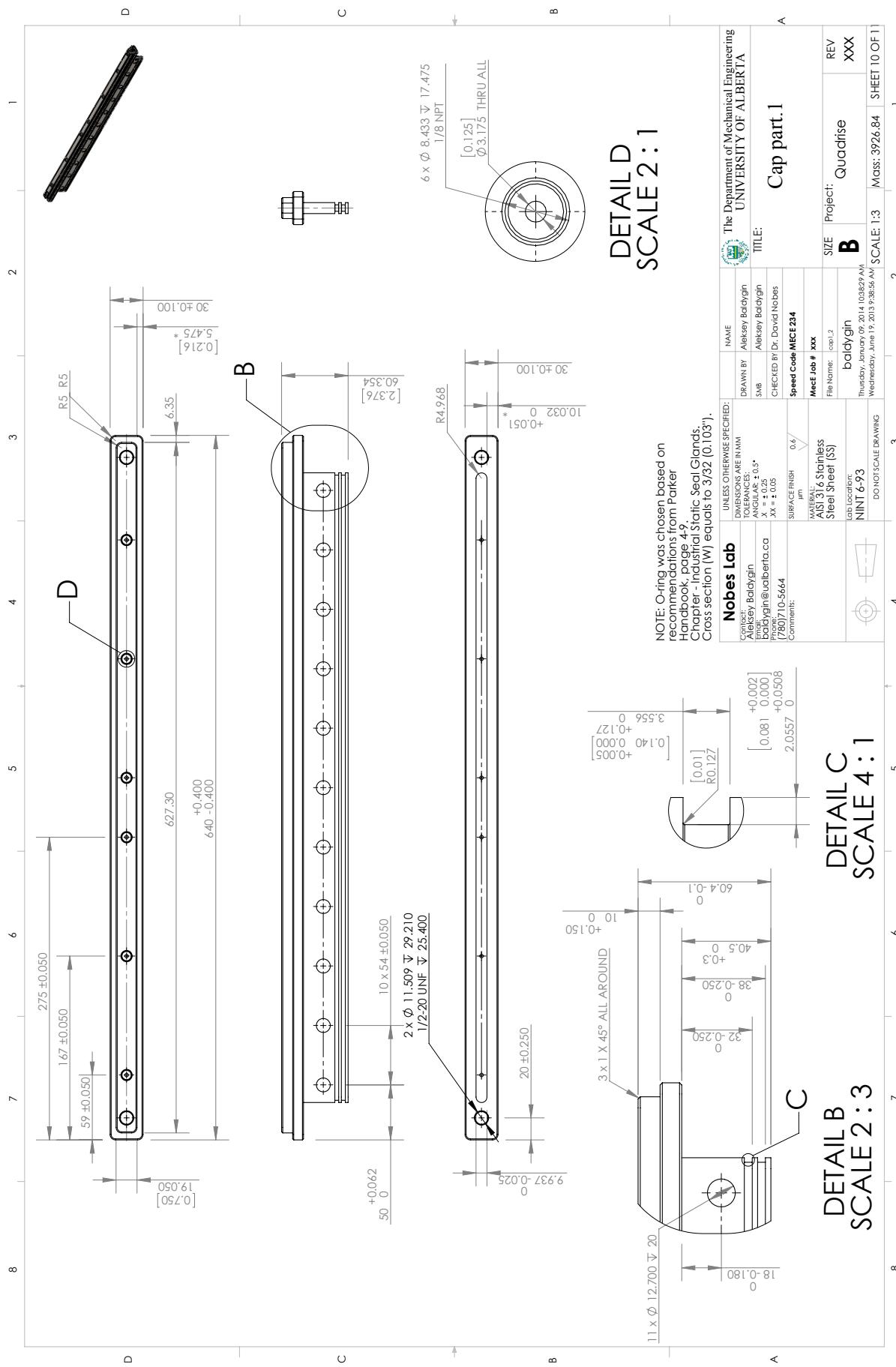


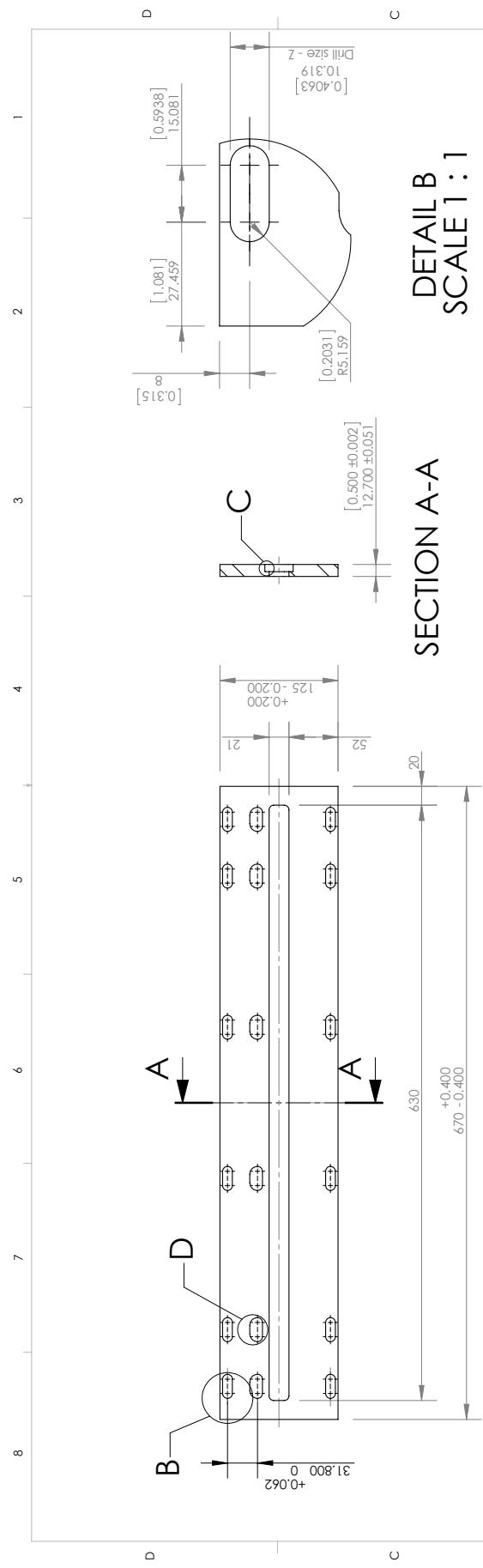






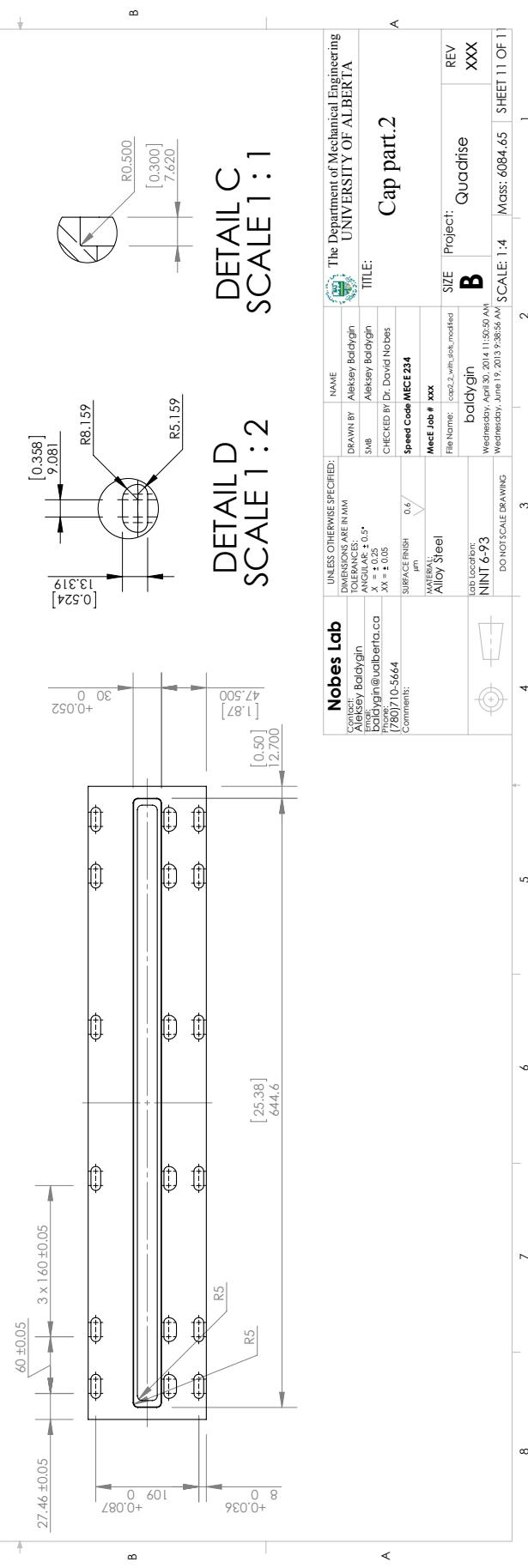






DETAIL B  
SCALE 1 : 1

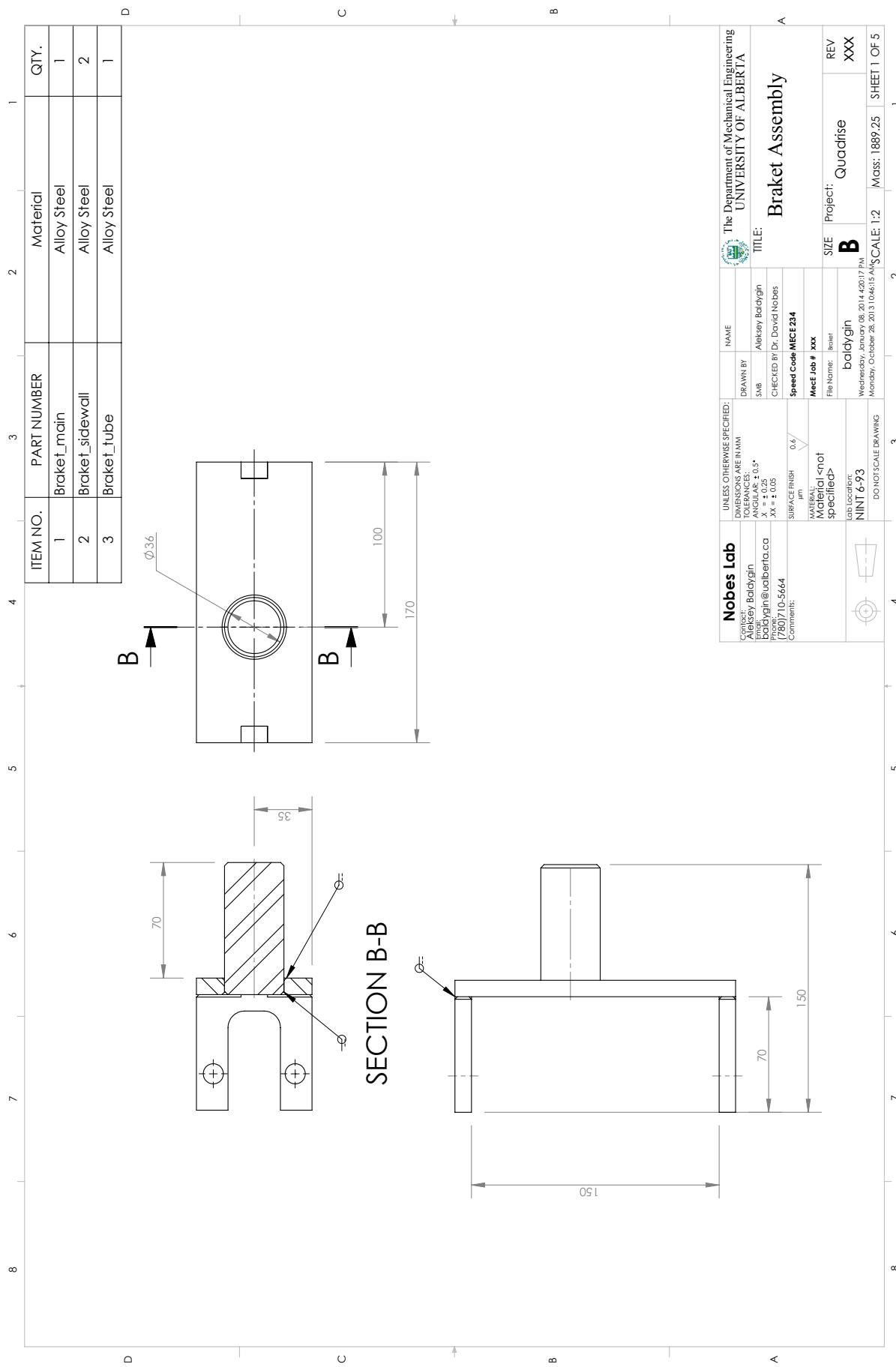
## SECTION A-A

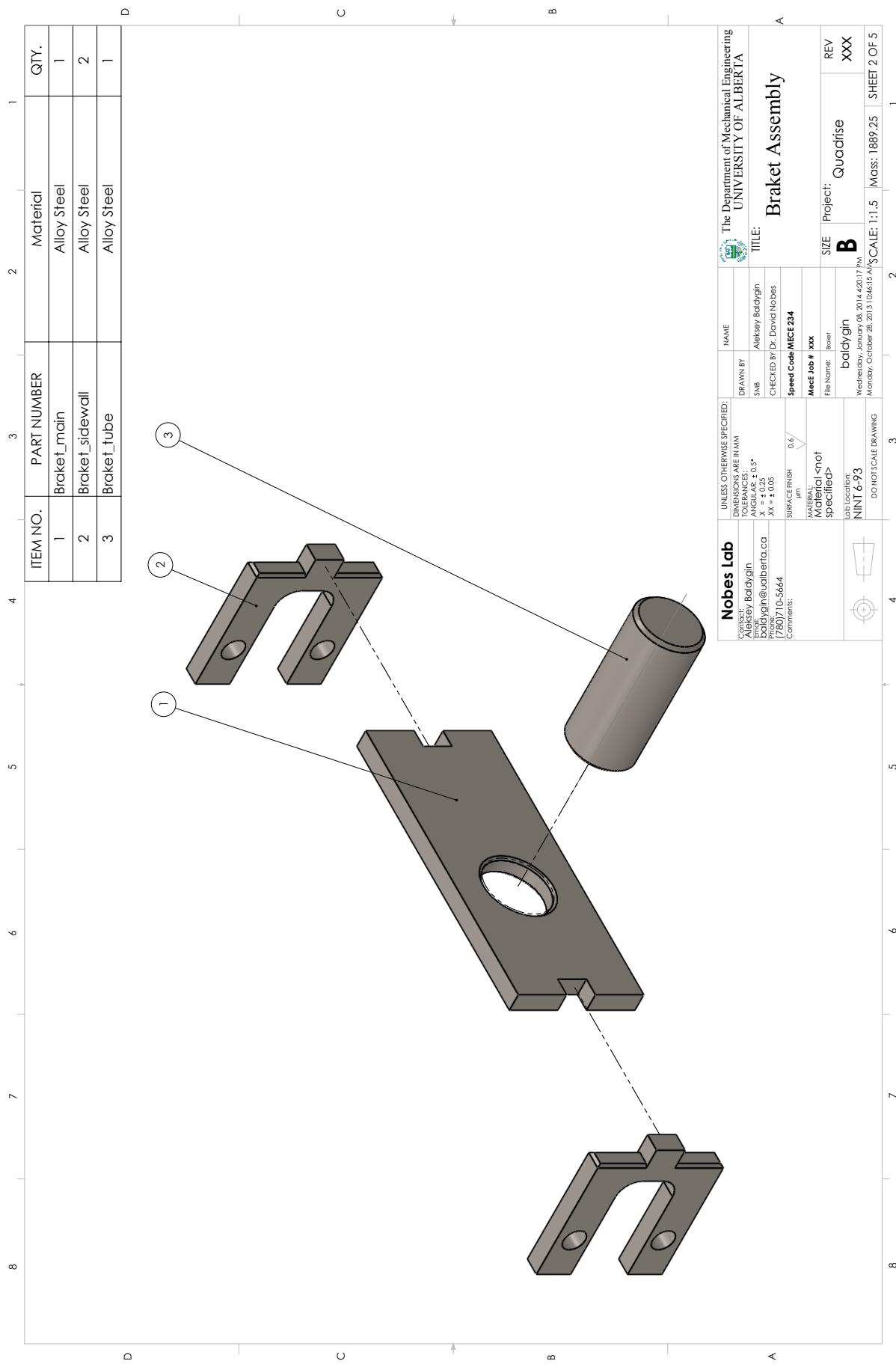


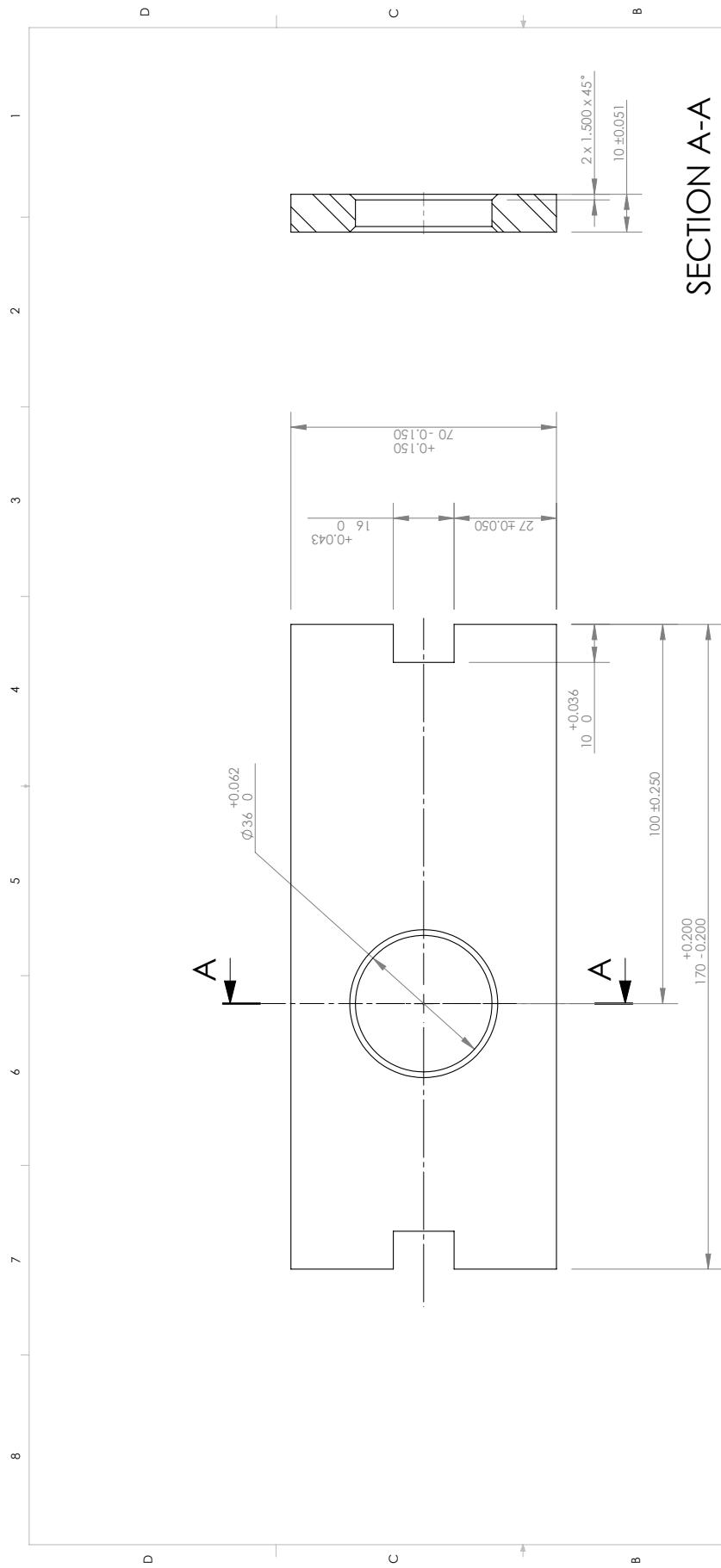
DETAIL SCALE 1 : 1

DETAIL D  
SCALE 1 : 2

The Department of Mechanical Engineering UNIVERSITY OF ALBERTA	
	NAME: Aleksy Badzyn
DRAWN BY Aleksy Badzyn	
DIMENSIONS ARE IN MM ANGLES IN DEGREES	
X = 0.25; 1.5° XX = 0.05	
SHEET FINISH: 0.6 mm	
UNLESS OTHERWISE SPECIFIED:	
Contact: Aleksy Badzyn Email: Aleksy.Badzyn@ualberta.ca Phone: (780) 492-5664 Comment:	
TITLE: Cap part.2	
CHECKED By Dr. David Nobes	
Speed Code: MEEC 234	
MECE Job #	xxx
File Name: cap2-with-scale-modified	
SIZE	Project: Quadrise
B	Mass: 6084.65
SCALE	Sheet 11 of 11
REV	XXX
Lab Location: NINT 6-93 DO NOT SCALE DRAWING	
Wednesday, April 30, 2014 11:50:50 AM Wednesday, June 19, 2013 9:36:56 AM	

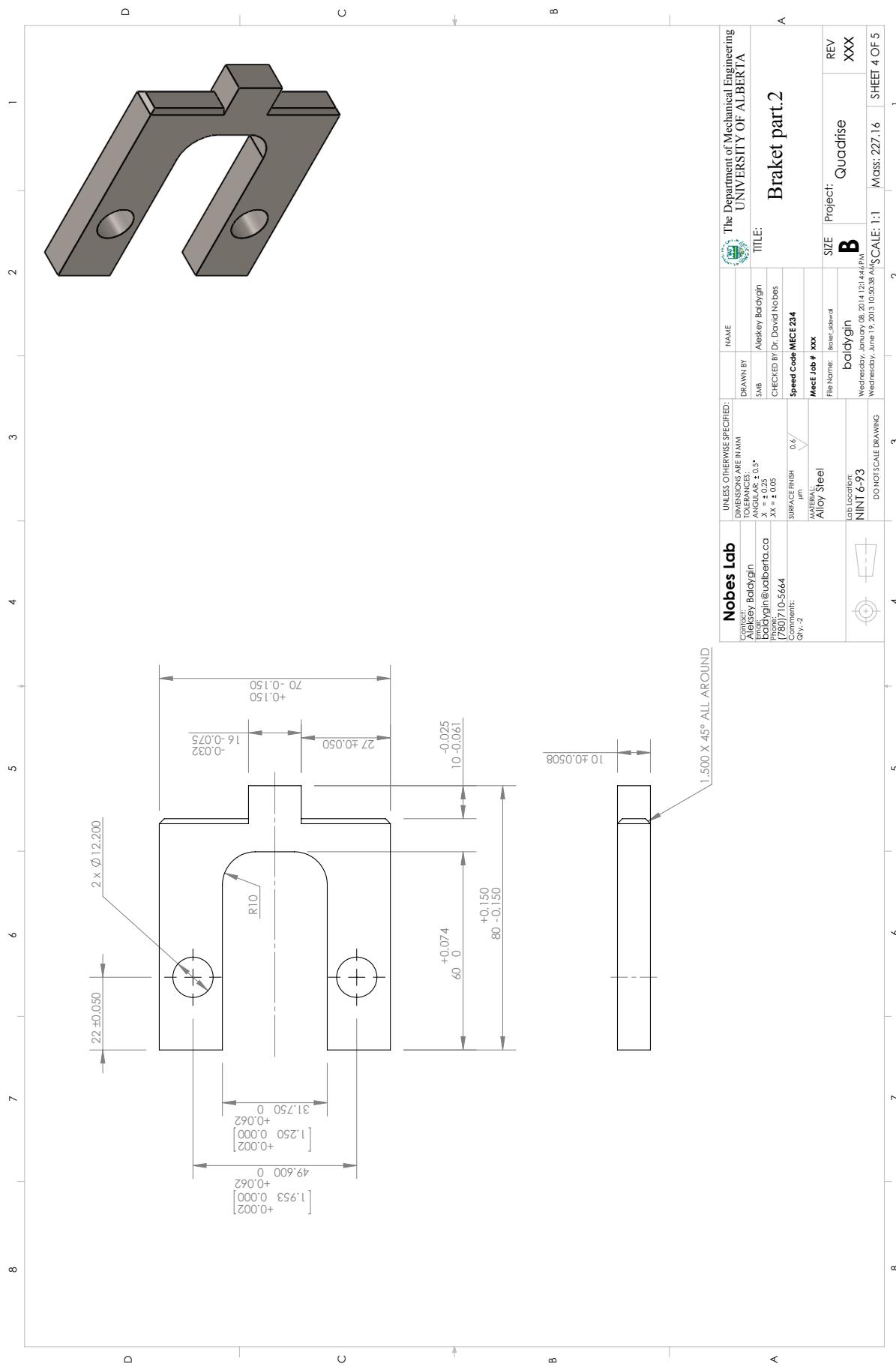


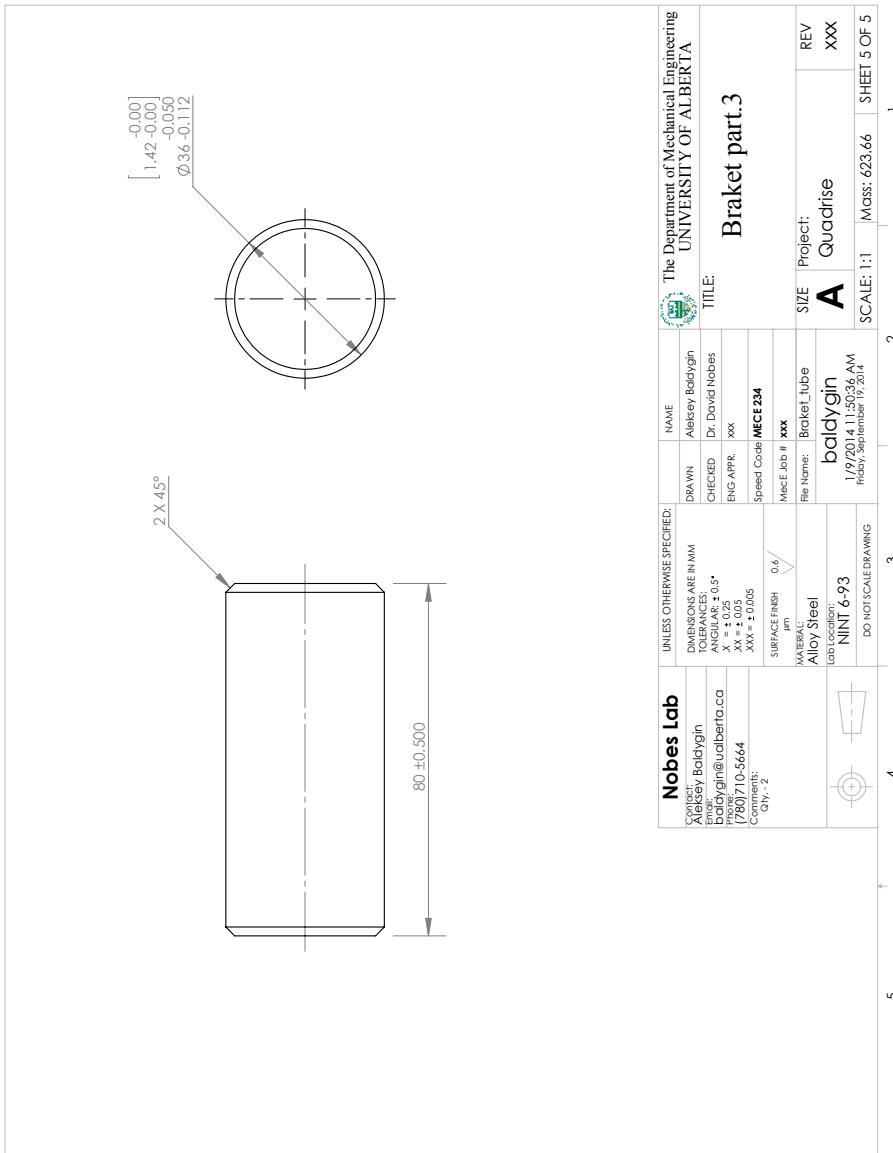


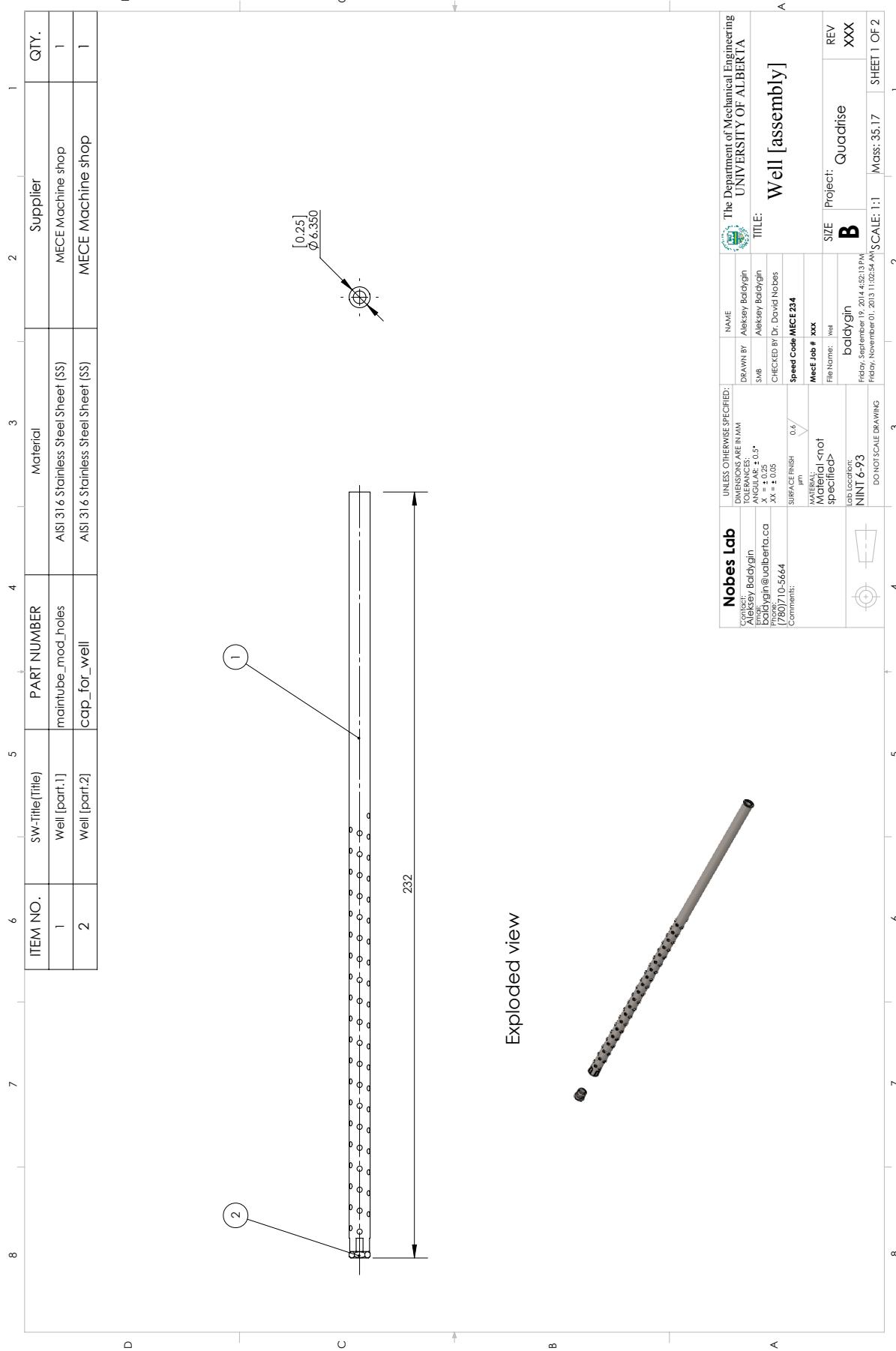


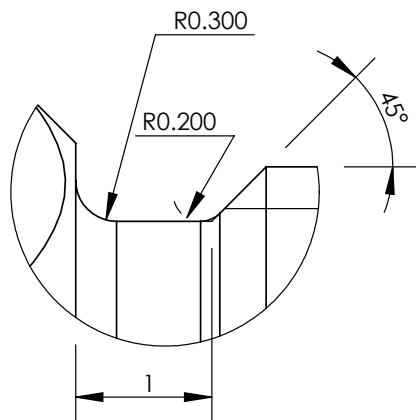
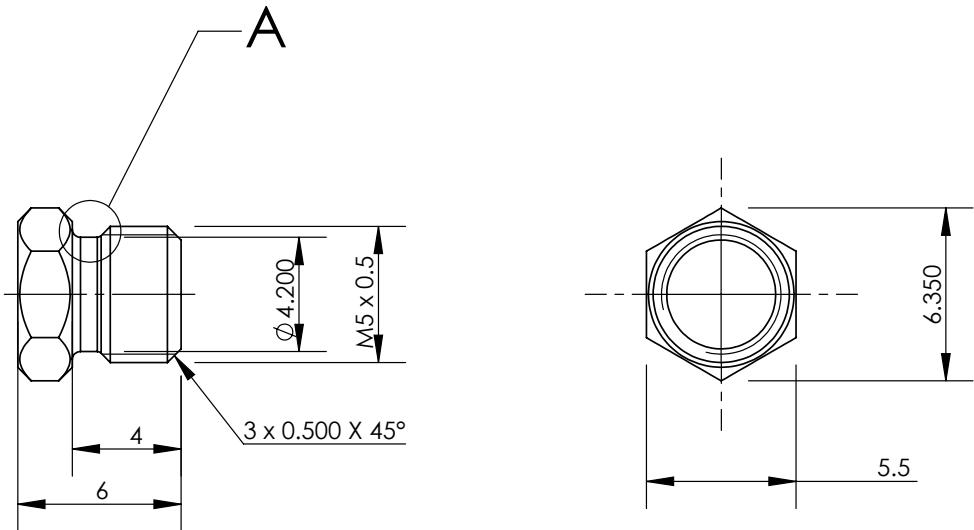
**SECTION A-A**

<b>Nobes Lab</b>		UNLESS OTHERWISE SPECIFIED: DIMENSIONS ARE IN MM TOLERANCES: ANGULAR: $\pm 0.5^\circ$ X = $\pm 0.25$ XX = $\pm 0.05$		NAME DRAWN BY Snb Aleksy Baldygin		The Department of Mechanical Engineering UNIVERSITY OF ALBERTA	
Address: Aleksy Baldygin Email: baldygin@ualberta.ca Phone: 780/747-5664 Comments: Qty - 2		Title: <b>Braket part.1</b>		Title:			
Speed Code: <b>MCE 234</b>		Checked by Dr. David Nokes					
MCE Job # <b>xxx</b>		File Name: baldygin		Project: <b>B</b>		REV <b>XXX</b>	
Lab location: <b>NINI 6/93</b>		Date drawn: Wednesday, January 08, 2014 (12:15:13 PM)		Scale: <b>1:1</b>		Mass: 811.27	
NOTES: DO NOT SCALE DRAWING		Wednesday, June 19, 2013 (10:50:38 AM)		SHEET 3 OF 5			



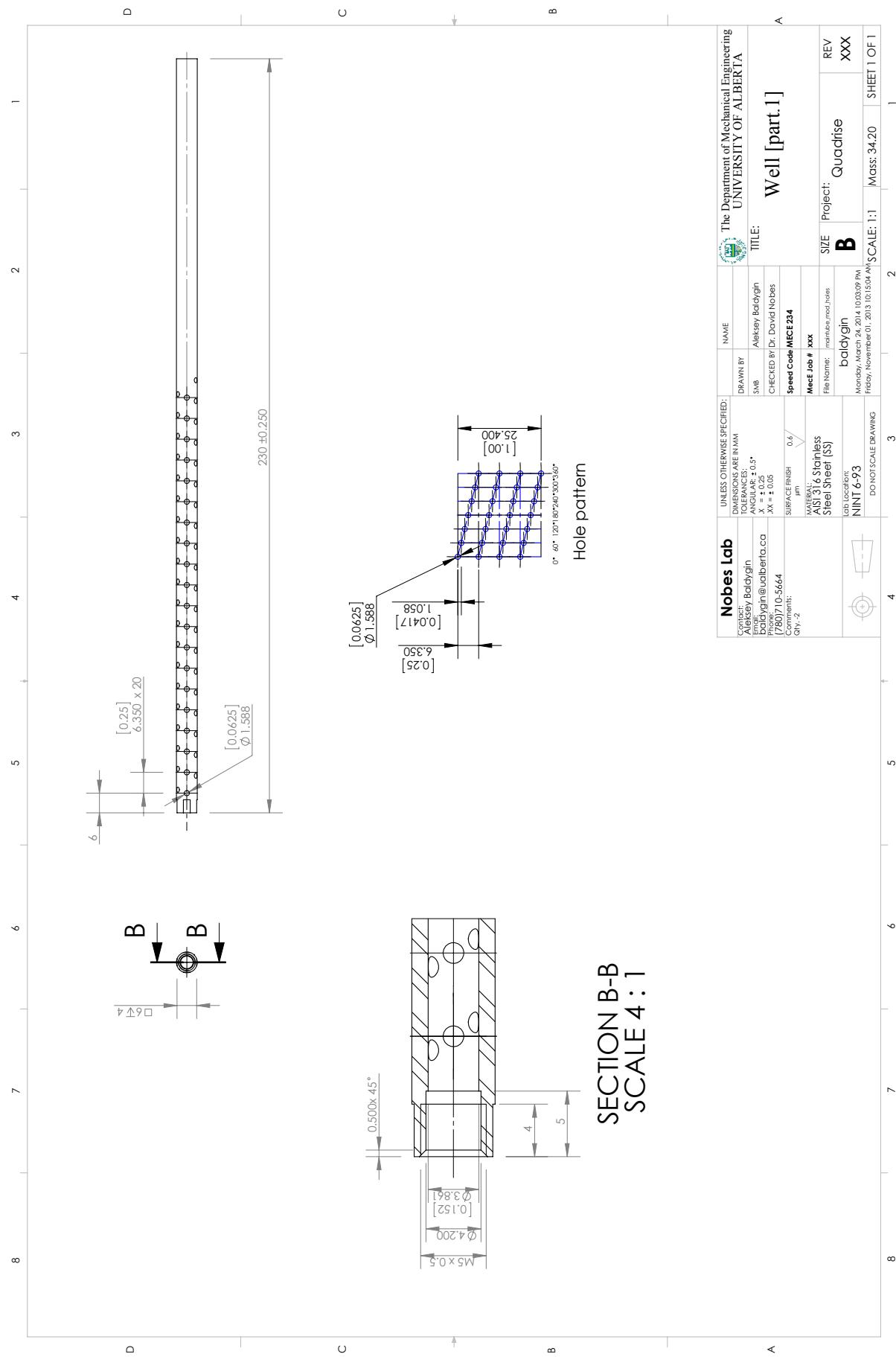


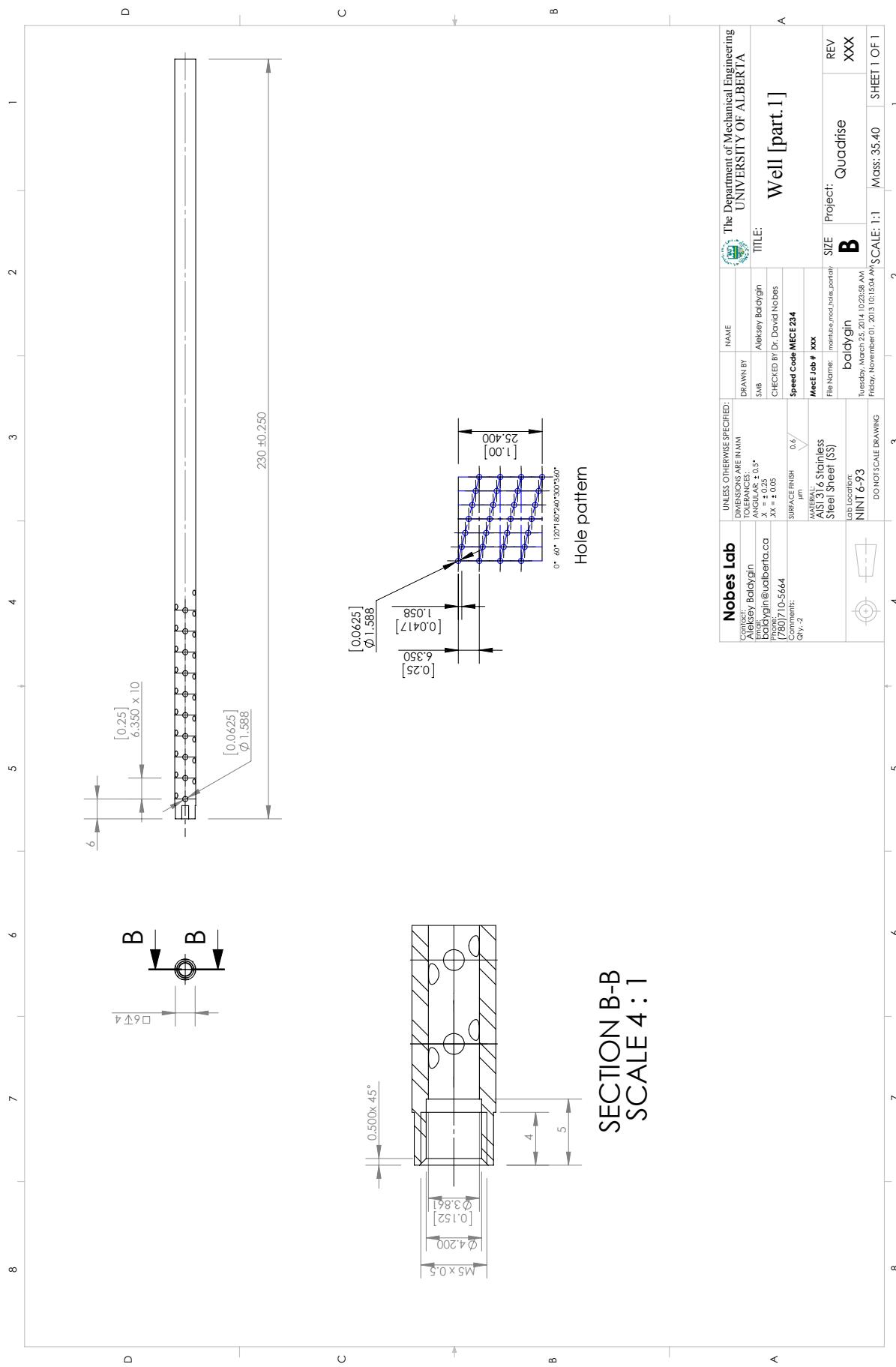


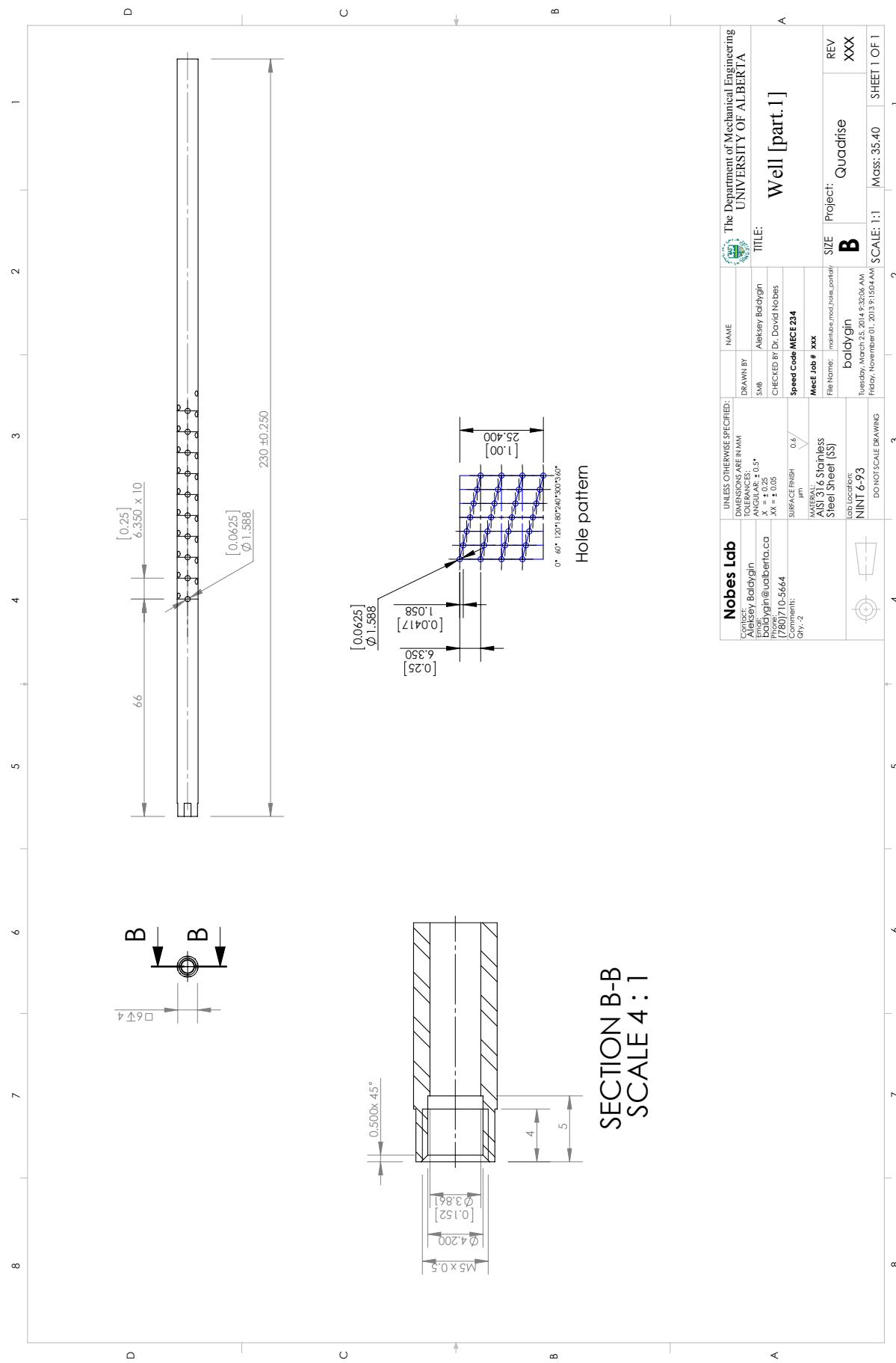


**DETAIL A**  
**SCALE 20 : 1**

<b>Nobes Lab</b> Contact: Aleksey Baldygin Email: baldygin@ualberta.ca Phone: (780)710-5664 Comments:	UNLESS OTHERWISE SPECIFIED:		NAME	The Department of Mechanical Engineering UNIVERSITY OF ALBERTA	
	DRAWN	Aleksey Baldygin			
	CHECKED	Aleksey Baldygin Dr. David Nobes			
	ENG APPR.				
	Speed Code	MECE 234			
	MecE Job #	xxx			
	File Name:	cap_for_well			
	baldygin				
	9/19/2014 4:52:13 PM				
	Friday, September 19, 2014				
			SIZE	Project: <b>Quadrise</b>	REV
			<b>A</b>		xxx
		DO NOT SCALE DRAWING	SCALE: 4:1	Mass: 0.97	SHEET 2 OF 2







## **A-7 Software flowchart**

The algorithm for the further software was developed and drawn as flowchart using diagramming software(Microsoft Visio Professional, Microsoft, Co.). It was modified and edited along project time, since new features were introduced from experiment to experiment. Final version is shown in Figure A-1.

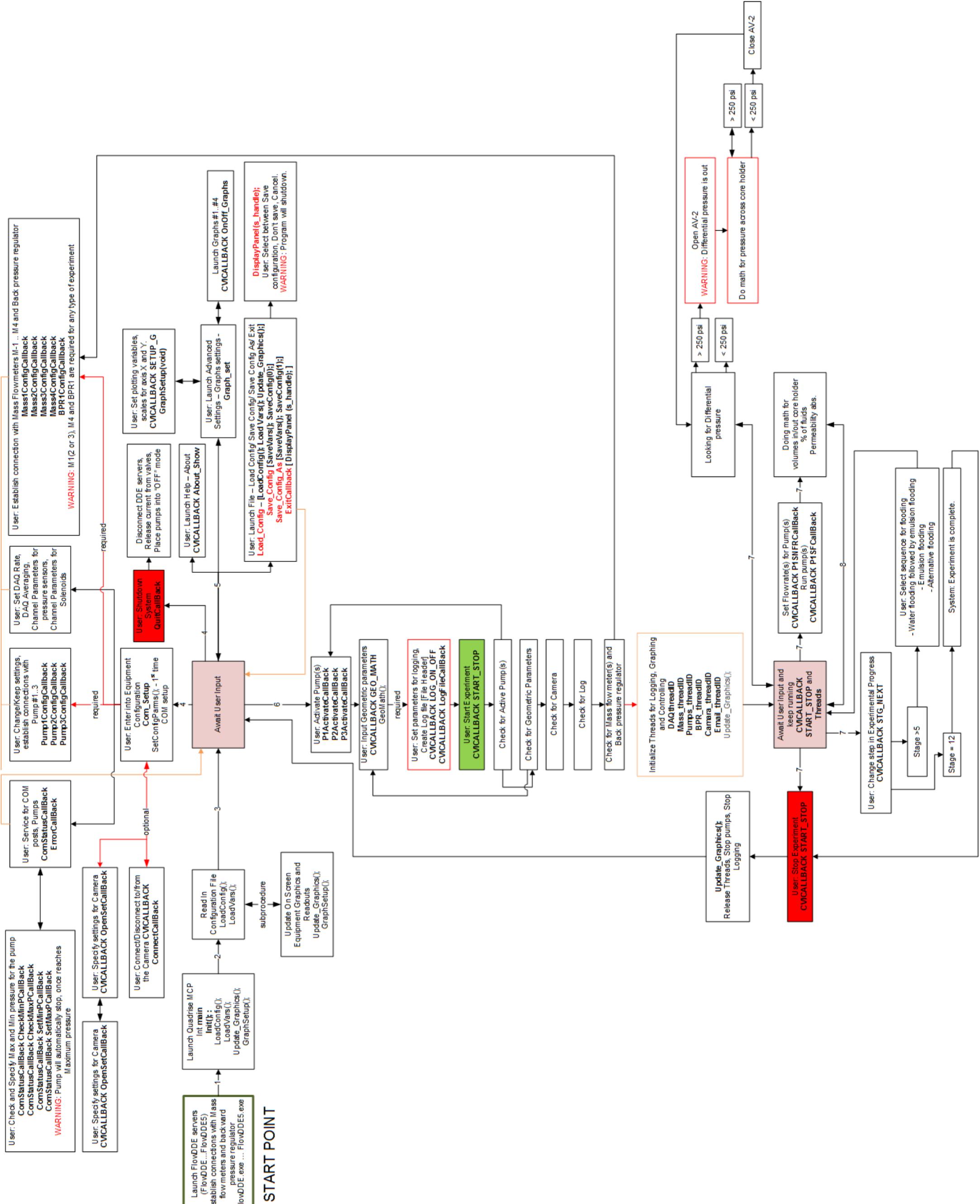


Figure A-1: Software flowchart

## A-8 Software source code

The following code was developed using custom design software (LabWindows CVI 10.0, National Instruments Inc.). The code consists of the five threads which allow to control and collect data from four mass flow meters, three dual piston pumps, 17 inline pressure sensors and one differential pressure sensor, one web-camera and single fraction collector. The code was developed based on source code presented earlier by Marc Evans in his MSc Thesis<sup>3</sup>.

---

<sup>3</sup>Available at Education & Research Archive <http://hdl.handle.net/10402/era.28390>

```

1 /*-----*/
2 /* Defines */                                     */
3 /*-----*/
4
5 #define TEXT_LENGTH      2000
6 #define QuitHelp         1
7 #define InputqHelp       2
8 #define NUM 500 //number of samples to hold for plotting
9
10#define subTRUE 1 //used same as dsnTRUE
11#define subFALSE 0 //used same as dsnFALSE
12
13#define DAQmxErrChk(functionCall) if( DAQmxFailed(error=(functionCall)) ) goto Error; else
14
15
16 // IMAQ
17
18#define SOURCE_WINDOW 0
19#define DEST_WINDOW 1
20#define IM_WIN 0
21
22#define TRUE    1
23#define FALSE   0
24
25#define OPEN    1
26#define CLOSE   0
27
28#include "nivision.h"                           /* NIVision used to operate different functions of camera */
29#include "NIIMAQdx.h"                          /* NIIMAQdx used to operate the camera */
30
31/*-----*/
32/* Module-globals */                         */
33/*-----*/
34
35 static int s_handle;           // Handle for Save MCP Config Panel
36 static int a_handle;           // Handle for About Panel
37 static int g_handle;           // Handle for Graphs configuration
38 static int config_handle;     // Handle for Configuration system
39 static int extra_g_handle;    // Handle for Extra Graph panel
40 static int sat_handle;        // Handle for setting volume of water injected
41 static int panelHandle;       // Handle for camera settings
42 static int TabPanelHandle;    // Handle for tab-settings
43 static int pressure_handle;
44 static int pumpservice_handle;
45
46 static IMAQdxSession session = 0;
47 static Image** images = NULL;          // Defining 2-D array variable for video
48 static Image* image_g = NULL;          // Defining 1-D array variable for images
49 static int imageArraySize = 0;
50 IMAQdxError error2;
51
52 static IMAQdxAttributeInformation* cameraAttributes;
53 static unsigned int selectedAttrIndex = 0;
54
55
56
57 int forcestop;
58
59 int panel_handle,
60 CP,
61 LED,
62 Just_Opened,
63 Just_Grabbed,
64 EM_Q, //For emergency stop
65 stage,
66 pumprun_1,pumprun_2,pumprun_3,
67
68 // Com ports settings
69 P1_comport, P2_comport, P3_comport,
70 P1_baudrate, P2_baudrate, P3_baudrate,
71 P1_portindex, P2_portindex, P3_portindex,
72 P1_parity, P2_parity, P3_parity,
73 P1.databits, P2.databits, P3.databits,
74 P1_stopbits, P2_stopbits, P3_stopbits,
75 P1_inputq, P2_inputq, P3_inputq,      /* Sets input queue length in OpenComConfig */
76 P1_outputq, P2_outputq, P3_outputq,    /* Sets output queue length in OpenComConfig */
77 P1_xmode, P2_xmode, P3_xmode,
78 P1_ctsmode, P2_ctsmode, P3_ctsmode,
79 P1_port_open,P2_port_open,P3_port_open,
80 com_num,
81 plcheck, p2check, p3check,
82
83 RS232Error,
84 config_flag,
85 com_status,
86 inqlen,           // Stores result from GetInQLen
87 outqlen,          // Stores result from GetOutQLen
88 test,             // variable parameter for testing
89
90 M1DDE_connection, M2DDE_connection, M3DDE_connection, M4DDE_connection, BPRDDE_connection,
91 m1check, m2check, m3check, m4check, bprcheck,
92
93
94 stringsize,
95 bytes_sent,
96 bytes_read,
97 read_term,

```

```

98     text_panel_name, // text inside the panel
99     PTEXT_panel_name,
100    panel_name; // panel name
101
102
103 // breakstatus,
104 // send mode,
105 // send_byte,
106 // send_term_index,
107 // read_term_index,
108
109
110 double wb_setpoint,pmax_setpoint,pmin_setpoint; // set point for flow rate
111
112 int hour_ref, min_ref, sec_ref, hour_cur, min_cur, sec_cur, check_first_time;
113
114
115 //-----
116 // GRAPH HANDLES
117 int SAMPLES;
118 int OnOff_G1,OnOff_G2,OnOff_G3,OnOff_G4,OnOff_G5,Onoff_G6; //turning graphs On_Off
119
120 // PLOTTING VARIABLES
121 int plotVar_G_1,plotVar_G_2,plotVar_G_3,plotVar_G_4,plotVar_G_5,plotVar_G_6;
122
123 double X_Range_G_1,X_Range_G_2,X_Range_G_3,X_Range_G_4;
124
125 int Y_Mode_G_1,Y_Mode_G_2,Y_Mode_G_3,Y_Mode_G_4,
126 X_Mode_G_5,Y_Mode_G_5;
127 double Y_Min_G_1,Y_Min_G_2,Y_Min_G_3,Y_Min_G_4,
128 X_Min_G_5,Y_Min_G_5;
129 double Y_Max_G_1,Y_Max_G_2,Y_Max_G_3,Y_Max_G_4,
130 X_Max_G_5,Y_Max_G_5;
131
132
133 //Core Geometry
134 double L_core, D_core, A_core, V_core, WAT_core, Por_core, Por_core_per, Perm_coef;
135
136
137
138 // LOGGING VARIABLES
139 int Is_P1, Is_P2, Is_P3,
140 Is_M1, Is_M2, Is_M3, Is_M4,
141 Is_BPR,
142 Is_DAQ,
143 Is_Cam,
144 Is_PRES,
145 Is_Log,
146 Is_Graph,
147 Log_File_Selected,
148 Type_exp;
149
150 int globalemail;
151
152 double timeDAQ, timeBPR, timeMFR;
153
154
155 // CONFIG VARIABLES
156 int Exp_Type;
157 // STAGES
158
159 int STG_1, STG_2, STG_3, STG_4, STG_5, STG_6, STG_7, STG_8, STG_9,
160     STG_10, STG_11, STG_12, STG_13, STG_14, STG_15, STG_16;
161
162
163
164 //-----
165 // Threading COMMUNICATION
166 //-----
167 // New thread to run the DAQ
168 int CVICALLBACK DAQThreadFunction (void *functionData);
169 static int DAQthreadID;
170 static int DAQquitflag = 0;
171 static int DAQcmtStatus;
172
173 // Thread to get data from Pumps
174 int CVICALLBACK Pumps_ThreadFunction (void *functionData);
175 static int Pumps_threadID;
176 static int Pumps_quitflag = 0;
177 static int Pumps_cmtStatus;
178
179 // Thread to get data from Mass flow meters
180 int CVICALLBACK Mass_ThreadFunction (void *functionData);
181 static int Mass_threadID;
182 static int Mass_quitflag = 0;
183 static int Mass_cmtStatus;
184
185 // Thread to control and receive data from Backward pressure regulator
186 int CVICALLBACK BPR_ThreadFunction (void *functionData);
187 static int BPR_threadID;
188 static int BPR_quitflag = 0;
189 static int BPR_cmtStatus;
190
191 // Thread to images from camera
192 int CVICALLBACK Camera_ThreadFunction (void *functionData);
193 static int Camera_threadID;
194 static int Camera_quitflag = 0;

```

```

195 static int Camera_cmtStatus;
196
197 // Thread to send email
198 int CVICALLBACK Email_ThreadFunction (void *functionData);
199 static int Email_threadID;
200 static int Email_quitflag = 0;
201 static int Email_cmtStatus;
202
203 CmtThreadLockHandle DAQ_lockHandle, Pumps_lockHandle, Mass_lockHandle, BPR_lockHandle, Camera_lockHandle, Email_lockHandle;
204
205
206 /*-----*/
207 // DDE client // 
208
209 static unsigned int hConv, hConv2, hConv3, hConv4, hConv5; //DDE Conversation_handle for different servers.
210
211 int DDECallback (unsigned handle, char *topicName,
212                   char *itemName, int xType, int dataFmt,
213                   int dataSize, void *dataPtr,
214                   void *callbackData);
215
216
217 short read_cnt;
218     read_len;
219
220 double P1_timeout, P2_timeout, P3_timeout;
221
222 double viscoef, permcoef;
223
224 char P1_devicename[30],
225     P2_devicename[30],
226     P3_devicename[30],
227     send_data[TEXT_LENGTH],
228     get_send_data[TEXT_LENGTH],
229     read_data[TEXT_LENGTH],
230
231     TP2channel[TEXT_LENGTH],
232
233     DP1channel_A[TEXT_LENGTH],
234     DP1channel_B[TEXT_LENGTH],
235
236     TP1channel[TEXT_LENGTH],
237
238     CP11_Achannel[TEXT_LENGTH],
239     CP11_Bchannel[TEXT_LENGTH],
240     CP12_Achannel[TEXT_LENGTH],
241     CP12_Bchannel[TEXT_LENGTH],
242     CP13_Achannel[TEXT_LENGTH],
243     CP13_Bchannel[TEXT_LENGTH],
244     CP14_Achannel[TEXT_LENGTH],
245     CP14_Bchannel[TEXT_LENGTH],
246     CP15_Achannel[TEXT_LENGTH],
247     CP15_Bchannel[TEXT_LENGTH],
248
249     CP21_Achannel[TEXT_LENGTH],
250     CP21_Bchannel[TEXT_LENGTH],
251     CP22_Achannel[TEXT_LENGTH],
252     CP22_Bchannel[TEXT_LENGTH],
253     CP23_Achannel[TEXT_LENGTH],
254     CP23_Bchannel[TEXT_LENGTH],
255     CP24_Achannel[TEXT_LENGTH],
256     CP24_Bchannel[TEXT_LENGTH],
257     CP25_Achannel[TEXT_LENGTH],
258     CP25_Bchannel[TEXT_LENGTH],
259
260     CP31_Achannel[TEXT_LENGTH],
261     CP31_Bchannel[TEXT_LENGTH],
262     CP32_Achannel[TEXT_LENGTH],
263     CP32_Bchannel[TEXT_LENGTH],
264     CP33_Achannel[TEXT_LENGTH],
265     CP33_Bchannel[TEXT_LENGTH],
266     CP34_Achannel[TEXT_LENGTH],
267     CP34_Bchannel[TEXT_LENGTH],
268     CP35_Achannel[TEXT_LENGTH],
269     CP35_Bchannel[TEXT_LENGTH],
270
271     read_m11data[TEXT_LENGTH],
272     read_m12data[TEXT_LENGTH],
273     read_m13data[TEXT_LENGTH],
274     read_m14data[TEXT_LENGTH],
275
276     read_m21data[TEXT_LENGTH],
277     read_m22data[TEXT_LENGTH],
278     read_m23data[TEXT_LENGTH],
279     read_m24data[TEXT_LENGTH],
280
281     read_m31data[TEXT_LENGTH],
282     read_m32data[TEXT_LENGTH],
283     read_m33data[TEXT_LENGTH],
284     read_m34data[TEXT_LENGTH],
285
286     read_m41data[TEXT_LENGTH],
287     read_m42data[TEXT_LENGTH],
288     read_m43data[TEXT_LENGTH],
289     read_m44data[TEXT_LENGTH],
290
291     read_bpri11data[TEXT_LENGTH],

```

```

292     read_bpr12data[TEXT_LENGTH],
293     read_bpr13data[TEXT_LENGTH],
294
295     tbox_read_data[TEXT_LENGTH],
296
297     SRP_read_data[TEXT_LENGTH],
298
299     com_msg[500],
300     msg[100];
301
302     char p1frwas[TEXT_LENGTH];
303     char p2frwas[TEXT_LENGTH];
304     char p3frwas[TEXT_LENGTH];
305
306
307     static char cfgfile[300];
308     static char logFile[300];
309     char dirname[MAX_PATHNAME_LEN];
310     char pathname[MAX_PATHNAME_LEN];
311
312     char camName[64];
313
314 //email featur
315     char currentresuts [500];
316
317     CVIAbsoluteTime timestamp;
318     CVIAbsoluteTime timestamp2;
319
320 /*-----*/
321 /* DATA LOGGING ARRAYS
322 /*-----*/
323
324     double step[NUM],
325         bpr_set, bpr_set_was;
326
327     double refwaterinj;
328
329     double //flow rates
330         PFR11[NUM], //pump #1
331         PFR21[NUM], //pump #2
332         PFR31[NUM], //pump #3
333
334         //pressure
335         P11[NUM], //pump #1
336         P21[NUM], //pump #2
337         P31[NUM], //pump #3
338
339         TP2[NUM], //inlet
340         DP1[NUM], //differential
341         DP1_A[NUM],
342         DP1_B[NUM],
343         TP1[NUM], //outlet
344
345         CP11[NUM],
346         CP11_A[NUM],
347         CP11_B[NUM],
348         CP12[NUM],
349         CP12_A[NUM],
350         CP12_B[NUM],
351         CP13[NUM],
352         CP13_A[NUM],
353         CP13_B[NUM],
354         CP14[NUM],
355         CP14_A[NUM],
356         CP14_B[NUM],
357         CP15[NUM],
358         CP15_A[NUM],
359         CP15_B[NUM],
360
361         CP21[NUM],
362         CP21_A[NUM],
363         CP21_B[NUM],
364         CP22[NUM],
365         CP22_A[NUM],
366         CP22_B[NUM],
367         CP23[NUM],
368         CP23_A[NUM],
369         CP23_B[NUM],
370         CP24[NUM],
371         CP24_A[NUM],
372         CP24_B[NUM],
373         CP25[NUM],
374         CP25_A[NUM],
375         CP25_B[NUM],
376
377         CP31[NUM],
378         CP31_A[NUM],
379         CP31_B[NUM],
380         CP32[NUM],
381         CP32_A[NUM],
382         CP32_B[NUM],
383         CP33[NUM],
384         CP33_A[NUM],
385         CP33_B[NUM],
386         CP34[NUM],
387         CP34_A[NUM],
388         CP34_B[NUM],
389         CP35[NUM],

```

```

389      CP35_A[NUM],
390      CP35_B[NUM],
391
392 //mass #1
393      M11[NUM],
394      M12[NUM],
395      M13[NUM],
396      M14[NUM], //extra
397 //mass #2
398      M21[NUM],
399      M22[NUM],
400      M23[NUM],
401      M24[NUM],
402 //mass #3
403      M31[NUM],
404      M32[NUM],
405      M33[NUM],
406      M34[NUM], //extra
407 //mass #4
408      M41[NUM],
409      M42[NUM],
410      M43[NUM],
411      M44[NUM],
412 // set point out. Mass flow meter
413      SETPOINTOUT[NUM],
414
415 // OIL AND WATER OUT!
416      WATERREC[NUM],
417      OILREC[NUM],
418      TEMPSTEP[NUM],
419      TEMPDELTAL[0],
420      Gtime[0],
421      Gtime_E[0], //current time for emulsion's mass flow meter
422
423      EMULIN[NUM],
424      TEMPDELTAL_E[0],
425      TEMPSTEP_E[0],
426
427      WATERREC_ST9[0],
428      OILREC_ST9[0],
429      MANUAL_TEST_TUBE[0],
430
431      WATERFLOODINJ[NUM],
432
433 // Emulsion flooding
434      RECEMUL[NUM],
435      OILREC_ST14[0],
436
437 // Atrenate emulsion flooding
438
439      RECEMUL_ALT[0],
440      OILREC_ALT[0],
441
442 //BPR #1
443      BPR11[NUM], //fmeasure
444      BPR12[NUM],
445      BPR13[NUM],
446      BPR14[NUM],
447      BPR15[NUM],
448      BPR16[NUM],
449      BPR17[NUM],
450      BPR18[NUM],
451      MATRIX[NUM], //extra
452
453      ZEROTP2[0],
454      ZERODP1[0],
455      ZEROTP1[0],
456
457      ZEROCP11[0],
458      ZEROCP12[0],
459      ZEROCP13[0],
460      ZEROCP14[0],
461      ZEROCP15[0],
462
463      ZEROCP21[0],
464      ZEROCP22[0],
465      ZEROCP23[0],
466      ZEROCP24[0],
467      ZEROCP25[0],
468
469      ZEROCP31[0],
470      ZEROCP32[0],
471      ZEROCP33[0],
472      ZEROCP34[0],
473      ZEROCP35[0],
474
475      G_WATERINJ[0],
476      G_OILLINJ[0],
477      G_EMULINJ[0],
478
479      WATERINJ[0],
480      WATERINJ2[0],
481      OILINJ[0],
482      EMULINJ[0],
483
484      WATERINJPV[0],
485      WATERINJ2PV[0],

```

```

486     OILINJPV[NUM],
487     EMULINJPV[NUM],
488
489     OUTLET[NUM],
490
491     PV[NUM],
492
493     SWI[NUM],
494
495     PERMWATERDP1[NUM],
496     PERMOILDPI1[NUM],
497     PERMEMULDPI1[NUM],
498
499     PERMWATERDELTA[NUM],
500     PERMOILDELTA[NUM],
501     PERMEMULDELTA[NUM],
502
503     BPR1TEMP[NUM],
504     Delta[NUM];
505
506 double VIS_WATER, VIS_OIL, VIS_EMUL;
507
508 // IMAQmx
509
510 int wholeNum, decNum;
511
512 /*-----
513 /* Internal function prototypes
514 */
515 /*-----*/
516 void Init(void);           // Init some parameters
517 void LoadConfig(void);    // Load config variables from a file
518 void SaveConfig(int type); // Save config vars to a file
519 void LoadVars(void);
520 void SaveVars(void);
521 void MainPanelQuit(void); // Main panel Quit
522 void LogFileHeader(void);
523 voidLogFile(void);
524 void UpdateGraphics(void);
525 void EMG_STOP(int enable); //Emergency stop mode
526 void BLINK(void);
527
528
529 void GeoMath(void);
530
531 void GraphSetup(void);
532 void GraphName(int Val, int GRAPH, int L1, int T1, int L2, int T2,
533                           int L3, int T3, int L4, int T4); // Put names on the graphs
534 void Graph(void);
535 void Graph_Select(int plotVar, int Panel_Graph);
536
537 void DSN_Run_DAQ(void);
538 void DSN_SHIFT_DAQ(void);
539 // void DSN_SHIFT_MASS(void);
540
541 void DSN_SHIFT_MASS(int instrument);
542
543
544 void DSN_SHIFT_Slow(int instrument);
545 void SHIFT_M1(void);
546 void SHIFT_M2(void);
547 void SHIFT_M3(void);
548 void SHIFT_M4(void);
549 void SHIFT_BPR1(void);
550
551
552
553 void DisplayRS232Error (void);
554 void DisplayHelp (int);
555
556 void EnablePumpPanelControls (int);
557 void DisplayComStatus (void);
558
559 //used already
560 void SetConfigParms (void);
561 void GetConfigParms (void);
562
563 void COM1_OPEN(void);
564 void COM2_OPEN(void);
565 void COM3_OPEN(void);
566
567 void ActivatePump1 (void);
568 void ActivatePump2 (void);
569 void ActivatePump3 (void);
570
571 void SNFRP_1 (void);
572
573 void LiquidsInj(void);
574 void vispermunit(void);
575 void Perm(void);
576
577 void P1_GetConfig (void);
578 void P2_GetConfig (void);
579 void P3_GetConfig (void);
580
581 void SendReadPump (void);
582 void SendReadPumpUPGRADE (void); //for pressure recording

```

```

583 void SetPumpFlowrate(void);
584 void CheckPressurePump1 (void);
585 void CheckPressurePump2 (void);
586 void CheckPressurePump3 (void);
587
588 void READ_FLOW_M_1(void);
589 void READ_FLOW_M_2(void);
590 void READ_FLOW_M_3(void);
591 void READ_FLOW_M_4(void);
592 void READ_BFR(void);
593
594 void SWITCHSOLENOID (void);
595 void SWITCHFRACTION (int channel1, int channel2, int channel3, int channel4);
596 void ThreadsRun (void);
597 void STOPPUMPS (void);
598 void STOPPUMPSSUB (void);
599 void STAGES_1_5 (void);
600 void STAGES_6_10 (void);
601 void STAGES_11_16 (void);
602
603 //Camera
604 void DSN_Init_Image(int panelHandle);           // Initilize frame for image
605 void DSN_Init_Camera(void);
606 void DeInit_Camera(void);
607 void DisplayError(IMAQdxError error);           // Defining error function DisplayError
608 void UpdateAttributeTab(void);
609 void Capture(void);
610 void SetMaxPressure(void);
611 void SetMinPressure(void);
612
613 int value;
614
615 //static int popHandle;                         // Pop-up Panel variable
616
617
618

```

```

1  /*-----*/
2  /* Include files */
3  /*-----*/
4  #include "toolbox.h"
5  #include <analysis.h>
6  #include <utility.h>
7  #include <ansi_c.h>
8  #include <cvirte.h>
9  #include <userint.h>
10 #include "Quadrise MCP.h"
11 #include "Quadrise MCP_Declare.h"
12 #include <ddesupp.h>
13 #include <rs232.h>
14 #include <formatio.h>
15 #include <string.h>
16 #include <NIDAQmx.h>           //cDAQ
17 #include <DAQmxIOCtrl.h>        //cDAQ
18 #include <nivision.h>
19 #include <NIIMAQdx.h>
20
21 int read_flag=0;
22 int OVERPRES=1;
23 // int error, Flag, Manual, Auto; //used to be before, NIIMAQdx was added
24 int error, Flag, Manual, Auto;
25 int pi=3.141593;
26
27 // DAQ MX
28
29 static Image* image=NULL;
30
31 #define DAQmxErrChk(functionCall) if( DAQmxFailed(error=(functionCall)) ) goto Error; else //DAQmx
32
33 // DAQ Globals
34 int32 DAQerror=0;
35 TaskHandle taskHandle=0;
36 char chan[256];
37 int32 DAQrate;
38 UInt32 DAQsampsPerChan;
39 int32 DAQnumRead;
40 UInt32 DAQnumChannels;
41 float64 *DAQdata=NULL;
42 float64 *DAQArray_Out=NULL;
43 int DAQlog;
44 char DAQerrBuff[2048]={'\0'};
45 double DAQoutMean=0;
46 int DAQ_Task_Started=0;
47
48 /*-----*/
49 /* This is the application's entry-point. */
50 // main : MCP main function
51 /*-----*/
52 int main (int argc, char *argv[])
53 {
54     if (InitCVIRTE (0, argv, 0) == 0)
55         return -1; /* out of memory */
56     if ((panel_handle = LoadPanel (0, "Quadrise MCP.uir", MAIN)) < 0)
57         return -1;
58
59 // Set the panel variables
60
61     config_handle = LoadPanel (0, "Quadrise MCP.uir", CONFIG);
62     s_handle = LoadPanel (0, "Quadrise MCP.uir", SAVE_con);
63     a_handle = LoadPanel (0, "Quadrise MCP.uir", ABOUT);
64     g_handle = LoadPanel (0, "Quadrise MCP.uir", G_SETUP);
65     extra_g_handle = LoadPanel (0, "Quadrise MCP.uir", EXTRA_G);
66     sat_handle = LoadPanel (0, "Quadrise MCP.uir", SAT); //Panel to enter saturation
67     panelHandle = LoadPanel (0, "Quadrise MCP.uir", PANEL); //Panel for camera settings
68     pressure_handle = LoadPanel (0, "Quadrise MCP.uir", PRESSURE);
69     pumpservice_handle = LoadPanel (0, "Quadrise MCP.uir", PUMP_SER);
70
71 //setup DAQmx
72     SetCtrlAttribute(config_handle,CONFIG_SOL_DECORATION,ATTR_FRAME_COLOR,VAL_RED);
73
74     NIDAQmx_NewPhysChanDOLineCtrl(config_handle,CONFIG_SOLCHANNEL,1);
75     NIDAQmx_NewPhysChanDOLineCtrl(config_handle,CONFIG_SOLCHANNEL_2,1);
76
77
78     DisplayPanel (panel_handle);
79     Init(); //initial initialization for program
80
81     SetSleepPolicy (VAL_SLEEP_MORE); // Use SetSleepPolicy to set the amount your program sleeps when LabWindows/CVI checks for events.
82                                         // The default policy is VAL_SLEEP_MORE
83
84     RunUserInterface ();
85     DiscardPanel (panel_handle);
86     CloseCVIRTE ();
87     return 0;
88 }
89
90 //***** */
91 // Init : Init some variable and do some setup
92 // build based on DSN_Init
93 //***** */
94 void Init()
95 {

```

```

97 // Initialize variables
98 Just_Grabbed = 1; //using for first time running
99 Just_Opened = 1; //using for first time running
100 Is_Log = 0;
101 wholeNum=1;
102 decNum=1;
103
104 // Is_Start_Stop = 0;
105 bpr_set_was0;
106 SAMPLES = 0;
107 Onoff_G1 = 1;
108 Onoff_G2 = 1;
109 OnOff_G3 = 1;
110 OnOff_G4 = 1;
111 OnOff_G5 = 1;
112 OnOff_G6 = 1;
113 OnOff_G6 = 1;
114
115 SETPOINTOUT[0]=930.0;
116 MANUAL_TEST_TUBE[0] = 127;
117 // Run some functions
118 LoadConfig(); //Load configuration file
119 LoadVars(); //Load variables from screen
120 Update_Graphics(); //Update graphics for panels, buttons, etc.
121
122 pumprun_1 = 12;
123 pumprun_2 = 22;
124 pumprun_3 = 32;
125
126 // Do some configuring
127 GraphSetup();
128
129 return;
130 }
131
132 void LoadConfig(void) //build based on DSN_Load_Config(void)
133 {
134 char keyword[50];
135 char value [50];
136 FILE *fp;
137
138 if(Just_Opened == subTRUE)
139 {
140
141     cfgfile[0] = '\0';
142     strcat(cfgfile, "Quadrise MCP.cfg");
143
144 // Set the path to the application directory
145 GetProjectDir (dirname);
146 MakePathname (dirname, cfgfile, pathname);
147 strcpy (cfgfile, pathname);
148 Just_Opened = 0; //second recall of Load Config will know that it's second attempt
149 }
150 else
151 {
152 //selecting the file to save to
153 FileSelectPopup ("", ".cfg", "",
154             "Enter the name of the file to LOAD",
155             VAL_LOAD_BUTTON, 0, 0, 1, 0, cfgfile);
156 }
157
158 //opening the file
159 fp = fopen( cfgfile, "r" );
160 if ( fp == NULL )
161 {
162     MessagePopup ("Config ERROR", "Could not find the config file");
163     return;
164 }
165
166 while( !feof( fp ) )
167 {
168
169     fscanf( fp, "%s\t%s\n", keyword, value );
170
171     //Camera
172     if ( !strcmp( keyword, "Camera_Name" ) )
173         strcpy(camName,value);
174
175 //COM PANEL
176     //COM 1 [Pump#1]
177     else if ( !strcmp( keyword, "P1_comport" ) )
178         P1_comport = (int)atoi( value );
179     else if ( !strcmp( keyword, "P1_baudrate" ) )
180         P1_baudrate = (int)atoi( value );
181     else if ( !strcmp( keyword, "P1_parity" ) )
182         P1_parity = (int)atoi( value );
183     else if ( !strcmp( keyword, "P1_databits" ) )
184         P1_databits = (int)atoi( value );
185     else if ( !strcmp( keyword, "P1_stopbits" ) )
186         P1_stopbits = (int)atoi( value );
187     else if ( !strcmp( keyword, "P1_inputq" ) )
188         P1_inputq = (int)atoi( value );
189     else if ( !strcmp( keyword, "P1_outputq" ) )
190         P1_outputq = (int)atoi( value );
191     else if ( !strcmp( keyword, "P1_ctsmode" ) )
192         P1_ctsmode = (int)atoi( value );
193     else if ( !strcmp( keyword, "P1_xmode" ) )

```

```

194     P1_xmode = (int)atoi( value );
195     else if ( !strcmp( keyword, "P1_timeout" ) )
196         P1_timeout = (double)atoi( value );
197     else if ( !strcmp( keyword, "P1_portindex" ) )
198         P1_portindex = (int)atoi( value );
199
200 //COM 2 [Pump#2]
201     else if ( !strcmp( keyword, "P2_comport" ) )
202         P2_comport = (int)atoi( value );
203     else if ( !strcmp( keyword, "P2_baudrate" ) )
204         P2_baudrate = (int)atoi( value );
205     else if ( !strcmp( keyword, "P2_parity" ) )
206         P2_parity = (int)atoi( value );
207     else if ( !strcmp( keyword, "P2_databits" ) )
208         P2_databits = (int)atoi( value );
209     else if ( !strcmp( keyword, "P2_stopbits" ) )
210         P2_stopbits = (int)atoi( value );
211     else if ( !strcmp( keyword, "P2_inputq" ) )
212         P2_inputq = (int)atoi( value );
213     else if ( !strcmp( keyword, "P2_outputq" ) )
214         P2_outputq = (int)atoi( value );
215     else if ( !strcmp( keyword, "P2_ctsmode" ) )
216         P2_ctsmode = (int)atoi( value );
217     else if ( !strcmp( keyword, "P2_xmode" ) )
218         P2_xmode = (int)atoi( value );
219     else if ( !strcmp( keyword, "P2_timeout" ) )
220         P2_timeout = (double)atoi( value );
221     else if ( !strcmp( keyword, "P2_portindex" ) )
222         P2_portindex = (int)atoi( value );
223
224 //COM 3 [Pump#3]
225     else if ( !strcmp( keyword, "P3_comport" ) )
226         P3_comport = (int)atoi( value );
227     else if ( !strcmp( keyword, "P3_baudrate" ) )
228         P3_baudrate = (int)atoi( value );
229     else if ( !strcmp( keyword, "P3_parity" ) )
230         P3_parity = (int)atoi( value );
231     else if ( !strcmp( keyword, "P3_databits" ) )
232         P3_databits = (int)atoi( value );
233     else if ( !strcmp( keyword, "P3_stopbits" ) )
234         P3_stopbits = (int)atoi( value );
235     else if ( !strcmp( keyword, "P3_inputq" ) )
236         P3_inputq = (int)atoi( value );
237     else if ( !strcmp( keyword, "P3_outputq" ) )
238         P3_outputq = (int)atoi( value );
239     else if ( !strcmp( keyword, "P3_ctsmode" ) )
240         P3_ctsmode = (int)atoi( value );
241     else if ( !strcmp( keyword, "P3_xmode" ) )
242         P3_xmode = (int)atoi( value );
243     else if ( !strcmp( keyword, "P3_timeout" ) )
244         P3_timeout = (double)atoi( value );
245     else if ( !strcmp( keyword, "P3_portindex" ) )
246         P3_portindex = (int)atoi( value );
247
248 // GRAPH PANEL
249 // Graph #1
250     else if ( !strcmp( keyword, "plotVar_G_1" ) )
251         plotVar_G_1 = (int)atoi( value );
252     else if ( !strcmp( keyword, "X_Range_G_1" ) )
253         X_Range_G_1 = (float)atof( value );
254     else If ( !strcmp( keyword, "Y_Mode_G_1" ) )
255         Y_Mode_G_1 = (int)atoi( value );
256     else If ( !strcmp( keyword, "Y_Min_G_1" ) )
257         Y_Min_G_1 = (float)atof( value );
258     else If ( !strcmp( keyword, "Y_Max_G_1" ) )
259         Y_Max_G_1 = (float)atof( value );
260 // Graph #2
261     else if ( !strcmp( keyword, "plotVar_G_2" ) )
262         plotVar_G_2 = (int)atoi( value );
263     else if ( !strcmp( keyword, "X_Range_G_2" ) )
264         X_Range_G_2 = (float)atof( value );
265     else If ( !strcmp( keyword, "Y_Mode_G_2" ) )
266         Y_Mode_G_2 = (int)atoi( value );
267     else If ( !strcmp( keyword, "Y_Min_G_2" ) )
268         Y_Min_G_2 = (float)atof( value );
269     else If ( !strcmp( keyword, "Y_Max_G_2" ) )
270         Y_Max_G_2 = (float)atof( value );
271 // Graph #3
272     else if ( !strcmp( keyword, "plotVar_G_3" ) )
273         plotVar_G_3 = (int)atoi( value );
274     else if ( !strcmp( keyword, "X_Range_G_3" ) )
275         X_Range_G_3 = (float)atof( value );
276     else If ( !strcmp( keyword, "Y_Mode_G_3" ) )
277         Y_Mode_G_3 = (int)atoi( value );
278     else If ( !strcmp( keyword, "Y_Min_G_3" ) )
279         Y_Min_G_3 = (float)atof( value );
280     else If ( !strcmp( keyword, "Y_Max_G_3" ) )
281         Y_Max_G_3 = (float)atof( value );
282 // Graph #4
283     else if ( !strcmp( keyword, "plotVar_G_4" ) )
284         plotVar_G_4 = (int)atoi( value );
285     else if ( !strcmp( keyword, "X_Range_G_4" ) )
286         X_Range_G_4 = (float)atof( value );
287     else If ( !strcmp( keyword, "Y_Mode_G_4" ) )
288         Y_Mode_G_4 = (int)atoi( value );
289     else If ( !strcmp( keyword, "Y_Min_G_4" ) )
290         Y_Min_G_4 = (float)atof( value );

```

```

291     else if ( !strcmp( keyword, "Y_Max_G_4" ) )
292         Y_Max_G_4 = (float)atof( value );
293
294     // Graph #5
295     else if ( !strcmp( keyword, "plotVar_G_5" ) )
296         plotVar_G_5 = (int)atoi( value );
297     else if ( !strcmp( keyword, "X_Mode_G_5" ) )
298         X_Mode_G_5 = (int)atoi( value );
299     else If ( !strcmp( keyword, "X_Min_G_5" ) )
300         X_Min_G_5 = (float)atof( value );
301     else If ( !strcmp( keyword, "X_Max_G_5" ) )
302         X_Max_G_5 = (float)atof( value );
303     else If ( !strcmp( keyword, "Y_Mode_G_5" ) )
304         Y_Mode_G_5 = (int)atoi( value );
305     else If ( !strcmp( keyword, "Y_Min_G_5" ) )
306         Y_Min_G_5 = (float)atof( value );
307     else If ( !strcmp( keyword, "Y_Max_G_5" ) )
308         Y_Max_G_5 = (float)atof( value );
309
310
311     // Equipment Setup
312     else if ( !strcmp( keyword, "Exp_Type" ) )
313         Exp_Type = (int)atoi( value );
314
315     //Logging Variables
316     else if ( !strcmp( keyword, "Is_P1" ) )
317         Is_P1 = (int)atoi( value );
318     else If ( !strcmp( keyword, "Is_P2" ) )
319         Is_P2 = (int)atoi( value );
320     else If ( !strcmp( keyword, "Is_P3" ) )
321         Is_P3 = (int)atoi( value );
322     else If ( !strcmp( keyword, "Is_M1" ) )
323         Is_M1 = (int)atoi( value );
324     else If ( !strcmp( keyword, "Is_M2" ) )
325         Is_M2 = (int)atoi( value );
326     else If ( !strcmp( keyword, "Is_M3" ) )
327         Is_M3 = (int)atoi( value );
328     else If ( !strcmp( keyword, "Is_M4" ) )
329         Is_M4 = (int)atoi( value );
330     else If ( !strcmp( keyword, "Is_PRES" ) )
331         Is_PRES = (int)atoi( value );
332     else If ( !strcmp( keyword, "Is_BPR" ) )
333         Is_BPR = (int)atol( value );
334     else If ( !strcmp( keyword, "Is_Graph" ) )
335         Is_Graph = (int)atoi( value );
336     else If ( !strcmp( keyword, "Is_DAQ" ) )
337         Is_DAQ = (int)atol( value );
338     else If ( !strcmp( keyword, "Is_Log" ) )
339         Is_Log = (int)atoi( value );
340
341     //pressure reading error
342     else if ( !strcmp(keyword, "ZEROTP2" ) )
343         ZEROTP2[0] = (double)atof( value );
344     else if ( !strcmp(keyword, "ZERODP1" ) )
345         ZERODP1[0] = (double)atof( value );
346     else If ( !strcmp(keyword, "ZEROTP1" ) )
347         ZEROTP1[0] = (double)atof( value );
348
349     else if ( !strcmp(keyword, "ZEROCP11" ) )
350         ZEROCP11[0] = (double)atof( value );
351     else If ( !strcmp(keyword, "ZEROCP12" ) )
352         ZEROCP12[0] = (double)atof( value );
353     else If ( !strcmp(keyword, "ZEROCP13" ) )
354         ZEROCP13[0] = (double)atof( value );
355     else If ( !strcmp(keyword, "ZEROCP14" ) )
356         ZEROCP14[0] = (double)atof( value );
357     else If ( !strcmp(keyword, "ZEROCP15" ) )
358         ZEROCP15[0] = (double)atof( value );
359
360     else If ( !strcmp(keyword, "ZEROCP21" ) )
361         ZEROCP21[0] = (double)atof( value );
362     else If ( !strcmp(keyword, "ZEROCP22" ) )
363         ZEROCP22[0] = (double)atof( value );
364     else If ( !strcmp(keyword, "ZEROCP23" ) )
365         ZEROCP23[0] = (double)atof( value );
366     else If ( !strcmp(keyword, "ZEROCP24" ) )
367         ZEROCP24[0] = (double)atof( value );
368     else If ( !strcmp(keyword, "ZEROCP25" ) )
369         ZEROCP25[0] = (double)atof( value );
370
371     else If ( !strcmp(keyword, "ZEROCP31" ) )
372         ZEROCP31[0] = (double)atof( value );
373     else If ( !strcmp(keyword, "ZEROCP32" ) )
374         ZEROCP32[0] = (double)atof( value );
375     else If ( !strcmp(keyword, "ZEROCP33" ) )
376         ZEROCP33[0] = (double)atof( value );
377     else If ( !strcmp(keyword, "ZEROCP34" ) )
378         ZEROCP34[0] = (double)atof( value );
379     else If ( !strcmp(keyword, "ZEROCP35" ) )
380         ZEROCP35[0] = (double)atof( value );
381
382
383
384     //restore last injection
385     else If ( !strcmp(keyword, "G_WATERINJ" ) )
386         G_WATERINJ[0] = (double)atof( value );
387     else If ( !strcmp(keyword, "G_OILINJ" ) )

```

```

388     G_OILINJ[0] = (double)atof (value);
389     else if ( !strcmp(keyword, "G_EMULINJ" ) )
390         G_EMULINJ[0] = (double)atof (value);
391
392     else if ( !strcmp(keyword, "OUTLET" ) )
393         OUTLET[0] = (double)atof (value);
394
395     else if ( !strcmp( keyword, "VIS_WATER" ) )
396         VIS_WATER = (double)atoi( value );
397     else if ( !strcmp( keyword, "VIS_OIL" ) )
398         VIS_OIL = (double)atoi( value );
399     else if ( !strcmp( keyword, "VIS_EMUL" ) )
400         VIS_EMUL = (double)atoi( value );
401
402     else if ( !strcmp( keyword, "viscoef" ) )
403         viscoef = (double)atoi( value );
404     else if ( !strcmp( keyword, "permcoef" ) )
405         permcoef = (double)atoi( value );
406
407     else
408         MessagePopup ("Missed Data ", keyword);
409     } //While
410
411     fclose( fp );
412     return;
413 }
414
415 void SaveConfig(int type) //build based on DSN_Save_Config(int type)
416 {
417     //int i, value2;
418     //double value;
419     FILE *fp;
420
421     if(type)
422     {
423         //selecting the file to save to
424         FileSelectPopup ("", "*.cfg", "", "Enter the name of the file to save",
425                         VAL_SAVE_BUTTON, 0, 0, 1, 1, cfgfile);
426         fp = fopen( cfgfile, "w" );
427     }
428
429     else
430     fp = fopen( pathname, "w" );
431     //Camera
432     fprintf( fp, "Camera_Name\t%s\n", camName);
433
434 //COM PANEL
435 //COM 1 [Pump#1]
436     fprintf( fp, "P1_comport\t%i\n", P1_comport);
437     fprintf( fp, "P1_baudrate\t%i\n", P1_baudrate);
438     fprintf( fp, "P1_parity\t%i\n", P1_parity);
439     fprintf( fp, "P1.databits\t%i\n", P1.databits);
440     fprintf( fp, "P1_stopbits\t%i\n", P1_stopbits);
441     fprintf( fp, "P1_inputq\t%i\n", P1_inputq);
442     fprintf( fp, "P1_outputq\t%i\n", P1_outputq);
443     fprintf( fp, "P1_ctsmode\t%i\n", P1_ctsmode);
444     fprintf( fp, "P1_xmode\t%i\n", P1_xmode);
445     fprintf( fp, "P1_timeout\t%f\n", P1_timeout);
446     fprintf( fp, "P1_portindex\t%i\n", P1_portindex);
447
448 //COM 2 [Pump#2]
449     fprintf( fp, "P2_comport\t%i\n", P2_comport);
450     fprintf( fp, "P2_baudrate\t%i\n", P2_baudrate);
451     fprintf( fp, "P2_parity\t%i\n", P2_parity);
452     fprintf( fp, "P2.databits\t%i\n", P2.databits);
453     fprintf( fp, "P2_stopbits\t%i\n", P2_stopbits);
454     fprintf( fp, "P2_inputq\t%i\n", P2_inputq);
455     fprintf( fp, "P2_outputq\t%i\n", P2_outputq);
456     fprintf( fp, "P2_ctsmode\t%i\n", P2_ctsmode);
457     fprintf( fp, "P2_xmode\t%i\n", P2_xmode);
458     fprintf( fp, "P2_timeout\t%f\n", P2_timeout);
459     fprintf( fp, "P2_portindex\t%i\n", P2_portindex);
460
461 //COM 3 [Pump#3]
462     fprintf( fp, "P3_comport\t%i\n", P3_comport);
463     fprintf( fp, "P3_baudrate\t%i\n", P3_baudrate);
464     fprintf( fp, "P3_parity\t%i\n", P3_parity);
465     fprintf( fp, "P3.databits\t%i\n", P3.databits);
466     fprintf( fp, "P3_stopbits\t%i\n", P3_stopbits);
467     fprintf( fp, "P3_inputq\t%i\n", P3_inputq);
468     fprintf( fp, "P3_outputq\t%i\n", P3_outputq);
469     fprintf( fp, "P3_ctsmode\t%i\n", P3_ctsmode);
470     fprintf( fp, "P3_xmode\t%i\n", P3_xmode);
471     fprintf( fp, "P3_timeout\t%f\n", P3_timeout);
472     fprintf( fp, "P3_portindex\t%i\n", P3_portindex);
473
474 // GRAPH PANEL
475 // Graph #1
476     fprintf( fp, "plotVar_G_1\t%i\n", plotVar_G_1);
477     fprintf( fp, "X_Range_G_1\t%f\n", X_Range_G_1);
478     fprintf( fp, "Y_Mode_G_1\t%i\n", Y_Mode_G_1);
479     fprintf( fp, "Y_Min_G_1\t%f\n", Y_Min_G_1);
480     fprintf( fp, "Y_Max_G_1\t%f\n", Y_Max_G_1);
481 // Graph #2
482     fprintf( fp, "plotVar_G_2\t%i\n", plotVar_G_2);
483     fprintf( fp, "X_Range_G_2\t%f\n", X_Range_G_2);
484     fprintf( fp, "Y_Mode_G_2\t%i\n", Y_Mode_G_2);

```

```

485     fprintf( fp, "Y_Min_G_2\t%f\n", Y_Min_G_2);
486     fprintf( fp, "Y_Max_G_2\t%f\n", Y_Max_G_2);
487 // Graph #3
488     fprintf( fp, "plotVar_G_3\t%i\n", plotVar_G_3);
489     fprintf( fp, "X_Range_G_3\t%f\n", X_Range_G_3);
490     fprintf( fp, "Y_Mode_G_3\t%i\n", Y_Mode_G_3);
491     fprintf( fp, "Y_Min_G_3\t%f\n", Y_Min_G_3);
492     fprintf( fp, "Y_Max_G_3\t%f\n", Y_Max_G_3);
493 // Graph #4
494     fprintf( fp, "plotVar_G_4\t%i\n", plotVar_G_4);
495     fprintf( fp, "X_Range_G_4\t%f\n", X_Range_G_4);
496     fprintf( fp, "Y_Mode_G_4\t%i\n", Y_Mode_G_4);
497     fprintf( fp, "Y_Min_G_4\t%f\n", Y_Min_G_4);
498     fprintf( fp, "Y_Max_G_4\t%f\n", Y_Max_G_4);
499
500 // Equipment Setup
501     fprintf( fp, "Exp_Type\t%i\n", Exp_Type);
502
503 //Logging Variables
504     fprintf( fp, "Is_P1\t%i\n", Is_P1);
505     fprintf( fp, "Is_P2\t%i\n", Is_P2);
506     fprintf( fp, "Is_P3\t%i\n", Is_P3);
507     fprintf( fp, "Is_M1\t%i\n", Is_M1);
508     fprintf( fp, "Is_M2\t%i\n", Is_M2);
509     fprintf( fp, "Is_M3\t%i\n", Is_M3);
510     fprintf( fp, "Is_M4\t%i\n", Is_M4);
511     fprintf( fp, "Is_PRES\t%i\n", Is_PRES);
512     fprintf( fp, "Is_BPR\t%i\n", Is_BPR);
513     fprintf( fp, "Is_Graph\t%i\n", Is_Graph);
514     fprintf( fp, "Is_DAQ\t%i\n", Is_DAQ);
515     fprintf( fp, "Is_Log\t%i\n", Is_Log);
516
517     fprintf( fp, "ZEROOTP2\t%f\n", ZEROOTP2[0]); //upstream
518     fprintf( fp, "ZERODP1\t%f\n", ZERODP1[0]);
519     fprintf( fp, "ZEROOTP1\t%f\n", ZEROOTP1[0]); //downstream
520
521     fprintf( fp, "ZEROCP11\t%f\n", ZEROCP11[0]);
522     fprintf( fp, "ZEROCP12\t%f\n", ZEROCP12[0]);
523     fprintf( fp, "ZEROCP13\t%f\n", ZEROCP13[0]);
524     fprintf( fp, "ZEROCP14\t%f\n", ZEROCP14[0]);
525     fprintf( fp, "ZEROCP15\t%f\n", ZEROCP15[0]);
526
527     fprintf( fp, "ZEROCP21\t%f\n", ZEROCP21[0]);
528     fprintf( fp, "ZEROCP22\t%f\n", ZEROCP22[0]);
529     fprintf( fp, "ZEROCP23\t%f\n", ZEROCP23[0]);
530     fprintf( fp, "ZEROCP24\t%f\n", ZEROCP24[0]);
531     fprintf( fp, "ZEROCP25\t%f\n", ZEROCP25[0]);
532
533     fprintf( fp, "ZEROCP31\t%f\n", ZEROCP31[0]);
534     fprintf( fp, "ZEROCP32\t%f\n", ZEROCP32[0]);
535     fprintf( fp, "ZEROCP33\t%f\n", ZEROCP33[0]);
536     fprintf( fp, "ZEROCP34\t%f\n", ZEROCP34[0]);
537     fprintf( fp, "ZEROCP35\t%f\n", ZEROCP35[0]);
538
539
540     fprintf( fp, "G_WATERINJ\t%f\n", G_WATERINJ[1]);
541     fprintf( fp, "G_OILINJ\t%f\n", G_OILINJ[1]);
542     fprintf( fp, "G_EMULINJ\t%f\n", G_EMULINJ[1]);
543
544     fprintf( fp, "OUTLET\t%f\n", OUTLET[1]);
545
546     fprintf( fp, "VIS_WATER\t%f\n", VIS_WATER);
547     fprintf( fp, "VIS_OIL\t%f\n", VIS_OIL);
548     fprintf( fp, "VIS_EMUL\t%f\n", VIS_EMUL);
549
550     fprintf( fp, "viscoef\t%f\n", viscoef);
551     fprintf( fp, "permcoef\t%f\n", permcoef);
552
553 fclose( fp );
554 return;
555 }
556
557 void EnableP1PanelControls (int enable) /* PUMP #1 buttons activation */
558 {
559 //pump
560     SetCtrlAttribute (panel_handle, MAIN_WAS_FR_P_1, ATTR_DIMMED, enable);
561     SetCtrlAttribute (panel_handle, MAIN_P1_START, ATTR_DIMMED, enable);
562     SetCtrlAttribute (panel_handle, MAIN_P1_STOP, ATTR_DIMMED, enable);
563     SetCtrlAttribute (panel_handle, MAIN_P1_PURGE, ATTR_DIMMED, enable);
564     SetCtrlAttribute (panel_handle, MAIN_P1_RESTART, ATTR_DIMMED, enable);
565     SetCtrlAttribute (panel_handle, MAIN_P1_SERR, ATTR_DIMMED, enable);
566     SetCtrlAttribute (panel_handle, MAIN_P1_SET_NFR, ATTR_DIMMED, enable);
567     SetCtrlAttribute (panel_handle, MAIN_P1_SNFR, ATTR_DIMMED, enable);
568     SetCtrlAttribute (panel_handle, MAIN_STATUS_P_1, ATTR_DIMMED, enable);
569     SetCtrlAttribute (panel_handle, MAIN_P1_TEXTMSG, ATTR_DIMMED, enable);
570 }
571
572 void EnableMassTurnControls (int enable) /* Allow user Connect|Disconnect with Mass flow meters */
573 {
574     SetCtrlAttribute (config_handle, CONFIG_CON_M_1, ATTR_DIMMED, enable);
575     SetCtrlAttribute (config_handle, CONFIG_CON_M_2, ATTR_DIMMED, enable);
576     SetCtrlAttribute (config_handle, CONFIG_CON_M_3, ATTR_DIMMED, enable);
577     SetCtrlAttribute (config_handle, CONFIG_CON_M_4, ATTR_DIMMED, enable);
578     SetCtrlAttribute (config_handle, CONFIG_CON_BPR, ATTR_DIMMED, enable);
579 }
580
581 void EnableM1PanelControls (int enable) /* MASS FLOW METER #1 buttons activation */

```



```

679          {
680              outqlen = GetOutQLen (P1_comport);
681              if (outqlen > 0)
682              {
683                  MessagePopup ("RS232 Message", "The output queue has\n"
684                               "data in it. Wait for device to receive\n"
685                               "the data or flush the queue.\n");
686                  break;
687              }
688              RS232Error = CloseCom (P1_comport);
689              if (RS232Error)
690                  DisplayRS232Error ();
691              SetCtrlVal (config_handle, CONFIG_P1_LED, 0);
692              SetCtrlVal (panel_handle, MAIN_P1_LED, 0);
693              SetCtrlAttribute (panel_handle, MAIN_WATER, ATTR_DIMMED, 1); //turn off dimmed status
694
695              P1_port_open=0;
696          }
697          else MessagePopup ("COM1 Port Message", "There was no open connection.");
698      }
699      break;
700  case EVENT_RIGHT_CLICK:
701      break;
702  }
703 return 0;
704}
705
706 //-----
707 // COM1_OPEN      : Opens the com #1 port
708 //-----
709
710 void COM1_OPEN(void)
711 { int test;
712
713     P1_GetConfig();
714
715     P1_port_open = 1; /* initialize flag to 0 - unopened */
716     GetConfigParms ();
717     DisableBreakOnLibraryErrors ();
718     RS232Error = OpenComConfig (P1_comport, "", P1_baudrate, P1_parity,
719                                P1_databits, P1_stopbits, P1_inputq, P1_outputq);
720     SetCtrlVal (config_handle, CONFIG_NUM, RS232Error); // show up RS232 error
721     EnableBreakOnLibraryErrors ();
722
723     if (RS232Error) DisplayRS232Error ();
724     if (RS232Error == 0)
725     {
726         P1_port_open = 1;
727         SetCtrlVal (config_handle, CONFIG_NUM, P1_port_open);
728
729         GetCtrlVal (config_handle, CONFIG_P1_XMODE, &P1_xmode);
730         SetXMode (P1_comport, P1_xmode);
731
732         GetCtrlVal (config_handle, CONFIG_P1_CTSMODE, &P1_ctsmode);
733         SetCTSMODE (P1_comport, P1_ctsmode);
734
735         GetCtrlVal (config_handle, CONFIG_P1_TIMEOUT, &P1_timeout);
736         SetComTime (P1_comport, P1_timeout);
737
738     }
739
740
741     if (P1_port_open)
742     {
743         SetCtrlAttribute (config_handle, CONFIG_P1_LED, ATTR_DIMMED, 0);
744
745         test=1; // show that COM #1 was opened
746         if(test)
747         {
748             SetCtrlVal (config_handle, CONFIG_P1_LED, 1);
749             SetCtrlVal (panel_handle, MAIN_P1_LED, 1);
750             SetCtrlAttribute (panel_handle, MAIN_WATER, ATTR_DIMMED, 0);
751         }
752     }
753     else
754     {
755         SetCtrlVal (config_handle, CONFIG_P1_LED, 0);
756         SetCtrlVal (panel_handle, MAIN_P1_LED, 0);
757         SetCtrlAttribute (panel_handle, MAIN_WATER, ATTR_DIMMED, 1);
758     }
759 }
760
761 return;
762}
763
764 void P1_GetConfig (void)
765 {
766     GetConfigParms ();
767     #ifdef NI_unix_
768         P1_devicename[0]=0;
769     #else
770         GetLabelFromIndex (config_handle, CONFIG_P1_COMPORT, P1_portindex,
771                           P1_devicename);
772     #endif
773 }
774
775 // COM#2 //

```

```

776 int CVICALLBACK Pump2ConfigCallback (int panel, int control, int event,
777     void *callbackData, int eventData1, int eventData2)
778 {
779     switch (event)
780     {
781         case EVENT_COMMIT: //sitting at COM3 (inside the program, read as COM2)
782             GetCtrlVal(config_handle, CONFIG_P2, &p2check);
783             if (p2check == 1) COM2_OPEN();
784             else
785             {
786                 if (P2_port_open)
787                 {
788                     outqlen = GetOutQLen (P2_comport);
789                     if (outqlen > 0)
790                     {
791                         MessagePopup ("RS232 Message", "The output queue has\n"
792                             "data in it. Wait for device to receive\n"
793                             "the data or flush the queue.\n");
794                     }
795                     RS232Error = CloseCom (P2_comport);
796                     if (RS232Error)
797                         DisplayRS232Error ();
798                     SetCtrlVal (config_handle, CONFIG_P2_LED, 0);
799                     SetCtrlVal (panel_handle, MAIN_P2_LED, 0);
800                     SetCtrlAttribute (panel_handle, MAIN_OIL, ATTR_DIMMED, 1);
801
802                     P2_port_open=0;
803                 }
804                 else MessagePopup ("COM2 Port Message", "There was no open connection.");
805             }
806             break;
807         case EVENT_RIGHT_CLICK:
808             break;
809     }
810     return 0;
811 }
812
813
814 //-----
815 // COM2_OPEN : Opens the com #2 port
816 //-----
817
818 void COM2_OPEN(void)
819 {
820     int test;
821
822     P2_GetConfig();
823
824     P2_port_open = 1; /* initialize flag to 0 - unopened */
825     GetConfigParams ();
826     DisableBreakOnLibraryErrors ();
827     RS232Error = OpenComConfig (P2_comport, "", P2_baudrate, P2_parity,
828                                 P2_databits, P2_stopbits, P2_inputq, P2_outputq);
829     SetCtrlVal (config_handle, CONFIG_NUM, RS232Error); // show up RS232 error
830     EnableBreakOnLibraryErrors ();
831
832     if (RS232Error) DisplayRS232Error ();
833     if (RS232Error == 0)
834     {
835         P2_port_open = 1;
836         SetCtrlVal (config_handle, CONFIG_NUM, P2_port_open);
837
838         GetCtrlVal (config_handle, CONFIG_P2_XMODE, &P2_xmode);
839         SetXMode (P2_comport, P2_xmode);
840
841         GetCtrlVal (config_handle, CONFIG_P2_CTSMODE, &P2_ctsmode);
842         SetCTSMODE (P2_comport, P2_ctsmode);
843
844         GetCtrlVal (config_handle, CONFIG_P2_TIMEOUT, &P2_timeout);
845         SetComTime (P2_comport, P2_timeout);
846
847     }
848
849
850     if (P2_port_open)
851     {
852         SetCtrlAttribute (config_handle, CONFIG_P2_LED, ATTR_DIMMED, 0);
853
854         test=1; // show that COM #2 was opened
855         if(test)
856         {
857             SetCtrlVal (config_handle, CONFIG_P2_LED, 1);
858             SetCtrlVal (panel_handle, MAIN_P2_LED, 1);
859             SetCtrlAttribute (panel_handle, MAIN_OIL, ATTR_DIMMED, 0);
860         }
861         else
862         {
863             SetCtrlVal (config_handle, CONFIG_P2_LED, 0);
864             SetCtrlVal (panel_handle, MAIN_P2_LED, 0);
865             SetCtrlAttribute (panel_handle, MAIN_OIL, ATTR_DIMMED, 1);
866         }
867     }
868
869     return;
870 }
871
872 void P2_GetConfig (void)

```

```

873     {
874         GetConfigParms();
875
876         #ifdef _NI_unix_
877             P2_devicename[0]=0;
878         #else
879             GetLabelFromIndex (config_handle, CONFIG_P2_COMPORT, P2_portindex,
880                                 P2_devicename);
881         #endif
882     }
883
884 // COM#3 //
885
886 int CVICALLBACK Pump3ConfigCallback (int panel, int control, int event,
887                                     void *callbackData, int eventData1, int eventData2)
888 {
889     switch (event)
890     {
891         case EVENT_COMMIT:          //sitting at COM5  (inside the program, read as COM3)
892             GetCtrlVal(config_handle, CONFIG_P3, &p3check);
893             if (p3check == 1) COM3_OPEN();
894             else
895             {
896                 if (P3_port_open)
897                 {
898                     outqlen = GetOutQLen (P3_comport);
899                     if (outqlen > 0)
900                     {
901                         MessagePopup ("RS232 Message", "The output queue has\n"
902                                         "data in it. Wait for device to receive\n"
903                                         "the data or flush the queue.\n");
904                     }
905                     RS232Error = CloseCom (P3_comport);
906                     if (RS232Error)
907                         DisplayRS232Error ();
908                     SetCtrlVal (config_handle, CONFIG_P3_LED, 0);
909                     SetCtrlVal (panel_handle, MAIN_P3_LED, 0);
910                     SetCtrlAttribute (panel_handle, MAIN_EMULSION, ATTR_DIMMED, 1);
911                     // SetCtrlVal (panel_handle, MAIN_LOG_P3, 1);
912                     P3_port_open=0;
913                 }
914                 else MessagePopup ("COM3 Port Message", "There was no open connection.");
915             }
916             break;
917         case EVENT_RIGHT_CLICK:
918             break;
919     }
920     return 0;
921 }
922
923 //-----
924 // COM3_OPEN      : Opens the com #3 port
925 //-----
926
927 void COM3_OPEN(void)
928 {
929     int test;
930
931     P3_GetConfig();
932
933     P3_port_open = 1; /* initialize flag to 0 - unopened */
934     GetConfigParms ();
935     DisableBreakOnLibraryErrors ();
936     RS232Error = OpenComConfig (P3_comport, "", P3_baudrate, P3_parity,
937                                 P3_databits, P3_stopbits, P3_inputq, P3_outputq);
938     SetCtrlVal (config_handle, CONFIG_NUM, RS232Error); // show up RS232 error
939     EnableBreakOnLibraryErrors ();
940
941     if (RS232Error) DisplayRS232Error ();
942     if (RS232Error == 0)
943     {
944         P3_port_open = 1;
945         SetCtrlVal (config_handle, CONFIG_NUM, P3_port_open);
946
947         GetCtrlVal (config_handle, CONFIG_P3_XMODE, &P3_xmode);
948         SetXMode (P3_comport, P3_xmode);
949
950         GetCtrlVal (config_handle, CONFIG_P3_CTSMODE, &P3_ctsmode);
951         SetCTSMODE (P3_comport, P3_ctsmode);
952
953         GetCtrlVal (config_handle, CONFIG_P3_TIMEOUT, &P3_timeout);
954         SetComTime (P3_comport, P3_timeout);
955
956     }
957
958     if (P3_port_open)
959     {
960         SetCtrlAttribute (config_handle, CONFIG_P3_LED, ATTR_DIMMED, 0);
961
962         test=1; // show that COM #3 was opened
963         if(test)
964         {
965             SetCtrlVal (config_handle, CONFIG_P3_LED, 1);
966             SetCtrlVal (panel_handle, MAIN_P3_LED, 1);
967             SetCtrlAttribute (panel_handle, MAIN_EMULSION, ATTR_DIMMED, 0);
968
969

```

```

970         }
971     }
972     else
973     {
974         SetCtrlVal (config handle, CONFIG_P3_LED, 0);
975         SetCtrlVal (panel_handle, MAIN_P3_LED, 0);
976         SetCtrlAttribute (panel handle, MAIN_EMULSION, ATTR_DIMMED, 1);
977     }
978 }
979 return;
980 }
981
982 void P3_GetConfig (void)
983 {
984     GetConfigParms ();
985
986 #ifdef _NI_unix_
987     P3_devicename[0]=0;
988 #else
989     GetLabelFromIndex (config handle, CONFIG_P3_COMPORT, P3_portindex,
990                         P3_devicename);
991 #endif
992 }
993
994 //***** ****
995 //***** ****
996
997 /*-----*/
998 /* Function send-read command to the pump */
999 /*-----*/
1000
1001 void SendReadPump (void) //function valid for any pump, required comport number.
1002 {
1003
1004     //CP= current comport
1005
1006     FlushOutQ (CP);
1007     FlushInQ (CP);
1008
1009     stringsize = StringLength (send_data);
1010     bytes_sent = ComWrt (CP, send_data, stringsize);
1011     Delay(0.05); /* 0.05 */
1012
1013     read_cnt = GetInQLen (CP);
1014
1015     read_data[0] = '\0';
1016     read_term = 13;
1017     bytes_read = ComRdTerm (CP, read_data, read_cnt, read_term);
1018
1019     CopyString (SRP_read_data, 0, read_data, 0, bytes_read);
1020     SetCtrlVal (panel_name, PTEXT_panel_name, SRP_read_data);
1021
1022     RS232Error = ReturnRS232Err ();
1023     if (RS232Error)
1024         DisplayRS232Error ();
1025
1026     send_data[0] = '\0';
1027
1028 }
1029
1030 void CheckPressurePump1 (void) // part of PumpsThread function. helps update information regarding pressure
1031 {
1032     int i;
1033     double probe_temp, probe_pressure, probe_pressure_psi;
1034     char temp [NUM];
1035 ///////////////
1036     panel_name=panel_handle;
1037     send_data[0] = '\0';
1038     Fmt (send_data, "%sPRESSURE?\r");
1039     CP=P1_comport;
1040     text_panel_name= MAIN_PRESSURE_P_1;
1041 ///////////////
1042
1043     FlushOutQ (CP);
1044     FlushInQ (CP);
1045
1046     stringsize = StringLength (send_data);
1047     bytes_sent = ComWrt (CP, send_data, stringsize);
1048     Delay(0.05); /* 0.05 */
1049
1050     read_cnt = GetInQLen (CP);
1051
1052     read_data[0] = '\0';
1053     read_term = 13;
1054     bytes_read = ComRdTerm (CP, read_data, read_cnt, read_term);
1055
1056     CopyString (tbox_read_data, 0, read_data, 0, bytes_read);
1057
1058     for (i=9; tbox_read_data[i]!='\0';i++) //Return is "Pressure:XX"
1059         temp[i-9]=tbox_read_data[i];
1060         temp[i-9]='\0'; //close by '\0'
1061
1062         probe_pressure = atof(temp) /10 ;
1063         probe_pressure_psi=probe_pressure * 14.5037738;
1064     ProcessSystemEvents ();
1065         SetCtrlVal (panel_name, text_panel_name, probe_pressure_psi);
1066

```

```

1067 CmtGetLock (Pumps_lockHandle);
1068 ///////////////////////////////////////////////////////////////////
1069 DSN_SHIFT_Slow(3); //pump #1
1070
1071 P11[0] = probe_pressure_psi; // Log value in P11 Array
1072 ///////////////////////////////////////////////////////////////////
1073 CmtReleaseLock (Pumps_lockHandle);
1074
1075 RS232Error = ReturnRS232Err ();
1076 if (RS232Error)
1077     DisplayRS232Error ();
1078
1079 send_data[0] = '\0';
1080
1081 }
1082
1083 void CheckPressurePump2 (void) // part of PumpsThread function. helps update information regarding pressure
1084 {
1085 int i;
1086 double probe_temp, probe_pressure, probe_pressure_psi;
1087 char temp [NUM];
1088 ///////////////////////////////////////////////////////////////////
1089 panel_name=panel_handle;
1090 send_data[0] = '\0';
1091 Fmt (send_data, "%s<PRESSURE?\r");
1092 CP=P2_comport;
1093 text_panel_name= MAIN_PRESSURE_P_2;
1094 ///////////////////////////////////////////////////////////////////
1095
1096 FlushOutQ (CP);
1097 FlushInQ (CP);
1098
1099 stringsize = StringLength (send_data);
1100 bytes_sent = ComWrt (CP, send_data, stringsize);
1101 Delay(0.05); /* 0.05 */
1102
1103 read_cnt = GetInQLen (CP);
1104
1105 read_data[0] = '\0';
1106 read_term = 13;
1107 bytes_read = ComRdTerm (CP, read_data, read_cnt, read_term);
1108
1109 CopyString (tbox_read_data, 0, read_data, 0, bytes_read);
1110
1111 for (i=9; tbox_read_data[i]!='\0';i++) //Return is "Pressure:XX"
1112     temp[i-9]=tbox_read_data[i];
1113     temp[i-9]='\0'; //close by '\0'
1114
1115 probe_pressure = atof(temp)/10;
1116 probe_pressure_psi=probe_pressure * 14.5037738;
1117 ProcessSystemEvents ();
1118 SetCtrival (panel_name, text_panel_name, probe_pressure_psi),
1119
1120
1121 CmtGetLock (Pumps_lockHandle);
1122 ///////////////////////////////////////////////////////////////////
1123 DSN_SHIFT_Slow(4); //pump #2
1124
1125 P21[0] = probe_pressure_psi; // Log value in P21 Array
1126 ///////////////////////////////////////////////////////////////////
1127 CmtReleaseLock (Pumps_lockHandle);
1128
1129 RS232Error = ReturnRS232Err ();
1130 if (RS232Error)
1131     DisplayRS232Error ();
1132
1133 send_data[0] = '\0';
1134
1135 }
1136
1137 void CheckPressurePump3 (void) // part of PumpsThread function. helps update information regarding pressure
1138 {
1139 int i;
1140 double probe_temp, probe_pressure, probe_pressure_psi;
1141 char temp [NUM];
1142 ///////////////////////////////////////////////////////////////////
1143 panel_name=panel_handle;
1144 send_data[0] = '\0';
1145 Fmt (send_data, "%s<PRESSURE?\r");
1146 CP=P3_comport;
1147 text_panel_name= MAIN_PRESSURE_P_3;
1148 ///////////////////////////////////////////////////////////////////
1149
1150
1151
1152 FlushOutQ (CP);
1153 FlushInQ (CP);
1154
1155 stringsize = StringLength (send_data);
1156 bytes_sent = ComWrt (CP, send_data, stringsize);
1157 Delay(0.05); /* 0.05 */
1158
1159 read_cnt = GetInQLen (CP);
1160
1161 read_data[0] = '\0';
1162 read_term = 13;

```

```

1164     bytes_read = ComRdTerm (CP, read_data, read_cnt, read_term);
1165     CopyString (tbox_read_data, 0, read_data, 0, bytes_read);
1166
1167
1168     for (i=9; tbox_read_data[i]!='\0';i++) //Return is "Pressure:XX"
1169         temp[i-9]=tbox_read_data[i];
1170         temp[i-9]='\0'; //close by '\0'
1171
1172         probe_pressure = atof(temp)/10;
1173         probe_pressure_psi=probe_pressure * 14.5037738;
1174     ProcessSystemEvents ();
1175     SetCtrlVal (panel_name, text_panel_name, probe_pressure_psi);
1176
1177
1178     CmtGetLock (Pumps_lockHandle);
1179 ///////////////////////////////////////////////////////////////////
1180 DSN SHIFT_Slow(5); //pump #2
1181 P31[0] = probe_pressure_psi; // Log value in P21 Array
1182 ///////////////////////////////////////////////////////////////////
1183 CmtReleaseLock (Pumps_lockHandle);
1184
1185
1186
1187
1188     RS232Error = ReturnRS232Err ();
1189     if (RS232Error)
1190         DisplayRS232Error ();
1191
1192     send_data[0] = '\0';
1193 }
1194
1195 /*-----*/
1196 /* Function SET NEW FLOW RATE command to the pump */
1197 /*-----*/
1198
1199 void SetPumpFlowrate(void) /* build based on DSN_Set_Bath_Setpoint*/
1200 {
1201     //CP= current comport
1202     //LD= LED to set ON
1203
1204     char ascii_setpoint[15],
1205     wholeNum_string[4],
1206     decNum_string[4];
1207
1208     char* setpointcode = "F";
1209
1210
1211     int wholeNum,
1212     decNum;
1213
1214
1215     wholeNum = wb_setpoint; // Captures the whole number portion of the setpoint
1216     decNum = (wb_setpoint-wholeNum)*1000; // Captures the 2 decimal places of the setpoint
1217
1218     sprintf(wholeNum_string, "%i", wholeNum);
1219     sprintf(decNum_string, "%i", decNum);
1220
1221     if (decNum == 0)
1222     {
1223         // Assembles the command as shown below e.g.
1224         strcpy(ascii_setpoint, setpointcode); // F F
1225         strcat(ascii_setpoint, wholeNum_string); // FX F1
1226         strcat(ascii_setpoint, decNum_string); // FXX F10
1227         strcat(ascii_setpoint, decNum_string); // FXXX F100
1228         strcat(ascii_setpoint, decNum_string); // FXXXX F1000
1229         strcat(ascii_setpoint, "\r"); // FXXXX\r
1230     }
1231     else
1232     {
1233         // Assembles the command as shown below
1234         strcpy(ascii_setpoint, setpointcode); // F
1235         strcat(ascii_setpoint, wholeNum_string); // FXXX
1236         strcat(ascii_setpoint, decNum_string); // FXXXXX
1237         strcat(ascii_setpoint, "\r"); // FXXXXX\r
1238     }
1239
1240     FlushOutQ (CP);
1241     FlushInQ (CP);
1242
1243     stringsize = StringLength (ascii_setpoint);
1244     ComWrt (CP, ascii_setpoint, stringsize); // Sends new setpoint to COM Port
1245
1246     Delay(0.5);
1247
1248     read_cnt = GetInQLen (CP);
1249
1250     read_term = 13;
1251
1252     bytes_read = ComRdTerm (CP, read_data, read_cnt, read_term);
1253     CopyString (tbox_read_data, 0, read_data, 0, bytes_read);
1254
1255
1256
1257
1258 /* SetCtrlVal (panel_handle, SERIAL_FLOWRATE_R, tbox_read_data); */
1259
1260

```

```

1261     if (tbox_read_data && "OK")
1262         SetCtrlVal (panel_handle, LED, 1);
1263     else
1264     {
1265         SetCtrlVal (panel_handle, LED, 0);
1266         MessagePopup ("Error","flow rate has not changed");
1267     }
1268
1269     RS232Error = ReturnRS232Err ();
1270     if (RS232Error)
1271         DisplayRS232Error ();
1272     /* Return LED back to the initial value */
1273     Delay(0.5);
1274     SetCtrlVal (panel_handle, LED, 0);
1275 }
1276
1277 // Pump #1 Start/Stop/Reset/5errors/Set new flow rate
1278
1279 int CVICALLBACK P1SFCallBack (int panel, int control, int event,
1280     void *callbackData, int eventData1, int eventData2)
1281 {
1282     switch (event)
1283     {
1284         case EVENT_COMMIT:
1285
1286         CmtGetLock (Pumps_lockHandle);
1287
1288         Delay (0.1);
1289         panel_name=panel_handle;
1290         CP=P1_comport;
1291         send_data[0] = '\0';
1292         Fmt (send_data, "%s<ON\r");
1293         PTEXT_panel_name= MAIN_STATUS_P_1; //show response from pump
1294         SendReadPump ();
1295
1296         pumprun_1 = 11;
1297
1298         CmtReleaseLock (Pumps_lockHandle);
1299         break;
1300     case EVENT_RIGHT_CLICK :
1301         MessagePopup ("Pump #1", "Will run Pump at current flow rate.");
1302         break;
1303     }
1304     return 0;
1305 }
1306
1307 int CVICALLBACK P1STOPCallBack (int panel, int control, int event,
1308     void *callbackData, int eventData1, int eventData2)
1309 {
1310     switch (event)
1311     {
1312         case EVENT_COMMIT:
1313         CmtGetLock (Pumps_lockHandle);
1314
1315         Delay (0.1);
1316         panel_name=panel_handle;
1317         CP=P1_comport;
1318         send_data[0] = '\0';
1319         Fmt (send_data, "%s<OFF\r");
1320         PTEXT_panel_name= MAIN_STATUS_P_1;
1321         SendReadPump ();
1322
1323         pumprun_1 = 12;
1324
1325         CmtReleaseLock (Pumps_lockHandle);
1326         break;
1327     }
1328     return 0;
1329 }
1330
1331 int CVICALLBACK P1PURGECallBack (int panel, int control, int event,
1332     void *callbackData, int eventData1, int eventData2)
1333 {
1334     switch (event)
1335     {
1336         case EVENT_COMMIT:
1337             panel_name=panel_handle;
1338             CP=P1_comport;
1339             send_data[0] = '\0';
1340             Fmt (send_data, "%s<PURGE\r");
1341             PTEXT_panel_name= MAIN_STATUS_P_1;
1342             SendReadPump ();
1343             break;
1344     }
1345     return 0;
1346 }
1347
1348 int CVICALLBACK P1RESTARTCallBack (int panel, int control, int event,
1349     void *callbackData, int eventData1, int eventData2)
1350 {
1351     switch (event)
1352     {
1353         case EVENT_COMMIT:
1354             panel_name=panel_handle;
1355             CP=P1_comport;
1356             send_data[0] = '\0';
1357             Fmt (send_data, "%s<RESET\r");

```

```

1358         PTEXT_panel_name= MAIN_STATUS_P_1;
1359         SendReadPump ();
1360
1361     break;
1362 }
1363 return 0;
1364 }
1365
1366 int CVICALLBACK P15ERRCallBack (int panel, int control, int event,
1367 void *callbackData, int eventData1, int eventData2)
1368 {
1369     switch (event)
1370     {
1371         case EVENT_COMMIT:
1372             panel_name=panel_handle;
1373             CP=P1_comport;
1374             send_data[0] = '\0';
1375             Fmt (send_data, "%s<ERRORS?\r");
1376             PTEXT_panel_name= MAIN_STATUS_P_1;
1377             SendReadPump ();
1378
1379         break;
1380     }
1381     return 0;
1382 }
1383
1384 int CVICALLBACK P1SNFRCallBack (int panel, int control, int event,
1385 void *callbackData, int eventData1, int eventData2)
1386 {
1387     switch (event)
1388     {
1389         case EVENT_COMMIT:
1390             CmtGetLock (Pumps_lockHandle);
1391             GetCtrlVal(panel_Handle, MAIN_P1_SET_NFR, &wb_setpoint);
1392             SNFRP_1();
1393             CmtReleaseLock (Pumps_lockHandle);
1394
1395         break;
1396     }
1397     return 0;
1398 }
1399
1400 void SNFRP_1 (void)
1401 {
1402     int i;
1403     double probe_temp;
1404     char temp [NUM];
1405
1406     CP=P1_comport;
1407     LED=MAIN_P1_OK_LED;
1408
1409     SetPumpFlowrate();
1410
1411     Delay(0.2);
1412     //update panel with new flow rate value//
1413
1414     ///////////
1415     panel_name=panel_handle;
1416     CP=P1_comport;
1417     text_panel_name= MAIN_WAS_FR_P_1;
1418     ///////////
1419
1420     FlushOutQ (CP);
1421     FlushInQ (CP);
1422
1423     send_data[0] = '\0';
1424     Fmt (send_data, "%s<F?\r");
1425     stringsize = StringLength (send_data);
1426
1427     bytes_sent = ComWrt (CP, send_data, stringsize);
1428     Delay(0.05); /* 0.05 */
1429
1430     read_cnt = GetInQLen (CP);
1431
1432     read_data[0] = '\0';
1433     read_term = 13;
1434
1435     bytes_read = ComRdTerm (CP, read_data, read_cnt, read_term);
1436
1437     CopyString (tbox_read_data, 0, read_data, 0, bytes_read);
1438
1439     for (i=2; tbox_read_data[i]!='\0';i++) //Return is "Pressure:XX"
1440         temp[i-2]=tbox_read_data[i];
1441         temp[i-2]='\0'; //close by '\0'
1442
1443     probe_temp = atof(temp);
1444     ProcessSystemEvents ();
1445     SetCtrlVal (panel_name, text_panel_name, probe_temp);
1446
1447     PFR11[0] = probe_temp; // Log value in PFR11 Array
1448
1449     RS232Error = ReturnRS232Err ();
1450     if (RS232Error)
1451         DisplayRS232Error ();
1452
1453     send_data[0] = '\0';
1454

```

```

1455
1456     return;
1457 }
1458 }
1459 // Pump #1 Start/Stop/Reset/Errors/Set new flow rate
1460
1461 /*-----*/
1462 /* Display pertinent error information. */
1463 /*-----*/
1464
1465 int CVICALLBACK ErrorCallBack (int panel, int control, int event,
1466                               void *callbackData, int eventData1,
1467                               int eventData2)
1468 {
1469     switch (event)
1470     {
1471         case EVENT_COMMIT:
1472             RS232Error = ReturnRS232Err ();
1473             DisplayRS232Error ();
1474             break;
1475         case EVENT_RIGHT_CLICK :
1476             break;
1477     }
1478     return 0;
1479 }
1480
1481 /*-----*/
1482 /* Get the status of the COM port and display it to the user. */
1483 /*-----*/
1484 int CVICALLBACK ComStatusCallBack (int panel, int control, int event,
1485                                   void *callbackData, int eventData1,
1486                                   int eventData2)
1487 {
1488     if (event == EVENT_COMMIT)
1489     {
1490         GetCtrlVal(config_handle, CONFIG_COMNUMBER, &com_num);
1491
1492         //help to protect from crashing, if some of com-ports was not active
1493         GetCtrlVal(config_handle, CONFIG_P1, &p1check);
1494         GetCtrlVal(config_handle, CONFIG_P2, &p2check);
1495         GetCtrlVal(config_handle, CONFIG_P3, &p3check);
1496
1497         if (com_num == 0)
1498             MessagePopup ("COM-service Message", "Select COM-port from the list");
1499         else if (com_num == 1 && p1check == 1)
1500         {
1501             com_status = GetComStat (P1_comport);
1502             DisplayComStatus ();
1503         }
1504
1505         else if (com_num == 2 && p2check == 1)
1506         {
1507             com_status = GetComStat (P2_comport);
1508             DisplayComStatus ();
1509         }
1510         else if (com_num == 2 && p2check == 0)
1511             MessagePopup ("COM-service Message", "COM port activation is required");
1512
1513         else if (com_num == 3 && p3check == 1)
1514         {
1515             com_status = GetComStat (P3_comport);
1516             DisplayComStatus ();
1517         }
1518         else if (com_num == 3 && p2check == 0)
1519             MessagePopup ("COM-service Message", "COM port activation is required");
1520
1521     }
1522     return 0;
1523 }
1524
1525
1526 /*-----*/
1527 /* Display status information to the user. */
1528 /*-----*/
1529 void DisplayComStatus ()
1530 {
1531     com_msg[0] = '\0';
1532     if (com_status & 0x0001)
1533         strcat (com_msg, "Input lost: Input queue"
1534                 " filled and characters were lost.\n");
1535     if (com_status & 0x0002)
1536         strcat (com_msg, "Asynch error: Problem "
1537                 "determining number of characters in input queue.\n");
1538     if (com_status & 0x0010)
1539         strcat (com_msg, "Parity error.\n");
1540     if (com_status & 0x0020)
1541         strcat (com_msg, "Overrun error: Received"
1542                 " characters were lost.\n");
1543     if (com_status & 0x0040)
1544         strcat (com_msg, "Framing error: Stop bits were not received"
1545                 " as expected.\n");
1546     if (com_status & 0x0080)
1547         strcat (com_msg, "Break: A break signal was detected.\n");
1548     if (com_status & 0x1000)
1549         strcat (com_msg, "Remote XOFF: An XOFF character was received."
1550                 "\nIf XON/XOFF was enabled, no characters are removed"
1551                 " from the output queue and sent to another device "

```

```

1552     "until that device sends an XON character.\n");
1553 if (com_status & 0x2000)
1554     strcat (com_msg, "Remote XON: An XON character was received."
1555             "\nTransmission can resume.\n");
1556 if (com_status & 0x4000)
1557     strcat (com_msg, "Local XOFF: An XOFF character was sent to\n"
1558             "the other device. If XON/XOFF was enabled, XOFF is\n"
1559             "transmitted when the input queue is 50%, 75%, and 90%\n"
1560             "full.\n");
1561 if (com_status & 0x8000)
1562     strcat (com_msg, "Local XON: An XON character was sent to\n"
1563             "the other device. If XON/XOFF was enabled, XON is\n"
1564             "transmitted when the input queue empties after XOFF\n"
1565             "was sent. XON tells the other device that it can\n"
1566             "resume sending data.\n");
1567 if (strlen (com_msg) == 0)
1568     strcat (com_msg, "No status bits are set.");
1569 MessagePopup ("RS232 Message", com_msg);
1570 }
1571
1572 /*-----*/
1573 /* Display Help on the Input Queue control. */
1574 /*-----*/
1575 int CVICALLBACK InputQCallBack (int panel, int control, int event,
1576                                 void *callbackData, int eventData1,
1577                                 int eventData2)
1578 {
1579     if (event == EVENT_RIGHT_CLICK)
1580         DisplayHelp (InputqHelp);
1581     return 0;
1582 }
1583
1584 /*-----*/
1585 /* Check the status of the queues and then terminate the RunUserInterface */
1586 /* loop and end the application...or just provide help. */
1587 /*-----*/
1588 int CVICALLBACK QuitCallBack (int panel, int control, int event,
1589                               void *callbackData, int eventData1,
1590                               int eventData2)
1591 {
1592     int i,test2;
1593
1594     switch (event)
1595     {
1596         case EVENT_COMMIT:
1597
1598             SaveVars();
1599             SaveConfig(0);
1600
1601             /* Add switching solenoids into initial position
1602             AV1_ONOFF
1603             AV2_ONOFF
1604             AV3_ONOFF
1605             */
1606
1607             if (P1_port_open)
1608             {
1609                 outqlen = GetOutQLen (P1_comport);
1610                 if (outqlen > 0)
1611                 {
1612                     MessagePopup ("RS232 Message", "The output queue has\n"
1613                             "data in it. Wait for device to receive\n"
1614                             "the data or flush the queue.\n");
1615                     break;
1616                 }
1617             RS232Error = CloseCom (P1_comport);
1618             if (RS232Error)
1619                 DisplayRS232Error ();
1620             }
1621
1622             if (P2_port_open)
1623             {
1624                 outqlen = GetOutQLen (P2_comport);
1625                 if (outqlen > 0)
1626                 {
1627                     MessagePopup ("RS232 Message", "The output queue has\n"
1628                             "data in it. Wait for device to receive\n"
1629                             "the data or flush the queue.\n");
1630                     break;
1631                 }
1632             RS232Error = CloseCom (P2_comport);
1633             if (RS232Error)
1634                 DisplayRS232Error ();
1635             }
1636
1637
1638             if (P3_port_open)
1639             {
1640                 outqlen = GetOutQLen (P3_comport);
1641                 if (outqlen > 0)
1642                 {
1643                     MessagePopup ("RS232 Message", "The output queue has\n"
1644                             "data in it. Wait for device to receive\n"
1645                             "the data or flush the queue.\n");
1646                     break;
1647                 }

```

```

1649     RS232Error = CloseCom (P3_comport);
1650     if (RS232Error)
1651         DisplayRS232Error ();
1652     }
1653
1654
1655 // Camera
1656
1657     GetCtrlVal (panel_handle, MAIN_GRAB_2, &test2); //check if the grab button is pressed
1658
1659     if(test2)
1660     {
1661         SetCtrlAttribute (panel_handle, MAIN_TIMER, ATTR_ENABLED, FALSE);
1662         // Stop the acquisition
1663         IMAQdxStopAcquisition (session);
1664         // Unconfigure the acquisition
1665         IMAQdxUnconfigureAcquisition (session);
1666     }
1667
1668     if(session) //if the camera session is still running
1669     {
1670         IMAQdxCloseCamera (session); //close the session and set the value to 0
1671         session = 0;
1672     }
1673
1674     // Delete any image in memory
1675     if(images) //if there are images from the manual sequential grab
1676     {
1677         for(i=0; i<imageArraySize; i++)
1678             imaqDispose (images[i]); //clear array completely
1679
1680         free(images);
1681         images = NULL;
1682     }
1683
1684     if(image_g) //if there are images from the grab function
1685     {
1686         imaqDispose(image_g); //Dispose the images
1687         image_g = NULL; //Set array to Null
1688     }
1689
1690     if(image) //if there is an image from the snap function
1691     {
1692         imaqDispose(image); //dispose the image
1693         image = NULL; // set value to null
1694     }
1695
1696     // Delete the Cam Attributes array in memory
1697     if (cameraAttributes)
1698     {
1699         free(cameraAttributes);
1700         cameraAttributes = NULL;
1701     }
1702
1703
1704
1705
1706
1707
1708     QuitUserInterface (0);
1709     break;
1710 case EVENT_RIGHT_CLICK :
1711     DisplayHelp (QuitHelp);
1712     break;
1713 }
1714 return 0;
1715 }
1716
1717 /*-----*/
1718 /* Display error information to the user. */
1719 /*-----*/
1720 void DisplayRS232Error (void)
1721 {
1722     char ErrorMessage[200];
1723     switch (RS232Error)
1724     {
1725         default :
1726             if (RS232Error < 0)
1727                 {
1728                     Fmt (ErrorMessage, "%s<RS232 error number %i", RS232Error);
1729                     MessagePopup ("RS232 Message", ErrorMessage);
1730                 }
1731             break;
1732 case 0 :
1733     MessagePopup ("RS232 Message", "No errors.");
1734     break;
1735 case -2 :
1736     Fmt (ErrorMessage, "%s", "Invalid port number (must be in the "
1737             "range 1 to 8).");
1738     MessagePopup ("RS232 Message", ErrorMessage);
1739     break;
1740 case -3 :
1741     Fmt (ErrorMessage, "%s", "No port is open.\n"
1742             "Check COM Port setting in Configure.");
1743     MessagePopup ("RS232 Message", ErrorMessage);
1744     break;
1745 case -99 :

```

```

1746     Fmt (ErrorMessage, "%s", "Timeout error.\n\n"
1747             "Either increase timeout value,\n"
1748             "check COM Port setting, or\n"
1749             "check device.");
1750     MessagePopup ("RS232 Message", ErrorMessage);
1751     break;
1752 }
1753 }
1754 /*-----*/
1755 /* Display help information to the user. */
1756 /*-----*/
1757 /*-----*/
1758 void DisplayHelp (int HelpId)
1759 {
1760     switch (HelpId)
1761     {
1762         case 1 :
1763             MessagePopup ("Quit Help",
1764                         "The Quit button closes the current COM port,\n"
1765                         "checks and displays any error messages,\n"
1766                         "and then exits this program.");
1767             break;
1768         case 2 :
1769             MessagePopup ("Input Queue Help",
1770                         "Specifies the size of the input queue for the "
1771                         "selected port.\n"
1772                         "Default Value: 512\n"
1773                         "Valid Range: 28 to 65516");
1774             break;
1775     }
1776 }
1777
1778 /* C8888D */
1779 //      DDD DDD EEEE      SSS EEEE RRRR V   V EEEE RRRR   SSS //
1780 //      D D D D E      S   E   R   R V   V E   R   R S   //
1781 //      D D D E EEE    SSS EEE RRRR V   V EEE RRRR   SSS //
1782 //      D D D D E      S E   R R   V V   E   R R   S   //
1783 //      DDD DDD EEEE    SSSS EEEE R RR   V   EEEE R RR SSSS //
1784 //      DDD DDD EEEE    SSSS EEEE R RR   V   EEEE R RR SSSS //
1785 //      C8888D */
1786 /*-----*/
1787
1788 int CVICALLBACK Mass1ConfigCallback (int panel, int control, int event,
1789                                     void *callbackData, int eventData1, int eventData2)
1790 {
1791     static int check_connection;
1792     static int check_disconnection;
1793
1794     switch (event)
1795     {
1796         case EVENT_COMMIT:
1797
1798             GetCtrlVal(config_handle, CONFIG_M1, &m1check);      // bring current position (1=ON, 0=OFF)
1799             GetCtrlVal(config_handle, CONFIG_P1, &p1check);      // bring current position of pump (1=ON, 0=OFF)
1800
1801     if (p1check == 1)
1802     {
1803         if (m1check == 1)
1804         {
1805             /*-----*/
1806             /*          ClientDDERead           */
1807             /*          Requests data for the server to send           */
1808             /*-----*/
1809             check_connection = ConnectToDDEServer (&hConv, "FlowDDE", "C(1)", DDEC callback, 0);
1810             // &hConv - unsigned *conversation handle
1811             // "FlowDDE" - server name, e.g. "Word" - for MicroSoft Word
1812             // "C(1)" - channel number - set by FlowDDE. topicName
1813             // DDEC callback - call back Function, required by DDE protocol. This function can receive only two messages: D
1814             DE_DISCONNECT and DDE_DATAREADY
1815
1816             /* More details can be found here - http://zone.ni.com/reference/en-XX/help/370051T-01/cvi/libref/cviconnect
1817             toddeserver/*/
1818             /* key word for searching @ ni.com: ConnectToDDEServer */
1819
1820             if (check_connection>=0)
1821             {
1822                 SetCtrlVal (config_handle, CONFIG_M1_LED, 1);
1823                 M1DDE_connection=1;
1824                 // In case of error during connection procedure - check DDE_Library_ERR_codes.txt
1825             }
1826             else MessagePopup ("","Connection to FlowDDE failure");
1827         }
1828         else //Mass flow meter should be disconnected from server//
1829         {
1830             /*-----*/
1831             /*          DisconnectFromDDEServer           */
1832             /*          Requests data for the server to send           */
1833             /*-----*/
1834             if (M1DDE_connection == 1) //checking for connection
1835             {
1836                 check_disconnection = DisconnectFromDDEServer (hConv); // disconnect from DDE server
1837
1838                 if (check_disconnection>=0)
1839                 {
1840                     SetCtrlVal (config_handle, CONFIG_M1_LED, 0);           // set LED in "OFF" position
1841                     M1DDE_connection =0;
1842                 }
1843             }
1844         }
1845     }
1846 }

```

```

1841             else MessagePopup ("","Disconnection from FlowDDE failure");
1842         }
1843     }
1844 }
1845 }
1846 else
1847 {
1848 MessagePopup ("Warning","Pump #1 connection is required");
1849 SetCtrlVal(config_handle, CONFIG_M1, 0);
1850 }
1851     break;
1852 }
1853 return 0;
1854 }
1855
1856 int CVICALLBACK Mass2ConfigCallback (int panel, int control, int event,
1857 void *callbackData, int eventData1, int eventData2)
1858 {
1859     static int check_connection;
1860     static int check_disconnection;
1861     switch (event)
1862     {
1863     case EVENT_COMMIT:
1864         GetCtrlVal(config_handle, CONFIG_M2, &m2check);
1865         GetCtrlVal(config_handle, CONFIG_P2, &p2check);
1866     if (p2check == 1)
1867     {
1868         if (m2check == 1)
1869         {
1870             check_connection = ConnectToDDEServer (&hConv2, "FlowDDE2", "C(1)", DDECallback, 0);
1871             if (check_connection>=0)
1872             {
1873                 SetCtrlVal (config_handle, CONFIG_M2_LED, 1);
1874                 M2DDE_connection=1;
1875             }
1876             else MessagePopup ("","Connection to FlowDDE2 failure");
1877         }
1878     else
1879     {
1880         if (M2DDE_connection == 1) //checking for connection
1881         {
1882             check_disconnection = DisconnectFromDDEServer (hConv2); // disconnect from DDE server
1883             if (check_disconnection>=0)
1884             {
1885                 SetCtrlVal (config_handle, CONFIG_M2_LED, 0); // set LED in "OFF" position
1886                 M2DDE_connection =0;
1887             }
1888             else MessagePopup ("","Disconnection from FlowDDE2 failure");
1889         }
1890         else MessagePopup ("","There is no connection to FlowDDE2");
1891     }
1892 }
1893 }
1894 else
1895 {
1896 MessagePopup ("Warning","Pump #2 connection is required");
1897 SetCtrlVal(config_handle, CONFIG_M2, 0);
1898 }
1899     break;
1900 }
1901 return 0;
1902 }
1903
1904 int CVICALLBACK Mass3ConfigCallback (int panel, int control, int event,
1905 void *callbackData, int eventData1, int eventData2)
1906 {
1907     static int check_connection;
1908     static int check_disconnection;
1909     switch (event)
1910     {
1911     case EVENT_COMMIT:
1912         GetCtrlVal(config_handle, CONFIG_M3, &m3check);
1913
1914     if (m3check == 1)
1915     {
1916         check_connection = ConnectToDDEServer (&hConv3, "FlowDDE3", "C(1)", DDECallback, 0);
1917         if (check_connection>=0)
1918         {
1919             SetCtrlVal (config_handle, CONFIG_M3_LED, 1);
1920             M3DDE_connection=1;
1921         }
1922         else MessagePopup ("","Connection to FlowDDE3 failure");
1923     }
1924     else
1925     {
1926         if (M3DDE_connection == 1) //checking for connection
1927         {
1928             check_disconnection = DisconnectFromDDEServer (hConv3); // disconnect from DDE server
1929             if (check_disconnection>=0)
1930             {
1931                 SetCtrlVal (config_handle, CONFIG_M3_LED, 0); // set LED in "OFF" position
1932                 M3DDE_connection =0;
1933             }
1934             else MessagePopup ("","Disconnection from FlowDDE3 failure");
1935     }
1936 }
1937 }
```

```

1938             else MessagePopup ("","There is no connection to FlowDDE3");
1939         }
1940     break;
1941   }
1942   return 0;
1943 }
1944
1945 int CVICALLBACK Mass4ConfigCallback (int panel, int control, int event,
1946   void *callbackData, int eventData1, int eventData2)
1947 {
1948   static int check_connection;
1949   static int check_disconnection;
1950   switch (event)
1951   {
1952     case EVENT_COMMIT:
1953       GetCtrlVal(config_handle, CONFIG_M4, &m4check);
1954
1955       if (m4check == 1)
1956       {
1957         check_connection = ConnectToDDEServer (&hConv4, "FlowDDE4", "C(1)", DDECallback, 0);
1958         if (check_connection>=0)
1959         {
1960           SetCtrlVal (config_handle, CONFIG_M4_LED, 1);
1961           M4DDE_connection=1;
1962         }
1963         else MessagePopup ("","Connection to FlowDDE4 failure");
1964       }
1965       else
1966       {
1967         if (M4DDE_connection == 1) //checking for connection
1968         {
1969           check_disconnection = DisconnectFromDDEServer (hConv4); // disconnect from DDE server
1970
1971           if (check_disconnection>=0)
1972           {
1973             SetCtrlVal (config_handle, CONFIG_M4_LED, 0); // set LED in "OFF" position
1974             M4DDE_connection =0;
1975           }
1976           else MessagePopup ("","Disconnection from FlowDDE4 failure");
1977         }
1978         else MessagePopup ("","There is no connection to FlowDDE4");
1979       }
1980     break;
1981   }
1982   return 0;
1983 }
1984
1985 int CVICALLBACK BPRConfigCallback (int panel, int control, int event,
1986   void *callbackData, int eventData1, int eventData2)
1987 {
1988   static int check_connection;
1989   static int check_disconnection;
1990   switch (event)
1991   {
1992     case EVENT_COMMIT:
1993       GetCtrlVal(config_handle, CONFIG_BPR, &bprcheck);
1994
1995       if (bprcheck == 1)
1996       {
1997         check_connection = ConnectToDDEServer (&hConv5, "FlowDDE5", "C(1)", DDECallback, 0);
1998         if (check_connection>=0)
1999         {
2000           SetCtrlVal (config_handle, CONFIG_BPR_LED, 1);
2001           BPRDDE_connection=1;
2002         }
2003         else MessagePopup ("","Connection to FlowDDE5 failure");
2004       }
2005       else
2006       {
2007         if (BPRDDE_connection == 1) //checking for connection
2008         {
2009           check_disconnection = DisconnectFromDDEServer (hConv5); // disconnect from DDE server
2010
2011           if (check_disconnection>=0)
2012           {
2013             SetCtrlVal (config_handle, CONFIG_BPR_LED, 0); // set LED in "OFF" position
2014             BPRDDE_connection =0;
2015           }
2016           else MessagePopup ("","Disconnection from FlowDDE5 failure");
2017         }
2018         else MessagePopup ("","There is no connection to FlowDDE5");
2019       }
2020     break;
2021   }
2022   return 0;
2023 }
2024
2025 /*-----*/
2026 //This function processes messages as the client of the DDE Server (FlowDDE).
2027 //If for some reason FlowDDE needs to shut down, it will issue wdisconnect messages to its clients
2028 //and this function processes messages from FlowDDE to its clients.
2029 /*-----*/
2030 int DDECallback (unsigned handle, char *topicName,
2031   char *itemName, int xType, int dataFmt,
2032   int dataSize, void *dataPtr,
2033   void *callbackData)
2034 {

```

```

2035     switch (xType) {
2036         case DDE_DISCONNECT:
2037             SetInputMode (config_handle, CONFIG_M1_LED, 0);
2038             MessagePopup("", "FlowDDE has shut down the connection");
2039             break;
2040     }
2041
2042     return 1;
2043 }
2044
2045 int CVICALLBACK P1ActivateCallBack (int panel, int control, int event,
2046                                     void *callbackData, int eventData1, int eventData2)
2047 {
2048
2049
2050     switch (event)
2051     {
2052         case EVENT_COMMIT:
2053             GetCtrlVal (panel_handle, MAIN_P1_ONOFF, &test);
2054             if (p1check == 1)
2055             {
2056                 if (Pumps_quitflag == 1)
2057                 {
2058                     CmtGetLock (Pumps_lockHandle);
2059                     ActivatePump1 ();
2060                     CmtReleaseLock (Pumps_lockHandle);
2061                 }
2062                 else ActivatePump1 ();
2063             }
2064             else
2065             {
2066                 MessagePopup ("Warning", "Connection to Pump #1 is required");
2067                 Delay(0.05);
2068                 SetCtrlVal(panel_handle, MAIN_P1_ONOFF, 0);
2069             }
2070         break;
2071     }
2072     return 0;
2073 }
2074
2075 void ActivatePump1 (void)
2076 {
2077     int i;
2078     double probe_temp;
2079     char temp [NUM];
2080     if(test==1)
2081     {
2082
2083         EnableP1PanelControls (0);
2084         SetCtrlAttribute (panel_handle, MAIN_WAS_FR_P_1, ATTR_VISIBLE, 1);
2085         SetCtrlAttribute (panel_handle, MAIN_PRESSURE_P_1, ATTR_VISIBLE, 1);
2086         SetCtrlVal (panel_handle, MAIN_P1_ONOFF_LED, 1);
2087
2088         ///////////
2089         panel_name=panel_handle;
2090         CP=P1_comport;
2091         text_panel_name= MAIN_WAS_FR_P_1;
2092         //////////////
2093
2094         FlushOutQ (CP);
2095         FlushInQ (CP);
2096
2097         send_data[0] = '\0';
2098         Fmt (send_data, "%sc<F?\r");
2099         stringsize = StringLength (send_data);
2100
2101         bytes_sent = ComWrt (CP, send_data, stringsize);
2102         Delay(0.05); /* 0.05 */
2103
2104         read_cnt = GetInQLen (CP);
2105
2106         read_data[0] = '\0';
2107         read_term = 13;
2108
2109         bytes_read = ComRdTerm (CP, read_data, read_cnt, read_term);
2110         CopyString (tbox_read_data, 0, read_data, 0, bytes_read);
2111
2112         for (i=2; tbox_read_data[i]!='\0';i++) //Return is "Pressure:XX"
2113             temp[i-2]=tbox_read_data[i];
2114             temp[i-2]='\0'; //close by '\0'
2115
2116         probe_temp = atof(temp);
2117         ProcessSystemEvents ();
2118         SetCtrlVal (panel_name, text_panel_name, probe_temp);
2119
2120         PFR11[0] = probe_temp; // Log value in PFR11 Array
2121
2122         RS232Error = ReturnRS232Err ();
2123         if (RS232Error)
2124             DisplayRS232Error ();
2125
2126         send_data[0] = '\0';
2127
2128         SetCtrlVal(panel_handle, MAIN_LOG_P1, 1); //activate logging pressure
2129         GetCtrlVal(panel_handle, MAIN_LOG_P1, &Is_P1);
2130     }
2131     else

```

```

2132     {
2133         SetCtrlVal(panel_handle, MAIN_LOG_P1, 0); //deactivate logging pressure
2134         GetCtrlVal(panel_handle, MAIN_LOG_P1, &Is_P1); //save new value
2135
2136
2137         EnableP1PanelControls (1); //dim all panels
2138         SetCtrlAttribute (panel_handle, MAIN_WAS_FR_P_1, ATTR_VISIBLE, 0);
2139         SetCtrlAttribute (panel_handle, MAIN_PRESSURE_P_1, ATTR_VISIBLE, 0);
2140         SetCtrlVal (panel_handle, MAIN_P1_ONOFF_LED, 0);
2141
2142         ///////////////
2143         panel_name=panel_handle;
2144         CP=P1_comport;
2145         PTEXT_panel_name= MAIN_STATUS_P_1;
2146         //////////////////
2147
2148         send_data[0] = '\0';
2149         Fmt_(send_data, "%s<OFF\r");
2150         SendReadPump ();
2151         PFR11[0] = '\0'; // Log value in PFR11 Array
2152     }
2153     return;
2154 }
2155
2156 //***** Load_Config : Load variables from config file
2157 //***** : Update screen from variables
2158 //***** : Orginally made by DSN
2159 //***** ****
2160 //***** ****
2161
2162 void CVICALLBACK Load_Config (int menuBar, int menuItem, void *callbackData,
2163     int panel)
2164 {
2165     LoadConfig();
2166     LoadVars();
2167     Update_Graphics();
2168
2169 }
2170
2171 //***** Save_Config : Save screen to variables
2172 //***** : Save variables to config file
2173 //***** : Orginally made by DSN
2174 //***** ****
2175 //***** ****
2176
2177 void CVICALLBACK Save_Config (int menuBar, int menuItem, void *callbackData,
2178     int panel)
2179 {
2180     SaveVars();
2181     SaveConfig(0);
2182 }
2183
2184 //***** Save_Config_As : Save screen to variables
2185 //***** : Save variables to config file
2186 //***** : Allow the config file to be selected
2187 //***** : Orginally made by DSN
2188 //***** ****
2189 //***** ****
2190
2191 void CVICALLBACK Save_Config_As (int menuBar, int menuItem, void *callbackData,
2192     int panel)
2193 {
2194     SaveVars();
2195     SaveConfig(1);
2196 }
2197
2198 void CVICALLBACK ExitCallback (int menuBar, int menuItem, void *callbackData, int panel) //dpne
2199 {
2200     DisplayPanel (s_handle);
2201 }
2202
2203 void CVICALLBACK Com_Setup (int menuBar, int menuItem, void *callbackData, int panel) //done
2204 {
2205     DisplayPanel(config_handle);
2206
2207     /* If user already has done configuration, then
2208        display those new parameters. If entering
2209        configuration for 1st time, set config_flag
2210        and use default settings.
2211     */
2212     if (config_flag) /* Configuration done at least once.*/
2213     SetConfigParms ();
2214     else /* 1st time.*/
2215         config_flag = 1;
2216
2217 }
2218
2219 void CVICALLBACK About_Show (int menuBar, int menuItem, void *callbackData, //Display About panel
2220     int panel)
2221 {
2222     DisplayPanel(a_handle);
2223 }
2224
2225 void CVICALLBACK Graph_Set (int menuBar, int menuItem, void *callbackData, //Display Graph panel
2226     int panel)
2227 {
2228     DisplayPanel(g_handle);

```

```

2229 }
230
231 ///////////////////////////////////////////////////////////////////
232 // SOLENOID VALVES ///////////////////////////////////////////////////////////////////
233 // OPEN - CLOSE ///////////////////////////////////////////////////////////////////
234 ///////////////////////////////////////////////////////////////////
235
236 int CVICALLBACK AV123CallBack (int panel, int control, int event,
237     void *callbackData, int eventData1, int eventData2)           // Build based on WriteDigChan.c
238 {
239
240 if( event==EVENT_COMMIT ) SWITCH_SOLENOID();
241
242 return 0;
243
244 }
245
246 /*
247 int      error=0;
248 TaskHandle taskHandleAV=0;
249 char      chanAV[256];
250 uint8    dataAV[8];
251 char      errBuffAV[2048]={'\0'};
252
253 if( event==EVENT_COMMIT )
254 {
255     GetCtrlVal(config_handle,CONFIG_SOLENOID,chanAV);
256     GetCtrlVal(panel_handle,MAIN_AV1_ONOFF,&dataAV[0]);    //##1 solenoid valve [inlet]
257     GetCtrlVal(panel_handle,MAIN_AV3_ONOFF,&dataAV[1]);    //##2 solenoid valve [outlet]
258     GetCtrlVal(panel_handle,MAIN_AV2_ONOFF,&dataAV[2]);    //##3 solenoid valve [dP valve]
259
260     if (dataAV[0] == 1) SetCtrlVal (panel_handle, MAIN_AV1_LED, 1); //Show up status of AV-1
261     else SetCtrlVal (panel_handle, MAIN_AV1_LED, 0);
262
263     if (dataAV[1] == 1) SetCtrlVal (panel_handle, MAIN_AV3_LED, 1); //Show up status of AV-2
264     else SetCtrlVal (panel_handle, MAIN_AV3_LED, 0);
265
266     if (dataAV[2] == 1) SetCtrlVal (panel_handle, MAIN_AV2_LED, 1); //Show up status of AV-3
267     else SetCtrlVal (panel_handle, MAIN_AV2_LED, 0);
268
269
270 //*****
271 // DAQmx Configure Code
272 //*****
273 SetWaitCursor(1);
274 DAQmxErrChk (DAQmxCreateTask("",&taskHandleAV));
275 DAQmxErrChk (DAQmxCreateDOChan(taskHandleAV,chanAV,"",DAQmx_Val_ChанForAllLines));
276
277
278 //*****
279 // DAQmx Start Code
280 //*****
281 DAQmxErrChk (DAQmxStartTask(taskHandleAV));
282
283
284 //*****
285 // DAQmx Write Code
286 //*****
287 DAQmxErrChk (DAQmxWriteDigitalLines(taskHandleAV,1,1,10.0,DAQmx_Val_GroupByChannel,dataAV,NULL,NULL));
288 }
289
290 Error:
291 SetWaitCursor(0);
292 if( DAQmxFailed(error) )
293     DAQmxGetExtendedErrorInfo(errBuffAV,2048);
294 if( taskHandleAV!=0 ) {
295
296 //*****
297 // DAQmx Stop Code
298 //*****
299 DAQmxStopTask(taskHandleAV);
300 DAQmxClearTask(taskHandleAV);
301
302 }
303
304 void SWITCH_SOLENOID (void)    //Function to switch solenoid valves
305 {
306 int      error=0;
307 TaskHandle taskHandleAV=0;
308 char      chanAV[256];
309 uint8    dataAV[8];
310 char      errBuffAV[2048]={'\0'};
311
312
313     GetCtrlVal(config_handle,CONFIG_SOLENOID,chanAV);
314     GetCtrlVal(panel_handle,MAIN_AV1_ONOFF,&dataAV[0]);    //##1 solenoid valve [inlet]
315
316     dataAV[1]=dataAV[0]; //##2 solenoid valve [outlet] if one set to close/open - same for second
317     SetCtrlVal(panel_handle, MAIN_AV3_ONOFF, dataAV[1]);    //##2 solenoid valve [outlet]
318
319 //     GetCtrlVal(panel_handle,MAIN_AV3_ONOFF,&dataAV[1]); //##2 solenoid valve [outlet]
320
321     GetCtrlVal(panel_handle,MAIN_AV2_ONOFF,&dataAV[2]);    //##3 solenoid valve [dP valve]
322
323     if (dataAV[0] == 1) SetCtrlVal (panel_handle, MAIN_AV1_LED, 1); //Show up status of AV-1
324     else SetCtrlVal (panel_handle, MAIN_AV1_LED, 0);
325

```

```

2326     if ( dataAV[1] == 1) SetCtrlVal (panel_handle, MAIN_AV3_LED, 1); //Show up status of AV-2
2327     else SetCtrlVal (panel_handle, MAIN_AV3_LED, 0);
2328
2329     if ( dataAV[2] == 1) SetCtrlVal (panel_handle, MAIN_AV2_LED, 1); //Show up status of AV-3
2330     else SetCtrlVal (panel_handle, MAIN_AV2_LED, 0);
2331
2332     /*****+
2333     // DAQmx Configure Code
2334     /*****+
2335     SetWaitCursor(1);
2336     DAQmxErrChk (DAQmxCreateTask("",&taskHandleAV));
2337     DAQmxErrChk (DAQmxCreateDOChan(taskHandleAV,chanAV,"",DAQmx_Val_ChanForAllLines));
2338
2339     /*****+
2340     // DAQmx Start Code
2341     /*****+
2342     DAQmxErrChk (DAQmxStartTask(taskHandleAV));
2343
2344     /*****+
2345     // DAQmx Write Code
2346     /*****+
2347     DAQmxErrChk (DAQmxWriteDigitalLines(taskHandleAV,1,1,10.0,DAQmx_Val_GroupByChannel,dataAV,NULL,NULL));
2348
2349
2350
2351 Error:
2352     SetWaitCursor(0);
2353     if( DAQmxFailed(error) )
2354         DAQmxGetExtendedErrorInfo(errBuffAV,2048);
2355     if( taskHandleAV!=0 ) {
2356         /*****+
2357         // DAQmx Stop Code
2358         /*****+
2359         DAQmxStopTask(taskHandleAV);
2360         DAQmxClearTask(taskHandleAV);
2361     }
2362     if( DAQmxFailed(error) )
2363         MessagePopup("DAQmx Error",errBuffAV);
2364
2365 return;
2366 }
2367
2368 void MainPanelQuit(void) //Function to close user interface
2369 {
2370 // int i;
2371     QuitUserInterface(0);
2372
2373     return;
2374 }
2375
2376
2377 int CVICALLBACK SaveYES_MCP_Config (int panel, int control, int event, //Shutdown program with sawing config
2378                                     void *callbackData, int eventData1, int eventData2)
2379 {
2380     switch (event)
2381     {
2382         case EVENT_COMMIT:
2383             SaveConfig(0);
2384             HidePanel (s_handle);
2385             MainPanelQuit();
2386             break;
2387         case EVENT_RIGHT_CLICK:
2388             break;
2389     }
2390     return 0;
2391 }
2392
2393 int CVICALLBACK SaveNO_MCP_Config (int panel, int control, int event, //Shutdown program without saving config
2394                                     void *callbackData, int eventData1, int eventData2)
2395 {
2396     switch (event)
2397     {
2398         case EVENT_COMMIT:
2399             HidePanel (s_handle);
2400             MainPanelQuit();
2401             break;
2402         case EVENT_RIGHT_CLICK:
2403             break;
2404     }
2405     return 0;
2406 }
2407
2408 int CVICALLBACK SaveCANCEL_MCP_Config (int panel, int control, int event, //Return back to program without saving config
2409                                         void *callbackData, int eventData1, int eventData2)
2410 {
2411     switch (event)
2412     {
2413         case EVENT_COMMIT:
2414             HidePanel (s_handle);
2415             break;
2416         case EVENT_RIGHT_CLICK:
2417             break;
2418     }
2419     return 0;
2420 }
2421
2422 int CVICALLBACK AboutCallBack (int panel, int control, int event, //Close About panel

```

```

2423     void *callbackData, int eventData1, int eventData2)
2424 {
2425     switch (event)
2426     {
2427         case EVENT_COMMIT:
2428             HidePanel (a_handle);
2429             break;
2430         case EVENT_RIGHT_CLICK:
2431             break;
2432     }
2433     return 0;
2434 }
2435
2436 int CVICALLBACK CloseGCallBack (int panel, int control, int event, //Close g_handle panel
2437                                 void *callbackData, int eventData1, int eventData2)
2438 {
2439     switch (event)
2440     {
2441         case EVENT_COMMIT:
2442             HidePanel (g_handle);
2443             break;
2444         case EVENT_RIGHT_CLICK:
2445             break;
2446     }
2447     return 0;
2448 }
2449
2450 int CVICALLBACK SETUP_G (int panel, int control, int event, //Setup Graph Scaling to Match the Graph Panel Values
2451                           void *callbackData, int eventData1, int eventData2)
2452 {
2453     switch (event)
2454     {
2455         case EVENT_COMMIT:
2456             GraphSetup(); //run settings for Graph
2457             break;
2458         case EVENT_RIGHT_CLICK:
2459             break;
2460     }
2461     return 0;
2462 }
2463
2464 //*****
2465 // GraphSetup      : Setup Graph Scaling to Match the Graph Panel Values
2466 // build based on DSN GraphSetup with additional function SetAxisScalingMode
2467 //*****
2468
2469 void GraphSetup(void)
2470 {
2471
2472 // Update the variables from the panels
2473 SaveVars();
2474
2475 //Read Graph #1
2476 if(Y_Mode_G_1) // Check for Auto mode
2477 {
2478     SetCtrlAttribute (g_handle, G_SETUP_Y_Mode_G_1, ATTR_LABEL_TEXT, "Auto");
2479     SetCtrlAttribute (g_handle, G_SETUP_Y_Min_G_1, ATTR_DIMMED, 1);
2480     SetCtrlAttribute (g_handle, G_SETUP_Y_Max_G_1, ATTR_DIMMED, 1);
2481
2482     SetAxisScalingMode (panel_handle, MAIN_G_1, VAL_BOTTOM_XAXIS, VAL_MANUAL, 0.0, X_Range_G_1);
2483     SetAxisScalingMode (panel_handle, MAIN_G_1, VAL_LEFT_YAXIS, VAL_AUTOSCALE, 0.0, 0.0);
2484 }
2485 else
2486 {
2487     SetCtrlAttribute (g_handle, G_SETUP_Y_Mode_G_1, ATTR_LABEL_TEXT, "Fixed");
2488     SetCtrlAttribute (g_handle, G_SETUP_Y_Min_G_1, ATTR_DIMMED, 0);
2489     SetCtrlAttribute (g_handle, G_SETUP_Y_Max_G_1, ATTR_DIMMED, 0);
2490
2491     SetAxisScalingMode (panel_handle, MAIN_G_1, VAL_BOTTOM_XAXIS, VAL_MANUAL, 0.0, X_Range_G_1);
2492     SetAxisScalingMode (panel_handle, MAIN_G_1, VAL_LEFT_YAXIS, VAL_MANUAL, Y_Min_G_1, Y_Max_G_1);
2493 }
2494
2495 GraphName(plotVar_G_1, MAIN_G_1,G_SETUP_G1_L_1,G_SETUP_G1_T_1,
2496           G_SETUP_G1_L_2,G_SETUP_G1_T_2,
2497           G_SETUP_G1_L_3,G_SETUP_G1_T_3,
2498           G_SETUP_G1_L_4,G_SETUP_G1_T_4);
2499
2500 //Read Graph #2
2501 if(Y_Mode_G_2) // Check for Auto mode
2502 {
2503     SetCtrlAttribute (g_handle, G_SETUP_Y_Mode_G_2, ATTR_LABEL_TEXT, "Auto");
2504     SetCtrlAttribute (g_handle, G_SETUP_Y_Min_G_2, ATTR_DIMMED, 1);
2505     SetCtrlAttribute (g_handle, G_SETUP_Y_Max_G_2, ATTR_DIMMED, 1);
2506
2507     SetAxisScalingMode (panel_handle, MAIN_G_2, VAL_BOTTOM_XAXIS, VAL_MANUAL, 0.0, X_Range_G_2);
2508     SetAxisScalingMode (panel_handle, MAIN_G_2, VAL_LEFT_YAXIS, VAL_AUTOSCALE, 0.0, 0.0);
2509 }
2510 else
2511 {
2512     SetCtrlAttribute (g_handle, G_SETUP_Y_Mode_G_2, ATTR_LABEL_TEXT, "Fixed");
2513     SetCtrlAttribute (g_handle, G_SETUP_Y_Min_G_2, ATTR_DIMMED, 0);
2514     SetCtrlAttribute (g_handle, G_SETUP_Y_Max_G_2, ATTR_DIMMED, 0);
2515
2516     SetAxisScalingMode (panel_handle, MAIN_G_2, VAL_BOTTOM_XAXIS, VAL_MANUAL, 0.0, X_Range_G_2);
2517     SetAxisScalingMode (panel_handle, MAIN_G_2, VAL_LEFT_YAXIS, VAL_MANUAL, Y_Min_G_2, Y_Max_G_2);
2518 }
2519

```

```

2520
2521
2522
2523
2524 //Read Graph #3
2525 if(Y_Mode_G_3) // Check for Auto mode
2526 {
2527 SetCtrlAttribute (g_handle, G_SETUP_Y_Mode_G_3, ATTR_LABEL_TEXT, "Auto");
2528 SetCtrlAttribute (g_handle, G_SETUP_Y_Min_G_3, ATTR_DIMMED, 1);
2529 SetCtrlAttribute (g_handle, G_SETUP_Y_Max_G_3, ATTR_DIMMED, 1);
2530
2531 SetAxisScalingMode (panel_handle, MAIN_G_3, VAL_BOTTOM_XAXIS, VAL_MANUAL, 0.0, X_Range_G_3);
2532 SetAxisScalingMode (panel_handle, MAIN_G_3, VAL_LEFT_YAXIS, VAL_AUTOSCALE, 0.0, 0.0);
2533 }
2534 else
2535 {
2536 SetCtrlAttribute (g_handle, G_SETUP_Y_Mode_G_3, ATTR_LABEL_TEXT, "Fixed");
2537 SetCtrlAttribute (g_handle, G_SETUP_Y_Min_G_3, ATTR_DIMMED, 0);
2538 SetCtrlAttribute (g_handle, G_SETUP_Y_Max_G_3, ATTR_DIMMED, 0);
2539
2540 SetAxisScalingMode (panel_handle, MAIN_G_3, VAL_BOTTOM_XAXIS, VAL_MANUAL, 0.0, X_Range_G_3);
2541 SetAxisScalingMode (panel_handle, MAIN_G_3, VAL_LEFT_YAXIS, VAL_MANUAL, Y_Min_G_3, Y_Max_G_3);
2542 }
2543
2544 GraphName(plotVar_G_3, MAIN_G_3, G_SETUP_G3_L_1,G_SETUP_G3_T_1,
2545 G_SETUP_G3_L_2,G_SETUP_G3_T_2,
2546 G_SETUP_G3_L_3,G_SETUP_G3_T_3,
2547 G_SETUP_G3_L_4,G_SETUP_G3_T_4);
2548 //Read Graph #4
2549 if(Y_Mode_G_4) // Check for Auto mode
2550 {
2551 SetCtrlAttribute (g_handle, G_SETUP_Y_Mode_G_4, ATTR_LABEL_TEXT, "Auto");
2552 SetCtrlAttribute (g_handle, G_SETUP_Y_Min_G_4, ATTR_DIMMED, 1);
2553 SetCtrlAttribute (g_handle, G_SETUP_Y_Max_G_4, ATTR_DIMMED, 1);
2554
2555 SetAxisScalingMode (panel_handle, MAIN_G_4, VAL_BOTTOM_XAXIS, VAL_MANUAL, 0.0, X_Range_G_4);
2556 SetAxisScalingMode (panel_handle, MAIN_G_4, VAL_LEFT_YAXIS, VAL_AUTOSCALE, 0.0, 0.0);
2557 }
2558 else
2559 {
2560 SetCtrlAttribute (g_handle, G_SETUP_Y_Mode_G_4, ATTR_LABEL_TEXT, "Fixed");
2561 SetCtrlAttribute (g_handle, G_SETUP_Y_Min_G_4, ATTR_DIMMED, 0);
2562 SetCtrlAttribute (g_handle, G_SETUP_Y_Max_G_4, ATTR_DIMMED, 0);
2563
2564 SetAxisScalingMode (panel_handle, MAIN_G_4, VAL_BOTTOM_XAXIS, VAL_MANUAL, 0.0, X_Range_G_4);
2565 SetAxisScalingMode (panel_handle, MAIN_G_4, VAL_LEFT_YAXIS, VAL_MANUAL, Y_Min_G_4, Y_Max_G_4);
2566 }
2567
2568 GraphName(plotVar_G_4, MAIN_G_4, G_SETUP_G4_L_1,G_SETUP_G4_T_1,
2569 G_SETUP_G4_L_2,G_SETUP_G4_T_2,
2570 G_SETUP_G4_L_3,G_SETUP_G4_T_3,
2571 G_SETUP_G4_L_4,G_SETUP_G4_T_4);
2572
2573 //Read Graph #5
2574 if(X_Mode_G_5) // Check for Auto mode X axis
2575 {
2576 SetCtrlAttribute (g_handle, G_SETUP_X_Mode_G_5, ATTR_LABEL_TEXT, "Auto");
2577 SetCtrlAttribute (g_handle, G_SETUP_X_Min_G_5, ATTR_DIMMED, 1);
2578 SetCtrlAttribute (g_handle, G_SETUP_X_Max_G_5, ATTR_DIMMED, 1);
2579 SetAxisScalingMode (extra_g_handle, EXTRA_G_G_5, VAL_BOTTOM_XAXIS, VAL_AUTOSCALE, 0.0, 0.0);
2580 }
2581 else
2582 {
2583 SetCtrlAttribute (g_handle, G_SETUP_X_Mode_G_5, ATTR_LABEL_TEXT, "Fixed");
2584 SetCtrlAttribute (g_handle, G_SETUP_X_Min_G_5, ATTR_DIMMED, 0);
2585 SetCtrlAttribute (g_handle, G_SETUP_X_Max_G_5, ATTR_DIMMED, 0);
2586 SetAxisScalingMode (extra_g_handle, EXTRA_G_G_5, VAL_BOTTOM_XAXIS, VAL_MANUAL, X_Min_G_5, X_Max_G_5);
2587 }
2588
2589 if(Y_Mode_G_5) // Check for Auto mode
2590 {
2591 SetCtrlAttribute (g_handle, G_SETUP_Y_Mode_G_5, ATTR_LABEL_TEXT, "Auto");
2592 SetCtrlAttribute (g_handle, G_SETUP_Y_Min_G_5, ATTR_DIMMED, 1);
2593 SetCtrlAttribute (g_handle, G_SETUP_Y_Max_G_5, ATTR_DIMMED, 1);
2594 SetAxisScalingMode (extra_g_handle, EXTRA_G_G_5, VAL_LEFT_YAXIS, VAL_AUTOSCALE, 0.0, 0.0);
2595 }
2596 else
2597 {
2598 SetCtrlAttribute (g_handle, G_SETUP_Y_Mode_G_5, ATTR_LABEL_TEXT, "Fixed");
2599 SetCtrlAttribute (g_handle, G_SETUP_Y_Min_G_5, ATTR_DIMMED, 0);
2600 SetCtrlAttribute (g_handle, G_SETUP_Y_Max_G_5, ATTR_DIMMED, 0);
2601 SetAxisScalingMode (extra_g_handle, EXTRA_G_G_5, VAL_LEFT_YAXIS, VAL_MANUAL, Y_Min_G_5, Y_Max_G_5);
2602 }
2603
2604 GraphName(plotVar_G_5, EXTRA_G_G_5, G_SETUP_G5_L_1,G_SETUP_G5_T_1,
2605 G_SETUP_G5_L_2,G_SETUP_G5_T_2,
2606 G_SETUP_G5_L_3,G_SETUP_G5_T_3,
2607 G_SETUP_G5_L_4,G_SETUP_G5_T_4);
2608
2609 return;
2610
2611 //***** ****
2612 // GraphName : Setup Graph Appearance
2613 //***** ****

```

```

2614 void GraphName(int Val, int GRAPH, int L1, int T1, int L2, int T2,
2615                                     int L3, int T3, int L4, int T4)
2616 {
2617     switch(Val)
2618     {
2619         case -2:
2620             SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2621             SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_YNAME, "Not Plotting");
2622             SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_RIGHT_YAXIS);
2623             SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_XNAME, "");
2624
2625             SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2626             SetCtrlVal (g_handle, T1, "");
2627             SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2628             SetCtrlVal (g_handle, T2, "");
2629             SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2630             SetCtrlVal (g_handle, T3, "");
2631             SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2632             SetCtrlVal (g_handle, T4, "");
2633         break;
2634         case -1:
2635             SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2636             SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Not Plotting");
2637             SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_RIGHT_YAXIS);
2638             SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "");
2639             SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2640             SetCtrlVal (g_handle, T1, "");
2641             SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2642             SetCtrlVal (g_handle, T2, "");
2643             SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2644             SetCtrlVal (g_handle, T3, "");
2645             SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2646             SetCtrlVal (g_handle, T4, "");
2647         break;
2648         case 0: // Pressure [Pump#1 & Inlet TP-2]
2649             SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2650             SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Pressure [psi]");
2651             SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2652             SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2653
2654             SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2655             SetCtrlVal (g_handle, T1, "Pressure Pump #1");
2656             SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_WHITE);
2657             SetCtrlVal (g_handle, T2, "Pressure Inlet TP-2");
2658
2659             SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2660             SetCtrlVal (g_handle, T3, "");
2661             SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2662             SetCtrlVal (g_handle, T4, "");
2663         break;
2664         case 1: // Pressure [Pump#2 & Inlet TP-2]
2665             SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2666             SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Pressure [psi]");
2667             SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2668             SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2669
2670             SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2671             SetCtrlVal (g_handle, T1, "Pressure Pump #2");
2672             SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_WHITE);
2673             SetCtrlVal (g_handle, T2, "Pressure Inlet TP-2");
2674
2675             SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2676             SetCtrlVal (g_handle, T3, "");
2677             SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2678             SetCtrlVal (g_handle, T4, "");
2679         break;
2680         case 2: // Pressure [Pump#3 & Inlet TP-2]
2681             SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2682             SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Pressure [psi]");
2683             SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2684             SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2685
2686             SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2687             SetCtrlVal (g_handle, T1, "Pressure Pump #3");
2688             SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_WHITE);
2689             SetCtrlVal (g_handle, T2, "Pressure Inlet TP-2");
2690
2691             SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2692             SetCtrlVal (g_handle, T3, "");
2693             SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2694             SetCtrlVal (g_handle, T4, "");
2695         break;
2696         case 3: // Mass flow rate [M#1] WATER
2697             SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2698             SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Mass flow rate [kg/min]");
2699             SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2700             SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2701             // SetCtrlAttribute (panel_handle, GRAPH, ATTR_XDIVISIONS, 3); number of divisions
2702
2703             SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2704             SetCtrlVal (g_handle, T1, "Mass flow rate [M#1] WATER");
2705
2706             SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2707             SetCtrlVal (g_handle, T2, "");
2708             SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2709             SetCtrlVal (g_handle, T3, "");

```

```

2711 SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2712     SetCtrlVal (g_handle, T4, "");
2713 break;
2714
2715 case 4: // Mass flow rate [M#2] OIL
2716 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2717 SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Mass flow rate [kg/min]");
2718 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2719 SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2720
2721 SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2722     SetCtrlVal (g_handle, T1, "Mass flow rate [M#2] OIL");
2723
2724 SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2725     SetCtrlVal (g_handle, T2, "");
2726 SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2727     SetCtrlVal (g_handle, T3, "");
2728 SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2729     SetCtrlVal (g_handle, T4, "");
2730
2731 break;
2732
2733 case 5: // Mass flow rate [M#3] EMULSION
2734 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2735 SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Mass flow rate [kg/min]");
2736 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2737 SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2738
2739 SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2740     SetCtrlVal (g_handle, T1, "Mass flow rate [M#3] EMULSION");
2741
2742 SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2743     SetCtrlVal (g_handle, T2, "");
2744 SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2745     SetCtrlVal (g_handle, T3, "");
2746 SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2747     SetCtrlVal (g_handle, T4, "");
2748
2749 break;
2750
2751 case 6: // Mass flow rate [M#4] Mixture
2752 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2753 SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Mass flow rate [kg/min]");
2754 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2755 SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2756
2757 SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2758     SetCtrlVal (g_handle, T1, "Mass flow rate [M#4] Mixture [outlet]");
2759
2760 SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2761     SetCtrlVal (g_handle, T2, "");
2762 SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2763     SetCtrlVal (g_handle, T3, "");
2764 SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2765     SetCtrlVal (g_handle, T4, "");
2766
2767 break;
2768
2769 case 7: // Density [M#1] WATER
2770 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2771 SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Density [gm/cm3]");
2772 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2773 SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2774
2775 SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2776     SetCtrlVal (g_handle, T1, "Density [M#1] WATER");
2777
2778 SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2779     SetCtrlVal (g_handle, T2, "");
2780 SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2781     SetCtrlVal (g_handle, T3, "");
2782 SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2783     SetCtrlVal (g_handle, T4, "");
2784
2785 break;
2786
2787 case 8: // Density [M#2] OIL
2788 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2789 SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Density [gm/cm3]");
2790 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2791 SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2792
2793 SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2794     SetCtrlVal (g_handle, T1, "Density [M#2] OIL");
2795
2796 SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2797     SetCtrlVal (g_handle, T2, "");
2798 SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2799     SetCtrlVal (g_handle, T3, "");
2800 SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2801     SetCtrlVal (g_handle, T4, "");
2802
2803 break;
2804
2805
2806 case 9: // Density [M#3] EMULSION
2807 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2808 SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Density [gm/cm3]");
2809 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2810 SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2811
2812 SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2813     SetCtrlVal (g_handle, T1, "Density [M#3] EMULSION");

```

```

2808
2809     SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2810     SetCtrlVal (g_handle, T2, "");
2811     SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2812     SetCtrlVal (g_handle, T3, "");
2813     SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2814     SetCtrlVal (g_handle, T4, "");
2815
2816     break;
2817
2818 case 10: // Density [M#4] Mixture
2819     SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2820     SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Density [gm/cm3]");
2821     SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2822     SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2823
2824     SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2825     SetCtrlVal (g_handle, T1, "Density [M#4] Mixture [outlet]");
2826
2827     SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2828     SetCtrlVal (g_handle, T2, "");
2829     SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2830     SetCtrlVal (g_handle, T3, "");
2831     SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2832     SetCtrlVal (g_handle, T4, "");
2833
2834     break;
2835
2836 case 11: // Pressure TP-2
2837     SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2838     SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Pressure [psi]");
2839     SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2840     SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2841
2842     SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2843     SetCtrlVal (g_handle, T1, "Pressure Inlet TP-2");
2844
2845     SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2846     SetCtrlVal (g_handle, T2, "");
2847     SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2848     SetCtrlVal (g_handle, T3, "");
2849     SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2850     SetCtrlVal (g_handle, T4, "");
2851
2852     break;
2853
2854 case 12: // Pressure dP1
2855     SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2856     SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Pressure [psi]");
2857     SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2858     SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2859
2860     SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2861     SetCtrlVal (g_handle, T1, "Differential pressure dP1");
2862
2863     SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2864     SetCtrlVal (g_handle, T2, "");
2865     SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2866     SetCtrlVal (g_handle, T3, "");
2867     SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2868     SetCtrlVal (g_handle, T4, "");
2869
2870     break;
2871
2872 case 13: // Pressure Delta
2873     SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2874     SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Pressure [psi]");
2875     SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2876     SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2877
2878     SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2879     SetCtrlVal (g_handle, T1, "Differential pressure TP-2 - BPR1");
2880
2881     SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2882     SetCtrlVal (g_handle, T2, "");
2883     SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2884     SetCtrlVal (g_handle, T3, "");
2885     SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2886     SetCtrlVal (g_handle, T4, "");
2887
2888     break;
2889
2890 case 14: // Pressure Delta vs dP1
2891     SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2892     SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Pressure [psi]");
2893     SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2894     SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2895
2896     SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2897     SetCtrlVal (g_handle, T1, "Differential pressure TP-2 - BPR1");
2898     SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_WHITE);
2899     SetCtrlVal (g_handle, T2, "Differential pressure dP1");
2900
2901     SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2902     SetCtrlVal (g_handle, T3, "");
2903     SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2904     SetCtrlVal (g_handle, T4, "");
2905
2906     break;
2907
2908 case 15: // Water inj
2909     SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2910     SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Volume [cc]");
2911

```

```

2905 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2906 SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2907
2908 SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2909     SetCtrlVal (g_handle, T1, "Water injected");
2910
2911 SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2912     SetCtrlVal (g_handle, T2, "");
2913 SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2914     SetCtrlVal (g_handle, T3, "");
2915 SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2916     SetCtrlVal (g_handle, T4, "");
2917
2918 break;
2919
2920 case 16: // Oil inj
2921 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2922 SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Volume [cc]");
2923 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2924 SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2925
2926 SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2927     SetCtrlVal (g_handle, T1, "Oil injected");
2928
2929 SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2930     SetCtrlVal (g_handle, T2, "");
2931 SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2932     SetCtrlVal (g_handle, T3, "");
2933 SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2934     SetCtrlVal (g_handle, T4, "");
2935
2936 break;
2937
2938 case 17: // Emulsion inj
2939 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2940 SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Volume [cc]");
2941 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2942 SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2943
2944 SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2945     SetCtrlVal (g_handle, T1, "Emulsion injected");
2946
2947 SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2948     SetCtrlVal (g_handle, T2, "");
2949 SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2950     SetCtrlVal (g_handle, T3, "");
2951 SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2952     SetCtrlVal (g_handle, T4, "");
2953
2954 break;
2955
2956 case 18: // Temperature water
2957 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2958 SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Temperature [degC]");
2959 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2960 SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2961
2962 SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2963     SetCtrlVal (g_handle, T1, "Water");
2964 SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_YELLOW);
2965     SetCtrlVal (g_handle, T2, "Oil");
2966 SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_DK_YELLOW);
2967     SetCtrlVal (g_handle, T3, "Emulsion");
2968 SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_DK_MAGENTA);
2969     SetCtrlVal (g_handle, T4, "Mixture");
2970
2971 break;
2972
2973
2974 case 19: // Water Flooding
2975 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2976 SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Volume [cc]");
2977 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2978 SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2979
2980 SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
2981     SetCtrlVal (g_handle, T1, "Water flooding");
2982
2983 SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2984     SetCtrlVal (g_handle, T2, "");
2985 SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2986     SetCtrlVal (g_handle, T3, "");
2987 SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
2988     SetCtrlVal (g_handle, T4, "");
2989
2990 break;
2991
2992
2993 case 20: // Water Flooding PV
2994 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
2995 SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Volume [PV]");
2996 SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
2997 SetCtrlAttribute (panel_handle, GRAPH, ATTR_XNAME, "Time [s]");
2998
2999 SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
3000     SetCtrlVal (g_handle, T1, "Water flooding");
3001
3002 SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
3003     SetCtrlVal (g_handle, T2, "");
3004 SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
3005     SetCtrlVal (g_handle, T3, "");
3006 SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
3007     SetCtrlVal (g_handle, T4, "");
3008
3009 break;

```

```

3002
3003     case 21: // WaterIN2PV vs DP1
3004         SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
3005         SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_YNAME, "Pressure [psi]");
3006         SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
3007         SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_XNAME, "Volume inj [PV]");
3008
3009         SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
3010         SetCtrlVal (g_handle, T1, "Differential pressure DP-1");
3011
3012         SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
3013         SetCtrlVal (g_handle, T2, "");
3014         SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
3015         SetCtrlVal (g_handle, T3, "");
3016         SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
3017         SetCtrlVal (g_handle, T4, "");
3018     break;
3019
3020
3021     case 22: // WaterIN2PV vs DP1
3022         SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
3023         SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_YNAME, "Pressure [psi]");
3024         SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
3025         SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_XNAME, "Volume inj [PV]");
3026
3027         SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
3028         SetCtrlVal (g_handle, T1, "REF Differential pressure Delta");
3029
3030         SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_LT_GRAY);
3031         SetCtrlVal (g_handle, T2, "");
3032         SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
3033         SetCtrlVal (g_handle, T3, "");
3034         SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
3035         SetCtrlVal (g_handle, T4, "");
3036     break;
3037
3038     case 23: // WaterIN2PV vs DP1
3039         SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
3040         SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_YNAME, "Pressure [psi]");
3041         SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_ACTIVE_XAXIS, VAL_BOTTOM_XAXIS);
3042         SetCtrlAttribute (extra_g_handle, GRAPH, ATTR_XNAME, "Volume inj [PV]");
3043
3044         SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_RED);
3045         SetCtrlVal (g_handle, T1, "REF Differential pressure Delta");
3046         SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_WHITE);
3047         SetCtrlVal (g_handle, T2, "Differential pressure DP-1");
3048
3049         SetCtrlAttribute (g_handle, L3, ATTR_FRAME_COLOR, VAL_LT_GRAY);
3050         SetCtrlVal (g_handle, T3, "");
3051         SetCtrlAttribute (g_handle, L4, ATTR_FRAME_COLOR, VAL_LT_GRAY);
3052         SetCtrlVal (g_handle, T4, "");
3053     break;
3054
3055     case 24: // Experiment Stage
3056         SetCtrlAttribute (panel_handle, GRAPH, ATTR_ACTIVE_YAXIS, VAL_LEFT_YAXIS);
3057
3058         SetCtrlAttribute (panel_handle, GRAPH, ATTR_YNAME, "Experiment Stage");
3059         SetCtrlAttribute (g_handle, L1, ATTR_FRAME_COLOR, VAL_LT_GRAY);
3060         SetCtrlVal (g_handle, T1, "0 (Temp), 1 (Active), 2 (Thixo.)");
3061         SetCtrlAttribute (panel_handle, GRAPH, ATTR_YDIVISIONS, 3);
3062         SetCtrlAttribute (g_handle, L2, ATTR_FRAME_COLOR, VAL_RED);
3063         SetCtrlVal (g_handle, T2, "");
3064     }
3065
3066
3067 //*****
3068 // Save Vars : Save screen to variables
3069 // build based on DSN_Save_Vars
3070 //*****
3071 void SaveVars(void)
3072 { // int i;
3073
3074 // MAIN PANEL
3075
3076
3077
3078
3079 // COM Ports
3080 GetCtrlVal(panel_handle, MAIN_LOG_P1, &Is_P1);
3081 GetCtrlVal(panel_handle, MAIN_LOG_P2, &Is_P2);
3082 GetCtrlVal(panel_handle, MAIN_LOG_P3, &Is_P3);
3083 // Mass Flow Meters
3084 GetCtrlVal(panel_handle, MAIN_LOG_M1, &Is_M1);
3085 GetCtrlVal(panel_handle, MAIN_LOG_M2, &Is_M2);
3086 GetCtrlVal(panel_handle, MAIN_LOG_M3, &Is_M3);
3087 GetCtrlVal(panel_handle, MAIN_LOG_M4, &Is_M4);
3088
3089 // Back Pressure Regulator
3090 GetCtrlVal(panel_handle, MAIN_LOG_BPR, &Is_BPR);
3091 // Main Parameters
3092 GetCtrlVal(panel_handle, MAIN_LOG_Graph, &Is_Graph);
3093
3094 GetCtrlVal(panel_handle, MAIN_LOG_DAQ, &Is_DAQ);
3095
3096 GetCtrlVal(panel_handle, MAIN_LOG_LOGToFile, &Is_Log);
3097 // Equipment Setup
3098

```

```

3099
3100
3101
3102 // GRAPH PANEL
3103 //Read Graph #1
3104 GetCtrlVal( g_handle, G_SETUP_Var_G_1, &plotVar_G_1);
3105 GetCtrlVal( g_handle, G_SETUP_X_Range_G_1, &x_Range_G_1);
3106 GetCtrlVal( g_handle, G_SETUP_Y_Mode_G_1, &y_Mode_G_1);
3107 GetCtrlVal( g_handle, G_SETUP_Y_Min_G_1, &y_Min_G_1);
3108 GetCtrlVal( g_handle, G_SETUP_Y_Max_G_1, &y_Max_G_1);
3109 if (Y_Min_G_1 >= Y_Max_G_1)
3110     Y_Min_G_1 = Y_Max_G_1-0.5;
3111 SetCtrlVal( g_handle, G_SETUP_Y_Min_G_1, Y_Min_G_1);
3112 //Read Graph #2
3113 GetCtrlVal( g_handle, G_SETUP_Var_G_2, &plotVar_G_2);
3114 GetCtrlVal( g_handle, G_SETUP_X_Range_G_2, &x_Range_G_2);
3115 GetCtrlVal( g_handle, G_SETUP_Y_Mode_G_2, &y_Mode_G_2);
3116 GetCtrlVal( g_handle, G_SETUP_Y_Min_G_2, &y_Min_G_2);
3117 GetCtrlVal( g_handle, G_SETUP_Y_Max_G_2, &y_Max_G_2);
3118 if (Y_Min_G_2 >= Y_Max_G_2)
3119     Y_Min_G_2 = Y_Max_G_2-0.5;
3120 SetCtrlVal( g_handle, G_SETUP_Y_Min_G_2, Y_Min_G_2);
3121 //Read Graph #3
3122 GetCtrlVal( g_handle, G_SETUP_Var_G_3, &plotVar_G_3);
3123 GetCtrlVal( g_handle, G_SETUP_X_Range_G_3, &x_Range_G_3);
3124 GetCtrlVal( g_handle, G_SETUP_Y_Mode_G_3, &y_Mode_G_3);
3125 GetCtrlVal( g_handle, G_SETUP_Y_Min_G_3, &y_Min_G_3);
3126 GetCtrlVal( g_handle, G_SETUP_Y_Max_G_3, &y_Max_G_3);
3127 if (Y_Min_G_3 >= Y_Max_G_3)
3128     Y_Min_G_3 = Y_Max_G_3-0.5;
3129 SetCtrlVal( g_handle, G_SETUP_Y_Min_G_3, Y_Min_G_3);
3130 //Read Graph #4
3131 GetCtrlVal( g_handle, G_SETUP_Var_G_4, &plotVar_G_4);
3132 GetCtrlVal( g_handle, G_SETUP_X_Range_G_4, &x_Range_G_4);
3133 GetCtrlVal( g_handle, G_SETUP_Y_Mode_G_4, &y_Mode_G_4);
3134 GetCtrlVal( g_handle, G_SETUP_Y_Min_G_4, &y_Min_G_4);
3135 GetCtrlVal( g_handle, G_SETUP_Y_Max_G_4, &y_Max_G_4);
3136 if (Y_Min_G_4 >= Y_Max_G_4)
3137     Y_Min_G_4 = Y_Max_G_4-0.5;
3138 SetCtrlVal( g_handle, G_SETUP_Y_Min_G_4, Y_Min_G_4);
3139 //Read Graph #5
3140 GetCtrlVal( g_handle, G_SETUP_Var_G_5, &plotVar_G_5);
3141 //X
3142 GetCtrlVal( g_handle, G_SETUP_X_Mode_G_5, &x_Mode_G_5);
3143 GetCtrlVal( g_handle, G_SETUP_X_Min_G_5, &x_Min_G_5);
3144 GetCtrlVal( g_handle, G_SETUP_X_Max_G_5, &x_Max_G_5);
3145 if (X_Min_G_5 >= X_Max_G_5)
3146     X_Min_G_5 = X_Max_G_5-0.5;
3147 SetCtrlVal( g_handle, G_SETUP_X_Min_G_5, X_Min_G_5);
3148 //Y
3149 GetCtrlVal( g_handle, G_SETUP_Y_Mode_G_5, &y_Mode_G_5);
3150 GetCtrlVal( g_handle, G_SETUP_Y_Min_G_5, &y_Min_G_5);
3151 GetCtrlVal( g_handle, G_SETUP_Y_Max_G_5, &y_Max_G_5);
3152 if (Y_Min_G_5 >= Y_Max_G_5)
3153     Y_Min_G_5 = Y_Max_G_5-0.5;
3154 SetCtrlVal( g_handle, G_SETUP_Y_Min_G_5, Y_Min_G_5);
3155 GetCtrlVal( panel_handle, MAIN_VIS_W, &VIS_WATER);
3156 GetCtrlVal( panel_handle, MAIN_VIS_O, &VIS_OIL);
3157 GetCtrlVal( panel_handle, MAIN_VIS_EM, &VIS_EMUL);
3158 //Units for permeability and viscosity
3159 vispermunit();
3160
3161
3162 // COM Panel
3163 GetConfigParms();
3164
3165 return;
3166 }
3167
3168 /*-----*/
3169 /* Get the port configuration parameters. */
3170 /*-----*/
3171
3172 void GetConfigParms (void)
3173 {
3174     GetCtrlVal (config_handle, CONFIG_CAMNAME, camName);
3175
3176     // COM Panel
3177     //#
3178     GetCtrlVal (config_handle, CONFIG_P1_COMPORT, &p1_comport);
3179     GetCtrlVal (config_handle, CONFIG_P1_BAUDRATE, &p1_baudrate);
3180     GetCtrlVal (config_handle, CONFIG_P1_PARITY, &p1_parity);
3181     GetCtrlVal (config_handle, CONFIG_P1_DATABITS, &p1.databits);
3182     GetCtrlVal (config_handle, CONFIG_P1_STOPBITS, &p1_stopbits);
3183     GetCtrlVal (config_handle, CONFIG_P1_INPUTQ, &p1_inputq);
3184     GetCtrlVal (config_handle, CONFIG_P1_OUTPUTQ, &p1_outputq);
3185     GetCtrlIndex (config_handle, CONFIG_P1_COMPORT, &p1_portindex);
3186     //#
3187     GetCtrlVal (config_handle, CONFIG_P2_COMPORT, &p2_comport);
3188     GetCtrlVal (config_handle, CONFIG_P2_BAUDRATE, &p2_baudrate);
3189     GetCtrlVal (config_handle, CONFIG_P2_PARITY, &p2_parity);
3190     GetCtrlVal (config_handle, CONFIG_P2_DATABITS, &p2.databits);
3191     GetCtrlVal (config_handle, CONFIG_P2_STOPBITS, &p2_stopbits);
3192     GetCtrlVal (config_handle, CONFIG_P2_INPUTQ, &p2_inputq);
3193     GetCtrlVal (config_handle, CONFIG_P2_OUTPUTQ, &p2_outputq);
3194     GetCtrlIndex (config_handle, CONFIG_P2_COMPORT, &p2_portindex);
3195     //#

```

```

3196 GetCtrlVal (config_handle, CONFIG_P3_COMPORT, &P3_comport);
3197 GetCtrlVal (config_handle, CONFIG_P3_BAUDRATE, &P3_baudrate);
3198 GetCtrlVal (config_handle, CONFIG_P3_PARITY, &P3_parity);
3199 GetCtrlVal (config_handle, CONFIG_P3_DATABITS, &P3.databits);
3200 GetCtrlVal (config_handle, CONFIG_P3_STOPBITS, &P3_stopbits);
3201 GetCtrlVal (config_handle, CONFIG_P3_INPUTQ, &P3_inputq);
3202 GetCtrlVal (config_handle, CONFIG_P3_OUTPUTQ, &P3_outputq);
3203 GetCtrlIndex (config_handle, CONFIG_P3_COMPORT, &P3_portindex);
3204
3205 }
3206 //***** Load_Vars : Load variables to the screen
3207 // build based on DSN Load_Vars
3208 //*****
3209
3210 void LoadVars(void)
3211 {
3212 //MAIN PANEL
3213 // Main Parameters
3214 SetCtrlVal(panel_handle, MAIN_LOG_Graph, Is_Graph);
3215 SetCtrlVal(panel_handle, MAIN_LOG_LogToFile, Is_Log);
3216 // COM Ports (data from pumps)
3217 SetCtrlVal(panel_handle, MAIN_LOG_P1, Is_P1);
3218 SetCtrlVal(panel_handle, MAIN_LOG_P2, Is_P2);
3219 SetCtrlVal(panel_handle, MAIN_LOG_P3, Is_P3);
3220 // Mass Flow Meters
3221 SetCtrlVal(panel_handle, MAIN_LOG_M1, Is_M1);
3222 SetCtrlVal(panel_handle, MAIN_LOG_M2, Is_M2);
3223 SetCtrlVal(panel_handle, MAIN_LOG_M3, Is_M3);
3224 SetCtrlVal(panel_handle, MAIN_LOG_M4, Is_M4);
3225 // Back Pressure Regulator
3226 SetCtrlVal(panel_handle, MAIN_LOG_BPR, Is_BPR);
3227 // DAQ
3228 SetCtrlVal(panel_handle, MAIN_LOG_DAQ, Is_DAQ);
3229
3230 // GRAPH PANEL
3231 //Read Graph #1
3232 SetCtrlVal( g_handle, G_SETUP_Var_G_1, plotVar_G_1);
3233 SetCtrlVal( g_handle, G_SETUP_X_Range_G_1, X_Range_G_1);
3234 SetCtrlVal( g_handle, G_SETUP_Y_Mode_G_1, Y_Mode_G_1);
3235 SetCtrlVal( g_handle, G_SETUP_Y_Min_G_1, Y_Min_G_1);
3236 SetCtrlVal( g_handle, G_SETUP_Y_Max_G_1, Y_Max_G_1);
3237 //Read Graph #2
3238 SetCtrlVal( g_handle, G_SETUP_Var_G_2, plotVar_G_2);
3239 SetCtrlVal( g_handle, G_SETUP_X_Range_G_2, X_Range_G_2);
3240 SetCtrlVal( g_handle, G_SETUP_Y_Mode_G_2, Y_Mode_G_2);
3241 SetCtrlVal( g_handle, G_SETUP_Y_Min_G_2, Y_Min_G_2);
3242 SetCtrlVal( g_handle, G_SETUP_Y_Max_G_2, Y_Max_G_2);
3243 //Read Graph #3
3244 SetCtrlVal( g_handle, G_SETUP_Var_G_3, plotVar_G_3);
3245 SetCtrlVal( g_handle, G_SETUP_X_Range_G_3, X_Range_G_3);
3246 SetCtrlVal( g_handle, G_SETUP_Y_Mode_G_3, Y_Mode_G_3);
3247 SetCtrlVal( g_handle, G_SETUP_Y_Min_G_3, Y_Min_G_3);
3248 SetCtrlVal( g_handle, G_SETUP_Y_Max_G_3, Y_Max_G_3);
3249 //Read Graph #4
3250 SetCtrlVal( g_handle, G_SETUP_Var_G_4, plotVar_G_4);
3251 SetCtrlVal( g_handle, G_SETUP_X_Range_G_4, X_Range_G_4);
3252 SetCtrlVal( g_handle, G_SETUP_Y_Mode_G_4, Y_Mode_G_4);
3253 SetCtrlVal( g_handle, G_SETUP_Y_Min_G_4, Y_Min_G_4);
3254 SetCtrlVal( g_handle, G_SETUP_Y_Max_G_4, Y_Max_G_4);
3255 //Read Graph #5
3256 SetCtrlVal( g_handle, G_SETUP_Var_G_5, plotVar_G_5);
3257 SetCtrlVal( g_handle, G_SETUP_X_Mode_G_5, X_Mode_G_5);
3258 SetCtrlVal( g_handle, G_SETUP_X_Min_G_5, X_Min_G_5);
3259 SetCtrlVal( g_handle, G_SETUP_X_Max_G_5, X_Max_G_5);
3260 SetCtrlVal( g_handle, G_SETUP_Y_Mode_G_5, Y_Mode_G_5);
3261 SetCtrlVal( g_handle, G_SETUP_Y_Min_G_5, Y_Min_G_5);
3262 SetCtrlVal( g_handle, G_SETUP_Y_Max_G_5, Y_Max_G_5);
3263
3264 SetCtrlVal (panel_handle, MAIN_WATERTANK, G_WATERINJ[0]);
3265 SetCtrlVal (panel_handle, MAIN_OILTANK, G_OILINJ[0]);
3266 SetCtrlVal (panel_handle, MAIN_EMULTANK, G_EMULINJ[0]);
3267
3268 SetCtrlVal (panel_handle, MAIN_OUTLETTANK, OUTLET[0]);
3269
3270 SetCtrlVal (panel_handle, MAIN_VIS_W, VIS_WATER);
3271 SetCtrlVal (panel_handle, MAIN_VIS_O, VIS_OIL);
3272 SetCtrlVal (panel_handle, MAIN_VIS_EM, VIS_EMUL);
3273
3274 if (viscoef == 1) SetCtrlVal (panel_handle, MAIN_VIS_UNIT, 2);
3275 else SetCtrlVal (panel_handle, MAIN_VIS_UNIT, 0);
3276 if (permcoef == 1) SetCtrlVal (panel_handle, MAIN_PERM_UNIT, 0);
3277 else SetCtrlVal (panel_handle, MAIN_PERM_UNIT, 1);
3278
3279 G_WATERINJ[1]=G_WATERINJ[0];
3280 G_OILINJ[1]= G_OILINJ[0];
3281 G_EMULINJ[1]=G_EMULINJ[0];
3282
3283 OUTLET[1]=OUTLET[0];
3284
3285 // COM_PANEL
3286 SetConfigParms ();
3287
3288
3289
3290
3291
3292

```

```

3293     return;
3294 }
3295
3296 /*-----*/
3297 /* Set configuration parameters. */
3298 /*-----*/
3299
3300 void SetConfigParms (void)
{
    // Camera
    SetCtrlVal (config_handle, CONFIG_CAMNAME,      camName);

    // COM Panel
    //#1
    SetCtrlVal (config_handle, CONFIG_P1_COMPORT,   P1_comport);
    SetCtrlVal (config_handle, CONFIG_P1_BAUDRATE,   P1_baudrate);
    SetCtrlVal (config_handle, CONFIG_P1_PARITY,     P1_parity);
    SetCtrlVal (config_handle, CONFIG_P1_DATABITS,   P1_datubits);
    SetCtrlVal (config_handle, CONFIG_P1_STOPBITS,   P1_stopbits);
    SetCtrlVal (config_handle, CONFIG_P1_INPUTQ,     P1_inputq);
    SetCtrlVal (config_handle, CONFIG_P1_OUTPUTQ,    P1_outputq);
    SetCtrlVal (config_handle, CONFIG_P1_CTSMODE,    P1_ctsmode);
    SetCtrlVal (config_handle, CONFIG_P1_XMODE,      P1_xmode);
    SetCtrlVal (config_handle, CONFIG_P1_TIMEOUT,    P1_timeout);
    SetCtrlIndex (config_handle, CONFIG_P1_COMPORT,P1_portindex);
    //#2
    SetCtrlVal (config_handle, CONFIG_P2_COMPORT,   P2_comport);
    SetCtrlVal (config_handle, CONFIG_P2_BAUDRATE,   P2_baudrate);
    SetCtrlVal (config_handle, CONFIG_P2_PARITY,     P2_parity);
    SetCtrlVal (config_handle, CONFIG_P2_DATABITS,   P2_datubits);
    SetCtrlVal (config_handle, CONFIG_P2_STOPBITS,   P2_stopbits);
    SetCtrlVal (config_handle, CONFIG_P2_INPUTQ,     P2_inputq);
    SetCtrlVal (config_handle, CONFIG_P2_OUTPUTQ,    P2_outputq);
    SetCtrlVal (config_handle, CONFIG_P2_CTSMODE,    P2_ctsmode);
    SetCtrlVal (config_handle, CONFIG_P2_XMODE,      P2_xmode);
    SetCtrlVal (config_handle, CONFIG_P2_TIMEOUT,    P2_timeout);
    SetCtrlIndex (config_handle, CONFIG_P2_COMPORT,P2_portindex);
    //#3
    SetCtrlVal (config_handle, CONFIG_P3_COMPORT,   P3_comport);
    SetCtrlVal (config_handle, CONFIG_P3_BAUDRATE,   P3_baudrate);
    SetCtrlVal (config_handle, CONFIG_P3_PARITY,     P3_parity);
    SetCtrlVal (config_handle, CONFIG_P3_DATABITS,   P3_datubits);
    SetCtrlVal (config_handle, CONFIG_P3_STOPBITS,   P3_stopbits);
    SetCtrlVal (config_handle, CONFIG_P3_INPUTQ,     P3_inputq);
    SetCtrlVal (config_handle, CONFIG_P3_OUTPUTQ,    P3_outputq);
    SetCtrlVal (config_handle, CONFIG_P3_CTSMODE,    P3_ctsmode);
    SetCtrlVal (config_handle, CONFIG_P3_XMODE,      P3_xmode);
    SetCtrlVal (config_handle, CONFIG_P3_TIMEOUT,    P3_timeout);
    SetCtrlIndex (config_handle, CONFIG_P3_COMPORT,P3_portindex);
}
3343
3344 //***** OnOff_Graphs : For Turning Graphs ON and OFF (Dimming)
3345 // same as DSN_OnOff_Graphs
3346 //*****
3347
3348
3349 int CVICALLBACK OnOff_Graphs (int panel, int control, int event,
3350     void *callbackData, int eventData1, int eventData2)
3351 {   int test;
3352     switch (event)
3353     {
3354         case EVENT_COMMIT:
3355             switch (control)
3356             {
3357                 case G_SETUP_OnOff_G_1:
3358                     GetCtrlVal (g_handle, G_SETUP_OnOff_G_1, &test);
3359                     if(test)
3360                     {
3361                         SetCtrlAttribute (panel_handle, MAIN_G_1, ATTR_VISIBLE, 1);
3362                         OnOff_G1 = 1;
3363                     }
3364                 else
3365                     {
3366                         SetCtrlAttribute (panel_handle, MAIN_G_1, ATTR_VISIBLE, 0);
3367                         OnOff_G1 = 0;
3368                     }
3369                 break;
3370             case G_SETUP_OnOff_G_2:
3371                 GetCtrlVal (g_handle, G_SETUP_OnOff_G_2, &test);
3372                 if(test)
3373                     {
3374                         SetCtrlAttribute (panel_handle, MAIN_G_2, ATTR_VISIBLE, 1);
3375                         OnOff_G2 = 1;
3376                     }
3377                 else
3378                     {
3379                         SetCtrlAttribute (panel_handle, MAIN_G_2, ATTR_VISIBLE, 0);
3380                         OnOff_G2 = 0;
3381                     }
3382                 break;
3383             case G_SETUP_OnOff_G_3:
3384                 GetCtrlVal (g_handle, G_SETUP_OnOff_G_3, &test);
3385                 if(test)
3386                     {
3387                         SetCtrlAttribute (panel_handle, MAIN_G_3, ATTR_VISIBLE, 1);
3388                         OnOff_G3 = 1;
3389                     }
}

```

```

3390     else
3391     {
3392         SetCtrlAttribute (panel_handle, MAIN_G_3, ATTR_VISIBLE, 0);
3393         OnOff_G3 = 0;
3394     }
3395     break;
3396 case G_SETUP_OnOff_G_4:
3397     GetCtrlVal (g_handle, G_SETUP_OnOff_G_4, &test);
3398     if(test)
3399     {
3400         SetCtrlAttribute (panel_handle, MAIN_G_4, ATTR_VISIBLE, 1);
3401         OnOff_G4 = 1;
3402     }
3403     else
3404     {
3405         SetCtrlAttribute (panel_handle, MAIN_G_4, ATTR_VISIBLE, 0);
3406         OnOff_G4 = 0;
3407     }
3408     break;
3409 case G SETUP OnOff_G_5:
3410     GetCtrlVal (g_handle, G_SETUP_OnOff_G_5, &test);
3411     if(test)
3412     {
3413         DisplayPanel(extra_g_handle);
3414         OnOff_G5 = 1;
3415     }
3416     else
3417     {
3418         HidePanel (extra_g_handle);
3419         OnOff_G5 = 0;
3420     }
3421     break;
3422 case G_SETUP_OnOff_G_6:
3423     GetCtrlVal (g_handle, G_SETUP_OnOff_G_6, &test);
3424     if(test)
3425     {
3426         OnOff_G6 = 1;
3427     }
3428     else
3429     {
3430         OnOff_G6 = 0;
3431     }
3432     break;
3433     }
3434     break;
3435     case EVENT_RIGHT_CLICK:
3436         break;
3437     }
3438 }
3439 return 0;
3440 }
3441
3442 int CVICALLBACK SHOW_Graphs (int panel, int control, int event,
3443     void *callbackData, int eventData1, int eventData2)
3444 {
3445     switch (event)
3446     {
3447         case EVENT_COMMIT:
3448             break;
3449         case EVENT_RIGHT_CLICK:
3450             DisplayPanel(g_handle);
3451             break;
3452         }
3453     }
3454     return 0;
3455 }
3456 }
3457 }
3458 */
3459 /* Pumps_ThreadFunction () : - Separate Thread for Pumps */
3460 */
3461
3462
3463 int CVICALLBACK Pumps_ThreadFunction (void *functionData) //connecting to the pumps
3464 {
3465
3466     while (Pumps_quitflag == 1)
3467     {
3468         ProcessSystemEvents ();
3469         Delay (0.5);
3470         if (Is_P1) { CheckPressurePump1(); } //update information about pressure
3471         Delay (0.5);
3472         if (Is_P2) { CheckPressurePump2(); } //update information about pressure
3473         Delay (0.5);
3474         if (Is_P3) { CheckPressurePump3(); } //update information about pressure
3475
3476         ProcessSystemEvents ();
3477     }
3478     return 0;
3479 }
3480
3481
3482 int CVICALLBACK Camera_ThreadFunction(void *functionData)
3483 {
3484     while (Camera_quitflag == 1)
3485     {
3486         ProcessSystemEvents ();

```

```

3487     Delay (0.5);
3488     if (Is_Cam)
3489     {
3490         //RUN the timer to do the GRAB and DISPLAY
3491         SetCtrlAttribute (panel_handle, MAIN_TIMER_2, ATTR_ENABLED, TRUE); }
3492     else // RUN the timer to do the GRAB and DISPLAY
3493         SetCtrlAttribute (panel_handle, MAIN_TIMER_2, ATTR_ENABLED, FALSE);
3494     //update information about pressure
3495     ProcessSystemEvents ();
3496 }
3497 }
3498
3499 int CVICALLBACK Email_ThreadFunction(void *functionData)
3500 {
3501     double temptube;
3502     while (Email_quitflag == 1)
3503     {
3504         ProcessSystemEvents ();
3505         Delay (0.5);
3506         if (globalemail == 1)
3507         {
3508             GetCtrlVal(panel_handle, MAIN_CUR_TTUBE, &temptube);
3509
3510             //Generate results
3511             sprintf(currentresults, "cmd.exe /c sendEmail -f cmcprojectlab@gmail.com -t 3666377@gmail.com -s smtp.gmail.com:587
-xu cmcprojectlab@gmail.com -xp cmcproject2013 -u \"cmcproject\" -m \"TEST TUBE = %3.1f WATER INJ = %4.2f EMUL INJ = %4.2f This
message has been sent by software\"", temptube,WATERINJ2PV[1],EMULIN[1]);
3512             //Send email with results
3513             system(currentresults);
3514             globalemail = 0;
3515         }
3516     }
3517     ProcessSystemEvents ();
3518 }
3519 }
3520 return 0;
3521 }
3522
3523
3524
3525
3526 int CVICALLBACK Mass_ThreadFunction (void *functionData) //connecting to the mass flow meters
3527 { int conreq_M1,
3528     conreq_M2,
3529     conreq_M3,
3530     conreq_M4;
3531
3532     while (Mass_quitflag == 1)
3533     {
3534         ProcessSystemEvents ();
3535
3536         GetCtrlVal(config_handle,CONFIG_CON_M_1,&conreq_M1);
3537         GetCtrlVal(config_handle,CONFIG_CON_M_2,&conreq_M2);
3538         GetCtrlVal(config_handle,CONFIG_CON_M_3,&conreq_M3);
3539         GetCtrlVal(config_handle,CONFIG_CON_M_4,&conreq_M4);
3540
3541         //Mass flow meter #1 Water//
3542         if(conreq_M1 == 1)
3543         {
3544             ConnectToDDEServer (&hConv, "FlowDDE", "C(1)", DDECallback, 0);
3545             conreq_M1=0; Is_M1=1;
3546             SetCtrlVal(config_handle,CONFIG_CON_M_1, conreq_M1);
3547             SetCtrlVal(panel_handle,MAIN_LOG_M1, Is_M1);
3548             SetCtrlVal (config_handle, CONFIG_M1_LED, 1);
3549             Update_Graphics();
3550         }
3551         else if (conreq_M1 == -1)
3552         {
3553             DisconnectFromDDEServer (hConv);
3554             conreq_M1=0; Is_M1=0;
3555             SetCtrlVal(config_handle,CONFIG_CON_M_1, conreq_M1);
3556             SetCtrlVal(panel_handle,MAIN_LOG_M1, Is_M1);
3557             SetCtrlVal (config_handle, CONFIG_M1_LED, 0);
3558             Update_Graphics();
3559         }
3560         if (Is_M1) READ_FLOW_M_1();
3561     //Mass flow meter #1 Water/
3562
3563     //Mass flow meter #2 Oil//
3564     if(conreq_M2 == 1)
3565     {
3566         ConnectToDDEServer (&hConv2, "FlowDDE2", "C(1)", DDECallback, 0);
3567         conreq_M2=0; Is_M2=1;
3568         SetCtrlVal(config_handle,CONFIG_CON_M_2, conreq_M2);
3569         SetCtrlVal(panel_handle,MAIN_LOG_M2, Is_M2);
3570         SetCtrlVal (config_handle, CONFIG_M2_LED, 1);
3571         Update_Graphics();
3572     }
3573     else if (conreq_M2 == -1)
3574     {
3575         DisconnectFromDDEServer (hConv2);
3576         conreq_M2=0; Is_M2=0;
3577         SetCtrlVal(config_handle,CONFIG_CON_M_2, conreq_M2);
3578         SetCtrlVal(panel_handle,MAIN_LOG_M2, Is_M2);
3579         SetCtrlVal (config_handle, CONFIG_M2_LED, 0);
3580         Update Graphics();
3581     }

```

```

3582     }
3583     if (Is_M2) READ_FLOW_M_2();
3584 //Mass flow meter #2 Oil//
3585
3586     //Mass flow meter #3 Emulsion//
3587     if(conreq_M3 == 1)
3588     {
3589         ConnectToDDEServer (&hConv3, "FlowDDE3", "C(1)", DDECallback, 0);
3590         conreq_M3=0; Is_M3=1;
3591         SetCtrlVal(config_handle,CONFIG_CON_M_3, conreq_M3);
3592         SetCtrlVal(panel_handle,MAIN_LOG_M3, Is_M3);
3593         SetCtrlVal (config_handle, CONFIG_M3_LED, 1);
3594         Update_Graphics();
3595     }
3596     else if (conreq_M3 == -1)
3597     {
3598         DisconnectFromDDEServer (hConv3);
3599         conreq_M3=0; Is_M3=0;
3600         SetCtrlVal(config_handle,CONFIG_CON_M_3, conreq_M3);
3601         SetCtrlVal(panel_handle,MAIN_LOG_M3, Is_M3);
3602         SetCtrlVal (config_handle, CONFIG_M3_LED, 0);
3603         Update_Graphics();
3604     }
3605     if (Is_M3) READ_FLOW_M_3();
3606 //Mass flow meter #3 Emulsion//
```

3607 //Mass flow meter #4 Mixture//

```

3608     if(conreq_M4 == 1)
3609     {
3610         ConnectToDDEServer (&hConv4, "FlowDDE4", "C(1)", DDECallback, 0);
3611         conreq_M4=0; Is_M4=1;
3612         SetCtrlVal(config_handle,CONFIG_CON_M_4, conreq_M4);
3613         SetCtrlVal(panel_handle,MAIN_LOG_M4, Is_M4);
3614         SetCtrlVal (config_handle, CONFIG_M4_LED, 1);
3615         Update_Graphics();
3616     }
3617     else if (conreq_M4 == -1)
3618     {
3619         DisconnectFromDDEServer (hConv4);
3620         conreq_M4=0; Is_M4=0;
3621         SetCtrlVal(config_handle,CONFIG_CON_M_4, conreq_M4);
3622         SetCtrlVal(panel_handle,MAIN_LOG_M4, Is_M4);
3623         SetCtrlVal (config_handle, CONFIG_M4_LED, 0);
3624         Update_Graphics();
3625     }
3626     if (Is_M4) READ_FLOW_M_4();
3627 //Mass flow meter #4 Mixture//
```

3628 ProcessSystemEvents ();

3629 }

3630 }

3631 }

3632 return 0;

3633 }

3634

3635 void READ\_FLOW\_M\_1(void)

3636 {

3637 double

3638 data,

3639 data2,

3640 data3,

3641 data4;

3642

3643 ProcessSystemEvents ();

3644

3645 Delay(0.01);

3646 ClientDDERead (hConv, "P(270)", CF\_TEXT, read\_m11data, 64, 0);

3647 data=atof(read\_m11data);

3648 SetCtrlVal (panel\_handle, MAIN\_DENSITY\_M\_1, data); // send value of "data" to panel

3649

3650 Delay(0.01);

3651 ClientDDERead (hConv, "P(142)", CF\_TEXT, read\_m12data, 64, 0);

3652 data2=atof(read\_m12data);

3653 SetCtrlVal (panel\_handle, MAIN\_TEMP\_M\_1, data2);

3654

3655 Delay(0.01);

3656 ClientDDERead (hConv, "P(205)", CF\_TEXT, read\_m13data, 64, 0);

3657 data3=atof(read\_m13data);

3658 SetCtrlVal (panel\_handle, MAIN\_MFR\_M\_1, data3);

3659

3660 data4=data3 \* data \* 0.001 ; // cc/min \* kg /m^3 = 0.001 \* gm/min

3661

3662 // Delay(0.01); //P(198)

3663 // ClientDDERead (hConv, "P(205)", CF\_TEXT, read\_m14data, 64, 0);

3664 // data4=atof(read\_m14data);

3665

3666 SetCtrlVal (panel\_handle, MAIN\_EXTRA1\_M\_1, data4);

3667

3668 CmtGetLock (Mass\_lockHandle);

3669 DSN SHIFT\_MASS(0);

3670 M11[0] = data;

3671 M12[0] = data2;

3672 M13[0] = data3; //volume flow rate cc/min \_ P205

3673 M14[0] = data4; //Real mass flow in kg/min

3674 CmtReleaseLock (Mass\_lockHandle);

3675

3676

3677 ProcessSystemEvents ();

3678 }

```

3679
3680 void READ_FLOW_M_2(void)
3681 {
3682     double data,
3683     data2,
3684     data3,
3685     data4;
3686
3687 ProcessSystemEvents ();
3688
3689     Delay(0.01);
3690     ClientDDERead (hConv2, "P(270)", CF_TEXT, read_m21data, 64, 0);
3691     data=atof(read_m21data);
3692     SetCtrlVal (panel_handle, MAIN_DENSITY_M_2, data); // send value of "data" to panel
3693
3694     Delay(0.01);
3695     ClientDDERead (hConv2, "P(142)", CF_TEXT, read_m22data, 64, 0);
3696     data2=atof(read_m22data);
3697     SetCtrlVal (panel_handle, MAIN_TEMP_M_2, data2);
3698
3699     Delay(0.01);
3700     ClientDDERead (hConv2, "P(205)", CF_TEXT, read_m23data, 64, 0);
3701     data3=atof(read_m23data);
3702     SetCtrlVal (panel_handle, MAIN_MFR_M_2, data3);
3703
3704     data4=data3 * data * 0.001 ; // cc/min * kg /m^3 = 0.001 * gm/min
3705
3706 // Delay(0.01); //P(198)
3707 // ClientDDERead (hConv2, "P(205)", CF_TEXT, read_m24data, 64, 0);
3708 // data4=atof(read_m24data);
3709
3710     SetCtrlVal (panel_handle, MAIN_EXTRA1_M_2, data4);
3711
3712
3713     CmtGetLock (Mass_lockHandle);
3714     DSN_SHIFT_MASS(1);
3715     M21[0] = data;
3716     M22[0] = data2;
3717     M23[0] = data3; //volume flow rate in cc/min
3718     M24[0] = data4; //real mass flow in kg/min
3719     CmtReleaseLock (Mass_lockHandle);
3720
3721
3722
3723
3724 ProcessSystemEvents ();
3725 }
3726
3727 void READ_FLOW_M_3(void)
3728 {
3729     double data,
3730     data2,
3731     data3,
3732     data4,
3733     temp_time_e=0.0,
3734     temp_delta_e=0.0,
3735     temp_emul_in=0.0,
3736     temp_emul_in_pv=0.0;
3737
3738 ProcessSystemEvents ();
3739
3740     Delay(0.01);
3741     ClientDDERead (hConv3, "P(270)", CF_TEXT, read_m31data, 64, 0);
3742     data=atof(read_m31data);
3743     SetCtrlVal (panel_handle, MAIN_DENSITY_M_3, data); // send value of "data" to panel
3744
3745     Delay(0.01);
3746     ClientDDERead (hConv3, "P(142)", CF_TEXT, read_m32data, 64, 0);
3747     data2=atof(read_m32data);
3748     SetCtrlVal (panel_handle, MAIN_TEMP_M_3, data2);
3749
3750     Delay(0.01);
3751     ClientDDERead (hConv3, "P(205)", CF_TEXT, read_m33data, 64, 0);
3752     data3=atof(read_m33data);
3753     SetCtrlVal (panel_handle, MAIN_MFR_M_3, data3);
3754
3755     data4=data3 * data * 0.001 ; // cc/min * kg /m^3 = 0.001 * gm/min
3756
3757 // Delay(0.01); //P(198)
3758 // ClientDDERead (hConv3, "P(205)", CF_TEXT, read_m34data, 64, 0);
3759 // data4=atof(read_m34data);
3760
3761     SetCtrlVal (panel_handle, MAIN_EXTRA1_M_3, data4);
3762
3763 Gtime_E [0] = Timer (); // Get Time
3764
3765 if (stage ==10 && pumprun_3 == 31) //emulsion flooding
3766 {
3767     temp_time_e = Gtime_E [0] - Gtime_E [1]; //delta time
3768     temp_delta_e=data3*temp_time_e/60; //delta mass
3769
3770     temp_emul_in = EMULIN[0] + temp_delta_e; //emulsion inj based on mass flow meter
3771
3772     temp_emul_in_pv = temp_emul_in / PV[0];
3773
3774     SetCtrlVal (panel_handle, MAIN_EMUL_IN, temp_emul_in);
3775     SetCtrlVal (panel_handle, MAIN_EMUL_IN_PV, temp_emul_in_pv);

```

```

3776
3777 }
3778
3779 if (stage ==11 && pumprun_3 == 31) //alternate emulsion flooding
3780 {
3781     temp_time_e = Gtime_E [0] - Gtime_E [1]; //delta time
3782     temp_delta_e=data3*temp_time_e/60; //delta mass
3783
3784     temp_emul_in = EMULIN[0] + temp_delta_e; //emulsion inj based on mass flow meter
3785
3786     temp_emul_in_pv = temp_emul_in / PV[0];
3787
3788     SetCtrlVal (panel_handle, MAIN_E_ALT_INJ, temp_emul_in);
3789     SetCtrlVal (panel_handle, MAIN_EMULSION_FV_INJ_ALT, temp_emul_in_pv);
3790 }
3791
3792
3793
3794
3795     CmtGetLock (Mass_lockHandle);
3796     DSN_SHIFT_MASS(2);
3797     M31[0] = data;
3798     M32[0] = data2;
3799     M33[0] = data3; //volume flow rate cc/min
3800     M34[0] = data4; //real mass flow in kg/min
3801
3802     if (stage >=10 && pumprun_3 == 31) //emulsion flooding or alternate emulsion flooding
3803     {
3804         TEMPSTEP_E[0] = temp_time_e;
3805         TEMPDELTA_E[0]= temp_delta_e;
3806         EMULIN[0] = temp_emul_in;
3807     }
3808
3809     CmtReleaseLock (Mass_lockHandle);
3810
3811 ProcessSystemEvents ();
3812 }
3813
3814 void READ_FLOW_M_4(void)
3815 {
3816     double data,
3817     data2,
3818     data3,
3819     data4,
3820     temp_delta=0.0,
3821     temp_time=0.0,
3822     temp_g_time=0.0,
3823     temp_waterflooding_inj = 0.0,
3824     temp_sior = 0.0 ,
3825     temp_water_rec=0.0, //waterflooding
3826     temp_oil_rec=0.0, //waterflooding
3827     temp_water_rec_st9=0.0, //oil saturation
3828     temp_oil_rec_st9=0.0, //oil saturation
3829     temp_swi = 0.0,
3830     temp_oil_rec_st14 = 0.0, //emulsion flooding
3831     temp_smth_rec_st14 = 0.0, //emulsion flooding
3832     temp_smth_rec_ALT = 0.0, //alternate flooding
3833     temp_oil_rec_ALT = 0.0; //alternate flooding
3834
3835 ProcessSystemEvents ();
3836
3837     Delay(0.01);
3838     ClientDDERead (hConv4, "P(270)", CF_TEXT, read_m41data, 64, 0);
3839     data=atof(read_m41data);
3840     SetCtrlVal (panel_handle, MAIN_DENSITY_M_4, data); // send value of "read_data" to panel
3841
3842     Delay(0.01);
3843     ClientDDERead (hConv4, "P(142)", CF_TEXT, read_m42data, 64, 0);
3844     data2=atof(read_m42data);
3845     SetCtrlVal (panel_handle, MAIN_TEMP_M_4, data2);
3846
3847     Delay(0.01);
3848     ClientDDERead (hConv4, "P(205)", CF_TEXT, read_m43data, 64, 0);
3849     data3=atof(read_m43data);
3850     SetCtrlVal (panel_handle, MAIN_MFR_M_4, data3);
3851
3852     data4=data3 * data * 0.001 ; // cc/min * kg /m^3 = 0.001 * gm/min
3853
3854 // Delay(0.01); //P(198)
3855 // ClientDDERead (hConv4, "P(205)", CF_TEXT, read_m44data, 64, 0);
3856 // data4=atof(read_m44data);
3857
3858     SetCtrlVal (panel_handle, MAIN_EXTRA1_M_4, data4);
3859
3860 Gtime[0] = Timer (); // Get Time
3861
3862 if (stage == 4 && pumprun_2 == 21) //oil saturation process [stage #4]
3863 {
3864
3865     temp_time = Gtime [0] - Gtime [1];
3866
3867     temp_delta=data3*temp_time/60;
3868
3869     if (M41[0] >= SETPOINTOUT[0])
3870     {
3871         temp_water_rec_st9 = WATERREC_ST9[0]+ temp_delta;
3872         temp_oil_rec_st9 = OILREC_ST9[0];

```

```

3873     }
3874   else
3875   {
3876     temp_oil_rec_st9 = OILREC_ST9[0] + temp_delta;
3877     temp_water_rec_st9 = WATERREC_ST9[0];
3878   }
3879
3880
3881 temp_swi = (PV[0] - temp_water_rec_st9 + 0.46) / PV[0]; //0.46 - shift-volume before and after CORE HOLDER
3882
3883 SetCtrlVal (panel_handle, MAIN_SIW_CORE, temp_swi);
3884
3885 SetCtrlVal (panel_handle, MAIN_WATER_REC, temp_water_rec_st9);
3886 SetCtrlVal (panel_handle, MAIN_OIL_REC, temp_oil_rec_st9);
3887 }
3888
3889 if (stage == 7 && pumprun_1 == 11) // native waterflooding
3890 {
3891   temp_time = Gtime [0] - Gtime [1];
3892   temp_delta=data3*temp_time/60;
3893
3894   if (M41[0] >= SETPOINTOUT[0])
3895   {
3896     temp_water_rec = WATERREC[0]+ temp_delta;
3897     temp_oil_rec = OILREC[0];
3898   }
3899   else
3900   {
3901     temp_oil_rec = OILREC[0] + temp_delta;
3902     temp_water_rec = WATERREC [0];
3903   }
3904
3905 temp_waterflooding_inj = WATERFLOODINJ [0] + PFR11[0] *temp_time/60; // water inject during waterflooding
3906
3907 // it is required to take into account water injected [temp_waterflooding_inj]
3908
3909 temp_swi= (PV[0] - WATERREC_ST9[0] - temp_water_rec + temp_waterflooding_inj + 0.46) / PV[0];
3910 temp_sior = 1 - temp_swi ;
3911
3912
3913 SetCtrlVal (panel_handle, MAIN_SIW_CORE, temp_swi);
3914 SetCtrlVal (panel_handle, MAIN_SIOR_CORE,temp_sior);
3915
3916
3917 SetCtrlVal (panel_handle, MAIN_WATER_REC, temp_water_rec);
3918 SetCtrlVal (panel_handle, MAIN_OIL_REC, temp_oil_rec);
3919 }
3920
3921 if (stage == 10 && pumprun_3 == 31) //emulsion flooding
3922 {
3923   temp_time = Gtime [0] - Gtime [1];
3924   temp_delta=data3*temp_time/60;
3925
3926   if (M41[0] >= SETPOINTOUT[0])
3927   {
3928     temp_smth_rec_st14 = RECEMUL[0] + temp_delta;
3929     temp_oil_rec_st14 = OILREC_ST14 [0];
3930   }
3931   else
3932   {
3933     temp_oil_rec_st14 = OILREC_ST14 [0] + temp_delta;
3934     temp_smth_rec_st14 = RECEMUL [0];
3935   }
3936
3937
3938 SetCtrlVal (panel_handle, MAIN_WATER_REC_2, temp_smth_rec_st14);
3939 SetCtrlVal (panel_handle, MAIN_OIL_REC_2, temp_oil_rec_st14);
3940 }
3941
3942 if (stage == 11 && pumprun_1 == 11) //alternate flooding [waterflooding]
3943 {
3944   SetCtrlVal (panel_handle, MAIN_ALT_P_1, 1); //on
3945   SetCtrlVal (panel_handle, MAIN_ALT_F_3, 0); //off
3946
3947   temp_time = Gtime [0] - Gtime [1];
3948   temp_delta=data3*temp_time/60;
3949
3950   if (M41[0] >= SETPOINTOUT[0])
3951   {
3952     temp_smth_rec_ALT = RECEMUL_ALT[0] + temp_delta;
3953     temp_oil_rec_ALT = OILREC_ALT[0];
3954   }
3955   else
3956   {
3957     temp_oil_rec_ALT = OILREC_ALT[0] + temp_delta;
3958     temp_smth_rec_ALT = RECEMUL_ALT[0];
3959   }
3960
3961 SetCtrlVal (panel_handle, MAIN_ALT_W_REC, temp_smth_rec_ALT);
3962 SetCtrlVal (panel_handle, MAIN_ALT_O_REC, temp_oil_rec_ALT);
3963 }
3964
3965 if (stage == 11 && pumprun_3 == 31) //alternate flooding [emulsion flooding]
3966 {
3967   SetCtrlVal (panel_handle, MAIN_ALT_P_1, 0); //off
3968   SetCtrlVal (panel_handle, MAIN_ALT_F_3, 1); //on
3969

```

```

3970 temp_time = Gtime [0] - Gtime [1];
3971 temp_delta=data3*temp_time/60;
3972
3973     if (M41[0] >= SETPOINTOUT[0])
3974     {
3975         temp_smth_rec_ALT = RECEMUL_ALT[0] + temp_delta;
3976         temp_oil_rec_ALT = OILREC_ALT [0];
3977     }
3978     else
3979     {
3980         temp_oil_rec_ALT = OILREC_ALT [0] + temp_delta;
3981         temp_smth_rec_ALT = RECEMUL_ALT [0];
3982     }
3983
3984 SetCtrlVal (panel_handle, MAIN_ALT_W_REC, temp_smth_rec_ALT);
3985 SetCtrlVal (panel_handle, MAIN_ALT_O_REC, temp_oil_rec_ALT);
3986 }
3987
3988 SetCtrlVal (panel_handle, MAIN_TIME_REAL, TimeStr());
3989
3990 //Save data to the massive elements
3991 CmtGetLock (Mass_lockHandle);
3992
3993     DSN_SHIFT_MASS(3);
3994
3995     M41[0] = data;
3996     M42[0] = data2;
3997     M43[0] = data3; //volume flow rate in cc/min
3998     M44[0] = data4; //real mass flow in kg/min
3999
4000     if (stage == 4 && pumprun_2 == 21) //oil saturation process
4001     {
4002         TEMPSTEP[0] = temp_time;
4003         TEMPDELTA[0]= temp_delta;
4004         WATERREC_ST9[0] = temp_water_rec_st9;
4005         OILREC_ST9[0] = temp_oil_rec_st9;
4006         SWI[0] = temp_swi;
4007     }
4008
4009     if (stage == 7 && pumprun_1 == 11) //native waterflooding
4010     {
4011         WATERREC[0] = temp_water_rec;
4012         OILREC[0] = temp_oil_rec;
4013         TEMPSTEP[0] = temp_time;
4014         TEMPDELTA[0]= temp_delta;
4015         WATERFLOODING[0]= temp_waterflooding_inj;
4016         SWI[0] = temp_swi;
4017     }
4018
4019     if (stage == 10 && pumprun_3 == 31) //emulsion flooding
4020     {
4021         TEMPSTEP[0] = temp_time;
4022         TEMPDELTA[0]= temp_delta;
4023         OILREC_ST14 [0] = temp_oil_rec_st14;
4024         RECEMUL[0] = temp_smth_rec_st14;
4025     }
4026
4027     if (stage == 11 && pumprun_1 == 11) //alternate flooding [water]
4028     {
4029         TEMPSTEP[0] = temp_time;
4030         TEMPDELTA[0]= temp_delta;
4031         OILREC_ALT [0] = temp_oil_rec_ALT;
4032         RECEMUL_ALT[0] = temp_smth_rec_ALT;
4033     }
4034
4035     if (stage == 11 && pumprun_3 == 31) //alternate flooding [emulsion]
4036     {
4037         TEMPSTEP[0] = temp_time;
4038         TEMPDELTA[0]= temp_delta;
4039         OILREC_ALT [0] = temp_oil_rec_ALT;
4040         RECEMUL_ALT[0] = temp_smth_rec_ALT;
4041     }
4042
4043 CmtReleaseLock (Mass_lockHandle);
4044
4045 ProcessSystemEvents ();
4046 }
4047
4048 void DSN_SHIFT_MASS(int instrument) //shifting data locally
4049 {
4050     switch (instrument)
4051     {
4052     case 0:
4053         Shift (M11, NUM, 1, M11);
4054         Shift (M12, NUM, 1, M12);
4055         Shift (M13, NUM, 1, M13);
4056         Shift (M14, NUM, 1, M14);
4057         break;
4058
4059     case 1:
4060         Shift (M21, NUM, 1, M21);
4061         Shift (M22, NUM, 1, M22);
4062         Shift (M23, NUM, 1, M23);
4063         Shift (M24, NUM, 1, M24);
4064         break;
4065
4066     case 2:

```

```

4067     Shift (M31, NUM, 1, M31);
4068     Shift (M32, NUM, 1, M32);
4069     Shift (M33, NUM, 1, M33);
4070     Shift (M34, NUM, 1, M34);
4071     Shift (Gtime_E, NUM, 1, Gtime_E);
4072
4073     if (stage >= 10 && pumprun_3 == 31 )           //emulsion injection into the cell
4074     {
4075         Shift (EMULIN, NUM, 1, EMULIN);
4076         Shift (TEMPSTEP_E, NUM, 1, TEMPSTEP_E);
4077         Shift (TEMPDELTA_E, NUM, 1, TEMPDELTA_E);
4078     }
4079     break;
4080
4081 case 3:
4082     Shift (M41, NUM, 1, M41);
4083     Shift (M42, NUM, 1, M42);
4084     Shift (M43, NUM, 1, M43);
4085     Shift (M44, NUM, 1, M44);
4086     Shift (Gtime, NUM, 1, Gtime);
4087
4088     if (stage == 4 && pumprun_2 == 21 ) // oil saturation process
4089     {
4090         Shift (WATERREC_ST9, NUM, 1, WATERREC_ST9);
4091         Shift (OILREC_ST9, NUM, 1, OILREC_ST9);
4092         Shift (TEMPSTEP, NUM, 1, TEMPSTEP);
4093         Shift (TEMPDELTA, NUM, 1, TEMPDELTA);
4094
4095         Shift (SWI, NUM, 1, SWI);
4096     }
4097
4098     if (stage == 7 && pumprun_1 == 11 ) // native waterflooding
4099     {
4100         Shift (WATERREC, NUM, 1, WATERREC);
4101         Shift (OILREC, NUM, 1, OILREC);
4102         Shift (TEMPSTEP, NUM, 1, TEMPSTEP);
4103         Shift (TEMPDELTA, NUM, 1, TEMPDELTA);
4104         Shift (WATERFLOODINJ, NUM, 1, WATERFLOODINJ);
4105
4106         Shift (SWI, NUM, 1, SWI);
4107     }
4108
4109     if (stage == 10 && pumprun_3 == 31 ) // emulsion flooding
4110     {
4111         Shift (RECEMUL, NUM, 1, RECEMUL);
4112         Shift (OILREC_ST14, NUM, 1, OILREC_ST14);
4113         Shift (TEMPSTEP, NUM, 1, TEMPSTEP);
4114         Shift (TEMPDELTA, NUM, 1, TEMPDELTA);
4115     }
4116
4117     if (stage == 11 && pumprun_1 == 11 ) // alternate flooding [water]
4118     {
4119         Shift (RECEMUL_ALT, NUM, 1, RECEMUL_ALT);
4120         Shift (OILREC_ALT, NUM, 1, OILREC_ALT);
4121         Shift (TEMPSTEP, NUM, 1, TEMPSTEP);
4122         Shift (TEMPDELTA, NUM, 1, TEMPDELTA);
4123     }
4124
4125     if (stage == 11 && pumprun_3 == 31 ) // alternate flooding [emulsion]
4126     {
4127         Shift (RECEMUL_ALT, NUM, 1, RECEMUL_ALT);
4128         Shift (OILREC_ALT, NUM, 1, OILREC_ALT);
4129         Shift (TEMPSTEP, NUM, 1, TEMPSTEP);
4130         Shift (TEMPDELTA, NUM, 1, TEMPDELTA);
4131     }
4132     break;
4133 }
4134 return;
4135 }
4136
4137 int CVICALLBACK BPR_ThreadFunction (void *functionData)
4138 {
4139     int conreq_BPR;
4140
4141     while (BPR_quitflag == 1)
4142     {
4143         ProcessSystemEvents ();
4144
4145         GetCtrlVal(config_handle,CONFIG_CON_BPR,&conreq_BPR);
4146
4147         if(conreq_BPR == 1)
4148         {
4149             ConnectToDDEServer (&hConv5, "FlowDDE5", "C(1)", DDECallback, 0);
4150             conreq_BPR=0; Is_BPR=1;
4151             SetCtrlVal(config_handle,CONFIG_CON_BPR, conreq_BPR);
4152             SetCtrlVal(panel_handle,MAIN_LOG_BPR, Is_BPR);
4153             SetCtrlVal (config_handle, CONFIG_BPR_LED, 1);
4154             Update_Graphics();
4155         }
4156         else if (conreq_BPR == -1)
4157         {
4158             DisconnectFromDDEServer (hConv5);
4159             conreq_BPR=0; Is_BPR=0;
4160             SetCtrlVal(config_handle,CONFIG_CON_BPR, conreq_BPR);
4161             SetCtrlVal(panel_handle,MAIN_LOG_BPR, Is_BPR);
4162             SetCtrlVal (config_handle, CONFIG_BPR_LED, 0);
4163             Update Graphics();

```

```

4164         }
4165         if (Is_BPR) READ_BPR();
4166     ProcessSystemEvents ();
4167 }
4169 return 0;
4170 }
4171
4172 void READ_BPR(void)
4173 {
4174     char temp[NUM];
4175     double data,
4176     data2,
4177     data3;
4178
4179     //fsetpoint [BPR1 pressure set point]
4180     GetCtrlVal(panel_handle,MAIN_BPR_SET,&bpr_set);
4181     if (bpr_set_was != bpr_set )
4182     {
4183         if (bpr_set >= 1449)
4184         {
4185             MessagePopup("Error","Pressure limited by 1450 psi");
4186             SetCtrlVal(panel_handle,MAIN_BPR_SET,1440.0);
4187             GetCtrlVal(panel_handle,MAIN_BPR_SET,&bpr_set);
4188
4189             sprintf(temp, NUM, "%g", bpr_set);
4190             ClientDDEWrite(hConv5, "P(206)", CF_TEXT, temp, 64, 0);
4191             SetCtrlVal (panel_handle, MAIN_LED_BPR_CHECK, 1);
4192             Delay (0.5);
4193             SetCtrlVal (panel_handle, MAIN_LED_BPR_CHECK, 0);
4194             bpr_set_was = 1440;
4195         }
4196     else
4197     {
4198         sprintf(temp, NUM, "%g", bpr_set);
4199         ClientDDEWrite(hConv5, "P(206)", CF_TEXT, temp, 64, 0);
4200         SetCtrlVal (panel_handle, MAIN_LED_BPR_CHECK, 1);
4201         Delay (0.5);
4202         SetCtrlVal (panel_handle, MAIN_LED_BPR_CHECK, 0);
4203         bpr_set_was = bpr_set;
4204     }
4205 }
4206
4207 ProcessSystemEvents ();
4208
4209 //fmeasure [BPR1 pressure measure point]
4210 Delay(0.1);
4211 ClientDDERead (hConv5, "P(205)", CF_TEXT, read_bpr11data, 64, 0);
4212 data=atof(read_bpr11data);
4213 BPR1TEMP[0] = data;
4214 SetCtrlVal (panel_handle, MAIN_BPR1, data);
4215
4216 //fsetpoint read
4217 Delay(0.1);
4218 ClientDDERead (hConv5, "P(206)", CF_TEXT, read_bpr12data, 64, 0);
4219 data2=atof(read_bpr12data);
4220 SetCtrlVal (panel_handle, MAIN_BPR_SETPOINT, data2);
4221
4222 //alarm info
4223 Delay(0.1);
4224 ClientDDERead (hConv5, "P(28)", CF_TEXT, read_bpr13data, 64, 0);
4225 data3=atof(read_bpr13data);
4226 SetCtrlVal (panel_handle, MAIN_BPR_ALARM, data3);
4227
4228 CmtGetLock (BPR_lockHandle);
4229
4230     Shift (BPR11, NUM, 1, BPR11);
4231     Shift (BPR12, NUM, 1, BPR12);
4232     Shift (BPR13, NUM, 1, BPR13);
4233
4234     BPR11[0] = data;
4235     BPR12[0] = data2;
4236     BPR13[0] = data3;
4237
4238     CmtReleaseLock (BPR_lockHandle);
4239
4240 ProcessSystemEvents ();
4241 }
4242
4243 //-----
4244 // DSN_Setup_DAQ : Sets up the DAQ Task and RTD Channels
4245 //-----
4246
4247 void DSN_Setup_DAQ(void)
4248 {
4249 // int i,count=0;
4250
4251     // Retrieve Averaging Number and Sampling Rate from Panel
4252
4253     GetCtrlVal(config_handle,CONFIG_DAQ_AVERAGING_NUMBER,&DAQsampsPerChan);
4254     GetCtrlVal(config_handle,CONFIG_DAQ_RATE,&DAQrate);
4255
4256     GetCtrlVal(config_handle,CONFIG_TP2CHANNEL,TP2channel);
4257
4258 //     GetCtrlVal(config_handle,CONFIG_DP1CHANNEL_A,DP1channel_A);
4259 //     GetCtrlVal(config_handle,CONFIG_DP1CHANNEL_B,DP1channel_B);
4260

```

```

4261 GetCtrlVal(config_handle,CONFIG_TP1CHANNEL,TP1channel);
4262
4263
4264 GetCtrlVal(config_handle,CONFIG_CP11_A,CP11_Achannel);
4265 GetCtrlVal(config_handle,CONFIG_CP11_B,CP11_Bchannel);
4266 GetCtrlVal(config_handle,CONFIG_CP12_A,CP12_Achannel);
4267 GetCtrlVal(config_handle,CONFIG_CP12_B,CP12_Bchannel);
4268 GetCtrlVal(config_handle,CONFIG_CP13_A,CP13_Achannel);
4269 GetCtrlVal(config_handle,CONFIG_CP13_B,CP13_Bchannel);
4270 GetCtrlVal(config_handle,CONFIG_CP14_A,CP14_Achannel);
4271 GetCtrlVal(config_handle,CONFIG_CP14_B,CP14_Bchannel);
4272 GetCtrlVal(config_handle,CONFIG_CP15_A,CP15_Achannel);
4273 GetCtrlVal(config_handle,CONFIG_CP15_B,CP15_Bchannel);
4274
4275 GetCtrlVal(config_handle,CONFIG_CP21_A,CP21_Achannel);
4276 GetCtrlVal(config_handle,CONFIG_CP21_B,CP21_Bchannel);
4277 GetCtrlVal(config_handle,CONFIG_CP22_A,CP22_Achannel);
4278 GetCtrlVal(config_handle,CONFIG_CP22_B,CP22_Bchannel);
4279 GetCtrlVal(config_handle,CONFIG_CP23_A,CP23_Achannel);
4280 GetCtrlVal(config_handle,CONFIG_CP23_B,CP23_Bchannel);
4281 GetCtrlVal(config_handle,CONFIG_CP24_A,CP24_Achannel);
4282 GetCtrlVal(config_handle,CONFIG_CP24_B,CP24_Bchannel);
4283 GetCtrlVal(config_handle,CONFIG_CP25_A,CP25_Achannel);
4284 GetCtrlVal(config_handle,CONFIG_CP25_B,CP25_Bchannel);
4285
4286 GetCtrlVal(config_handle,CONFIG_CP31_A,CP31_Achannel);
4287 GetCtrlVal(config_handle,CONFIG_CP31_B,CP31_Bchannel);
4288 GetCtrlVal(config_handle,CONFIG_CP32_A,CP32_Achannel);
4289 GetCtrlVal(config_handle,CONFIG_CP32_B,CP32_Bchannel);
4290 GetCtrlVal(config_handle,CONFIG_CP33_A,CP33_Achannel);
4291 GetCtrlVal(config_handle,CONFIG_CP33_B,CP33_Bchannel);
4292 GetCtrlVal(config_handle,CONFIG_CP34_A,CP34_Achannel);
4293 GetCtrlVal(config_handle,CONFIG_CP34_B,CP34_Bchannel);
4294 GetCtrlVal(config_handle,CONFIG_CP35_A,CP35_Achannel);
4295 GetCtrlVal(config_handle,CONFIG_CP35_B,CP35_Bchannel);
4296
4297 //*****
4298 // Create the DAQ task
4299 // ****
4300
4301 DAQmxErrChk(DAQmxCreateTask("",&taskHandle));
4302
4303 //*****
4304 // Create all the Necessary Channels
4305 // ****
4306
4307 // Sensor is a Pressure Transducer TP-2
4308 // "cDAQ1Mod5/ai11"
4309 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, TP2channel,
4310 "Voltage_1A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4311
4312 // Sensor is a Pressure Transducer dP1
4313
4314 // "cDAQ1Mod5/ai20"
4315 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, DP1channel_A,
4316 "Voltage_1B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4317 // "cDAQ1Mod5/ai21"
4318 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, DP1channel_B,
4319 "Voltage_1C", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4320 // "cDAQ1Mod5/ai16"
4321 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, TP1channel,
4322 "Voltage_1D", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4323 // Sensor is a Pressure Transducer TP-1
4324 // "cDAQ1Mod5/ai16"
4325 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, TP1channel,
4326 "Voltage_1E", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4327
4328 //Pressure sensors 1.1 ,1.2, 1.3, 1.4, 1.5
4329 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP11_Achannel,
4330 "Voltage_11_A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4331 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP11_Bchannel,
4332 "Voltage_11_B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4333 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP12_Achannel,
4334 "Voltage_12_A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4335 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP12_Bchannel,
4336 "Voltage_12_B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4337 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP13_Achannel,
4338 "Voltage_13_A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4339 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP13_Bchannel,
4340 "Voltage_13_B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4341 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP14_Achannel,
4342 "Voltage_14_A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4343 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP14_Bchannel,
4344 "Voltage_14_B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4345 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP15_Achannel,
4346 "Voltage_15_A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4347 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP15_Bchannel,
4348 "Voltage_15_B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4349
4350 //Pressure sensors 2.1 ,2.2, 2.3, 2.4, 2.5
4351 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP21_Achannel,
4352 "Voltage_21_A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4353 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP21_Bchannel,
4354 "Voltage_21_B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4355 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP22_Achannel,
4356 "Voltage_22_A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4357 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP22_Bchannel,

```

```

4358     "Voltage_22_B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4359 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP23_Achannel,
4360     "Voltage_23_A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4361 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP23_Bchannel,
4362     "Voltage_23_B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4363 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP24_Achannel,
4364     "Voltage_24_A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4365 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP24_Bchannel,
4366     "Voltage_24_B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4367 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP25_Achannel,
4368     "Voltage_25_A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4369 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP25_Bchannel,
4370     "Voltage_25_B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4371
4372 //Pressure sensors 3.1 ,3.2, 3.3, 3.4, 3.5
4373 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP31_Achannel,
4374     "Voltage_31_A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4375 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP31_Bchannel,
4376     "Voltage_31_B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4377 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP32_Achannel,
4378     "Voltage_32_A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4379 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP32_Bchannel,
4380     "Voltage_32_B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4381 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP33_Achannel,
4382     "Voltage_33_A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4383 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP33_Bchannel,
4384     "Voltage_33_B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4385 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP34_Achannel,
4386     "Voltage_34_A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4387 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP34_Bchannel,
4388     "Voltage_34_B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4389 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP35_Achannel,
4390     "Voltage_35_A", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4391 DAQmxErrChk(DAQmxCreateAIVoltageChan(taskHandle, CP35_Bchannel,
4392     "Voltage_35_B", DAQmx_Val_RSE, 0, 10, DAQmx_Val_Volts, ""));
4393
4394 //*****
4395 // Setup the DAQ Timing and Number of Channels /
4396 //*****
4397
4398 // Set the clock timing
4399 DAQmxErrChk (DAQmxCfgSampClkTiming (taskHandle,"", DAQrate,
4400     DAQmx_Val_Rising, DAQmx_Val_ContSamps, DAQsampsPerChan));
4401
4402 // Set the number of channels to scan
4403 DAQmxErrChk (DAQmxGetTaskAttribute(taskHandle,DAQmx_Task_NumChans,&DAQnumChannels));
4404
4405 // Make space for the data
4406 if( (DAQdata=malloc(DAQsampsPerChan*DAQnumChannels*sizeof(float64)))==NULL )
4407 {
4408     MessagePopup("Error","Not enough memory");
4409     goto Error;
4410 }
4411 // Make space for the averaging array
4412 if( (DAQArray_Out=malloc(DAQsampsPerChan*sizeof(float64)))==NULL )
4413 {
4414     MessagePopup("Error","Not enough memory");
4415     goto Error;
4416 }
4417
4418 //Exit
4419 Error:
4420     if( DAQmxFailed(DAQerror) )
4421     {
4422         DAQmxGetExtendedErrorInfo(DAQerrBuff,2048);
4423         DAQquitflag =0;
4424     }
4425
4426     if( DAQmxFailed(DAQerror) )
4427         MessagePopup("DAQmx Error",DAQerrBuff);
4428 }
4429
4430 //*****
4431 /* DAQThreadFunction(): - Separate Thread for DAQ */
4432 /* - Logs to file/graphs*/
4433 //*****
4434 int CVICALLBACK DAQThreadFunction (void *functionData)
4435 { // double T1; // T2,Hz;
4436
4437 // int i, j, k = 0;
4438 // int count = 0;
4439
4440 // Start a loop that will process events for this thread
4441 while (DAQquitflag == 1)
4442 {
4443     ++SAMPLES;
4444
4445     // T1 = Timer ();// Start TIME
4446     ProcessSystemEvents ();
4447
4448     //-----
4449
4450     step[0] = Timer ();           // Get Time
4451
4452
4453 }
```

```

4455     if(Is_DAQ)
4456     {
4457         DSN_Run_DAQ();
4458     }
4459 //-----
4460
4461     ProcessSystemEvents ();
4462     SetCtrlVal(panel_handle, MAIN_SAMPLES, SAMPLES);
4463
4464 //-----
4465
4466     LiquidsInj();
4467
4468     Perm();
4469
4470 //TIME STAMP
4471     GetCurrentCVIAbsoluteTime (&timestamp);
4472
4473     CVIAbsoluteTimeToCVIUILTime (timestamp, &timeDAQ);
4474
4475     if(Is_Log)
4476        LogFile();           // Log to File
4477
4478     ProcessSystemEvents ();
4479
4480     CmtGetLock (DAQ_lockHandle);
4481
4482     if(Is_Graph)
4483         Graph();           // Do Graphing
4484
4485     CmtReleaseLock (DAQ_lockHandle);
4486
4487     DSN_SHIFT_DAQ();      // SHIFT all DAQ arrays
4488 //-----
4489
4490
4491 }
4492 return 0;
4493 }
4494
4495 void LiquidsInj(void)
4496 {
4497     double temp, temp2, temp3, outlettemp, currtube;
4498     int a;
4499
4500 //WATER
4501 if (pumprun_1 == 11)
4502 {
4503     temp=PFR11[0]*(step[0]-step[1])/60;
4504     G_WATERINJ[0] = G_WATERINJ[1] - temp;
4505     OUTLET[0]=OUTLET[1]+temp;
4506
4507     if (stage >=0 && stage <=3) WATERINJ[0]=WATERINJ[1] + temp; //PV
4508
4509     if (stage == 3 ) WATERINJPV[0]=WATERINJ[0]/PV[0]; //saturation process
4510
4511     if (stage >=7) //waterflooding
4512     {
4513         WATERINJ2[0]=WATERINJ2[1] + temp;
4514         WATERINJ2PV[0]=WATERINJ2[0]/PV[0];
4515         WATERINJ[0]=WATERINJ[1];
4516     }
4517 SetCtrlVal (panel_handle, MAIN_WATERTANK, G_WATERINJ[0]);
4518 SetCtrlVal (panel_handle, MAIN_OUTLETTANK, OUTLET[0]); //set new value to TANK
4519
4520
4521 GetCtrlAttribute (panel_handle, MAIN_OUTLETTANK,ATTR_MAX_VALUE, &outlettemp);
4522 GetCtrlVal (panel_handle, MAIN_CUR_TTUBE, &currtube);
4523
4524 if (OUTLET[0] >= outlettemp && stage >= 7)
4525 {//change to the new tube at fraction collector
4526     SWITCH_FRACTION (0, 1, 0, 0);
4527     Delay (0.5);
4528     SWITCH_FRACTION (0, 0, 0, 0);
4529     MANUAL_TEST_TUBE[0] = currtube + 1;
4530     SetCtrlVal(panel_handle, MAIN_CUR_TTUBE, MANUAL_TEST_TUBE[0]);
4531
4532     globalemail = 1; //set command to send email
4533
4534
4535 // clean the outlet
4536     OUTLET[1]=0.0;
4537     OUTLET[0]=0.0;
4538     SetCtrlVal (panel_handle, MAIN_OUTLETTANK, OUTLET[0]); //set new value to TANK
4539 }
4540 return;
4541 }
4542 if (pumprun_1 == 12)
4543 {
4544
4545 //temp for time test
4546 //temp=PFR11[0]*(step[0]-step[1])/60;
4547 //WATERINJ[0]=WATERINJ[1] + temp;
4548 //SetCtrlVal (panel_handle, MAIN_WATER_TEST, WATERINJ[0]);
4549
4550     G_WATERINJ[0]=G_WATERINJ[1];
4551     WATERINJ2[0]=WATERINJ2[1];

```

```

4552         WATERINJ[0]=WATERINJ[1];
4553         OUTLET[0]=OUTLET[1];
4554
4555     if (stage == 3)  WATERINJPV[0]=WATERINJPV[1];
4556     if (stage >= 7)  WATERINJ2PV[0]=WATERINJ2PV[1];
4557
4558 SetCtrlVal (panel_handle, MAIN_WATERTANK, G_WATERINJ[0]);
4559 SetCtrlVal (panel_handle, MAIN_OUTLETTANK, OUTLET[0]); //set new value to TANK
4560 }
4561
4562 //OIL
4563 if (pumprun_2 == 21)
4564 {
4565     temp2=PFR21[0]*(step[0]-step[1])/60;
4566     OILINJ[0]=OILINJ[1] + temp2;
4567     G_OILINJ[0] = G_OILINJ[1] - temp2;
4568     OUTLET[0]=OUTLET[1]+temp2;
4569
4570     if (stage >= 3) OILINJPV[0]=OILINJ[0]/PV[0];
4571
4572 SetCtrlVal (panel_handle, MAIN_OILTANK, G_OILINJ[0]);
4573 SetCtrlVal (panel_handle, MAIN_OUTLETTANK, OUTLET[0]); //set new value to TANK
4574
4575 return;
4576 }
4577
4578 if (pumprun_2 == 22)
4579 {
4580     G_OILINJ[0]= G_OILINJ[1];
4581     OILINJ[0]=OILINJ[1];
4582     OUTLET[0]=OUTLET[1];
4583
4584     if (stage >= 3) OILINJPV[0]=OILINJPV[1];
4585
4586     SetCtrlVal (panel_handle, MAIN_OILTANK, G_OILINJ[0]);
4587     SetCtrlVal (panel_handle, MAIN_OUTLETTANK, OUTLET[0]); //set new value to TANK
4588
4589 }
4590
4591
4592 //EMULSION
4593 if (pumprun_3 == 31)
4594 {
4595
4596     temp3=PFR31[0]*(step[0]-step[1])/60;
4597     EMULINJ[0]=EMULINJ[1] + temp3;
4598     G_EMULINJ[0]= G_EMULINJ[1] - temp3 ;
4599     OUTLET[0]=OUTLET[1]+temp3;
4600
4601     if (stage >= 3) EMULINJPV[0]=EMULINJ[0]/PV[0];
4602
4603     SetCtrlVal (panel_handle, MAIN_EMULTANK, G_EMULINJ[0]);
4604     SetCtrlVal (panel_handle, MAIN_OUTLETTANK, OUTLET[0]); //set new value to TANK
4605
4606 GetCtrlAttribute (panel_handle, MAIN_OUTLETTANK,ATTR_MAX_VALUE, &outlettemp);
4607 GetCtrlVal (panel_handle, MAIN_CUR_TTUBE, &curttube);
4608
4609 if (OUTLET[0] >= outlettemp && stage >= 7)
4610 { //change to the new tube at fraction collector
4611     SWITCH_FRACTION (0, 1, 0, 0);
4612     Delay (0.5);
4613     SWITCH_FRACTION (0, 0, 0, 0);
4614     MANUAL_TEST_TUBE[0] = curttube + 1;
4615     SetCtrlVal(panel_handle, MAIN_CUR_TTUBE, MANUAL_TEST_TUBE[0]);
4616     // clean the outlet
4617     OUTLET[1]=0.0;
4618     OUTLET[0]=0.0;
4619     SetCtrlVal (panel_handle, MAIN_OUTLETTANK, OUTLET[0]); //set new value to TANK
4620
4621 }
4622     return;
4623 }
4624     if (pumprun_3 == 32)
4625 {
4626     EMULINJ[0]=EMULINJ[1];
4627     G_EMULINJ[0]=G_EMULINJ[1];
4628     OUTLET[0]=OUTLET[1];
4629
4630     if (stage >= 3) EMULINJPV[0]=EMULINJPV[1];
4631
4632     SetCtrlVal (panel_handle, MAIN_EMULTANK, G_EMULINJ[0]);
4633     SetCtrlVal (panel_handle, MAIN_OUTLETTANK, OUTLET[0]); //set new value to TANK
4634
4635 }
4636
4637 SetCtrlVal (panel_handle, MAIN_WATERTANK, G_WATERINJ[0]);
4638 SetCtrlVal (panel_handle, MAIN_OILTANK, G_OILINJ[0]);
4639 SetCtrlVal (panel_handle, MAIN_EMULTANK, G_EMULINJ[0]);
4640 SetCtrlVal (panel_handle, MAIN_OUTLETTANK, OUTLET[0]); //set new value to TANK
4641
4642
4643
4644 return;
4645 }
4646
4647 void Perm(void)
4648 {

```

```

4649 double data,data2,data3;
4650 double showdata_11,showdata_12,showdata_21,showdata_22,showdata_31,showdata_32;
4651
4652 //Water
4653 if (pumprun_1 == 11)
4654 {
4655 data = Perm_coef * PFR11[0] * VIS_WATER;
4656
4657 PERMWATERDP1[0] = data / DP1[0]; //Darcy
4658
4659 PERMWATERDELTA[0] = data / Delta[0]; //Darcy
4660
4661 showdata_11 = permcoef * PERMWATERDP1[0];
4662 showdata_12 = permcoef * PERMWATERDELTA[0];
4663
4664 SetCtrlVal(panel_handle, MAIN_PERM_W_1,showdata_11);
4665 SetCtrlVal(panel_handle, MAIN_PERM_W_2,showdata_12);
4666
4667 return;
4668 }
4669 if (pumprun_1 == 12)
4670 {
4671 PERMWATERDP1[0]=0;
4672 PERMWATERDELTA[0]=0;
4673 showdata_11 = permcoef * PERMWATERDP1[0];
4674 showdata_12 = permcoef * PERMWATERDELTA[0];
4675
4676 SetCtrlVal(panel_handle, MAIN_PERM_W_1,showdata_11);
4677 SetCtrlVal(panel_handle, MAIN_PERM_W_2,showdata_12);
4678
4679
4680 }
4681
4682 //Oil
4683 if (pumprun_2 == 21)
4684 {
4685 data2= Perm_coef * PFR21[0] * VIS_OIL;
4686
4687 PERMOILDP1[0] = data2 / DP1[0]; //Darcy
4688
4689 PERMOILDELTA[0] = data2 / Delta[0]; //Darcy
4690
4691 showdata_21 = permcoef * PERMOILDP1[0];
4692
4693 showdata_22 = permcoef * PERMOILDELTA[0];
4694
4695 SetCtrlVal(panel_handle, MAIN_PERM_O_1,showdata_21);
4696 SetCtrlVal(panel_handle, MAIN_PERM_O_2,showdata_22);
4697 return;
4698 }
4699
4700 if (pumprun_2 == 22)
4701 {
4702 PERMOILDP1[0]=0;
4703 PERMOILDELTA[0]=0;
4704
4705 showdata_21 = permcoef * PERMOILDP1[0];
4706 showdata_22 = permcoef * PERMOILDELTA[0];
4707
4708 SetCtrlVal(panel_handle, MAIN_PERM_O_1,showdata_21);
4709 SetCtrlVal(panel_handle, MAIN_PERM_O_2,showdata_22);
4710
4711 }
4712
4713 //Emulsion
4714 if (pumprun_3 == 31)
4715 {
4716 data3 = Perm_coef * PFR31[0] * VIS_EMUL;
4717
4718 PERMEMULD1[0] = data3 / DP1[0];
4719 PERMEMULDELTA[0] = data3 / Delta[0];
4720
4721 showdata_31 = permcoef * PERMEMULD1[0];
4722 showdata_32 = permcoef * PERMEMULDELTA[0];
4723
4724 SetCtrlVal(panel_handle, MAIN_PERM_E_1,showdata_31);
4725 SetCtrlVal(panel_handle, MAIN_PERM_E_2,showdata_32);
4726 return;
4727 }
4728
4729
4730 if (pumprun_3 == 32)
4731 {
4732 PERMEMULD1[0]=0;
4733 PERMEMULDELTA[0]=0;
4734
4735 showdata_31 = permcoef * PERMEMULD1[0];
4736 showdata_32 = permcoef * PERMEMULDELTA[0];
4737
4738 SetCtrlVal(panel_handle, MAIN_PERM_E_1,showdata_31);
4739 SetCtrlVal(panel_handle, MAIN_PERM_E_2,showdata_32);
4740
4741
4742
4743 return;
4744 }
4745

```

```

4746 //-----
4747 // DSN_Run_DAQ : Run the DAQ Task and RTD Channels
4748 //-----
4749
4750 void DSN_Run_DAQ(void)      // Getting data from DAQ for pressure sensors
4751 {
4752     int i;
4753     double pressure_scaling_factor_P = 150;      // psi per Volt
4754     double pressure_scaling_factor_dP = 15;        // psi per Volt
4755     double pressure_scaling_factor_dP_120 = 12;    // psi per Volt
4756     double pressure_scaling_factor_dP_80 = 8;       // psi per Volt
4757
4758
4759 // int error=0;
4760
4761 //-----
4762 // DAQmx Start DAQ Task      /
4763 //-----
4764
4765
4766 if(DAQ_Task_Start)
4767 {
4768     // Do not attempt to start task
4769 }
4770 else
4771 {
4772     DAQmxErrChk (DAQmxStartTask(taskHandle));
4773 }
4774
4775 DAQ_Task_Start = 1;
4776 ProcessDrawEvents();
4777
4778 //-----
4779 // DAQmx Read Code          /
4780 //-----
4781
4782 Clear1D (DAQdata, DAQsampsPerChan*DAQnumChannels);
4783
4784 DAQmxReadAnalogF64(taskHandle,DAQsampsPerChan,10.0,DAQmx_Val_GroupByChannel,
4785 DAQdata,DAQsampsPerChan*DAQnumChannels,&DAQnumRead,NULL),
4786
4787 if( DAQnumRead>0 )
4788 for(i=0;i<DAQnumChannels;i++)
4789 {
4790 // Extract Data for one Channel
4791 Subset1D (DAQdata, DAQnumChannels*DAQnumRead, i*DAQnumRead, DAQnumRead, DAQArray_Out);
4792
4793 // Average the Data Points
4794 Mean (DAQArray_Out,DAQnumRead, &DAQoutMean);
4795
4796 switch(i)
4797 {
4798     case 0: //upstream
4799         DAQoutMean = DAQoutMean * pressure_scaling_factor_P - ZEROTP2[0];
4800         SetCtrlVal(panel_handle,MAIN_TP2,DAQoutMean);
4801         TP2[0] = DAQoutMean;
4802         //Danger for membrane
4803         if (TP2[0] >= 1450.00)
4804         {
4805             STOPPUMPS(); //will stop pumps which are in use
4806             SetCtrlAttribute(panel_handle,MAIN_ERROR_RELEASE_2,ATTR_VISIBLE, 1);
4807             SetCtrlAttribute(panel_handle,MAIN_TP2_OVER_1450,ATTR_VISIBLE, 1);
4808         }
4809         break;
4810 //     case 1:
4811 //         DAQoutMean = DAQoutMean * pressure_scaling_factor_dP;
4812 //         DP1_A[0] = DAQoutMean;
4813 //         break;
4814 //     case 2:
4815 //         DAQoutMean = DAQoutMean * pressure_scaling_factor_dP;
4816 //         DP1_B[0] = DAQoutMean;
4817 //         break;
4818 //     case 1: //downstream
4819 //         DAQoutMean = DAQoutMean * pressure_scaling_factor_P - ZEROTP1[0];
4820 //         SetCtrlVal(panel_handle,MAIN_TP1,DAQoutMean);
4821 //         TP1[0] = DAQoutMean;
4822 //         //Danger for membrane
4823 //         if (TP1[0] >= 1450.00)
4824 //         {
4825             STOPPUMPS(); //will stop pumps which are in use
4826             SetCtrlAttribute(panel_handle,MAIN_ERROR_RELEASE_7,ATTR_VISIBLE, 1);
4827             SetCtrlAttribute(panel_handle,MAIN_TP1_OVER_1450,ATTR_VISIBLE, 1);
4828         }
4829         break;
4830 //     case 2:
4831 //         DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4832 //         CP11_A[0] = DAQoutMean;
4833 //         break;
4834 //     case 3:
4835 //         DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4836 //         CP11_B[0] = DAQoutMean;
4837 //         break;
4838 //     case 4:
4839 //         DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4840 //         CP12_A[0] = DAQoutMean;
4841 //         break;
4842 //     case 5:

```

```

4843 DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4844 CP12_B[0] = DAQoutMean;
4845 break;
4846 case 6:
4847     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4848     CP13_A[0] = DAQoutMean;
4849     break;
4850 case 7:
4851     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4852     CP13_B[0] = DAQoutMean;
4853     break;
4854 case 8:
4855     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_80;
4856     CP14_A[0] = DAQoutMean;
4857     break;
4858 case 9:
4859     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_80;
4860     CP14_B[0] = DAQoutMean;
4861     break;
4862 case 10:
4863     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_80;
4864     CP15_A[0] = DAQoutMean;
4865     break;
4866 case 11:
4867     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_80;
4868     CP15_B[0] = DAQoutMean;
4869     break;
4870 case 12:
4871     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4872     CP21_A[0] = DAQoutMean;
4873     break;
4874 case 13:
4875     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4876     CP21_B[0] = DAQoutMean;
4877     break;
4878 case 14:
4879     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4880     CP22_A[0] = DAQoutMean;
4881     break;
4882 case 15:
4883     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4884     CP22_B[0] = DAQoutMean;
4885     break;
4886 case 16:
4887     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4888     CP23_A[0] = DAQoutMean;
4889     break;
4890 case 17:
4891     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4892     CP23_B[0] = DAQoutMean;
4893     break;
4894 case 18:
4895     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_80;
4896     CP24_A[0] = DAQoutMean;
4897     break;
4898 case 19:
4899     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_80;
4900     CP24_B[0] = DAQoutMean;
4901     break;
4902 case 20:
4903     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_80;
4904     CP25_A[0] = DAQoutMean;
4905     break;
4906 case 21:
4907     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_80;
4908     CP25_B[0] = DAQoutMean;
4909     break;
4910 case 22:
4911     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4912     CP31_A[0] = DAQoutMean;
4913     break;
4914 case 23:
4915     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4916     CP31_B[0] = DAQoutMean;
4917     break;
4918 case 24:
4919     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4920     CP32_A[0] = DAQoutMean;
4921     break;
4922 case 25:
4923     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_120;
4924     CP32_B[0] = DAQoutMean;
4925     break;
4926 case 26:
4927     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_80;
4928     CP33_A[0] = DAQoutMean;
4929     break;
4930 case 27:
4931     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_80;
4932     CP33_B[0] = DAQoutMean;
4933     break;
4934 case 28:
4935     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_80;
4936     CP34_B[0] = DAQoutMean;
4937     break;
4938 case 29:
4939     DAQoutMean = DAQoutMean * pressure scaling factor dP 80;

```

```

4940 CP34_B[0] = DAQoutMean;
4941 break;
4942 case 30:
4943     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_80;
4944     CP35_A[0] = DAQoutMean;
4945     break;
4946 case 31:
4947     DAQoutMean = DAQoutMean * pressure_scaling_factor_dP_80;
4948     CP35_B[0] = DAQoutMean;
4949     break;
4950 }
4951
4952 // DP1[0]=DP1_B[0]-DP1_A[0] - ZERODP1[0];
4953 // SetCtrlVal(panel_handle,MAIN_DP1,DP1[0]);
4954
4955 CP11[0]=CP11_B[0]-CP11_A[0] - ZEROCP11[0];
4956 SetCtrlVal(pressure_handle,PRESSURE_CP1_1,CP11[0]);
4957 CP12[0]=CP12_B[0]-CP12_A[0] - ZEROCP12[0];
4958 SetCtrlVal(pressure_handle,PRESSURE_CP1_2,CP12[0]);
4959 CP13[0]=CP13_B[0]-CP13_A[0] - ZEROCP13[0];
4960 SetCtrlVal(pressure_handle,PRESSURE_CP1_3,CP13[0]);
4961 CP14[0]=CP14_B[0]-CP14_A[0] - ZEROCP14[0];
4962 SetCtrlVal(pressure_handle,PRESSURE_CP1_4,CP14[0]);
4963 CP15[0]=CP15_B[0]-CP15_A[0] - ZEROCP15[0];
4964 SetCtrlVal(pressure_handle,PRESSURE_CP1_5,CP15[0]);
4965
4966 CP21[0]=CP21_B[0]-CP21_A[0] - ZEROCP21[0];
4967 SetCtrlVal(pressure_handle,PRESSURE_CP2_1,CP21[0]);
4968 CP22[0]=CP22_B[0]-CP22_A[0] - ZEROCP22[0];
4969 SetCtrlVal(pressure_handle,PRESSURE_CP2_2,CP22[0]);
4970 CP23[0]=CP23_B[0]-CP23_A[0] - ZEROCP23[0];
4971 SetCtrlVal(pressure_handle,PRESSURE_CP2_3,CP23[0]);
4972 CP24[0]=CP24_B[0]-CP24_A[0] - ZEROCP24[0];
4973 SetCtrlVal(pressure_handle,PRESSURE_CP2_4,CP24[0]);
4974 CP25[0]=CP25_B[0]-CP25_A[0] - ZEROCP25[0];
4975 SetCtrlVal(pressure_handle,PRESSURE_CP2_5,CP25[0]);
4976
4977 CP31[0]=CP31_B[0]-CP31_A[0] - ZEROCP31[0];
4978 SetCtrlVal(pressure_handle,PRESSURE_CP3_1,CP31[0]);
4979 CP32[0]=CP32_B[0]-CP32_A[0] - ZEROCP32[0];
4980 SetCtrlVal(pressure_handle,PRESSURE_CP3_2,CP32[0]);
4981 CP33[0]=CP33_B[0]-CP33_A[0] - ZEROCP33[0];
4982 SetCtrlVal(pressure_handle,PRESSURE_CP3_3,CP33[0]);
4983 CP34[0]=CP34_B[0]-CP34_A[0] - ZEROCP34[0];
4984 SetCtrlVal(pressure_handle,PRESSURE_CP3_4,CP34[0]);
4985 CP35[0]=CP35_B[0]-CP35_A[0] - ZEROCP35[0];
4986 SetCtrlVal(pressure_handle,PRESSURE_CP3_5,CP35[0]);
4987
4988 //Danger for membrane
4989     if (DP1[0] >= 140.00 && OVERPRES == 1)
4990     {
4991         SetCtrlVal(panel_handle, MAIN_AV2_ONOFF, 0);
4992         SetCtrlAttribute(panel_handle,MAIN_ERROR_RELEASE_1,ATTR_VISIBLE, 1);
4993         SetCtrlAttribute(panel_handle,MAIN_DIFF_OVER_150,ATTR_VISIBLE, 1);
4994         SWITCH SOLENOID ();
4995         OVERPRES = 0;
4996     }
4997
4998 //Delta[0]=TP2[0]-BPR1TEMP[0]; removed from software, since new pressure sensor was added November 22, 2013
4999 Delta[0]=TP2[0]-TP1[0];
5000
5001 SetCtrlVal(panel_handle,MAIN_DP1_2,Delta[0]);
5002 }
5003 //Exit
5004 Error:
5005     if( DAQmxFailed(DAQerror) )
5006     {
5007         DAQmxGetExtendedErrorInfo(DAQerrBuff,2048);
5008         DAQquitflag = 0;
5009     }
5010 }
5011
5012 //*****DSN_SHIFT_DAQ : Will step data along an array*****
5013 // : For all data that can be plotted
5014 // : For all data that can be plotted
5015 //*****DSN_SHIFT_DAQ : Will step data along an array*****
5016 void DSN_SHIFT_DAQ(void)
5017 {
5018 Shift (step,      NUM, 1,step);
5019
5020 Shift (OILINJ,      NUM, 1,OILINJ);
5021 Shift (OILINJPV,    NUM, 1,OILINJPV);
5022
5023 Shift (EMULINJ,    NUM, 1,EMULINJ);
5024 Shift (EMULINJPV,  NUM, 1,EMULINJPV);
5025
5026 if (stage >=0 && stage <=3)
5027     Shift (WATERINJ,  NUM, 1,WATERINJ);
5028
5029 if (stage == 3)
5030     Shift (WATERINJPV, NUM, 1,WATERINJPV); //saturation
5031
5032 if (stage >= 7)
5033 {
5034     Shift (WATERINJ,  NUM, 1,WATERINJ);
5035     Shift (WATERINJ2, NUM, 1,WATERINJ2);
5036     Shift (WATERINJ2PV, NUM, 1,WATERINJ2PV);

```

```

5037         }
5038
5039     Shift (PERMWATERDP1,NUM, 1,PERMWATERDP1);
5040     Shift (PERMWATERDELTA, NUM, 1,PERMWATERDELTA);
5041
5042     Shift (PERMOILD1, NUM, 1,PERMOILD1);
5043     Shift (PERMOILDELTA,NUM, 1,PERMOILDELTA);
5044
5045     Shift (PERMEMULDP1, NUM, 1,PERMEMULDP1);
5046     Shift (PERMEMULDELTA, NUM, 1,PERMEMULDELTA);
5047
5048 if (G_WATERINJ[0] != G_WATERINJ[1])
5049             Shift (G_WATERINJ, NUM, 1,G_WATERINJ);
5050 if (G_OILINJ[0] != G_OILINJ[1])
5051             Shift (G_OILINJ, NUM, 1,G_OILINJ);
5052 if (G_EMULINJ[0] != G_EMULINJ[1])
5053             Shift (G_EMULINJ, NUM, 1,G_EMULINJ);
5054
5055     Shift (OUTLET, NUM, 1,OUTLET);
5056     Shift (TP2, NUM, 1,TP2); //inlet
5057     Shift (DP1, NUM, 1,DP1); //dP-1 sensor
5058     Shift (TP1, NUM, 1,TP1); //outlet
5059     Shift (Delta, NUM, 1,Delta); // TP2-TP1 delta pressure
5060
5061     Shift (CP11, NUM, 1,CP11); //inlet
5062     Shift (CP12, NUM, 1,CP12); //inlet
5063     Shift (CP13, NUM, 1,CP13); //inlet
5064     Shift (CP14, NUM, 1,CP14); //inlet
5065     Shift (CP15, NUM, 1,CP15); //inlet
5066
5067     Shift (CP21, NUM, 1,CP21); //inlet
5068     Shift (CP22, NUM, 1,CP22); //inlet
5069     Shift (CP23, NUM, 1,CP23); //inlet
5070     Shift (CP24, NUM, 1,CP24); //inlet
5071     Shift (CP25, NUM, 1,CP25); //inlet
5072
5073     Shift (CP31, NUM, 1,CP31); //inlet
5074     Shift (CP32, NUM, 1,CP32); //inlet
5075     Shift (CP33, NUM, 1,CP33); //inlet
5076     Shift (CP34, NUM, 1,CP34); //inlet
5077     Shift (CP35, NUM, 1,CP35); //inlet
5078
5079
5080     Shift (MANUAL_TEST_TUBE, NUM, 1, MANUAL_TEST_TUBE);
5081 return;
5082 }
5083
5084 //*****DSN_SHIFT_Slow : Will step data along an array
5085 // : For all data that can be plotted
5086 //*****DSN SHIFT Slow
5087 //*****
5088
5089 void DSN_SHIFT_Slow(int instrument)
5090 {
5091     switch(instrument)
5092     {
5093         case 0: // Pump #1 Volume flow rate
5094             Shift (PFR11,NUM, 1, PFR11);
5095             break;
5096         case 1: // Pump #2 Volume flow rate
5097             Shift (PFR21,NUM, 1, PFR21);
5098             break;
5099         case 2: // Pump #3 Volume flow rate
5100             Shift (PFR31,NUM, 1, PFR31);
5101             break;
5102         case 3: // Pump #1 Pressure
5103             Shift (P11,NUM, 1, P11);
5104             break;
5105         case 4: // Pump #2 Pressure
5106             Shift (P21,NUM, 1, P21);
5107             break;
5108         case 5: // Pump #3 Pressure
5109             Shift (P31,NUM, 1, P31);
5110             break;
5111     }
5112 return;
5113 }
5114
5115 //*****DSN_Graph : Calls Graphing Function and Scales X Axes
5116 // build based on DSN_Graph
5117 //*****
5118 //*****
5119 void Graph(void)
5120 {
5121 // GRAPH #1
5122     if(OnOff_G1)
5123     {
5124         Graph.Select(plotVar_G_1, MAIN_G_1);
5125         if(plotVar_G_1>=0)
5126             SetAxisScalingMode (panel_handle, MAIN_G_1, VAL_XAXIS, VAL_MANUAL, step[0]-X_Range_G_1, step[0]);
5127     }
5128 // GRAPH #2
5129     if(OnOff_G2)
5130     {
5131         Graph.Select(plotVar_G_2, MAIN_G_2);
5132         if(plotVar_G_2>=0)
5133             SetAxisScalingMode (panel handle, MAIN_G_2, VAL_XAXIS, VAL MANUAL, step[0]-X Range G_2, step[0]);

```

```

5134     }
5135 // GRAPH #3
5136     if(OnOff_G3)
5137     {
5138         Graph_Select(plotVar_G_3, MAIN_G_3);
5139         if(plotVar_G_3>=0)
5140             SetAxisScalingMode (panel_handle, MAIN_G_3, VAL_XAXIS, VAL_MANUAL, step[0]-X_Range_G_3, step[0]);
5141     }
5142 // GRAPH #4
5143     if(OnOff_G4)
5144     {
5145         Graph_Select(plotVar_G_4, MAIN_G_4);
5146         if(plotVar_G_4>=0)
5147             SetAxisScalingMode (panel_handle, MAIN_G_4, VAL_XAXIS, VAL_AUTOSCALE, step[0]-X_Range_G_4, step[0]);
5148     }
5149 // GRAPH #5
5150     if(OnOff_G5)
5151     {
5152         Graph_Select(plotVar_G_5, EXTRA_G_G_5);
5153     }
5154
5155 // GRAPH #6 _ showing percentage of each liquid
5156     if(OnOff_G6)
5157     {
5158         plotVar_G_6=25;
5159         Graph_Select(plotVar_G_6, MAIN_G_6);
5160         if(plotVar_G_6>=0)
5161             SetAxisScalingMode (panel_handle, MAIN_G_6, VAL_XAXIS, VAL_AUTOSCALE, step[0]-250, step[0]);
5162     }
5163
5164 return;
5165 }
5166
5167 //***** ****
5168 // Graph_Select : Plots the Selected Variable
5169 // build based on DSN_Graph_Select
5170 //***** ****
5171 void Graph_Select(int plotVar, int Panel_Graph)
5172 {
5173     switch(plotVar)
5174     {
5175         case -2:
5176             DeleteGraphPlot (extra_g_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5177             break;
5178         case -1:
5179             DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5180             break;
5181         case 0: // Pressure [Pump #1 and TP-2]
5182             DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5183
5184             PlotXY (panel_handle, Panel_Graph, step, P11, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
5185             1, VAL_RED);
5186             PlotXY (panel_handle, Panel_Graph, step, TP2, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_FAT_LINE, VAL_EMPTY_SQUARE, VAL_SOLID,
5187             1, VAL_WHITE);
5188             break;
5189         case 1: // Pressure [Pump #3 and TP-2]
5190             DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5191
5192             PlotXY (panel_handle, Panel_Graph, step, P21, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
5193             1, VAL_RED);
5194             PlotXY (panel_handle, Panel_Graph, step, TP2, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_FAT_LINE, VAL_EMPTY_SQUARE, VAL_SOLID,
5195             1, VAL_WHITE);
5196             break;
5197         case 2: // Pressure [Pump #3 and TP-2]
5198             DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5199
5200             PlotXY (panel_handle, Panel_Graph, step, P21, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
5201             1, VAL_RED);
5202             PlotXY (panel_handle, Panel_Graph, step, TP2, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_FAT_LINE, VAL_EMPTY_SQUARE, VAL_SOLID,
5203             1, VAL_WHITE);
5204             break;
5205
5206         case 3: // Mass Flow Rate M#1
5207             DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5208
5209             PlotXY (panel_handle, Panel_Graph, step, M13, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
5210             1, VAL_RED);
5211             break;
5212
5213         case 4: // Mass Flow Rate M#2
5214             DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5215
5216             PlotXY (panel_handle, Panel_Graph, step, M23, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
5217             1, VAL_RED);
5218             break;
5219
5220         case 5: // Mass Flow Rate M#3
5221             DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5222
5223             PlotXY (panel_handle, Panel_Graph, step, M33, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
5224             1, VAL_RED);
5225             break;
5226
5227         case 6: // Mass Flow Rate M#4
5228             DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5229
5230             PlotXY (panel_handle, Panel_Graph, step, M43, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,

```

```

1, VAL_RED);
5222     break;
5223
5224     case 7: // Density M#1 Water
5225         DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5226
5227         PlotXY (panel_handle, Panel_Graph, step, M11, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
1, VAL_RED);
5228     break;
5229
5230     case 8: // Density M#2 Oil
5231         DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5232
5233         PlotXY (panel_handle, Panel_Graph, step, M21, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
1, VAL_RED);
5234     break;
5235
5236     case 9: // Density M#3 Emulsion
5237         DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5238
5239         PlotXY (panel_handle, Panel_Graph, step, M31, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
1, VAL_RED);
5240     break;
5241
5242     case 10:// Density M#4 Mixture out
5243         DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5244
5245         PlotXY (panel_handle, Panel_Graph, step, M41, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
1, VAL_RED);
5246     break;
5247
5248     case 11:// Pressure Inlet TP-2
5249         DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5250
5251         PlotXY (panel_handle, Panel_Graph, step, TP2, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
1, VAL_RED);
5252     break;
5253
5254     case 12:// Differential pressure dP1
5255         DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5256
5257         PlotXY (panel_handle, Panel_Graph, step, DP1, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
1, VAL_RED);
5258     break;
5259
5260     case 13://Delta pressure TP-2 - BRP-1
5261         DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5262
5263         PlotXY (panel_handle, Panel_Graph, step, Delta, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
1, VAL_RED);
5264     break;
5265
5266     case 14://Delta pressure TP-2 - BRP-1 vs dP1
5267         DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5268
5269         PlotXY (panel_handle, Panel_Graph, step, Delta, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID
1, VAL_RED);
5270         PlotXY (panel_handle, Panel_Graph, step, DP1, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_FAT_LINE, VAL_EMPTY_SQUARE, VAL_SOLID,
1, VAL_WHITE);
5271
5272     break;
5273
5274     case 15://Water injected
5275         DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5276
5277         PlotXY (panel_handle, Panel_Graph, step, WATERINJ, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SO
LID, 1, VAL_RED);
5278     break;
5279
5280     case 16://OIL injected
5281         DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5282
5283         PlotXY (panel_handle, Panel_Graph, step, OILINJ, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SO
D, 1, VAL_RED);
5284     break;
5285
5286     case 17://Emulsion injected
5287         DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5288
5289         PlotXY (panel_handle, Panel_Graph, step, EMULINJ, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SO
ID, 1, VAL_RED);
5290     break;
5291
5292     case 18:// Temperature M#1 Water
5293         DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5294
5295         PlotXY (panel_handle, Panel_Graph, step, M12, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
1, VAL_RED);
5296         PlotXY (panel_handle, Panel_Graph, step, M22, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
1, VAL_YELLOW);
5297         PlotXY (panel_handle, Panel_Graph, step, M32, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
1, VAL_DK_YELLOW);
5298         PlotXY (panel_handle, Panel_Graph, step, M42, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
1, VAL_DK_MAGENTA);
5299     break;
5300
5301     case 19:// Water flooding

```

```

5302     DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5303
5304     PlotXY (panel_handle, Panel_Graph, step, WATERINJ2, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_S
OLID, 1, VAL_RED);
5305     break;
5306
5307     case 20:// Water flooding PV
5308     DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5309
5310     PlotXY (panel_handle, Panel_Graph, step, WATERINJ2PV, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL
_SOLID, 1, VAL_RED);
5311     break;
5312
5313     case 21:// Oil recovered vs Water injected PV
5314     DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5315
5316     PlotXY (panel_handle, Panel_Graph, WATERINJ2PV, OILREC, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, V
AL_SOLID, 1, VAL_RED);
5317     break;
5318
5319     case 22:// Oil recovered vs Time
5320     DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5321
5322     PlotXY (panel_handle, Panel_Graph, step, OILREC, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_S
OLID, 1, VAL_RED);
5323     break;
5324
5325     case 23://Swi vs Time
5326     DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5327
5328     PlotXY (panel_handle, Panel_Graph, step, SWI, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
1, VAL_RED);
5329     break;
5330
5331     case 24://Oil out at stage 9
5332     DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5333
5334     PlotXY (panel_handle, Panel_Graph, step, OILREC_ST9, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_
SOLID, 1, VAL_RED);
5335     break;
5336
5337     case 25://Water out at stage 9
5338
5339     DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5340
5341     PlotXY (panel_handle, Panel_Graph, step, WATERREC_ST9, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VA
L_SOLID, 1, VAL_RED);
5342     break;
5343
5344
5345     case 26:// Water inj PV vs Pressure drop
5346     DeleteGraphPlot (extra_g_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5347
5348     PlotXY (extra_g_handle, Panel_Graph, WATERINJ2PV, DP1, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VA
L_SOLID, 1, VAL_RED);
5349     break;
5350
5351
5352     case 27:// Water inj PV vs Ref. pressure drop
5353     DeleteGraphPlot (extra_g_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5354
5355     PlotXY (extra_g_handle, Panel_Graph, WATERINJ2PV, Delta, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE,
VAL_SOLID, 1, VAL_RED);
5356     break;
5357
5358
5359     case 28:// Water inj PV vs Ref. pressure drop vs DP1
5360     DeleteGraphPlot (extra_g_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5361
5362     PlotXY (extra_g_handle, Panel_Graph, WATERINJ2PV, Delta, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE,
VAL_SOLID, 1, VAL_RED);
5363     PlotXY (extra_g_handle, Panel_Graph, WATERINJ2PV, DP1, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VA
L_SOLID, 1, VAL_WHITE);
5364     break;
5365
5366
5367
5368     case 29:// Experimental stage [option underconstruction]
5369     DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5370
5371     break;
5372
5373     case 30:// Only for GRAPH #6
5374     DeleteGraphPlot (panel_handle, Panel_Graph, -1,VAL_IMMEDIATE_DRAW);
5375
5376     PlotXY (panel_handle, Panel_Graph, step, M41, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL_SOLID,
1, VAL_RED);
5377     PlotXY (panel_handle, Panel_Graph, step, SETPOINTOUT, NUM, VAL_DOUBLE, VAL_DOUBLE, VAL_SCATTER, VAL_SOLID_CIRCLE, VAL
_SOLID, 1, VAL_RED);
5378     break;
5379
5380
5381 }
5382 return;
5383 }
5384
5385 int CVICALLBACK LOG ON OFF (int panel, int control, int event,

```

```

5386     void *callbackData, int eventData1, int eventData2)
5387 {
5388     switch (event)
5389     {
5390         case EVENT_COMMIT:
5391             // COM Ports
5392             GetCtrlVal(panel_handle, MAIN_LOG_P1, &Is_P1);
5393             if (p1check == 0) SetCtrlVal(panel_handle, MAIN_LOG_P1, 0);
5394
5395             GetCtrlVal(panel_handle, MAIN_LOG_P2, &Is_P2);
5396             if (p2check == 0) SetCtrlVal(panel_handle, MAIN_LOG_P2, 0);
5397
5398             GetCtrlVal(panel_handle, MAIN_LOG_P3, &Is_P3);
5399             if (p3check == 0) SetCtrlVal(panel_handle, MAIN_LOG_P3, 0);
5400
5401             // Mass Flow Meters
5402             GetCtrlVal(panel_handle, MAIN_LOG_M1, &Is_M1);
5403             GetCtrlVal(panel_handle, MAIN_LOG_M2, &Is_M2);
5404             GetCtrlVal(panel_handle, MAIN_LOG_M3, &Is_M3);
5405             GetCtrlVal(panel_handle, MAIN_LOG_M4, &Is_M4);
5406
5407             // Back Pressure Regulator
5408             GetCtrlVal(panel_handle, MAIN_LOG_BPR, &Is_BPR);
5409
5410             // Main Parameters
5411             GetCtrlVal(panel_handle, MAIN_LOG_Graph, &Is_Graph);
5412             GetCtrlVal(panel_handle, MAIN_LOG_LOGToFile, &Is_Log);
5413
5414             // DAQ
5415             GetCtrlVal(panel_handle, MAIN_LOG_DAQ, &Is_DAQ);
5416
5417             // Camera
5418             GetCtrlVal(panel_handle, MAIN_LOG_CAM, &Is_Cam);
5419
5420             Update_Graphics(); // Update On-screen Graphics
5421             break;
5422         }
5423
5424     void Update_Graphics(void)
5425     {
5426         // double zero = 0;
5427         int Experiment_On;
5428
5429         GetCtrlVal(panel_handle, MAIN_START_STOP, &Experiment_On); // Check to see if experiment is running
5430
5431         if(Experiment_On) // Experiment is running
5432         {
5433
5434             EnableMassTurnControls(0);
5435
5436             if (Is_M1) EnableM1PanelControls(0);
5437             else EnableM1PanelControls(1);
5438
5439             if (Is_M2) EnableM2PanelControls(0);
5440             else EnableM2PanelControls(1);
5441
5442             if (Is_M3) EnableM3PanelControls(0);
5443             else EnableM3PanelControls(1);
5444
5445             if (Is_M4) EnableM4PanelControls(0);
5446             else EnableM4PanelControls(1);
5447
5448             if (Is_BPR) EnableBPRPanelControls(0);
5449             else EnableBPRPanelControls(1);
5450
5451             SetCtrlAttribute (panel_handle, MAIN_P1_PURGE, ATTR_DIMMED, 0);
5452             SetCtrlAttribute (panel_handle, MAIN_P1_RESTART, ATTR_DIMMED, 0);
5453             SetCtrlAttribute (panel_handle, MAIN_P1_5ERR, ATTR_DIMMED, 0);
5454
5455
5456
5457             if (STG_1) // check system
5458             {
5459                 SetCtrlAttribute (panel_handle, MAIN_STG_2, ATTR_DIMMED, 0);
5460                 SetCtrlAttribute (panel_handle, MAIN_WATER_INJ, ATTR_DIMMED, 0);
5461                 SetCtrlVal (panel_handle, MAIN_EXP_PROGRESS, 8.5);
5462             }
5463
5464             if (STG_2) // once confirmed - ask for water volume
5465             {
5466                 SetCtrlAttribute (panel_handle, MAIN_STG_3, ATTR_DIMMED, 0);
5467                 SetCtrlAttribute (panel_handle, MAIN_WATER_pv_INJ, ATTR_DIMMED, 0);
5468                 SetCtrlVal (panel_handle, MAIN_EXP_PROGRESS, 17.0);
5469             }
5470
5471
5472             if (STG_3) // waterflooding
5473             {
5474                 SetCtrlAttribute (panel_handle, MAIN_STG_4, ATTR_DIMMED, 0);
5475                 SetCtrlAttribute (panel_handle, MAIN_OIL_pv_INJ, ATTR_DIMMED, 0);
5476                 SetCtrlVal (panel_handle, MAIN_EXP_PROGRESS, 25.5);
5477             }
5478
5479             if (STG_4) // Stop water flooding - Start oil flooding
5480             {
5481                 SetCtrlAttribute (panel handle, MAIN_STG_5, ATTR DIMMED, 0);

```

```

5483     SetCtrlAttribute (panel_handle, MAIN_WATER_LEFT, ATTR_DIMMED, 0);
5484     SetCtrlVal (panel_handle, MAIN_EXP_PROGRESS, 34.00);
5485 }
5486
5487 if (STG_5) // No more water coming out
5488 {
5489     SetCtrlAttribute (panel_handle, MAIN_STG_6, ATTR_DIMMED, 0);
5490     SetCtrlVal (panel_handle, MAIN_EXP_PROGRESS, 42.50);
5491 }
5492
5493
5494 if (STG_6) // Select experiment
5495 {
5496     SetCtrlAttribute (panel_handle, MAIN_STG_7, ATTR_DIMMED, 0);
5497     SetCtrlAttribute (panel_handle, MAIN_WATER_PV_INJ_2, ATTR_DIMMED, 0);
5498     SetCtrlVal (panel_handle, MAIN_EXP_PROGRESS, 51.0);
5499
5500     GetCtrlVal (panel_handle, MAIN_SETEXP, &Type_exp);
5501
5502     if (Type_exp == 2) // Emulsion flooding
5503     {
5504         SetCtrlVal (panel_handle, MAIN_STG_7, 1);
5505         SetCtrlVal (panel_handle, MAIN_STG_8, 1);
5506         SetCtrlVal (panel_handle, MAIN_STG_9, 1);
5507         STG_7 = 1;
5508         STG_8 = 1;
5509         STG_9 = 1;
5510     }
5511     else if (Type_exp == 3) // Alternate emulsion flooding
5512     {
5513         SetCtrlVal (panel_handle, MAIN_STG_7, 1);
5514         SetCtrlVal (panel_handle, MAIN_STG_8, 1);
5515         SetCtrlVal (panel_handle, MAIN_STG_9, 1);
5516         SetCtrlVal (panel_handle, MAIN_STG_10, 1);
5517         STG_7 = 1;
5518         STG_8 = 1;
5519         STG_9 = 1;
5520         STG_10 = 1;
5521     }
5522 }
5523
5524
5525 if (STG_7) // Waterflooding
5526 {
5527     SetCtrlAttribute (panel_handle, MAIN_STG_8, ATTR_DIMMED, 0);
5528     SetCtrlAttribute (panel_handle, MAIN_OIL_REC_PV, ATTR_DIMMED, 0);
5529     SetCtrlVal (panel_handle, MAIN_EXP_PROGRESS, 59.5);
5530 }
5531
5532
5533 if (STG_8) // No more oil comming out
5534 {
5535     SetCtrlAttribute (panel_handle, MAIN_STG_9, ATTR_DIMMED, 0);
5536     SetCtrlVal (panel_handle, MAIN_EXP_PROGRESS, 68.00);
5537 }
5538
5539 if (STG_9) // Stop water flooding - start emulsion flooding
5540 {
5541     SetCtrlAttribute (panel_handle, MAIN_STG_10, ATTR_DIMMED, 0);
5542     SetCtrlAttribute (panel_handle, MAIN_EMULSION_PV_INJ, ATTR_DIMMED, 0);
5543     SetCtrlVal (panel_handle, MAIN_EXP_PROGRESS, 76.5);
5544 }
5545
5546 if (STG_10) // End for emulsion flooding
5547 {
5548     SetCtrlAttribute (panel_handle, MAIN_STG_11, ATTR_DIMMED, 0);
5549
5550     SetCtrlAttribute (panel_handle, MAIN_W_ALT_INJ, ATTR_DIMMED, 0); //water injection cc
5551     SetCtrlAttribute (panel_handle, MAIN_WATER_PV_INJ_ALT, ATTR_DIMMED, 0); //water injection PV
5552     SetCtrlAttribute (panel_handle, MAIN_E_ALT_INJ, ATTR_DIMMED, 0); //emulsion injection cc
5553     SetCtrlAttribute (panel_handle, MAIN_EMULSION_PV_INJ_ALT, ATTR_DIMMED, 0); //emulsion injection PV
5554
5555     SetCtrlAttribute (panel_handle, MAIN_END_TEXT, ATTR_VISIBLE, 1 );
5556     SetCtrlVal (panel_handle, MAIN_EXP_PROGRESS, 84.50);
5557 }
5558
5559 if (STG_11) // Alternate method
5560 {
5561     SetCtrlAttribute (panel_handle, MAIN_STG_12, ATTR_DIMMED, 0);
5562     SetCtrlVal (panel_handle, MAIN_EXP_PROGRESS, 93.00);
5563 }
5564
5565 if (STG_12) //End of experiment
5566 {
5567     MessagePopup("Info message","Experiment has been completed. Good luck with Data.");
5568     SetCtrlVal (panel_handle, MAIN_EXP_PROGRESS, 100.00);
5569 }
5570
5571 }
5572 else // Experiment is NOT running
5573 {
5574
5575     EnableMassTurnControls(1);
5576
5577 // SetCtrlAttribute (panel_handle, MAIN_L_CORE, ATTR_CTRL_MODE, VAL_HOT);
5578 // SetCtrlAttribute (panel_handle, MAIN_D_CORE, ATTR_CTRL_MODE, VAL_HOT);
5579 // SetCtrlAttribute (panel_handle, MAIN_V_CORE, ATTR_CTRL_MODE, VAL_HOT);

```

```

5580 // SetCtrlAttribute(panel_handle, MAIN_POR_CORE, ATTR_CTRL_MODE, VAL_HOT);
5581 // Dimmed M1..4, BPR panels
5582
5583     EnableM1PanelControls(1);
5584     EnableM2PanelControls(1);
5585     EnableM3PanelControls(1);
5586     EnableM4PanelControls(1);
5587     EnableBPRPanelControls(1);
5588
5589 }
5590 return;
5591 }
5592
5593 ///////////////////////////////////////////////////////////////////
5594 ///////////////////////////////////////////////////////////////////
5595
5596 int CVICALLBACK START_STOP (int panel, int control, int event,
5597 void *callbackData, int eventData1, int eventData2)
5598 { int test2;
5599 int i; // ,j,delay;
5600
5601 switch (event)
5602 {
5603     case EVENT_COMMIT:
5604
5605         GetCtrlVal(panel_handle, MAIN_START_STOP, &test2);
5606
5607         SaveVars();
5608         Update_Graphics();
5609
5610         SetCtrlVal(panel_handle, MAIN_SAMPLES, SAMPLES);
5611
5612         if (!test2) // Stop experiment
5613         {
5614             forcestop = 1;
5615             Update_Graphics();
5616
5617             SetCtrlAttribute(panel_handle,MAIN_SNAP_SAVE,ATTR_DIMMED,1);
5618
5619             //-----
5620             // STOP DAQ
5621             //-----
5622             if(Is_DAQ)
5623             {
5624                 DAQquitflag = 0;
5625                 Pumps_quitflag=0;
5626                 Mass_quitflag=0; //close Mass_Thread loop
5627                 BPR_quitflag=0; //close BPR_Thread loop
5628                 Camera_quitflag=0; //close Camera_Thread loop
5629                 Email_quitflag=0; //close Email_Thread loop
5630
5631                 Delay(1);
5632
5633                 DAQmxStopTask(taskHandle);
5634                 DAQmxClearTask(taskHandle);
5635                 DAO_Task_Start = 0;
5636
5637                 if( DAQdata )
5638                     free(DAQdata);
5639                 if( DAQArray_Out )
5640                     free(DAQArray_Out);
5641
5642                     CmtReleaseThreadPoolFunctionID (DEFAULT_THREAD_POOL_HANDLE, DAQthreadID);
5643                     CmtReleaseThreadPoolFunctionID (DEFAULT_THREAD_POOL_HANDLE, Mass_threadID);
5644                     CmtReleaseThreadPoolFunctionID (DEFAULT_THREAD_POOL_HANDLE, Pumps_threadID);
5645                     CmtReleaseThreadPoolFunctionID (DEFAULT_THREAD_POOL_HANDLE, BPR_threadID);
5646                     CmtReleaseThreadPoolFunctionID (DEFAULT_THREAD_POOL_HANDLE, Camera_threadID);
5647                     CmtReleaseThreadPoolFunctionID (DEFAULT_THREAD_POOL_HANDLE, Email_threadID);
5648
5649
5650                 Delay(1);
5651             }
5652
5653             // Stop PUMPS #1-3
5654
5655             STOPPUMPS();
5656
5657             Delay(1);
5658
5659             CmtDiscardLock (DAO_lockHandle);
5660         }
5661         else // Start experiment
5662         {
5663
5664             forcestop = 0;
5665
5666             GeoMath();
5667             /*
5668             if (V_core == 0)
5669             {
5670                 MessagePopup ("Warning","Geometry of sand pack is required.");
5671                 SetCtrlVal(panel_handle, MAIN_START_STOP, 0);
5672                 SetCtrlAttribute(panel_handle,MAIN_CORE HOLDER,ATTR_FRAME_COLOR,VAL_RED);
5673                 break;
5674             }
5675             else    SetCtrlAttribute(panel_handle,MAIN_CORE HOLDER,ATTR_FRAME_COLOR,VAL_LT_GRAY);
5676         */
5677
5678
5679
5680
5681
5682
5683
5684
5685
5686
5687
5688
5689
5690
5691
5692
5693
5694
5695
5696
5697
5698
5699
5700
5701
5702
5703
5704
5705
5706
5707
5708
5709
5710
5711
5712
5713
5714
5715
5716
5717
5718
5719
5720
5721
5722
5723
5724
5725
5726
5727
5728
5729
5730
5731
5732
5733
5734
5735
5736
5737
5738
5739
5740
5741
5742
5743
5744
5745
5746
5747
5748
5749
5750
5751
5752
5753
5754
5755
5756
5757
5758
5759
5760
5761
5762
5763
5764
5765
5766
5767
5768
5769
5770
5771
5772
5773
5774
5775
5776
5777
5778
5779
5780
5781
5782
5783
5784
5785
5786
5787
5788
5789
5790
5791
5792
5793
5794
5795
5796
5797
5798
5799
5800
5801
5802
5803
5804
5805
5806
5807
5808
5809
5810
5811
5812
5813
5814
5815
5816
5817
5818
5819
5820
5821
5822
5823
5824
5825
5826
5827
5828
5829
5830
5831
5832
5833
5834
5835
5836
5837
5838
5839
5840
5841
5842
5843
5844
5845
5846
5847
5848
5849
5850
5851
5852
5853
5854
5855
5856
5857
5858
5859
5860
5861
5862
5863
5864
5865
5866
5867
5868
5869
5870
5871
5872
5873
5874
5875
5876
5877
5878
5879
5880
5881
5882
5883
5884
5885
5886
5887
5888
5889
5890
5891
5892
5893
5894
5895
5896
5897
5898
5899
5900
5901
5902
5903
5904
5905
5906
5907
5908
5909
5910
5911
5912
5913
5914
5915
5916
5917
5918
5919
5920
5921
5922
5923
5924
5925
5926
5927
5928
5929
5930
5931
5932
5933
5934
5935
5936
5937
5938
5939
5940
5941
5942
5943
5944
5945
5946
5947
5948
5949
5950
5951
5952
5953
5954
5955
5956
5957
5958
5959
5960
5961
5962
5963
5964
5965
5966
5967
5968
5969
5970
5971
5972
5973
5974
5975
5976
5977
5978
5979
5980
5981
5982
5983
5984
5985
5986
5987
5988
5989
5990
5991
5992
5993
5994
5995
5996
5997
5998
5999
5999

```

```

5677 // Thread for Instruments, Logs, etc.
5678 ThreadsRun();
5679
5680 SetCtrlAttribute(panel_handle,MAIN_SNAP_SAVE,ATTR_DIMMED,0);
5681
5682 // Undim Monitored Readouts and Adjust Control Types
5683
5684 Update_Graphics();
5685
5686
5687
5688 //Enter into Experiment process
5689
5690
5691 stage = 1;
5692 while (STG_1 != 1)
5693 {
5694     ProcessSystemEvents ();
5695
5696     GetCtrlVal (panel_handle, MAIN_EMERGENCY, &EM_Q);
5697     BLINK();
5698     if (EM_Q==1 || forcestop==1)
5699     {
5700         goto Flag;
5701     }
5702     ProcessSystemEvents ();
5703
5704
5705     DisplayPanel(sat_handle);
5706
5707     stage = 2;
5708     while (STG_2 !=1)
5709     {
5710         ProcessSystemEvents ();
5711         GetCtrlVal (panel_handle, MAIN_EMERGENCY, &EM_Q);
5712         BLINK();
5713         if (EM_Q==1 || forcestop==1)
5714         {
5715             goto Flag;
5716         }
5717         ProcessSystemEvents ();
5718
5719     }
5720
5721     stage = 3;
5722
5723     CmtGetLock (Pumps_lockHandle);
5724     Delay (0.1);
5725
5726     wb_setpoint = 0.500;
5727     SetCtrlVal(panel_handle, MAIN_P1_SET_NFR, wb_setpoint);
5728
5729     SNFRP_1();
5730
5731     pumprun_1 = 11;    //save status about pump #1
5732
5733     panel_name=panel_handle;
5734     CP=P1_comport;
5735     send_data[0] = '\0';
5736     Fmt (send_data, "%s<ON\r");
5737     PTEXT_panel_name= MAIN_STATUS_P_1; //show response from pump
5738     SendReadPump ();
5739
5740     CmtReleaseLock (Pumps_lockHandle);
5741
5742
5743     while (STG_3 !=1)
5744     {
5745         ProcessSystemEvents ();
5746
5747         SetCtrlVal(panel_handle,MAIN_WATER_PV_INJ,WATERINJPV[1]); //ok //Show up value for the water
flooding
5748
5749         GetCtrlVal (panel_handle, MAIN_EMERGENCY, &EM_Q);
5750         BLINK();
5751         if (EM_Q==1 || forcestop==1)
5752         {
5753             goto Flag;
5754         }
5755         ProcessSystemEvents ();
5756
5757
5758         if (STG_3 == 1) STOPPUMPS(); //ok //stop ALL PUMPS [read as - waterflooding]
5759
5760         stage = 4;           //stop waterflooding - start oil flooding
5761         while (STG_4 !=1)
5762         {
5763             ProcessSystemEvents ();
5764
5765             SetCtrlVal(panel_handle,MAIN_OIL_PV_INJ,OILINJPV[1]); //ok
5766
5767             GetCtrlVal (panel_handle, MAIN_EMERGENCY, &EM_Q);
5768             BLINK();
5769             if (EM_Q==1 || forcestop==1)
5770             {
5771                 goto Flag;
5772             }

```

```

5773         ProcessSystemEvents ();
5774     }
5775
5776     if (SWI[0] != 0.00) SetCtrlVal (panel_handle, MAIN_WATER_LEFT, SWI[0]); //set value to the
5777     panel.
5778     else SetCtrlVal (panel_handle, MAIN_WATER_LEFT, SWI[1]);
5779
5780     stage = 5;
5781     while (STG_5 !=1)
5782     {
5783         ProcessSystemEvents ();
5784         BLINK();
5785         GetCtrlVal (panel_handle, MAIN_EMERGENCY, &EM_Q);
5786
5787         if (EM_Q==1 || forcestop==1)
5788         {
5789             goto Flag;
5790         }
5791         ProcessSystemEvents ();
5792     }
5793
5794
5795     if (STG_5 == 1) MessagePopup ("Warning","Please select flooding order.");
5796
5797     stage = 6;
5798     while (STG_6 !=1) //ok //select experimental type
5799     {
5800
5801         ProcessSystemEvents ();
5802         BLINK();
5803         GetCtrlVal (panel_handle, MAIN_EMERGENCY, &EM_Q);
5804
5805
5806         if (EM_Q==1 || forcestop==1)
5807         {
5808             goto Flag;
5809         }
5810         ProcessSystemEvents ();
5811     }
5812
5813
5814 //start fraction collector
5815
5816     SWITCH_FRACTION (1, 0, 0, 0);
5817     Delay (0.5);
5818     SWITCH_FRACTION (0, 0, 0, 0);
5819
5820
5821     stage = 7;
5822     while (STG_7 != 1) //waterflooding
5823     {
5824         ProcessSystemEvents ();
5825         SetCtrlVal(panel_handle,MAIN_WATER_PV_INJ_2,WATERINJ2PV[1]); //ok
5826
5827         BLINK();
5828         GetCtrlVal (panel_handle, MAIN_EMERGENCY, &EM_Q);
5829         if (EM_Q==1 || forcestop==1)
5830         {
5831             goto Flag;
5832         }
5833         ProcessSystemEvents ();
5834     }
5835
5836     if (STG_7 == 1) STOPPUMPS(); //stop waterflooding
5837
5838
5839     stage = 8;
5840     while (STG_8 !=1)
5841     {
5842         ProcessSystemEvents ();
5843         BLINK();
5844         GetCtrlVal (panel_handle, MAIN_EMERGENCY, &EM_Q);
5845
5846         if (EM_Q==1 || forcestop==1)
5847         {
5848             goto Flag;
5849         }
5850         ProcessSystemEvents ();
5851
5852
5853     stage = 9;
5854     while (STG_9 !=1)
5855     {
5856         ProcessSystemEvents ();
5857         BLINK();
5858
5859         GetCtrlVal (panel_handle, MAIN_EMERGENCY, &EM_Q);
5860         if (EM_Q==1 || forcestop==1)
5861         {
5862             goto Flag;
5863         }
5864         ProcessSystemEvents ();
5865
5866
5867     stage = 10;
5868     while (STG_10 !=1) //emulsion flooding

```

```

5869 {
5870     ProcessSystemEvents ();
5871     SetCtrlVal(panel_handle,MAIN_EMULSION_PV_INJ,EMULINJPV[1]);
5872     BLINK();
5873
5874     GetCtrlVal (panel_handle, MAIN_EMERGENCY, &EM_Q);
5875     if (EM_Q==1 || forcestop==1)
5876     {
5877         goto Flag;
5878     }
5879     ProcessSystemEvents ();
5880 }
5881
5882
5883     if (STG_10 == 1) STOPPUMPS(); //double check that all pumps are stopped
5884
5885     stage = 11;
5886     while (STG_11 !=1) //alternate flooding
5887     {
5888         ProcessSystemEvents ();
5889
5890         if (pumprun_1 == 11)
5891         {
5892             SetCtrlVal(panel_handle,MAIN_W_ALT_INJ,WATERINJ2[1]);
5893             SetCtrlVal(panel_handle,MAIN_WATER_PV_INJ_ALT,WATERINJ2PV[1]);
5894         }
5895
5896         BLINK();
5897
5898         GetCtrlVal (panel_handle, MAIN_EMERGENCY, &EM_Q);
5899         if (EM_Q==1 || forcestop==1)
5900         {
5901             goto Flag;
5902         }
5903         ProcessSystemEvents ();
5904
5905
5906
5907         if (STG_11 == 1) STOPPUMPS(); //double check that all pumps are stopped
5908
5909         stage = 12;
5910         while (STG_12 !=1) //done
5911         {
5912             ProcessSystemEvents ();
5913             BLINK();
5914
5915
5916             GetCtrlVal (panel_handle, MAIN_EMERGENCY, &EM_Q);
5917             if (EM_Q==1 || forcestop==1)
5918             {
5919                 goto Flag;
5920             }
5921             ProcessSystemEvents ();
5922         }
5923
5924 Flag:
5925     if (EM_Q==1 || forcestop==1)
5926     {
5927         MessagePopup ("Warning","Experiment progress has been released.");
5928         // EMG_STOP(1);
5929     }
5930
5931     }
5932
5933     break;
5934 }
5935 }
5936 return 0;
5937 }
5938
5939 int CVICALLBACK GEO_MATH (int panel, int control, int event,
5940     void *callbackData, int eventData1, int eventData2)
5941 {
5942     switch (event)
5943     {
5944         case EVENT_COMMIT:
5945             GeoMath();
5946
5947             break;
5948
5949     }
5950     return 0;
5951 }
5952
5953 void GeoMath(void)
5954 {
5955     int temp;
5956
5957     GetCtrlVal(panel_handle, MAIN_2D_CH, &temp);
5958
5959     if (temp == TRUE)
5960     {
5961         V_core = 2391.63 ; //2D configuration
5962         A_core = 20*2 ; //2D configuration
5963     }
5964     else
5965     {
5966         GetCtrlVal(panel handle, MAIN_L_CORE, &L core);

```

```

5966     GetCtrlVal(panel_handle, MAIN_D_CORE, &D_core);
5967     A_core= pi*D_core*D_core / 4;
5968     V_core= A_core*L_core;      //bulk volume of rock
5969 }
5970     SetCtrlVal(panel_handle, MAIN_V_CORE, V_core);
5971
5972 // for permeability
5973     Perm_coef = 0.242 * L_core / A_core ;
5974
5975 // Porosity calculations, based on water saturation
5976     GetCtrlVal(panel_handle, MAIN_WATER_CORE, &WAT_core);
5977     Por_core=WAT_core/V_core;           //porosity = pore volume / bulk volume
5978     Por_core_per=Por_core*100;
5979     SetCtrlVal(panel_handle, MAIN_POR_CORE, Por_core_per);
5980
5981 return;
5982 }
5983
5984 int CVICALLBACK STG_NEXT (int panel, int control, int event,
5985     void *callbackData, int eventData1, int eventData2)
5986 {
5987     switch (event)
5988     {
5989         case EVENT_COMMIT:
5990
5991 // Equipment Setup
5992     GetCtrlVal(panel_handle, MAIN_STG_1, &STG_1);
5993     GetCtrlVal(panel_handle, MAIN_STG_2, &STG_2);
5994     GetCtrlVal(panel_handle, MAIN_STG_3, &STG_3);
5995     GetCtrlVal(panel_handle, MAIN_STG_4, &STG_4);
5996     GetCtrlVal(panel_handle, MAIN_STG_5, &STG_5);
5997     GetCtrlVal(panel_handle, MAIN_STG_6, &STG_6);
5998     GetCtrlVal(panel_handle, MAIN_STG_7, &STG_7);
5999     GetCtrlVal(panel_handle, MAIN_STG_8, &STG_8);
6000     GetCtrlVal(panel_handle, MAIN_STG_9, &STG_9);
6001     GetCtrlVal(panel_handle, MAIN_STG_10, &STG_10);
6002     GetCtrlVal(panel_handle, MAIN_STG_11, &STG_11);
6003     GetCtrlVal(panel_handle, MAIN_STG_12, &STG_12);
6004
6005     Update_Graphics();      // Update On-screen Graphics
6006
6007     break;
6008 }
6009     return 0;
6010 }
6011
6012 void EMG_STOP(int enable )
6013 {
6014
6015     SetCtrlAttribute(panel_handle, MAIN_STG_1, ATTR_CTRL_MODE, VAL_INDICATOR,enable);
6016     SetCtrlAttribute(panel_handle, MAIN_STG_2, ATTR_CTRL_MODE, VAL_INDICATOR,enable);
6017     SetCtrlAttribute(panel_handle, MAIN_STG_3, ATTR_CTRL_MODE, VAL_INDICATOR,enable);
6018     SetCtrlAttribute(panel_handle, MAIN_STG_4, ATTR_CTRL_MODE, VAL_INDICATOR,enable);
6019     SetCtrlAttribute(panel_handle, MAIN_STG_5, ATTR_CTRL_MODE, VAL_INDICATOR,enable);
6020     SetCtrlAttribute(panel_handle, MAIN_STG_6, ATTR_CTRL_MODE, VAL_INDICATOR,enable);
6021     SetCtrlAttribute(panel_handle, MAIN_STG_7, ATTR_CTRL_MODE, VAL_INDICATOR,enable);
6022     SetCtrlAttribute(panel_handle, MAIN_STG_8, ATTR_CTRL_MODE, VAL_INDICATOR,enable);
6023     SetCtrlAttribute(panel_handle, MAIN_STG_9, ATTR_CTRL_MODE, VAL_INDICATOR,enable);
6024     SetCtrlAttribute(panel_handle, MAIN_STG_10, ATTR_CTRL_MODE, VAL_INDICATOR,enable);
6025     SetCtrlAttribute(panel_handle, MAIN_STG_11, ATTR_CTRL_MODE, VAL_INDICATOR,enable);
6026     SetCtrlAttribute(panel_handle, MAIN_STG_12, ATTR_CTRL_MODE, VAL_INDICATOR,enable);
6027
6028 //SetPanelAttribute(panel_handle,ATTR_BACKCOLOR,VAL_RED);
6029
6030     return;
6031 }
6032
6033 void BLINK (void)
6034 {
6035     SetCtrlAttribute(panel_handle,MAIN_BLINK_TEXT,ATTR_TEXT_COLOR, VAL_WHITE);
6036     ProcessSystemEvents ();
6037     Delay (0.1);
6038     SetCtrlAttribute(panel_handle,MAIN_BLINK_TEXT,ATTR_TEXT_COLOR, VAL_GREEN);
6039
6040     return;
6041 }
6042
6043 void ThreadsRun (void)
6044 {
6045     // SETUP Pump's pressure monitoring system
6046
6047     // Start a new thread function in the Default Thread Pool
6048     Pumps_cmtStatus = CmtScheduleThreadPoolFunction (DEFAULT_THREAD_POOL_HANDLE,
6049             Pumps_ThreadFunction, NULL, &Pumps_threadID);
6050     Pumps_quitflag = 1;
6051     CmtNewLock (NULL, 0, &Pumps_lockHandle);
6052
6053     // SETUP Mass flow meters
6054     // Start a new thread function for mass flow meters in the Default Thread Pool
6055     Mass_cmtStatus = CmtScheduleThreadPoolFunction (DEFAULT_THREAD_POOL_HANDLE,
6056             Mass_ThreadFunction, NULL, &Mass_threadID);
6057     Mass_quitflag = 1;
6058     CmtNewLock (NULL, 0, &Mass_lockHandle);
6059
6060     // SETUP Backward pressure regulator
6061     // Start a new thread function for Back Pressure regulator in the Default Thread Pool
6062

```

```

6063     BPR_cmtStatus = CmtScheduleThreadPoolFunction (DEFAULT_THREAD_POOL_HANDLE,
6064                                     BPR_ThreadFunction, NULL, &BPR_threadID);
6065     BPR_quitflag = 1;
6066     CmtNewLock (NULL, 0, &BPR_lockHandle);
6067
6068 // SETUP thread for camera
6069     Camera_cmtStatus = CmtScheduleThreadPoolFunction (DEFAULT_THREAD_POOL_HANDLE,
6070                                     Camera_ThreadFunction, NULL, &Camera_threadID);
6071     Camera_quitflag = 1;
6072     CmtNewLock (NULL, 0, &Camera_lockHandle);
6073
6074 // SETUP thread for email
6075     Email_cmtStatus = CmtScheduleThreadPoolFunction (DEFAULT_THREAD_POOL_HANDLE,
6076                                     Email_ThreadFunction, NULL, &Email_threadID);
6077     Email_quitflag = 1;
6078     CmtNewLock (NULL, 0, &Email_lockHandle);
6079
6080
6081 // SETUP DAQ
6082     if (Is_DAQ)
6083     {
6084         DSN_Setup_DAQ();
6085 // Start a new thread function in the Default Thread Pool
6086         DAQcmtStatus = CmtScheduleThreadPoolFunction (DEFAULT_THREAD_POOL_HANDLE,
6087                                         DAQThreadFunction, NULL, &DAQthreadID);
6088         DAQquitflag = 1;
6089         CmtNewLock (NULL, 0, &DAQ_lockHandle);
6090     }
6091     return;
6092 }
6093
6094 void STOPPUMPS (void)
6095 {
6096     if (Pumps_quitflag == 1)
6097     {
6098         CmtGetLock (Pumps_lockHandle);
6099         Delay (0.1);
6100         STOPPUMPSSub();
6101         CmtReleaseLock (Pumps_lockHandle);
6102     }
6103 else STOPPUMPSSub();
6104     return;
6105 }
6106
6107 void STOPPUMPSSub (void)
6108 {
6109     if (Is_P1) //off pump #1
6110     {
6111         FlushOutQ (P1_comport);
6112         FlushInQ (P1_comport);
6113
6114         send_data[0] = '\0';
6115         Fmt (send_data, "%s<OFF\r");
6116
6117         stringsize = StringLength (send_data);
6118         bytes_sent = ComWrt (P1_comport, send_data, stringsize);
6119         Delay(0.05); // 0.05
6120
6121         read_cnt = GetInQLen (P1_comport);
6122
6123         read_data[0] = '\0';
6124         read_term = 13;
6125         bytes_read = ComRdTerm (P1_comport, read_data, read_cnt, read_term);
6126
6127         CopyString (tbox read_data, 0, read_data, 0, bytes_read);
6128         SetCtrlVal (panel_handle, MAIN_STATUS_P_1, tbox_read_data);
6129
6130         pumprun_1 = 12;
6131
6132 //ERROR EVENT LIST
6133 SetCtrlAttribute(panel_handle,MAIN_STOP_P_1,ATTR_VISIBLE, 1);
6134 SetCtrlAttribute(panel_handle,MAIN_ERROR_RELEASE_3,ATTR_VISIBLE, 1);
6135
6136 RS232Error = ReturnRS232Err ();
6137     if (RS232Error)
6138         DisplayRS232Error ();
6139     send_data[0] = '\0';
6140
6141     if (Is_P2) //off pump #2
6142     {
6143         FlushOutQ (P2_comport);
6144         FlushInQ (P2_comport);
6145
6146         send_data[0] = '\0';
6147         Fmt (send_data, "%s<OFF\r");
6148
6149         stringsize = StringLength (send_data);
6150         bytes_sent = ComWrt (P2_comport, send_data, stringsize);
6151         Delay(0.05); // 0.05
6152
6153         read_cnt = GetInQLen (P2_comport);
6154
6155         read_data[0] = '\0';
6156         read_term = 13;
6157         bytes_read = ComRdTerm (P2_comport, read_data, read_cnt, read_term);
6158
6159         CopyString (tbox read_data, 0, read_data, 0, bytes_read);

```

```

6160     SetCtrlVal (panel_handle, MAIN_STATUS_P_2, tbox_read_data);
6161
6162     pumprun_2 = 22;
6163
6164     //ERROR EVENT LIST
6165     SetCtrlAttribute(panel_handle,MAIN_STOP_P_2,ATTR_VISIBLE, 1);
6166     SetCtrlAttribute(panel_handle,MAIN_ERROR_RELEASE_4,ATTR_VISIBLE, 1);
6167
6168     RS232Error = ReturnRS232Err ();
6169     if (RS232Error)
6170         DisplayRS232Error ();
6171     send_data[0] = '\0';
6172
6173     if (Is_P3) //off pump #3
6174     {
6175         FlushOutQ (P3_comport);
6176         FlushInQ (P3_comport);
6177
6178         send_data[0] = '\0';
6179         Fmt (send_data, "%s<OFF\r");
6180
6181         stringsize = StringLength (send_data);
6182         bytes_sent = ComWrt (P3_comport, send_data, stringsize);
6183         Delay(0.05); // 0.05
6184
6185         read_cnt = GetInQLen (P3_comport);
6186
6187         read_data[0] = '\0';
6188         read_term = 13;
6189         bytes_read = ComRdTerm (P3_comport, read_data, read_cnt, read_term);
6190
6191         CopyString (tbox_read_data, 0, read_data, 0, bytes_read);
6192         SetCtrlVal (panel_handle, MAIN_STATUS_P_3, tbox_read_data);
6193
6194         pumprun_3 = 32;
6195
6196         //ERROR EVENT LIST
6197         SetCtrlAttribute(panel_handle,MAIN_STOP_P_3,ATTR_VISIBLE, 1);
6198         SetCtrlAttribute(panel_handle,MAIN_ERROR_RELEASE_5,ATTR_VISIBLE, 1);
6199
6200         RS232Error = ReturnRS232Err ();
6201         if (RS232Error)
6202             DisplayRS232Error ();
6203         send_data[0] = '\0';
6204     }
6205     return;
6206 }
6207
6208 int CVICALLBACK ZeroErrorCallBack (int panel, int control, int event,
6209         void *callbackData, int eventData1, int eventData2)
6210 {
6211     double data;
6212
6213     switch (event)
6214     {
6215         case EVENT_COMMIT:
6216
6217             switch(control)
6218             {
6219                 case MAIN_ZERO_TP2: //upstream
6220
6221                     GetCtrlVal(panel_handle,MAIN_TP2, &data);
6222
6223                     ZEROTP2[0]=ZEROTP2[0] + data;
6224                     break;
6225                 case MAIN_ZERO_DP1:
6226
6227                     GetCtrlVal(panel_handle,MAIN_DP1, &data);
6228                     ZERODP1[0]=ZERODP1[0] + data;
6229                     break;
6230                 case MAIN_ZERO_TP1: //downstream
6231
6232                     GetCtrlVal(panel_handle,MAIN_TP1, &data);
6233                     ZEROTP1[0]=ZEROTP1[0] + data;
6234                     break;
6235
6236
6237                 case PRESSURE_ZERO_CP1_1: // CP1_1
6238                     GetCtrlVal(pressure_handle,PRESSURE_CP1_1, &data);
6239                     ZEROCP11[0]=ZEROCP11[0] + data;
6240                     break;
6241                 case PRESSURE_ZERO_CP1_2: // CP1_2
6242                     GetCtrlVal(pressure_handle,PRESSURE_CP1_2, &data);
6243                     ZEROCP12[0]=ZEROCP12[0] + data;
6244                     break;
6245                 case PRESSURE_ZERO_CP1_3: // CP1_3
6246                     GetCtrlVal(pressure_handle,PRESSURE_CP1_3, &data);
6247                     ZEROCP13[0]=ZEROCP13[0] + data;
6248                     break;
6249                 case PRESSURE_ZERO_CP1_4: // CP1_4
6250                     GetCtrlVal(pressure_handle,PRESSURE_CP1_4, &data);
6251                     ZEROCP14[0]=ZEROCP14[0] + data;
6252                     break;
6253                 case PRESSURE_ZERO_CP1_5: // CP1_5
6254                     GetCtrlVal(pressure_handle,PRESSURE_CP1_5, &data);
6255                     ZEROCP15[0]=ZEROCP15[0] + data;
6256                     break;

```

```

6257
6258     case PRESSURE_ZERO_CP2_1: // CP2_1
6259         GetCtrlVal(pressure_handle,PRESSURE_CP2_1, &data);
6260         ZEROCP21[0]=ZEROCP21[0] + data;
6261     break;
6262     case PRESSURE_ZERO_CP2_2: // CP2_2
6263         GetCtrlVal(pressure_handle,PRESSURE_CP2_2, &data);
6264         ZEROCP22[0]=ZEROCP22[0] + data;
6265     break;
6266     case PRESSURE_ZERO_CP2_3: // CP2_3
6267         GetCtrlVal(pressure_handle,PRESSURE_CP2_3, &data);
6268         ZEROCP23[0]=ZEROCP23[0] + data;
6269     break;
6270     case PRESSURE_ZERO_CP2_4: // CP2_4
6271         GetCtrlVal(pressure_handle,PRESSURE_CP2_4, &data);
6272         ZEROCP24[0]=ZEROCP24[0] + data;
6273     break;
6274     case PRESSURE_ZERO_CP2_5: // CP2_5
6275         GetCtrlVal(pressure_handle,PRESSURE_CP2_5, &data);
6276         ZEROCP25[0]=ZEROCP25[0] + data;
6277     break;
6278
6279     case PRESSURE_ZERO_CP3_1: // CP3_1
6280         GetCtrlVal(pressure_handle,PRESSURE_CP3_1, &data);
6281         ZEROCP31[0]=ZEROCP31[0] + data;
6282     break;
6283     case PRESSURE_ZERO_CP3_2: // CP3_2
6284         GetCtrlVal(pressure_handle,PRESSURE_CP3_2, &data);
6285         ZEROCP32[0]=ZEROCP32[0] + data;
6286     break;
6287     case PRESSURE_ZERO_CP3_3: // CP3_3
6288         GetCtrlVal(pressure_handle,PRESSURE_CP3_3, &data);
6289         ZEROCP33[0]=ZEROCP33[0] + data;
6290     break;
6291     case PRESSURE_ZERO_CP3_4: // CP3_4
6292         GetCtrlVal(pressure_handle,PRESSURE_CP3_4, &data);
6293         ZEROCP34[0]=ZEROCP34[0] + data;
6294     break;
6295     case PRESSURE_ZERO_CP3_5: // CP3_5
6296         GetCtrlVal(pressure_handle,PRESSURE_CP3_5, &data);
6297         ZEROCP35[0]=ZEROCP35[0] + data;
6298     break;
6299 }
6300 break;
6301
6302     case EVENT_RIGHT_CLICK:
6303         break;
6304 }
6305 return 0;
6306 }

6307
6308 int CVICALLBACK ErrReleaseCallBack (int panel, int control, int event,
6309     void *callbackData, int eventData1, int eventData2)
6310 {
6311     switch (event)
6312     {
6313         case EVENT_COMMIT:
6314             switch(control)
6315             {
6316                 case MAIN_ERROR_RELEASE_1:
6317                     SetCtrlAttribute(panel_handle,MAIN_DIFF_OVER_150,ATTR_VISIBLE, 0);
6318                     SetCtrlVal(panel_handle,MAIN_ERROR_RELEASE_3,0);
6319                     OVERPRES = 1;
6320                     break;
6321                 case MAIN_ERROR_RELEASE_2:
6322                     SetCtrlAttribute(panel_handle,MAIN_TP2_OVER_1450,ATTR_VISIBLE, 0);
6323                     SetCtrlAttribute(panel_handle,MAIN_ERROR_RELEASE_2,ATTR_VISIBLE, 0);
6324                     break;
6325                 case MAIN_ERROR_RELEASE_3:
6326                     SetCtrlAttribute(panel_handle,MAIN_STOP_P_1,ATTR_VISIBLE, 0);
6327                     SetCtrlAttribute(panel_handle,MAIN_ERROR_RELEASE_3,ATTR_VISIBLE, 0);
6328                     break;
6329                 case MAIN_ERROR_RELEASE_4:
6330                     SetCtrlAttribute(panel_handle,MAIN_STOP_P_2,ATTR_VISIBLE, 0);
6331                     SetCtrlAttribute(panel_handle,MAIN_ERROR_RELEASE_4,ATTR_VISIBLE, 0);
6332                     break;
6333                 case MAIN_ERROR_RELEASE_5:
6334                     SetCtrlAttribute(panel_handle,MAIN_STOP_P_3,ATTR_VISIBLE, 0);
6335                     SetCtrlAttribute(panel_handle,MAIN_ERROR_RELEASE_5,ATTR_VISIBLE, 0);
6336                     break;
6337                 case MAIN_ERROR_RELEASE_6:
6338                     SetCtrlAttribute(panel_handle,MAIN_ERR_BPR_ALARM,ATTR_VISIBLE, 0);
6339                     SetCtrlAttribute(panel_handle,MAIN_ERROR_RELEASE_6,ATTR_VISIBLE, 0);
6340                     break;
6341                 case MAIN_ERROR_RELEASE_7:
6342                     SetCtrlAttribute(panel_handle,MAIN_TP1_OVER_1450,ATTR_VISIBLE, 0);
6343                     SetCtrlAttribute(panel_handle,MAIN_ERROR_RELEASE_7,ATTR_VISIBLE, 0);
6344                     break;
6345             }
6346         break;
6347     }
6348 return 0;
6349 }

6350
6351 int CVICALLBACK UnitCallBack (int panel, int control, int event,
6352     void *callbackData, int eventData1, int eventData2)
6353 {

```

```

6354 int visunit, permunit;
6355
6356     switch (event)
6357     {
6358         case EVENT_COMMIT:
6359             vispermunit();
6360             SaveConfig(0);
6361             break;
6362     }
6363     return 0;
6364 }
6365
6366 void vispermunit(void)
6367 {
6368     int visunit, permunit;
6369     GetCtrlVal(panel_handle,MAIN_VIS_UNIT, &visunit);
6370     GetCtrlVal(panel_handle,MAIN_PERM_UNIT, &permunit);
6371
6372         if (visunit == 0) viscoef= 0.001 ;
6373         else if (visunit == 1) viscoef= 1;
6374         else viscoef= 1;
6375
6376         if (permunit == 0) permcoef= 1;
6377         else permcoef= 1000;
6378     return;
6379 }
6380
6381 int CVICALLBACK CleanoutCallBack (int panel, int control, int event,
6382         void *callbackData, int eventData1, int eventData2)
6383 {
6384     double temp;
6385
6386     switch (event)
6387     {
6388         case EVENT_COMMIT:
6389             switch(control)
6390             {
6391                 case MAIN_SET_OUT:
6392
6393                     GetCtrlVal (panel_handle, MAIN_UPLIM_OUT, &temp);
6394                     SetCtrlAttribute (panel_handle, MAIN_OUTLETTANK,ATTR_MAX_VALUE, temp);
6395
6396                 break;
6397                 case MAIN_SET_AND_CLEAN_OUT:
6398
6399                     GetCtrlVal (panel_handle, MAIN_UPLIM_OUT, &temp);
6400                     SetCtrlAttribute (panel_handle, MAIN_OUTLETTANK,ATTR_MAX_VALUE, temp);
6401
6402                     OUTLET[1]=0.0;
6403                     OUTLET[0]=0.0;
6404                     SetCtrlVal (panel_handle, MAIN_OUTLETTANK, OUTLET[0]); //set new value to TANK
6405
6406                 break;
6407                 case MAIN_CLEAN_OUT:
6408
6409                     OUTLET[1]=0.0;
6410                     OUTLET[0]=0.0;
6411                     SetCtrlVal (panel_handle, MAIN_OUTLETTANK, OUTLET[0]); //set new value to TANK
6412
6413
6414             }
6415             break;
6416     }
6417     return 0;
6418 }
6419
6420 int CVICALLBACK OilWaterCallBack (int panel, int control, int event,
6421         void *callbackData, int eventData1, int eventData2)
6422 {
6423     double temp;
6424
6425     switch (event)
6426     {
6427         case EVENT_COMMIT:
6428             SetCtrlVal (panel_handle, MAIN_LED_NEWSSET_PLOT_CHECK, 1);
6429             Delay (0.1);
6430             GetCtrlVal (panel_handle, MAIN_OILWATER_SET, &temp);
6431
6432             SETPOINTOUT[0]=temp;
6433
6434             SetCtrlVal (panel_handle, MAIN_LED_NEWSSET_PLOT_CHECK, 0);
6435
6436             break;
6437     }
6438     return 0;
6439 }
6440
6441 int CVICALLBACK WaterinjCallBack (int panel, int control, int event,
6442         void *callbackData, int eventData1, int eventData2)
6443 {
6444     switch (event)
6445     {
6446         case EVENT_COMMIT:
6447
6448             GetCtrlVal (sat_handle, SAT_WATER_INJ, &PV[0]);
6449             SetCtrlVal (panel_handle, MAIN_STG_2, 1);
6450

```

```

6451     GetCtrlVal(panel_handle, MAIN_STG_2, &STG_2);
6452     Update_Graphics();
6453
6454
6455     SetCtrlVal(panel_handle,MAIN_WATER_INJ,PV[0]); // 
6456     SetCtrlVal(panel_handle,MAIN_WATER_CORE,PV[0]); //
6457
6458
6459     GeoMath();
6460
6461     Delay(0.1);
6462
6463     DiscardPanel (sat_handle);
6464
6465     break;
6466 }
6467 return 0;
6468 }
6469
6470
6471 void SWITCH_FRACTION (int channel1, int channel2, int channel3, int channel4) //Function to switch solenoid valves
6472 {
6473     int error=0;
6474     TaskHandle taskHandleAV2=0;
6475     char chanAV2[256];
6476     uint8 dataAV2[4];
6477     char errBuffAV2[2048]=('0');

6478
6479     GetCtrlVal(config_handle,CONFIG_SOLCHANNEL_2,chanAV2);

6480
6481
6482
6483     dataAV2[0] = channel1; // green run [start]
6484     dataAV2[1] = channel2; // red run [test tube]
6485     dataAV2[2] = channel3; // white run [stop]
6486     dataAV2[3] = channel4; // restart run [restart]
6487
6488     if (dataAV2[0] == 1) SetCtrlVal (panel_handle, MAIN_LED_FC, 1); //Show up status of Fraction collector
6489
6490     //*****
6491     // DAQmx Configure Code
6492     //*****
6493     SetWaitCursor(1);
6494     DAQmxErrChk (DAQmxCreateTask("",&taskHandleAV2));
6495     DAQmxErrChk (DAQmxCreateDOChan(taskHandleAV2,chanAV2,"",DAQmx_Val_ChanForAllLines));
6496
6497     //*****
6498     // DAQmx Start Code
6499     //*****
6500     DAQmxErrChk (DAQmxStartTask(taskHandleAV2));
6501
6502     //*****
6503     // DAQmx Write Code
6504     //*****
6505     DAQmxErrChk (DAQmxWriteDigitalLines(taskHandleAV2,1,1,10.0,DAQmx_Val_GroupByChannel,dataAV2,NULL,NULL));
6506
6507
6508 Error:
6509     SetWaitCursor(0);
6510     if( DAQmxFailed(error) )
6511         DAQmxGetExtendedErrorInfo(errBuffAV2,2048);
6512     if( taskHandleAV2!=0 ) {
6513         //*****
6514         // DAQmx Stop Code
6515         //*****
6516         DAQmxStopTask(taskHandleAV2);
6517         DAQmxClearTask(taskHandleAV2);
6518     }
6519     if( DAQmxFailed(error) )
6520         MessagePopup("DAQmx Error",errBuffAV2);
6521
6522 return;
6523 }
6524
6525 int CVICALLBACK ConnectCallBack (int panel, int control, int event,
6526     void *callbackData, int eventData1, int eventData2)
6527 {
6528     int temp;
6529     switch (event)
6530     {
6531         case EVENT_COMMIT:
6532             GetCtrlVal(config_handle, CONFIG_CONNECT, &temp);
6533             if (temp == TRUE) DSN_Init_Camera();
6534             else DeInit_Camera();
6535             break;
6536     }
6537     return 0;
6538 }
6539
6540 // DSN_Init_Image : Init the Image position
6541
6542 void DSN_Init_Image(int panelHandle)
6543 {
6544     Point windowPos;
6545     int firstWindowWidth;
6546     int mainPanelTop;
6547     int mainPanelHeight;

```

```

6548     int mainPanelWidth;
6549     int mainPanelLeft;
6550
6551     int Mon_height;
6552     int Mon_width;
6553     int MONITOR_ID;
6554     int im_width;
6555     int im_height;
6556     int imWin_width, imWin_height;
6557
6558     GetMonitorAttribute (1, ATTR_NEXT_MONITOR, &MONITOR_ID);
6559
6560 // Get the location of the top of the panel
6561 GetPanelAttribute( panelHandle, ATTR_TOP, &mainPanelTop );
6562 // Get the location of the left side of the panel
6563 GetPanelAttribute( panelHandle, ATTR_LEFT, &mainPanelLeft );
6564 // Get the height of the panel
6565 GetPanelAttribute( panelHandle, ATTR_HEIGHT, &mainPanelHeight );
6566 // Get the width of the panel
6567 GetPanelAttribute (panelHandle, ATTR_WIDTH, &mainPanelWidth);
6568 // Set up windowPos
6569 windowPos.x = mainPanelLeft + mainPanelWidth;
6570 windowPos.y = mainPanelTop - 25;
6571
6572     imaqMoveWindow( SOURCE_WINDOW, windowPos );
6573
6574 // Reduces size of the imaqWindow
6575 GetCtrlVal(panelHandle, PANEL_im_height, &im_height);
6576 GetCtrlVal(panelHandle, PANEL_im_width, &im_width);
6577
6578     imaqSetWindowSize      (SOURCE_WINDOW, im_height , im_width);
6579     imaqSetWindowZoomToFit (SOURCE_WINDOW, TRUE);
6580
6581     GetMonitorAttribute (1, ATTR_HEIGHT, &Mon_height);
6582     GetMonitorAttribute (1, ATTR_WIDTH, &Mon_width);
6583     SetCtrlVal(panelHandle, PANEL_Mon_height, Mon_height);
6584     SetCtrlVal(panelHandle, PANEL_Mon_width, Mon_width);
6585
6586 // Set the size of the image window
6587     imWin_width = Mon_width - mainPanelWidth - mainPanelLeft;
6588     imWin_height = Mon_height - 25;
6589
6590 return;
6591 }
6592 // Convert the error to a string and present to user
6593 void DisplayError(IMAQdxError error)
6594 {
6595     char errorString[256];
6596     IMAQdxGetErrorString(error, errorString, sizeof(errorString));
6597     MessagePopup("Error", errorString);
6598 }
6599
6600 // DSN_Init_Camera: Init the Camera: Get information
6601 void DSN_Init_Camera(void)
6602 {
6603     unsigned int attributeCount;
6604     int i=0;
6605
6606
6607     IMAQdxError error2 = IMAQdxErrorSuccess;
6608
6609 // CAMERA INITIALIZATION
6610     // Get the interface name
6611     GetCtrlVal (config_handle, CONFIG_CAMNAME, camName);
6612
6613
6614     SetCtrlAttribute(config_handle,CONFIG_OpenSet,ATTR_VISIBLE,1 );
6615
6616 // Dispose any images that were previously created
6617 if(images)
6618 {
6619     for(i=0; i<imageArraySize; i++)
6620         imaqDispose (images[i]);
6621         free(images);
6622         images = NULL;
6623 }
6624 // Open a session on the selected camera
6625 error2 = IMAQdxOpenCamera (camName, IMAQdxCameraControlModeController, &session);
6626 // Return if we did not open the camera
6627 if(error2)
6628 {
6629     DisplayError(error2);
6630     //return 0;
6631 }
6632
6633 // Set up the CAMERA ATTRIBUTES DIALOG
6634
6635 // Enumerate the attributes supported by the camera
6636
6637     ClearListCtrl (panelHandle, PANEL_CAM_ATTR);
6638     error2 = IMAQdxEnumerateAttributes (session, NULL, &attributeCount, NULL);
6639     if (error2)
6640     {
6641         // break;
6642     }
6643     cameraAttributes = (IMAQdxAttributeInformation *)malloc(attributeCount * sizeof(IMAQdxAttributeInformation));
6644     error2 = IMAQdxEnumerateAttributes (session, cameraAttributes, &attributeCount, NULL);

```

```

6645         if (error2)
6646         {
6647             // break;
6648         }
6649     //Populate the available attributes into the table control
6650     for (i=0; i < attributeCount; i++)
6651     {
6652         InsertListItem (panelHandle, PANEL_CAM_ATTR, -1, cameraAttributes[i].Name, i);
6653     }
6654     // Display the details for the current attribute
6655     UpdateAttributeTab();
6656
6657 // Turn the GRAB on
6658
6659     SetCtrlAttribute (panel_handle, MAIN_SNAP, ATTR_DIMMED, 0);
6660 //     SetCtrlAttribute (panel_handle, MAIN_SNAP_SAVE, ATTR_DIMMED, 0);
6661     SetCtrlAttribute (panel_handle, MAIN_GRAB_2, ATTR_DIMMED, 0);
6662 }
6663
6664 void DeInit_Camera(void)
6665 {
6666     unsigned int attributeCount;
6667     int i=0;
6668     IMAQdxError error2 = IMAQdxErrorSuccess;
6669
6670 // Camera De-initialization
6671
6672     if(images)
6673     {
6674         for(i=0; i<imageArraySize; i++)
6675             imagDispose (images[i]);
6676             free(images);
6677             images = NULL;
6678     }
6679
6680
6681     SetCtrlAttribute (panel_handle, MAIN_SNAP, ATTR_DIMMED, 1);
6682 //     SetCtrlAttribute (panel_handle, MAIN_SNAP_SAVE, ATTR_DIMMED, 1);
6683     SetCtrlAttribute (panel_handle, MAIN_GRAB_2, ATTR_DIMMED, 1);
6684
6685     error2 = IMAQdxCloseCamera (session);
6686
6687 // Return if we did not close the camera
6688     if(error2)
6689     {
6690         DisplayError(error2);
6691     }
6692
6693
6694 // Diable up the CAMERA ATTRIBUTES DIALOG
6695 SetCtrlAttribute(config_handle,CONFIG_OpenSet,ATTR_VISIBLE, 0);
6696
6697
6698 int CVICALLBACK OpenSetCallBack (int panel, int control, int event,
6699                                 void *callbackData, int eventData1, int eventData2)
6700 {
6701     switch (event)
6702     {
6703         case EVENT_COMMIT:
6704             DisplayPanel(panelHandle);
6705             break;
6706         }
6707         return 0;
6708     }
6709
6710
6711 int CVICALLBACK CloseSetCallBack (int panel, int control, int event,
6712                                   void *callbackData, int eventData1, int eventData2)
6713 {
6714     switch (event)
6715     {
6716         case EVENT_COMMIT:
6717             HidePanel(panelHandle);
6718             break;
6719         }
6720         return 0;
6721     }
6722
6723 }
6724
6725 int CVICALLBACK Start_Grab (int panel, int control, int event,
6726                               void *callbackData, int eventData1, int eventData2)
6727 {
6728     int test,i;
6729     double time;
6730
6731     switch (event)
6732     {
6733         case EVENT_COMMIT:
6734
6735             IMAQdxUnconfigureAcquisition(session);
6736             IMAQdxConfigureGrab (session);
6737
6738             GetCtrlVal (panel_handle, MAIN_GRAB_2, &test);
6739             if(test)
6740             {
6741                 // Create an image

```

```

6742     if(image_g)
6743         imaqDispose(image_g);
6744     image_g = imaqCreateImage (IMAQ_IMAGE_U8, 0);
6745     // Configure the acquisition
6746     IMAQdxConfigureAcquisition (session, TRUE, 3);
6747     // Start the acquisition
6748     IMAQdxStartAcquisition (session);
6749     // RUN the timer to do the GRAB and DISPLAY
6750     SetCtrlAttribute (panel_handle, MAIN_TIMER, ATTR_ENABLED, TRUE);
6751 }
6752 else
6753 {
6754     // Stop the Imaq Loop
6755     SetCtrlAttribute (panel_handle, MAIN_TIMER, ATTR_ENABLED, FALSE);
6756     // Stop the acquisition
6757     IMAQdxStopAcquisition (session);
6758     // Unconfigure the acquisition
6759     IMAQdxUnconfigureAcquisition (session);
6760
6761     if(image_g)
6762     {
6763         imaqDispose(image_g);
6764         image_g = NULL;
6765     }
6766 }
6767 break;
6768 }
6769 return 0;
6770 }
6771
6772 int CVICALLBACK Imaq_loop (int panel, int control, int event,
6773     void *callbackData, int eventData1, int eventData2)
6774 {
6775
6776     const double frameRateInterval = 0.5;
6777     static double lastTick = 0;
6778     double newTick;
6779     static unsigned int lastBufferNumber = - 1;
6780     unsigned int bufferNumber;
6781     unsigned int temp;
6782     IMAQdxError error2 = IMAQdxErrorSuccess;
6783
6784     switch (event)
6785     {
6786         case EVENT_TIMER_TICK:
6787             newTick = Timer();
6788
6789             // Get the next frame
6790             error2 = IMAQdxGrab (session, image_g, TRUE, &bufferNumber);
6791             if (error2)
6792             {
6793                 break;
6794             }
6795
6796             // Display using NI Vision
6797             imaqDisplayImage (image_g, 0, TRUE);
6798
6799             // Set settings to the NI Vision window
6800             if (Just_Grabbed == TRUE)
6801             {
6802                 DSN_Init_Image(panelHandle);
6803                 Just_Grabbed = 0;
6804             }
6805
6806             // Calculate the number of frame per seconds
6807             if ((newTick - lastTick) >= frameRateInterval)
6808             {
6809                 double frameRate = (double)(bufferNumber - lastBufferNumber) / (newTick - lastTick);
6810                 lastTick = newTick;
6811                 lastBufferNumber = bufferNumber;
6812             }
6813             break;
6814     }
6815
6816     if (error2) { DisplayError(error2); }
6817
6818 return 0;
6819 }
6820
6821
6822 // UpdateAttributeTab : Load and display the ATTRIBUTES
6823 void UpdateAttributeTab(void) {
6824     char          Units[IMAQDX_MAX_API_STRING_LENGTH];
6825     char          Tooltip[IMAQDX_MAX_API_STRING_LENGTH];
6826     unsigned int   U32minimum = 0;
6827     unsigned int   U32maximum = 1;
6828     unsigned int   U32increment = 1;
6829     double        DBLminimum = 0;
6830     double        DBLmaximum = 1;
6831     double        DBLincrement = 0;
6832     BOOL          Readable = 0;
6833     BOOL          Writable = 0;
6834     int           i = 0;
6835     unsigned int   U32current = 0;
6836     double        DBLcurrent = 0;
6837     char          STRcurrent[IMAQDX_MAX_API_STRING_LENGTH];
6838     unsigned int   EnumCurrent = 0;

```

```

6839     BOOL          BOOLcurrent = FALSE;
6840
6841     SetCtrlVal(panelHandle, PANEL_LED_EXP_7, 1,
6842
6843     // Get the selected attribute, and make the tab control visible
6844     GetCtrlVal (panelHandle, PANEL_CAM_ATTR, &selectedAttrIndex);
6845     SetCtrlVal (panelHandle, PANEL_Cam_List_Num, selectedAttrIndex);
6846     SetCtrlAttribute (panelHandle, PANEL_CAM_TAB, ATTR_VISIBLE, TRUE);
6847
6848     // Get the units for the attribute and the tooltip
6849     IMAQdxGetAttributeUnits (session, cameraAttributes[selectedAttrIndex].Name, Units, IMAQDX_MAX_API_STRING_LENGTH);
6850     SetCtrlVal (panelHandle, PANEL_UNITS, Units);
6851     IMAQdxGetAttributeTooltip (session, cameraAttributes[selectedAttrIndex].Name, Tooltip, IMAQDX_MAX_API_STRING_LENGTH);
6852     ResetTextBox (panelHandle, PANEL_TOOLTIPS, Tooltip);
6853     SetCtrlAttribute (panelHandle, PANEL_TOOLTIPS, ATTR_WRAP_MODE, VAL_WORD_WRAP);
6854
6855     // Determine the data type for the attribute, display associated tab
6856     // Determine if the attribute is writable, readable, or neither, and dim/hide control accordingly
6857     // For U32, get minimum, maximum, increment, and current value from driver, and configure the control
6858     if (cameraAttributes[selectedAttrIndex].Type == IMAQdxAttributeTypeU32)
6859     {
6860         U32current = 0;
6861         SetActiveTabPage (panelHandle, PANEL_CAM_TAB, 0);
6862         GetPanelHandleFromTabPage (panelHandle, PANEL_CAM_TAB, 0, &TabPanelHandle);
6863         IMAQdxGetAttributeMinimum (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeU32, &U32minimum);
6864         IMAQdxGetAttributeMaximum (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeU32, &U32maximum);
6865         IMAQdxGetAttributeIncrement (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeU32, &U32increment);
6866         IMAQdxIsAttributeReadable (session, cameraAttributes[selectedAttrIndex].Name, &Readable);
6867         IMAQdxIsAttributeWritable (session, cameraAttributes[selectedAttrIndex].Name, &Writable);
6868         if (Readable == TRUE)
6869             IMAQdxGetAttribute (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeU32, &U32current);
6870         SetCtrlAttribute (TabPanelHandle, U32TAB_U32CTL, ATTR_MIN_VALUE, U32minimum);
6871         SetCtrlAttribute (TabPanelHandle, U32TAB_U32CTL, ATTR_MAX_VALUE, U32maximum);
6872         SetCtrlAttribute (TabPanelHandle, U32TAB_U32CTL, ATTR_INCR_VALUE, U32increment);
6873         SetCtrlVal (TabPanelHandle, U32TAB_U32CTL, U32current);
6874         if (Writable == TRUE)
6875             SetCtrlAttribute (TabPanelHandle, U32TAB_U32CTL, ATTR_DIMMED, FALSE);
6876             SetCtrlAttribute (TabPanelHandle, U32TAB_U32CTL, ATTR_VISIBLE, TRUE);
6877     }
6878     else if (Readable == TRUE)
6879         SetCtrlAttribute (TabPanelHandle, U32TAB_U32CTL, ATTR_DIMMED, TRUE);
6880         SetCtrlAttribute (TabPanelHandle, U32TAB_U32CTL, ATTR_VISIBLE, TRUE);
6881     }
6882     else
6883         SetCtrlAttribute (TabPanelHandle, U32TAB_U32CTL, ATTR_VISIBLE, FALSE);
6884 }
6885
6886 // For I64, get minimum, maximum, increment, and current value from driver, and configure the control
6887 // Note: Since CVI does not support 64-bit integer types, we will use doubles for it.
6888 else if (cameraAttributes[selectedAttrIndex].Type == IMAQdxAttributeTypeI64)
6889 {
6890     SetActiveTabPage (panelHandle, PANEL_CAM_TAB, 1);
6891     GetPanelHandleFromTabPage (panelHandle, PANEL_CAM_TAB, 1, &TabPanelHandle);
6892     IMAQdxGetAttributeMinimum (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeF64, &DBLminimum);
6893     IMAQdxGetAttributeMaximum (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeF64, &DBLmaximum);
6894     IMAQdxGetAttributeIncrement (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeF64, &DBLincrement);
6895     IMAQdxIsAttributeReadable (session, cameraAttributes[selectedAttrIndex].Name, &Readable);
6896     IMAQdxIsAttributeWritable (session, cameraAttributes[selectedAttrIndex].Name, &Writable);
6897     if (Readable == TRUE)
6898         IMAQdxGetAttribute (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeF64, &DBLcurrent);
6899     SetCtrlAttribute (TabPanelHandle, I64TAB_I64CTL, ATTR_MIN_VALUE, DBLminimum);
6900     SetCtrlAttribute (TabPanelHandle, I64TAB_I64CTL, ATTR_MAX_VALUE, DBLmaximum);
6901     SetCtrlAttribute (TabPanelHandle, I64TAB_I64CTL, ATTR_INCR_VALUE, DBLincrement);
6902     SetCtrlVal (TabPanelHandle, I64TAB_I64CTL, DBLcurrent);
6903     if (Writable == TRUE)
6904         SetCtrlAttribute (TabPanelHandle, I64TAB_I64CTL, ATTR_DIMMED, FALSE);
6905         SetCtrlAttribute (TabPanelHandle, I64TAB_I64CTL, ATTR_VISIBLE, TRUE);
6906     }
6907     else if (Readable == TRUE)
6908         SetCtrlAttribute (TabPanelHandle, I64TAB_I64CTL, ATTR_DIMMED, TRUE);
6909         SetCtrlAttribute (TabPanelHandle, I64TAB_I64CTL, ATTR_VISIBLE, TRUE);
6910     }
6911     else
6912         SetCtrlAttribute (TabPanelHandle, I64TAB_I64CTL, ATTR_VISIBLE, FALSE);
6913 }
6914
6915 // For DBL (F64), get minimum, maximum and current value from driver, and configure the control
6916 else if (cameraAttributes[selectedAttrIndex].Type == IMAQdxAttributeTypeF64)
6917 {
6918     SetActiveTabPage (panelHandle, PANEL_CAM_TAB, 2);
6919     GetPanelHandleFromTabPage (panelHandle, PANEL_CAM_TAB, 2, &TabPanelHandle);
6920     IMAQdxGetAttributeMinimum (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeF64, &DBLminimum);
6921     IMAQdxGetAttributeMaximum (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeF64, &DBLmaximum);
6922     IMAQdxIsAttributeReadable (session, cameraAttributes[selectedAttrIndex].Name, &Readable);
6923     IMAQdxIsAttributeWritable (session, cameraAttributes[selectedAttrIndex].Name, &Writable);
6924     if (Readable == TRUE)
6925         IMAQdxGetAttribute (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeF64, &DBLcurrent);
6926     SetCtrlAttribute (TabPanelHandle, DBLTAB_DBLCRTL, ATTR_MIN_VALUE, DBLminimum);
6927     SetCtrlAttribute (TabPanelHandle, DBLTAB_DBLCRTL, ATTR_MAX_VALUE, DBLmaximum);
6928     SetCtrlVal (TabPanelHandle, DBLTAB_DBLCRTL, DBLcurrent);
6929     if (Writable == TRUE)
6930         SetCtrlAttribute (TabPanelHandle, DBLTAB_DBLCRTL, ATTR_DIMMED, FALSE);
6931         SetCtrlAttribute (TabPanelHandle, DBLTAB_DBLCRTL, ATTR_VISIBLE, TRUE);
6932     }
6933     else if (Readable == TRUE)
6934         SetCtrlAttribute (TabPanelHandle, DBLTAB_DBLCRTL, ATTR_DIMMED, TRUE);
6935         SetCtrlAttribute (TabPanelHandle, DBLTAB_DBLCRTL, ATTR_VISIBLE, TRUE);

```

```

6936     }
6937     else
6938         SetCtrlAttribute (TabPanelHandle, DBLTAB_DBLCRTL, ATTR_VISIBLE, FALSE);
6939     }
6940
6941 // For String, get current value from driver, display current value in control
6942 else if (cameraAttributes[selectedAttrIndex].Type == IMAQdxAttributeTypeString)
6943 {
6944     SetActiveTabPage (panelHandle, PANEL_CAM_TAB, 3);
6945     GetPanelHandleFromTabPage (panelHandle, PANEL_CAM_TAB, 3, &TabPanelHandle);
6946     IMAQdxIsAttributeReadable (session, cameraAttributes[selectedAttrIndex].Name, &Readable);
6947     IMAQdxIsAttributeWritable (session, cameraAttributes[selectedAttrIndex].Name, &Writable);
6948     if (Readable == TRUE)
6949         IMAQdxGetAttribute (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeString, STRcurrent);
6950     SetCtrlVal (TabPanelHandle, STRTAB_STRCTL, STRcurrent);
6951     if (Writable == TRUE) {
6952         SetCtrlAttribute (TabPanelHandle, STRTAB_STRCTL, ATTR_DIMMED, FALSE);
6953         SetCtrlAttribute (TabPanelHandle, STRTAB_STRCTL, ATTR_VISIBLE, TRUE);
6954     }
6955     else if (Readable == TRUE) {
6956         SetCtrlAttribute (TabPanelHandle, STRTAB_STRCTL, ATTR_DIMMED, TRUE);
6957         SetCtrlAttribute (TabPanelHandle, STRTAB_STRCTL, ATTR_VISIBLE, TRUE);
6958     }
6959     else
6960         SetCtrlAttribute (TabPanelHandle, STRTAB_STRCTL, ATTR_VISIBLE, FALSE);
6961 }
6962
6963 // For Enum, get the list of available items and the current value from driver, populate the control
6964 else if (cameraAttributes[selectedAttrIndex].Type == IMAQdxAttributeTypeEnum)
6965 {
6966     unsigned int EnumCount = 0;
6967     IMAQdxEnumItem* EnumList = NULL;
6968
6969     SetActiveTabPage (panelHandle, PANEL_CAM_TAB, 4);
6970     GetPanelHandleFromTabPage (panelHandle, PANEL_CAM_TAB, 4, &TabPanelHandle);
6971     ClearListCtrl (TabPanelHandle, ENUMTAB_ENUMCTL);
6972     IMAQdxEnumerateAttributeValues (session, cameraAttributes[selectedAttrIndex].Name, NULL, &EnumCount);
6973     EnumList = (IMAQdxEnumItem *)malloc(EnumCount * sizeof(IMAQdxEnumItem));
6974     IMAQdxEnumerateAttributeValues (session, cameraAttributes[selectedAttrIndex].Name, EnumList, &EnumCount);
6975     for (i=0; i < EnumCount; i++)
6976     {
6977         InsertListItem (TabPanelHandle, ENUMTAB_ENUMCTL, -1, EnumList[i].Name, EnumList[i].Value);
6978     }
6979     IMAQdxIsAttributeReadable (session, cameraAttributes[selectedAttrIndex].Name, &Readable);
6980     IMAQdxIsAttributeWritable (session, cameraAttributes[selectedAttrIndex].Name, &Writable);
6981     if (Readable == TRUE)
6982         IMAQdxGetAttribute (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeU32, &EnumCurrent);
6983
6984     SetCtrlVal (TabPanelHandle, ENUMTAB_ENUMCTL, EnumCurrent);
6985     if (Writable == TRUE) {
6986         SetCtrlAttribute (TabPanelHandle, ENUMTAB_ENUMCTL, ATTR_DIMMED, FALSE);
6987         SetCtrlAttribute (TabPanelHandle, ENUMTAB_ENUMCTL, ATTR_VISIBLE, TRUE);
6988     }
6989     else if (Readable == TRUE) {
6990         SetCtrlAttribute (TabPanelHandle, ENUMTAB_ENUMCTL, ATTR_DIMMED, TRUE);
6991         SetCtrlAttribute (TabPanelHandle, ENUMTAB_ENUMCTL, ATTR_VISIBLE, TRUE);
6992     }
6993     else
6994         SetCtrlAttribute (TabPanelHandle, ENUMTAB_ENUMCTL, ATTR_VISIBLE, FALSE);
6995     if (EnumList)
6996     {
6997         free (EnumList);
6998         EnumList = NULL;
6999     }
7000 }
7001 // For Boolean, get current value from driver, display current value in control
7002 else if (cameraAttributes[selectedAttrIndex].Type == IMAQdxAttributeTypeBool)
7003 {
7004     SetActiveTabPage (panelHandle, PANEL_CAM_TAB, 5);
7005     GetPanelHandleFromTabPage (panelHandle, PANEL_CAM_TAB, 5, &TabPanelHandle);
7006     IMAQdxIsAttributeReadable (session, cameraAttributes[selectedAttrIndex].Name, &Readable);
7007     IMAQdxIsAttributeWritable (session, cameraAttributes[selectedAttrIndex].Name, &Writable);
7008     if (Readable == TRUE)
7009         IMAQdxGetAttribute (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeBool, &BOOLcurrent);
7010     SetCtrlVal (TabPanelHandle, BOOLTAB_BOOLCTL, BOOLcurrent);
7011     if (Writable == TRUE) {
7012         SetCtrlAttribute (TabPanelHandle, BOOLTAB_BOOLCTL, ATTR_DIMMED, FALSE);
7013         SetCtrlAttribute (TabPanelHandle, BOOLTAB_BOOLCTL, ATTR_VISIBLE, TRUE);
7014     }
7015     else if (Readable == TRUE) {
7016         SetCtrlAttribute (TabPanelHandle, BOOLTAB_BOOLCTL, ATTR_DIMMED, TRUE);
7017         SetCtrlAttribute (TabPanelHandle, BOOLTAB_BOOLCTL, ATTR_VISIBLE, TRUE);
7018     }
7019     else
7020         SetCtrlAttribute (TabPanelHandle, BOOLTAB_BOOLCTL, ATTR_VISIBLE, FALSE);
7021 }
7022
7023 // For Command
7024 else if (cameraAttributes[selectedAttrIndex].Type == IMAQdxAttributeTypeCommand)
7025 {
7026     SetActiveTabPage (panelHandle, PANEL_CAM_TAB, 6);
7027     GetPanelHandleFromTabPage (panelHandle, PANEL_CAM_TAB, 6, &TabPanelHandle);
7028     IMAQdxIsAttributeReadable (session, cameraAttributes[selectedAttrIndex].Name, &Readable);
7029     IMAQdxIsAttributeWritable (session, cameraAttributes[selectedAttrIndex].Name, &Writable);
7030     if (Writable == TRUE) {
7031         SetCtrlAttribute (TabPanelHandle, CMDTAB_CMDCTL, ATTR_DIMMED, FALSE);

```

```

7032     SetCtrlAttribute (TabPanelHandle, CMDTAB_CMDCTL, ATTR_VISIBLE, TRUE);
7033 }
7034 else if (Readable == TRUE) {
7035     SetCtrlAttribute (TabPanelHandle, CMDTAB_CMDCTL, ATTR_DIMMED, TRUE);
7036     SetCtrlAttribute (TabPanelHandle, CMDTAB_CMDCTL, ATTR_VISIBLE, TRUE);
7037 }
7038 else
7039     SetCtrlAttribute (TabPanelHandle, CMDTAB_CMDCTL, ATTR_VISIBLE, FALSE);
7040 }
7041 //SetCtrlVal(panelHandle, PANEL_LED_EXP_8, 1);
7042 }
7043 }
7044
7045
7046 int CVICALLBACK Flush (int panel, int control, int event,
7047 void *callbackData, int eventData1, int eventData2)
7048 {
7049     unsigned int U32current = 0;
7050     unsigned int U32increment = 0;
7051     double DBLcurrent = 0;
7052     double DBLincrement = 0;
7053     char STRcurrent[IMAQDX_MAX_API_STRING_LENGTH];
7054     unsigned int EnumCurrent = 0;
7055     BOOL BOOLcurrent = FALSE;
7056
7057     switch (event)
7058     {
7059         case EVENT_COMMIT:
7060
7061             // Get active attribute from table
7062             GetCtrlVal (panelHandle, PANEL_CAM_ATTR, &selectedAttrIndex);
7063
7064             // Read the new value from the control, and write to the driver
7065             if (cameraAttributes[selectedAttrIndex].Type == IMAQdxAttributeTypeU32)
7066             {
7067                 GetCtrlVal (TabPanelHandle, U32TAB_U32CTL, &U32current);
7068                 // Silently coerce to the increment value and update the control
7069                 GetCtrlAttribute (TabPanelHandle, U32TAB_U32CTL, ATTR_INCR_VALUE, &U32increment);
7070                 U32current = (unsigned int)(U32current / U32increment + 0.5) * U32increment;
7071                 SetCtrlVal (TabPanelHandle, U32TAB_U32CTL, U32current);
7072                 IMAQdxSetAttribute (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeU32, U32current);
7073             }
7074             else if (cameraAttributes[selectedAttrIndex].Type == IMAQdxAttributeTypeI64)
7075             {
7076                 GetCtrlVal (TabPanelHandle, I64TAB_I64CTL, &DBLcurrent);
7077                 // Silently coerce to the increment value and update the control
7078                 GetCtrlAttribute (TabPanelHandle, U32TAB_U32CTL, ATTR_INCR_VALUE, &DBLincrement);
7079                 DBLcurrent = (unsigned int)(DBLcurrent / DBLincrement + 0.5) * DBLincrement;
7080                 SetCtrlVal (TabPanelHandle, I64TAB_I64CTL, DBLcurrent);
7081                 IMAQdxSetAttribute (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeF64, DBLcurrent);
7082             }
7083             else if (cameraAttributes[selectedAttrIndex].Type == IMAQdxAttributeTypeF64)
7084             {
7085                 GetCtrlVal (TabPanelHandle, DBLTAB_DBLCCTL, &DBLcurrent);
7086                 IMAQdxSetAttribute (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeF64, DBLcurrent);
7087             }
7088             else if (cameraAttributes[selectedAttrIndex].Type == IMAQdxAttributeTypeString)
7089             {
7090                 GetCtrlVal (TabPanelHandle, STRTAB_STRCTL, &STRcurrent);
7091                 IMAQdxSetAttribute (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeString, STRcurrent);
7092             }
7093             else if (cameraAttributes[selectedAttrIndex].Type == IMAQdxAttributeTypeEnum)
7094             {
7095                 GetCtrlVal (TabPanelHandle, ENUMTAB_ENUMCTL, &EnumCurrent);
7096                 IMAQdxSetAttribute (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeU32, EnumCurrent);
7097             }
7098             else if (cameraAttributes[selectedAttrIndex].Type == IMAQdxAttributeTypeBool)
7099             {
7100                 GetCtrlVal (TabPanelHandle, BOOLTAB_BOOLCTL, &BOOLcurrent);
7101                 IMAQdxSetAttribute (session, cameraAttributes[selectedAttrIndex].Name, IMAQdxValueTypeBool, BOOLcurrent);
7102             }
7103         break;
7104     }
7105     return 0;
7106 }
7107
7108 int CVICALLBACK Snap (int panel, int control, int event,
7109 void *callbackData, int eventData1, int eventData2)
7110 {
7111     int a;
7112     switch (event)
7113     {
7114         case EVENT_COMMIT: // Creates an image
7115             SetCtrlAttribute (panelHandle, MAIN_Save, ATTR_DIMMED, 1);
7116             if (!image)
7117             {
7118                 SetCtrlAttribute (panelHandle, MAIN_Save, ATTR_DIMMED, 1);
7119                 image = imaqCreateImage (IMAO_IMAGE_U8, 0);
7120
7121             // snap a picture
7122             error2 = IMAQdxSnap (session, image);
7123
7124             if (error2)
7125             {
7126                 DisplayError(error2);
7127                 break;
7128             }
7129     }
7130 }

```

```

7129     }
7130 
7131     // Display using IMAQ Vision
7132     imaqDisplayImage (image, 0, TRUE);
7133 
7134     // Set settings to the NI Vision window
7135     if (Just_Grabbed == TRUE)
7136     {
7137         DSN_Init_Image(panelHandle);
7138         Just_Grabbed = 0;
7139     }
7140 
7141     SetCtrlAttribute (panel_handle, MAIN_Save, ATTR_DIMMED, 0);
7142     break;
7143 }
7144 
7145 if(image)
7146 {
7147     SetCtrlAttribute (panel_handle, MAIN_Save, ATTR_DIMMED, 1);
7148     imaqDispose(image);
7149     image = NULL;
7150     image = imaqCreateImage (IMAO_IMAGE_U8, 0);
7152 
7153     // snap a picture
7154     error2 = IMAQdxSnap (session, image);
7155     if (error2)
7156     {
7157         break;
7158     }
7159 
7160     // Display using IMAQ Vision
7161     imaqDisplayImage (image, 0, TRUE);
7162     SetCtrlAttribute (panel_handle, MAIN_Save, ATTR_DIMMED, 0);
7163     break;
7164 }
7165 }
7166 return 0;
7167 }
7168 
7169 int CVICALLBACK save (int panel, int control, int event,
7170     void *callbackData, int eventData1, int eventData2)
7171 {
7172     char filename[MAX_PATHNAME_LEN];
7173     switch (event)
7174     {
7175         case EVENT_COMMIT:
7176             imaqWriteTIFFFile (image,"DATA\\Stage2_time3.tiff", FALSE, NULL);
7177             break;
7178     }
7179 return 0;
7180 }
7181 
7182 int CVICALLBACK ReSetCallBack (int panel, int control, int event,
7183     void *callbackData, int eventData1, int eventData2)
7184 {
7185     switch (event)
7186     {
7187         case EVENT_COMMIT:
7188             DSN_Init_Image(panelHandle);
7189             break;
7190     }
7191     return 0;
7192 }
7193 
7194 int CVICALLBACK Imaq_loop2 (int panel, int control, int event,
7195     void *callbackData, int eventData1, int eventData2)
7196 {
7197     unsigned int bufferNumber;
7198     char setpoint[100], wholeNum_string[4], decNum_string[4];
7199     char* setpointcode = "DATA\\Stage";
7200     IMAQdxError error2 = IMAQdxErrorSuccess;
7201 
7202     switch (event)
7203     {
7204         case EVENT_TIMER_TICK:
7205             // Get the next frame
7206             error2 = IMAQdxGrab (session, image_g, TRUE, &bufferNumber);
7207             if (error2)
7208             {
7209                 break;
7210             }
7211 
7212             // Display using NI Vision
7213             imaqDisplayImage (image_g, 0, TRUE);
7214 
7215             // wholeNum=wholeNum+1;
7216             // decNum=decNum+1;
7217 
7218             sprintf(wholeNum_string, "%i", wholeNum);
7219             sprintf(decNum_string, "%i", decNum);
7220 
7221             sprintf(setpoint, "DATA\\Stage%dTtube%2.0fWin%2.3fOIn%2.3fWInR%2.3fEInR%2.3f.tiff",
7222                     stage, MANUAL_TEST_TUBE[0], WATERINJPV[1], OILINJPV[1], WATERINJ2PV[1], EMULINJPV[1]);
7223             //Description for acronyms:
7224             //Ttube - test tube number
7225             //WIN - water flooding during initial saturation process and permeability measurements

```

```

7226     //OIn - oil injected during saturation process
7227     //WInR - water flooding during recovery process
7228     //EInR - emulsion flooding during recovery process
7229
7230     imaqWriteTIFFFile (image_g, setpoint, FALSE, NULL);
7231
7232     // Set settings to the NI Vision window
7233     if (Just_Grabbed == TRUE)
7234     {
7235         DSN_Init_Image(panelHandle);
7236         Just_Grabbed = 0;
7237     }
7238     break;
7239 }
7240 }
7241 if (error2) { DisplayError(error2); }
7242 return 0;
7243 }
7244
7245 int CVICALLBACK SnapSave (int panel, int control, int event,
7246     void *callbackData, int eventData1, int eventData2)
7247 {
7248     int test,i;
7249     double time;
7250     switch (event)
7251     {
7252         case EVENT_COMMIT:
7253             IMAQdxUnconfigureAcquisition(session);
7254             IMAQdxConfigureGrab (session);
7255             GetCtrlVal (panel_handle, MAIN_SNAP_SAVE, &test);
7256
7257             if(test)
7258             {
7259                 // Create an image
7260                 if(image_g)
7261                     imaqDispose(image_g);
7262                 image_g = imaqCreateImage (IMAQ_IMAGE_U8, 0);
7263                 // Configure the acquisition
7264                 IMAQdxConfigureAcquisition (session, TRUE, 3);
7265                 // Start the acquisition
7266                 IMAQdxStartAcquisition (session);
7267                 // RUN the timer to do the GRAB and DISPLAY
7268                 // SetCtrlAttribute (panel_handle, MAIN_TIMER_2, ATTR_ENABLED, TRUE);
7269                 Is_Cam= 1;
7270                 SetCtrlVal(panel_handle,MAIN_LOG_CAM, Is_Cam);
7271                 SetCtrlAttribute(panel_handle,MAIN_SNAP, ATTR_DIMMED, 1);
7272                 SetCtrlAttribute(panel_handle,MAIN_Save, ATTR_DIMMED, 1);
7273                 SetCtrlAttribute(panel_handle,MAIN_GRAB_2,ATTR_DIMMED, 1);
7274             }
7275         else
7276         {
7277             // Stop the Imag Loop
7278             // SetCtrlAttribute (panel_handle, MAIN_TIMER_2, ATTR_ENABLED, FALSE);
7279             // Stop the acquisition
7280             IMAQdxStopAcquisition (session);
7281             // Unconfigure the acquisition
7282             IMAQdxUnconfigureAcquisition (session);
7283
7284             Is_Cam= 0;
7285             SetCtrlVal(panel_handle,MAIN_LOG_CAM, Is_Cam);
7286             SetCtrlAttribute(panel_handle,MAIN_SNAP, ATTR_DIMMED, 0);
7287             SetCtrlAttribute(panel_handle,MAIN_Save, ATTR_DIMMED, 0);
7288             SetCtrlAttribute(panel_handle,MAIN_GRAB_2,ATTR_DIMMED, 0);
7289
7290             if(image_g)
7291             {
7292                 imaqDispose(image_g);
7293                 image_g = NULL;
7294             }
7295         }
7296         break;
7297     }
7298     return 0;
7299 }
7300
7301 int CVICALLBACK SetTimer (int panel, int control, int event,
7302     void *callbackData, int eventData1, int eventData2)
7303 {
7304     double temp,temp2;
7305     switch (event)
7306     {
7307         case EVENT_COMMIT:
7308             GetCtrlVal(panel_handle,MAIN_NUMERIC,&temp);
7309             temp2 = temp * 60;
7310             SetCtrlAttribute (panel_handle, MAIN_TIMER_2, ATTR_INTERVAL, temp2);
7311             break;
7312     }
7313     return 0;
7314 }
7315
7316 int CVICALLBACK OnAttributeSelect (int panel, int control, int event,
7317     void *callbackData, int eventData1, int eventData2)
7318 {
7319     switch (event)
7320     {
7321         case EVENT_VAL_CHANGED:
7322             SetCtrlVal(panelHandle, PANEL_LED_EXP_6, 0);

```

```

7323     SetCtrlVal(panelHandle, PANEL_LED_EXP_7, 0);
7324     SetCtrlVal(panelHandle, PANEL_LED_EXP_8, 0);
7325     SetCtrlVal(panelHandle, PANEL_LED_EXP_9, 0);
7326
7327     UpdateAttributeTab();
7328     break;
7329 }
7330 return 0;
7331 }
7332
7333 int CVICALLBACK QUICK_CAM_ATT (int panel, int control, int event,
7334     void *callbackData, int eventData1, int eventData2)
7335 {
7336     int line_num =0;
7337     switch (event)
7338     {
7339         case EVENT_COMMIT:
7340             switch (control)
7341             {
7342                 case PANEL_QUICK_EXP:
7343                     SetCtrlVal (panelHandle, PANEL_CAM_ATTR, 35);
7344                     break;
7345                 case PANEL_QUICK_GAIN:
7346                     SetCtrlVal (panelHandle, PANEL_CAM_ATTR, 41);
7347                     break;
7348                 case PANEL_QUICK_OTHER:
7349                     GetCtrlVal (panelHandle, PANEL_Other_Num, &line_num);
7350                     SetCtrlVal (panelHandle, PANEL_CAM_ATTR, line_num);
7351                     break;
7352                 case PANEL_QUICK_AOI:
7353                     SetCtrlVal (panelHandle, PANEL_CAM_ATTR, 272);
7354                     break;
7355                 case PANEL_QUICK_BPP:
7356                     SetCtrlVal (panelHandle, PANEL_CAM_ATTR, 23);
7357                     break;
7358             }
7359             UpdateAttributeTab();
7360             break;
7361     }
7362 return 0;
7363 }
7364
7365 int CVICALLBACK ClosePreCallBack (int panel, int control, int event,
7366     void *callbackData, int eventData1, int eventData2)
7367 {
7368     switch (event)
7369     {
7370         case EVENT_COMMIT:
7371             HidePanel (pressure_handle);
7372             break;
7373     }
7374 return 0;
7375 }
7376
7377 int CVICALLBACK PressureMapCallBack (int panel, int control, int event,
7378     void *callbackData, int eventData1, int eventData2)
7379 {
7380     switch (event)
7381     {
7382         case EVENT_COMMIT:
7383             DisplayPanel(pressure_handle);
7384             break;
7385     }
7386 return 0;
7387 }
7388
7389 int CVICALLBACK OpenServiceCallBack (int panel, int control, int event,
7390     void *callbackData, int eventData1, int eventData2)
7391 {
7392     switch (event)
7393     {
7394         case EVENT_COMMIT:
7395             DisplayPanel(pumpservice_handle);
7396             break;
7397     }
7398 return 0;
7399 }
7400
7401 int CVICALLBACK ClosePumpSeviceCallback (int panel, int control, int event,
7402     void *callbackData, int eventData1, int eventData2)
7403 {
7404     switch (event)
7405     {
7406         case EVENT_COMMIT:
7407             HidePanel (pumpservice_handle);
7408             break;
7409     }
7410 return 0;
7411 }
7412
7413 int CVICALLBACK CheckMinPCallBack (int panel, int control, int event,
7408     void *callbackData, int eventData1, int eventData2)
7415 {
7416     int i,pump;
7417     double probe_temp;
7418     char temp [NUM];
7419

```

```

7420 switch (event)
7421 {
7422     case EVENT_COMMIT:
7423
7424
7425     ///////////////
7426     panel_name=pumpservice_handle;
7427     GetCtrlVal(pumpservice_handle,PUMP_SER_COMMNUMBER, &pump);
7428     if (pump == 1) CP=P1_comport;
7429     else if (pump == 2) CP=P2_comport;
7430     else if (pump == 3) CP=P3_comport;
7431     else if (pump == 0)
7432     {
7433         MessagePopup ("Warning","Please select the pump.");
7434         break;
7435     }
7436
7437     text_panel_name= PUMP_SER_PRESSURE_MIN_READ;
7438
7439
7440     FlushOutQ (CP);
7441     FlushInQ (CP);
7442
7443     send_data[0] = '\0';
7444     Fmt (send_data, "%s<PMIN10?\r");
7445     stringsize = StringLength (send_data);
7446
7447     bytes_sent = ComWrt (CP, send_data, stringsize);
7448     Delay(0.05); /* 0.05 */
7449
7450     read_cnt = GetInQLen (CP);
7451
7452     read_data[0] = '\0';
7453     read_term = 13;
7454
7455     bytes_read = ComRdTerm (CP, read_data, read_cnt, read_term);
7456     CopyString (tbox_read_data, 0, read_data, 0, bytes_read);
7457
7458     for (i=2; tbox_read_data[i]!='\0';i++)
7459     {
7460         temp[i-2]=tbox_read_data[i];
7461         temp[i-2]='\0'; //close by '\0'
7462
7463         probe_temp = atof(temp);
7464         ProcessSystemEvents ();
7465         SetCtrlVal (panel_name, text_panel_name, probe_temp); /* */
7466
7467         SetCtrlVal (panel_name, text_panel_name, tbox_read_data); //temporary
7468
7469         RS232Error = ReturnRS232Err ();
7470         if (RS232Error)
7471             DisplayRS232Error ();
7472
7473         send_data[0] = '\0';
7474     }
7475     break;
7476 }
7477
7478 int CVICALLBACK CheckMaxPCallBack (int panel, int control, int event,
7479                                     void *callbackData, int eventData1, int eventData2)
7480 {
7481     int i,pump;
7482     double probe_temp;
7483     char temp [NUM];
7484
7485     switch (event)
7486     {
7487         case EVENT_COMMIT:
7488
7489         ///////////////
7490         panel_name=pumpservice_handle;
7491         GetCtrlVal(pumpservice_handle,PUMP_SER_COMMNUMBER, &pump);
7492         if (pump == 1) CP=P1_comport;
7493         else if (pump == 2) CP=P2_comport;
7494         else if (pump == 3) CP=P3_comport;
7495         else if (pump == 0)
7496         {
7497             MessagePopup ("Warning","Please select the pump.");
7498             break;
7499         }
7500
7501         text_panel_name= PUMP_SER_PRESSURE_MIN_READ;
7502
7503
7504         FlushOutQ (CP);
7505         FlushInQ (CP);
7506
7507         send_data[0] = '\0';
7508         Fmt (send_data, "%s<PMAX10?\r");
7509         stringsize = StringLength (send_data);
7510
7511         bytes_sent = ComWrt (CP, send_data, stringsize);
7512         Delay(0.05); /* 0.05 */
7513
7514         read_cnt = GetInQLen (CP);
7515
7516         read_data[0] = '\0';
7517         read_term = 13;

```

```

7517
7518     bytes_read = ComRdTerm (CP, read_data, read_cnt, read_term);
7519     CopyString (tbox_read_data, 0, read_data, 0, bytes_read);
7520     /*
7521         for (i=2; tbox_read_data[i]!='\0';i++) //Return is "Pressure:XX"
7522             temp[i-2]=tbox_read_data[i];
7523             temp[i-2]='\0'; //close by '\0'
7524
7525         probe_temp = atof(temp);
7526         ProcessSystemEvents ();
7527         SetCtrlVal (panel_name, text_panel_name, probe_temp); */
7528
7529     SetCtrlVal (panel_name, text_panel_name, tbox_read_data); //temporary
7530
7531     RS232Error = ReturnRS232Err ();
7532     if (RS232Error)
7533         DisplayRS232Error ();
7534
7535     send_data[0] = '\0';
7536     break;
7537 }
7538     return 0;
7539 }
7540
7541
7542
7543 int CVICALLBACK SetMinPCallBack (int panel, int control, int event,
7544     void *callbackData, int eventData1, int eventData2)
7545 { int pump;
7546     switch (event)
7547     {
7548         case EVENT_COMMIT:
7549             GetCtrlVal(pumpServiceHandle, PUMP_SER_COMMNUMBER, &pump);
7550             if (pump == 1) CP=P1_comport;
7551             else if (pump == 2) CP=P2_comport;
7552             else if (pump == 3) CP=P3_comport;
7553             else if (pump == 0)
7554             {
7555                 MessagePopup ("Warning","Please select the pump.");
7556                 break;
7557             }
7558
7559             GetCtrlVal(pumpServiceHandle, PUMP_SER_PRESSURE_MIN_SEND, &pmin_setpoint);
7560             SetMinPressure();
7561             break;
7562     }
7563     return 0;
7564 }
7565
7566 int CVICALLBACK SetMaxPCallBack (int panel, int control, int event,
7567     void *callbackData, int eventData1, int eventData2)
7568 { int pump;
7569     switch (event)
7570     {
7571         case EVENT_COMMIT:
7572             GetCtrlVal(pumpServiceHandle, PUMP_SER_COMMNUMBER, &pump);
7573             if (pump == 1) CP=P1_comport;
7574             else if (pump == 2) CP=P2_comport;
7575             else if (pump == 3) CP=P3_comport;
7576             else if (pump == 0)
7577             {
7578                 MessagePopup ("Warning","Please select the pump.");
7579                 break;
7580             }
7581
7582             GetCtrlVal(pumpServiceHandle, PUMP_SER_PRESSURE_MAX_SEND, &pmax_setpoint);
7583             SetMaxPressure();
7584             break;
7585     }
7586     return 0;
7587 }
7588
7589
7590
7591
7592
7593 void SetMaxPressure(void) /* build based on DSN_Set_Bath_Setpoint*/
7594 {
7595     //CP= current comport
7596     //LD= LED to set ON
7597
7598     char ascii_setpoint[15],
7599         wholeNum_string[4],
7600         decNum_string[4];
7601
7602     char* setpointcode = "PMAX10:";
7603
7604     int wholeNum,
7605         decNum;
7606
7607     wholeNum = pmax_setpoint; // Captures the whole number portion of the setpoint
7608     decNum = (pmax_setpoint-wholeNum)*1000; // Captures the 2 decimal places of the setpoint
7609
7610     sprintf(wholeNum_string, "%i", wholeNum);
7611     sprintf(decNum_string, "%i", decNum);
7612
7613

```

```

7614 if (decNum == 0)
7615 {
7616     // Assembles the command as shown below      e.g.
7617     strcpy(ascii_setpoint, setpointcode);          // P
7618     strcat(ascii_setpoint, wholeNum_string);       // P10
7619     strcat(ascii_setpoint, ".");                  // P10.
7620     strcat(ascii_setpoint, decNum_string);         // P10.00
7621     strcat(ascii_setpoint, decNum_string);         // P10.000
7622     strcat(ascii_setpoint, "\r");                 // P10.000\r
7623 }
7624
7625 else
7626 {
7627     // Assembles the command as shown below
7628     strcpy(ascii_setpoint, setpointcode);          // P
7629     strcat(ascii_setpoint, wholeNum_string);       // P10
7630     strcat(ascii_setpoint, ".");                  // P10.
7631     strcat(ascii_setpoint, decNum_string);         // P10.XXX
7632     strcat(ascii_setpoint, "\r");                 // P10.XXX\r
7633 }
7634
7635 SetCtrlVal(pumpservice_handle,PUMP_SER_PRESSURE_MAX_READ_2,ascii_setpoint);
7636
7637 FlushOutQ (CP);
7638 FlushInQ (CP);
7639
7640 stringsize = StringLength (ascii_setpoint);
7641 ComWrt (CP, ascii_setpoint, stringsize);        // Sends new setpoint to COM Port
7642
7643 Delay(0.5);
7644
7645 read_cnt = GetInQLen (CP);
7646
7647 read_term = 13;
7648
7649 bytes_read = ComRdTerm (CP, read_data, read_cnt, read_term);
7650 CopyString (tbox_read_data, 0, read_data, 0, bytes_read);
7651
7652
7653 // SetCtrlVal (panel_handle, SERIAL_FLOWRATE_R, tbox_read_data);
7654 /*
7655
7656     if (tbox_read_data && "OK")
7657         SetCtrlVal (panel_handle, LED, 1);
7658     else
7659     {
7660         SetCtrlVal (panel_handle, LED, 0);
7661         MessagePopup ("Error","flow rate has not changed");
7662     }
7663
7664 RS232Error = ReturnRS232Err ();
7665     if (RS232Error)
7666         DisplayRS232Error ();
7667 // Return LED back to the initial value
7668 Delay(0.5);
7669 SetCtrlVal (panel_handle, LED, 0);    */
7670 }
7671 }
7672
7673
7674
7675 void SetMinPressure(void) /* build based on DSN_Set_Bath_Setpoint*/
7676 {
7677     //CP= current comport
7678     //LD= LED to set ON
7679
7680     char ascii_setpoint[15],
7681         wholeNum_string[4],
7682         decNum_string[4];
7683
7684     char* setpointcode = "PMIN10:";
7685
7686     int wholeNum,
7687         decNum;
7688
7689     wholeNum = pmax_setpoint;           // Captures the whole number portion of the setpoint
7690     decNum = (pmax_setpoint-wholeNum)*1000; // Captures the 2 decimal places of the setpoint
7691
7692     sprintf(wholeNum_string, "%i", wholeNum);
7693     sprintf(decNum_string, "%i", decNum);
7694
7695     if (decNum == 0)
7696     {
7697         // Assembles the command as shown below      e.g.
7698         strcpy(ascii_setpoint, setpointcode);          // P
7699         strcat(ascii_setpoint, wholeNum_string);       // P10
7700         strcat(ascii_setpoint, ".");                  // P10.
7701         strcat(ascii_setpoint, decNum_string);         // P10.00
7702         strcat(ascii_setpoint, decNum_string);         // P10.000
7703         strcat(ascii_setpoint, "\r");                 // P10.000\r
7704     }
7705
7706     else
7707     {
7708         // Assembles the command as shown below
7709         strcpy(ascii_setpoint, setpointcode);          // P

```

```

7711     strcat(ascii_setpoint, wholeNum_string);      // P10
7712     strcat(ascii_setpoint, ".");
7713     strcat(ascii_setpoint, decNum_string);        // P10.XXX
7714     strcat(ascii_setpoint, "\r");                 // P10.XXX\r
7715 }
7716 SetCtrlVal(pumpservice_handle,PUMP_SER_PRESSURE_MAX_READ_2,ascii_setpoint);
7717 FlushOutQ (CP);
7718 FlushInQ (CP);
7719
7720
7721
7722
7723
7724
7725
7726
7727
7728
7729
7730
7731
7732
7733
7734
7735
7736 // SetCtrlVal (panel_handle, SERIAL_FLOWRATE_R, tbox_read_data);
7737 /*
7738
7739 if (tbox_read_data && "OK")
7740     SetCtrlVal (panel_handle, LED, 1);
7741 else
7742 {
7743     SetCtrlVal (panel_handle, LED, 0);
7744     MessagePopup ("Error","flow rate has not changed");
7745 }
7746
7747 RS232Error = ReturnRS232Err ();
7748 if (RS232Error)
7749     DisplayRS232Error ();
7750 // Return LED back to the initial value
7751 Delay(0.5);
7752 SetCtrlVal (panel_handle, LED, 0);  */
7753 }

```

```

1 //////// Quadrixe MCP_pump.c includes controls for Pump#2 and Pump#3
2 //////// with same logic as written for Pump#1 in Quadrixe MCP.c
3
4 #include <rs232.h>
5 #include <utility.h>
6 #include <formatio.h>
7 #include <userint.h>
8 #include "Quadrixe MCP.h"
9 #include "Quadrixe MCP_Declare.h"
10
11 //Extra stuff
12 void EnableP2PanelControls (int enable) /* PUMP #1 buttons activation */
13 {
14     //pump
15     SetCtrlAttribute (panel_handle, MAIN_WAS_FR_P_2, ATTR_DIMMED, enable);
16     SetCtrlAttribute (panel_handle, MAIN_P2_START, ATTR_DIMMED, enable);
17     SetCtrlAttribute (panel_handle, MAIN_P2_STOP, ATTR_DIMMED, enable);
18     SetCtrlAttribute (panel_handle, MAIN_P2_PURGE, ATTR_DIMMED, enable);
19     SetCtrlAttribute (panel_handle, MAIN_P2_RESTART, ATTR_DIMMED, enable);
20     SetCtrlAttribute (panel_handle, MAIN_P2_5ERR, ATTR_DIMMED, enable);
21     SetCtrlAttribute (panel_handle, MAIN_P2_SET_NFR, ATTR_DIMMED, enable);
22     SetCtrlAttribute (panel_handle, MAIN_P2_SNFR, ATTR_DIMMED, enable);
23     SetCtrlAttribute (panel_handle, MAIN_STATUS_P_2, ATTR_DIMMED, enable);
24     SetCtrlAttribute (panel_handle, MAIN_P2_TEXTEMSG, ATTR_DIMMED, enable);
25 }
26
27 void EnableP3PanelControls (int enable) /* PUMP #3 buttons activation */
28 {
29     //pump
30     SetCtrlAttribute (panel_handle, MAIN_WAS_FR_P_3, ATTR_DIMMED, enable);
31     SetCtrlAttribute (panel_handle, MAIN_P3_START, ATTR_DIMMED, enable);
32     SetCtrlAttribute (panel_handle, MAIN_P3_STOP, ATTR_DIMMED, enable);
33     SetCtrlAttribute (panel_handle, MAIN_P3_PURGE, ATTR_DIMMED, enable);
34     SetCtrlAttribute (panel_handle, MAIN_P3_RESTART, ATTR_DIMMED, enable);
35     SetCtrlAttribute (panel_handle, MAIN_P3_5ERR, ATTR_DIMMED, enable);
36     SetCtrlAttribute (panel_handle, MAIN_P3_SET_NFR, ATTR_DIMMED, enable);
37     SetCtrlAttribute (panel_handle, MAIN_P3_SNFR, ATTR_DIMMED, enable);
38     SetCtrlAttribute (panel_handle, MAIN_STATUS_P_3, ATTR_DIMMED, enable);
39     SetCtrlAttribute (panel_handle, MAIN_P3_TEXTEMSG, ATTR_DIMMED, enable);
40 }
41
42 /////////////////
43 // Pump #3 On.Off/Start/Stop/Reset/5errors/Set new flow rate
44
45 int CVICALLBACK P3SNFRCallBack (int panel, int control, int event, //New Flow rate
46                                 void *callbackData, int eventData1, int eventData2)
47 {
48
49     int i;
50     double probe_temp;
51     char temp [NUM];
52
53     switch (event)
54     {
55         case EVENT_COMMIT:
56             CmtGetLock (Pumps_LockHandle);
57
58             GetCtrlVal(panel_handle, MAIN_P3_SET_NFR, &wb_setpoint);
59             CP=P3_comport;
60             LED=MAIN_P3_OK_LED;
61
62             SetPumpFlowrate();
63
64             Delay(0.2);
65             //update panel with new flow rate value//
66
67             ///////////
68             panel_name=panel_handle;
69             CP=P3_comport;
70             text_panel_name= MAIN_WAS_FR_P_3;
71             ///////////
72
73             FlushOutQ (CP);
74             FlushInQ (CP);
75
76             send_data[0] = '\0';
77             Fmt (&send_data, "%s<F?\r");
78             stringsize = StringLength (send_data);
79
80             bytes_sent = ComWr (CP, send_data, stringsize);
81             Delay(0.05); /* 0.05 */
82
83             read_cnt = GetInQLen (CP);
84
85             read_data[0] = '\0';
86             read_term = 13;
87
88             bytes_read = ComRdTerm (CP, read_data, read_cnt, read_term);
89             CopyString (tbox_read_data, 0, read_data, 0, bytes_read);
90
91             for (i=2; tbox_read_data[i]!='\0';i++) //Return is "Pressure:XX"
92                 temp[i-2]=tbox_read_data[i];
93                 temp[i-2]='\0'; //close by '\0'
94
95             probe_temp = atof(temp);
96             ProcessSystemEvents ();
97             SetCtrlVal (panel name, text panel name, probe temp);

```

```

98         PFR31[0] = probe_temp;      // Log value in PFR11 Array
100
101        RS232Error = ReturnRS232Err ();
102        if (RS232Error)
103            DisplayRS232Error ();
104
105        send_data[0] = '\0';
106
107 CmtReleaseLock (Pumps_lockHandle);
108         break;
109     }
110     return 0;
111 }
112
113 int CVICALLBACK P3ActivateCallBack (int panel, int control, int event,
114         void *callbackData, int eventData1, int eventData2)
115 {
116     switch (event)
117     {
118         case EVENT_COMMIT:
119             GetCtrlVal (panel_handle, MAIN_P3_ONOFF, &test);
120         if (p3check == 1)
121     {
122             if (Pumps_quitflag == 1)
123             {
124                 CmtGetLock (Pumps_lockHandle);
125                 ActivatePump3 ();
126                 CmtReleaseLock (Pumps_lockHandle);
127             }
128             else ActivatePump3 ();
129     }
130         else
131     {
132         MessagePopup ("Warning", "Connection to Pump #3 is required");
133         Delay(0.05);
134         SetCtrlVal(panel_handle, MAIN_P3_ONOFF, 0);
135     }
136         break;
137     }
138     return 0;
139 }
140
141 void ActivatePump3 (void)
142 {
143     int i;
144     double probe_temp;
145     char temp [NUM];
146     if(test==1)
147     {
148         EnableP3PanelControls (0);
149         SetCtrlAttribute (panel_handle, MAIN_WAS_FR_P_3, ATTR_VISIBLE, 1);
150         SetCtrlAttribute (panel_handle, MAIN_PRESSURE_P_3, ATTR_VISIBLE, 1);
151         SetCtrlVal (panel_handle, MAIN_P3_ONOFF_LED, 1);
152
153         ///////////
154         panel_name=panel_handle;
155         CP=P3_comport;
156         text_panel_name= MAIN WAS FR_P_3;
157         ///////////
158
159         FlushOutQ (CP);
160         FlushInQ (CP);
161
162         send_data[0] = '\0';
163         Fmt (send_data, "%s<F?\r");
164         stringsize = StringLength (send_data);
165
166         bytes_sent = ComWrt (CP, send_data, stringsize);
167         Delay(0.05); /* 0.05 */
168
169         read_cnt = GetInQLen (CP);
170
171         read_data[0] = '\0';
172         read_term = 13;
173
174         bytes_read = ComRdTerm (CP, read_data, read_cnt, read_term);
175         CopyString (tbox_read_data, 0, read_data, 0, bytes_read);
176
177         for (i=2; tbox_read_data[i]!='\0';i++) //Return is "Pressure:XX"
178             temp[i-2]=tbox_read_data[i];
179             temp[i-2]='\0';           //close by '\0'
180
181         probe_temp = atof(temp);
182         ProcessSystemEvents ();
183         SetCtrlVal (panel_name, text_panel_name, probe_temp);
184
185         PFR31[0] = probe_temp;      // Log value in PFR31 Array
186
187         RS232Error = ReturnRS232Err ();
188         if (RS232Error)
189             DisplayRS232Error ();
190
191         send_data[0] = '\0';
192
193         SetCtrlVal(panel_handle, MAIN_LOG_P3, 1); //activate logging pressure
194         GetCtrlVal(panel_handle, MAIN_LOG_P3, &is_P3);

```

```

195     }
196     else
197     {
198         SetCtrlVal(panel_handle, MAIN_LOG_P3, 0); //deactivate logging pressure
199         GetCtrlVal(panel_handle, MAIN_LOG_P3, &Is_P3); //save new value
200
201         EnableP3PanelControls (1); //dim all panels
202         SetCtrlAttribute (panel_handle, MAIN_WAS_FR_P_3, ATTR_VISIBLE, 0);
203         SetCtrlAttribute (panel_handle, MAIN_PRESSURE_P_3, ATTR_VISIBLE, 0);
204         SetCtrlVal (panel_handle, MAIN_P3_ONOFF_LED, 0);
205
206         ///////////////
207         panel_name=panel_handle;
208         CP=P3_comport;
209         PTEXT_panel_name= MAIN_STATUS_P_3;
210         ///////////////
211
212         send_data[0] = '\0';
213         Fmt (send_data, "%s<OFF\r");
214         SendReadPump ();
215         PFR31[0] = '\0'; // Log value in PFR11 Array
216     }
217     return;
218 }
219
220
221
222 int CVICALLBACK P3SFCallBack (int panel, int control, int event,
223     void *callbackData, int eventData1, int eventData2)
224 {
225     switch (event)
226     {
227         case EVENT_COMMIT:
228             CmtGetLock (Pumps_lockHandle);
229             Delay (0.1);
230             panel_name=panel_handle;
231             CP=P3_comport;
232             send_data[0] = '\0';
233             Fmt (send_data, "%s<ON\r");
234             PTEXT_panel_name= MAIN_STATUS_P_3; //show response from pump
235             SendReadPump ();
236
237             pumprun_3 = 31;
238
239             CmtReleaseLock (Pumps_lockHandle);
240             break;
241         case EVENT_RIGHT_CLICK :
242             MessagePopup ("Pump #3", "Will run Pump at current flow rate.");
243             break;
244     }
245     return 0;
246 }
247
248 int CVICALLBACK P3STOPCallBack (int panel, int control, int event,
249     void *callbackData, int eventData1, int eventData2)
250 {
251     switch (event)
252     {
253         case EVENT_COMMIT:
254             CmtGetLock (Pumps_lockHandle);
255             Delay (0.1);
256             panel_name=panel_handle;
257             CP=P3_comport;
258             send_data[0] = '\0';
259             Fmt (send_data, "%s<OFF\r");
260             PTEXT_panel_name= MAIN_STATUS_P_3;
261             SendReadPump ();
262
263             pumprun_3 = 32;
264
265             CmtReleaseLock (Pumps_lockHandle);
266             break;
267     }
268     return 0;
269 }
270
271 int CVICALLBACK P3PURGECallBack (int panel, int control, int event,
272     void *callbackData, int eventData1, int eventData2)
273 {
274     switch (event)
275     {
276         case EVENT_COMMIT:
277             panel_name=panel_handle;
278             CP=P3_comport;
279             send_data[0] = '\0';
280             Fmt (send_data, "%s<PURGE\r");
281             PTEXT_panel_name= MAIN_STATUS_P_3;
282             SendReadPump ();
283             break;
284     }
285     return 0;
286 }
287
288 int CVICALLBACK P3RESTARTCallBack (int panel, int control, int event,
289     void *callbackData, int eventData1, int eventData2)
290 {
291     switch (event)

```

```

292     {
293         case EVENT_COMMIT:
294             panel_name=panel_handle;
295             CP=P3_comport;
296             send_data[0] = '\0';
297             Fmt (send_data, "%s<RESET\r");
298             PTEXT_panel_name= MAIN_STATUS_P_3;
299             SendReadPump ();
300             break;
301     }
302     return 0;
303 }
304
305 int CVICALLBACK P35ERRCallBack (int panel, int control, int event,
306                                 void *callbackData, int eventData1, int eventData2)
307 {
308     switch (event)
309     {
310         case EVENT_COMMIT:
311             panel_name=panel_handle;
312             CP=P3_comport;
313             send_data[0] = '\0';
314             Fmt (send_data, "%s<ERRORS?\r");
315             PTEXT_panel_name= MAIN_STATUS_P_3;
316             SendReadPump ();
317             break;
318     }
319     return 0;
320 }
321
322 ///////////////////////////////////////////////////////////////////
323 // Pump #3 On.Off/Start/Stop/Reset/5errors/Set new flow rate
324 ///////////////////////////////////////////////////////////////////
325 ///////////////////////////////////////////////////////////////////
326
327 ///////////////////////////////////////////////////////////////////
328 // Pump #2 On.Off/Start/Stop/Reset/5errors/Set new flow rate
329 ///////////////////////////////////////////////////////////////////
330 ///////////////////////////////////////////////////////////////////
331
332
333 int CVICALLBACK P2SNFRCallBack (int panel, int control, int event,
334                                 void *callbackData, int eventData1, int eventData2)
335 {
336
337     int i;
338     double probe_temp;
339     char temp [NUM];
340
341     switch (event)
342     {
343         case EVENT_COMMIT:
344             CmtGetLock (Pumps_lockHandle);
345
346             GetCtrlVal(panel_handle, MAIN_P2_SET_NFR, &wb_setpoint);
347             CP=P2_comport;
348             LED=MAIN_P2_OK_LED;
349
350             SetPumpFlowrate();
351
352             Delay(0.2);
353             //update panel with new flow rate value//
354
355             ///////////////
356             panel_name=panel_handle;
357             CP=P2_comport;
358             text_panel_name= MAIN_WAS_FR_P_2;
359             //////////////////
360
361             FlushOutQ (CP);
362             FlushInQ (CP);
363
364             send_data[0] = '\0';
365             Fmt (send_data, "%s<F?\r");
366             stringsize = Stringlength (send_data);
367
368             bytes_sent = ComWrt (CP, send_data, stringsize);
369             Delay(0.05); /* 0.05 */
370
371             read_cnt = GetInQLen (CP);
372
373             read_data[0] = '\0';
374             read_term = 13;
375
376             bytes_read = ComRdTerm (CP, read_data, read_cnt, read_term);
377             CopyString (tbox_read_data, 0, read_data, 0, bytes_read);
378
379             for (i=2; tbox_read_data[i]!='\0';i++) //Return is "Pressure:XX"
380                 temp[i-2]=tbox_read_data[i];
381                 temp[i-2]='\0'; //close by '\0'
382
383             probe_temp = atof(temp);
384             ProcessSystemEvents ();
385             SetCtrlVal (panel_name, text_panel_name, probe_temp);
386
387             PFR21[0] = probe_temp; // Log value in PFR11 Array
388

```

```

389     RS232Error = ReturnRS232Err ();
390     if (RS232Error)
391         DisplayRS232Error ();
392
393     send_data[0] = '\0';
394
395     CmtReleaseLock (Pumps_lockHandle);
396     break;
397 }
398
399 return 0;
400 }

401 int CVICALLBACK P2ActivateCallBack (int panel, int control, int event,
402 void *callbackData, int eventData1, int eventData2)
403 {
404
405 switch (event)
406 {
407     case EVENT_COMMIT:
408         GetCtrlVal (panel_handle, MAIN_P2_ONOFF, &test);
409         if (p2check == 1)
410         {
411             if (Pumps_quitflag == 1)
412             {
413                 CmtGetLock (Pumps_lockHandle);
414                 ActivatePump2 ();
415                 CmtReleaseLock (Pumps_lockHandle);
416             }
417             else ActivatePump2 ();
418         }
419         else
420         {
421             MessagePopup ("Warning", "Connection to Pump #2 is required");
422             Delay(0.05);
423             SetCtrlVal(panel_handle, MAIN_P2_ONOFF, 0);
424         }
425     break;
426 }
427 return 0;
428 }

429 void ActivatePump2 (void)
430 {
431
432     int i;
433     double probe_temp;
434     char temp [NUM];
435     if(test==1)
436     {
437
438         EnableP2PanelControls (0);
439         SetCtrlAttribute (panel_handle, MAIN_WAS_FR_P_2, ATTR_VISIBLE, 1);
440         SetCtrlAttribute (panel_handle, MAIN_PRESSURE_P_2, ATTR_VISIBLE, 1);
441         SetCtrlVal (panel_handle, MAIN_P2_ONOFF_LED, 1);
442
443         ///////////////
444         panel_name=panel_handle;
445         CP=P2_comport;
446         text_panel_name= MAIN_WAS_FR_P_2;
447         //////////////////
448
449         FlushOutQ (CP);
450         FlushInQ (CP);
451
452         send_data[0] = '\0';
453         Fmt (send_data, "%s<F?\r");
454         stringsize = StringLength (send_data);
455
456         bytes_sent = ComWrt (CP, send_data, stringsize);
457         Delay(0.05); /* 0.05 */
458
459         read_cnt = GetInQLen (CP);
460
461         read_data[0] = '\0';
462         read_term = 13;
463
464         bytes_read = ComRdTerm (CP, read_data, read_cnt, read_term);
465         CopyString (tbox_read_data, 0, read_data, 0, bytes_read);
466
467         for (i=2; tbox_read_data[i]!='\0';i++) //Return is "Pressure:XX"
468             temp[i-2]=tbox_read_data[i];
469             temp[i-2]='\0'; //close by '\0'
470
471         probe_temp = atof(temp);
472         ProcessSystemEvents ();
473         SetCtrlVal (panel_name, text_panel_name, probe_temp);
474
475         PFR21[0] = probe_temp; // Log value in PFR21 Array
476
477         RS232Error = ReturnRS232Err ();
478         if (RS232Error)
479             DisplayRS232Error ();
480
481         send_data[0] = '\0';
482
483         SetCtrlVal(panel_handle, MAIN_LOG_P2, 1); //activate logging pressure
484         GetCtrlVal(panel_handle, MAIN_LOG_P2, &Is_P2);
485     }

```

```

486     else
487     {
488         SetCtrlVal(panel_handle, MAIN_LOG_P2, 0); //deactivate logging pressure
489         GetCtrlVal(panel_handle, MAIN_LOG_P2, &Is_P2); //save new value
490
491         EnableP2PanelControls (1); //dim all panels
492         SetCtrlAttribute (panel_handle, MAIN_WAS_FR_P_2, ATTR_VISIBLE, 0);
493         SetCtrlAttribute (panel_handle, MAIN_PRESSURE_P_2, ATTR_VISIBLE, 0);
494         SetCtrlVal (panel_handle, MAIN_P2_ONOFF_LED, 0);
495
496         /////////////
497         panel_name=panel_handle;
498         CP=P2_comport;
499         PTEXT_panel_name= MAIN_STATUS_P_2;
500         ///////////
501
502         send_data[0] = '\0';
503         Fmt (send_data, "%s<OFF\r");
504         SendReadPump ();
505         PFR21[0] = '\0'; // Log value in PFR11 Array
506
507     return;
508 }
509
510
511 int CVICALLBACK P2SFCallBack (int panel, int control, int event,
512     void *callbackData, int eventData1, int eventData2)
513 {
514     switch (event)
515     {
516         case EVENT_COMMIT:
517             CmtGetLock (Pumps_lockHandle);
518             Delay (0.1);
519             panel_name=panel_handle;
520             CP=P2_comport;
521             send_data[0] = '\0';
522             Fmt (send_data, "%s<ON\r");
523             PTEXT_panel_name= MAIN_STATUS_P_2; //show response from pump
524             SendReadPump ();
525
526             pumprun_2 = 21;
527
528             CmtReleaseLock (Pumps_lockHandle);
529             break;
530         case EVENT_RIGHT_CLICK :
531             MessagePopup ("Pump #2", "Will run Pump at current flow rate.");
532             break;
533     }
534     return 0;
535 }
536
537 int CVICALLBACK P2STOPCallBack (int panel, int control, int event,
538     void *callbackData, int eventData1, int eventData2)
539 {
540     switch (event)
541     {
542         case EVENT_COMMIT:
543             CmtGetLock (Pumps_lockHandle);
544             Delay (0.1);
545             panel_name=panel_handle;
546             CP=P2_comport;
547             send_data[0] = '\0';
548             Fmt (send_data, "%s<OFF\r");
549             PTEXT_panel_name= MAIN_STATUS_P_2;
550             SendReadPump ();
551
552             pumprun_2 = 22;
553
554             CmtReleaseLock (Pumps_lockHandle);
555             break;
556     }
557     return 0;
558 }
559
560 int CVICALLBACK P2PURGECallBack (int panel, int control, int event,
561     void *callbackData, int eventData1, int eventData2)
562 {
563     switch (event)
564     {
565         case EVENT_COMMIT:
566             panel_name=panel_handle;
567             CP=P2_comport;
568             send_data[0] = '\0';
569             Fmt (send_data, "%s<PURGE\r");
570             PTEXT_panel_name= MAIN_STATUS_P_2;
571             SendReadPump ();
572             break;
573     }
574     return 0;
575 }
576
577 int CVICALLBACK P2RESTARTCallBack (int panel, int control, int event,
578     void *callbackData, int eventData1, int eventData2)
579 {
580     switch (event)
581     {
582         case EVENT_COMMIT:

```

```

583     panel_name=panel_handle;
584     CP=P2_comport;
585     send_data[0] = '\0';
586     Fmt (send_data, "%s<RESET\r");
587     PTEXT_panel_name= MAIN_STATUS_P_2;
588     SendReadPump ();
589     break;
590   }
591   return 0;
592 }
593
594 int CVICALLBACK P25ERRCallBack (int panel, int control, int event,
595   void *callbackData, int eventData1, int eventData2)
596 {
597   switch (event)
598   {
599     case EVENT_COMMIT:
600       panel_name=panel_handle;
601       CP=P2_comport;
602       send_data[0] = '\0';
603       Fmt (send_data, "%s<ERRORS?\r");
604       PTEXT_panel_name= MAIN_STATUS_P_2;
605       SendReadPump ();
606       break;
607   }
608   return 0;
609 }
610
611 ///////////////////////////////////////////////////////////////////
612 // Pump #2 On.Off/Start/Stop/Reset/5errors/Set new flow rate
613 ///////////////////////////////////////////////////////////////////
614
615

```

```

1 #include <ansi_c.h>
2 #include <utility.h>
3 #include <userint.h>
4 #include "Quadrise MCP.h"
5 #include "Quadrise MCP_Declare.h"
6
7 int CVICALLBACK LogFileCallBack (int panel, int control, int event,
8         void *callbackData, int eventData1, int eventData2)
9 {
10     switch (event)
11     {
12         case EVENT_COMMIT:
13             LogFileHeader();
14             break;
15         case EVENT_RIGHT_CLICK:
16             break;
17     }
18 }
19 return 0;
20 }
21
22
23 void LogFileHeader(void) //build based on DSN_LogFileHeader
24 {
25     FILE *fp;
26     char *DATE;
27     char *TIME;
28
29 //selecting the file to save to
30 Log_File_Selected = FileSelectPopup ("", "*.log", "", 
31         "Enter the name of the LOG FILE", VAL_SAVE_BUTTON,
32         0, 0, 1, 0, logFile);
33
34 if (Log_File_Selected>0) // File Selected
35 {
36     fp = fopen (logFile, "w");
37     // Date and Time
38     DATE = DateStr ();
39     TIME = TimeStr ();
40     fprintf( fp, "Quadrise MCP System Log File \nDate\t%t\Time\t%t\n",DATE,TIME);
41     fprintf(fp, "*****\n");
42 }
43 else // No File Selected
44 {
45     // Do nothing
46 }
47
48 //calibration data
49 if (Log_File_Selected>0) // File Selected
50 {
51 // LOGGED DATA VARIABLE NAMES
52
53     fprintf (fp, "CS\t"); //current stage
54
55
56     fprintf (fp, "P1_run\t"); //running pump #
57     fprintf (fp, "P2_run\t"); //running pump #
58     fprintf (fp, "P3_run\t"); //running pump #
59
60     fprintf (fp, "TimeREF\t"); //reference time
61
62     fprintf( fp, "TIME\t");
63
64     fprintf( fp, "G TIME\t");
65
66
67     fprintf( fp, "Flow rate P1\t");
68
69     fprintf( fp, "Water inj P1\t");
70     fprintf( fp, "Water inj P1 PV\t");
71
72     fprintf( fp, "Water flooding\t");
73     fprintf( fp, "Water flooding PV\t");
74
75     fprintf( fp, "Pore Volume [PV]\t");
76
77     fprintf( fp, "DP1.Permeability.water\t");
78     fprintf( fp, "Delta.Permeability.water\t");
79
80     fprintf( fp, "Flow rate P2\t");
81     fprintf( fp, "Oil inj P2\t");
82     fprintf( fp, "Oil inj P2 [PV]\t");
83
84     fprintf( fp, "DP1.Permeability.oil\t");
85     fprintf( fp, "Delta.Permeability.oil\t");
86
87     fprintf( fp, "Flow rate P3\t");
88     fprintf( fp, "Emulsion inj P1\t");
89     fprintf( fp, "DP1.Permeability.emulsion\t");
90     fprintf( fp, "Delta.Permeability.emulsion\t");
91
92
93     fprintf( fp, "Pressure P1\t");
94     fprintf( fp, "Pressure P2\t");
95     fprintf( fp, "Pressure P3\t");
96

```

```

97     fprintf( fp, "Pressure inlet\t");
98     fprintf( fp, "Diff pressure\t");
99
100    fprintf( fp, "Pressure differential [TP2-BPR1] , psi\t");
101
102    fprintf( fp, "M11\t");
103    fprintf( fp, "M12\t");
104    fprintf( fp, "M13\t");
105    fprintf( fp, "M14\t");
106
107    fprintf( fp, "M21\t");
108    fprintf( fp, "M22\t");
109    fprintf( fp, "M23\t");
110    fprintf( fp, "M24\t");
111
112    fprintf( fp, "M31\t");
113    fprintf( fp, "M32\t");
114    fprintf( fp, "M33\t");
115    fprintf( fp, "M34\t");
116
117    fprintf( fp, "M41\t");
118    fprintf( fp, "M42\t");
119    fprintf( fp, "M43\t");
120    fprintf( fp, "M44\t");
121
122    fprintf( fp, "BPR11\t");
123    fprintf( fp, "BPR12\t");
124    fprintf( fp, "BPR13\t");
125
126    fprintf( fp, "WATER REC\t");
127    fprintf( fp, "OIL REC\t");
128    fprintf( fp, "TEMP time\t");
129    fprintf( fp, "TEMP delta\t");
130
131    fprintf( fp, "WATER REC_ST9\t");
132    fprintf( fp, "OIL REC_ST9\t");
133
134    printf( fp, "TEST TUBE\t");
135
136    printf( fp, "Residual W_sat\t");
137
138    printf( fp, "WATER_EMUL_REC_ST14\t");
139    printf( fp, "OIL REC_ST14\t");
140
141    printf( fp, "EMULSION IN\t"); //Based on Mass flow meter
142    printf( fp, "TEMP_E delta\t");
143    printf( fp, "TEMP_E time\t");
144
145    printf( fp, "Waterflooding_temp\t"); //used for Swir calculations
146
147    printf( fp, "WATER_EMUL_REC_ALT\t");
148    printf( fp, "OIL REC_ALT\t");
149
150    printf( fp, "SETPOINT\t");
151
152    printf( fp, "CP1.1\t");
153    printf( fp, "CP1.2\t");
154    printf( fp, "CP1.3\t");
155    printf( fp, "CP1.4\t");
156    printf( fp, "CP1.5\t");
157
158    printf( fp, "CP2.1\t");
159    printf( fp, "CP2.2\t");
160    printf( fp, "CP2.3\t");
161    printf( fp, "CP2.4\t");
162    printf( fp, "CP2.5\t");
163
164    printf( fp, "CP3.1\t");
165    printf( fp, "CP3.2\t");
166    printf( fp, "CP3.3\t");
167    printf( fp, "CP3.4\t");
168    printf( fp, "CP3.5\t");
169
170    printf( fp, "\n"); // NEW LINE
171    fclose( fp );
172 }
173 }
174
175 //*****
176 // LogFile : Save DATA to the log file
177 // build based on DSN_LogFile
178 //*****
179 void LogFile(void)
180 {
181     FILE *fp;
182     //opening the file
183     fp = fopen (logFile, "a");
184     //
185     // LOGGED DATA VARIABLES - DAQ
186     //Reference time
187
188     printf( fp, "%i\t",stage); //ok
189
190
191     printf( fp, "%i\t",pumprun_1); //ok
192     printf( fp, "%i\t",pumprun_2); //ok
193     printf( fp, "%i\t",pumprun_3); //ok

```

```

194      // 11 - pump #1 start 12 - pump #1 stop
195      // 21 - pump #2 start 22 - pump #2 stop
196      // 31 - pump #3 start 32 - pump #3 stop
197
198      fprintf( fp, "%1.4f\t",timeDAQ); //ok
199      fprintf( fp, "%1.2f\t",step[0]); //ok
200      fprintf( fp, "%2.4f\t", Gtime[0]);
201
202      //Flow rates and volumes injected for pumps
203
204      fprintf( fp, "%1.4f\t",PFR11[0]); //ok
205
206      fprintf( fp, "%4.4f\t",WATERINJ[0]); //ok
207      fprintf( fp, "%4.4f\t",WATERINJPV[0]); //ok
208
209      fprintf( fp, "%4.4f\t",WATERINJ2[0]); //ok
210      fprintf( fp, "%4.4f\t",WATERINJ2PV[0]); //ok
211
212      fprintf( fp, "%4.4f\t",PV[0]); //ok
213
214      fprintf( fp, "%2.8f\t",PERMWATERDP1[0]); //ok
215      fprintf( fp, "%2.8f\t",PERMWATERDELTA[0]); //ok
216
217      //oil
218      fprintf( fp, "%1.4f\t",PFR21[0]); //ok
219      fprintf( fp, "%4.4f\t",OILINJ[0]); //ok
220      fprintf( fp, "%4.4f\t",OILINJPV[0]); //ok
221
222      fprintf( fp, "%2.8f\t",PERMOILDP1[0]); //ok
223      fprintf( fp, "%2.8f\t",PERMOILDELTA[0]); //ok
224
225      //emulsion
226      fprintf( fp, "%1.4f\t",PFR31[0]); //ok
227      fprintf( fp, "%4.4f\t",EMULINJ[0]); //ok
228      fprintf( fp, "%2.8f\t",PERMEMULDP1[0]); //ok
229      fprintf( fp, "%2.8f\t",PERMEMULDELTA[0]); //ok
230
231      //Pressure from pumps
232      fprintf( fp, "%1.4f\t",P11[0]); //ok
233      fprintf( fp, "%1.4f\t",P21[0]); //ok
234      fprintf( fp, "%1.4f\t",P31[0]); //ok
235
236      //Pressure inlet
237      fprintf( fp, "%4.4f\t",TP2[0]); //ok MAX 1500.00psi
238
239      //Pressure differential
240      fprintf( fp, "%3.4f\t",DP1[0]); //ok MAX 250.00 psi
241
242      fprintf( fp, "%4.4f\t",Delta[0]); //ok MAX 1500 psi
243
244      //Mass flow meter #
245      fprintf( fp, "%4.3f\t",M11[0]); //ok
246      fprintf( fp, "%4.3f\t",M12[0]); //ok
247      fprintf( fp, "%4.3f\t",M13[0]); //ok
248      fprintf( fp, "%4.3f\t",M14[0]); //ok
249
250
251      //Mass flow meter #
252      fprintf( fp, "%4.3f\t",M21[0]); //ok
253      fprintf( fp, "%4.3f\t",M22[0]); //ok
254      fprintf( fp, "%4.3f\t",M23[0]); //ok
255      fprintf( fp, "%4.3f\t",M24[0]); //ok
256
257
258      //Mass flow meter #
259      fprintf( fp, "%4.3f\t",M31[0]); //ok
260      fprintf( fp, "%4.3f\t",M32[0]); //ok
261      fprintf( fp, "%4.3f\t",M33[0]); //ok
262      fprintf( fp, "%4.3f\t",M34[0]); //ok
263
264
265      //Mass flow meter #
266      fprintf( fp, "%4.3f\t",M41[0]); //ok
267      fprintf( fp, "%4.3f\t",M42[0]); //ok
268      fprintf( fp, "%4.3f\t",M43[0]); //ok
269      fprintf( fp, "%4.3f\t",M44[0]); //ok
270
271
272      //Back pressure regulator
273      fprintf( fp, "%1.4f\t",BPR11[0]); //ok
274      fprintf( fp, "%1.4f\t",BPR12[0]); //ok
275      fprintf( fp, "%1.4f\t",BPR13[0]); //ok
276
277
278      fprintf( fp, "%4.3f\t",WATERREC[0]);
279      fprintf( fp, "%4.3f\t",OILREC[0]);
280      fprintf( fp, "%4.3f\t",TEMPSTEP[0]);
281      fprintf( fp, "%4.3f\t",TEMPDELTA[0]);
282
283      fprintf( fp, "%4.3f\t",WATERREC_ST9[0]);
284      fprintf( fp, "%4.3f\t",OILREC_ST9[0]);
285
286      fprintf( fp, "%2.0f\t", MANUAL_TEST_TUBE[0]);
287
288      fprintf( fp, "%1.4f\t", SWI[0]);
289
290      fprintf( fp, "%4.3f\t", RECEMUL[0]);
291      fprintf( fp, "%4.3f\t", OILREC_ST14[0]);
292
293      fprintf( fp, "%4.3f\t", EMULIN[0]);
294      fprintf( fp, "%4.3f\t", TEMPDELTA_E[0]);

```

```

291   fprintf( fp, "%4.3f\t", TEMPSTEP_E[0]);
292   fprintf( fp, "%4.3f\t", WATERFLOODINJ[0]);
293   fprintf( fp, "%4.3f\t", RECEMUL_ALT[0]);
294   fprintf( fp, "%4.3f\t", OILREC_ALT[0]);
295   fprintf( fp, "%3.2f\t", SETPOINTOUT[0]);
296
297
298
299
300
301   fprintf( fp, "%1.4f\t",CP11[0]); //ok
302   fprintf( fp, "%1.4f\t",CP12[0]); //ok
303   fprintf( fp, "%1.4f\t",CP13[0]); //ok
304   fprintf( fp, "%1.4f\t",CP14[0]); //ok
305   fprintf( fp, "%1.4f\t",CP15[0]); //ok
306
307   fprintf( fp, "%1.4f\t",CP21[0]); //ok
308   fprintf( fp, "%1.4f\t",CP22[0]); //ok
309   fprintf( fp, "%1.4f\t",CP23[0]); //ok
310   fprintf( fp, "%1.4f\t",CP24[0]); //ok
311   fprintf( fp, "%1.4f\t",CP25[0]); //ok
312
313   fprintf( fp, "%1.4f\t",CP31[0]); //ok
314   fprintf( fp, "%1.4f\t",CP32[0]); //ok
315   fprintf( fp, "%1.4f\t",CP33[0]); //ok
316   fprintf( fp, "%1.4f\t",CP34[0]); //ok
317   fprintf( fp, "%1.4f\t",CP35[0]); //ok
318
319   fprintf( fp, "\n"); // NEW LINE
320   fclose( fp );
321   return;
322 }
323
324
325
326

```