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### THE UNIVERSITY OF ALBERTA

MEAN FIELD ELECTRODYNAMICS AND
DYNAMO THEORIES OF PLANETARY MAGNETIC FIELDS

by

O JOHN MICHAEL GILLILAND

### A THESIS

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GEOPHYSICS :

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# THE UNIVERSITY OF ALBERTA FACULTY OF GRADUATE STUDIES AND RESEARCH

The undersigned certify that they have read, and recommend to the Faculty of Graduate Studies and Research, for acceptance, a thesis entitled -MEAN FIELD ELECTRO-DYNAMICS AND DYNAMO THEORIES OF PLANETARY MAGNETIC FIELDS JOHN MICHAEL GILLILAND submitted by in partial fulfilment of the requirements for the degree of Doctor of Philosophy in Geophysics.

External Examiner

27th February 1973

Date

Dedicated with gratitude and affection to my parents

DEAN AND MRS. HENRY C. GILLILAND and to my wife

MARGARET,

without whose continuing encouragement and loyal support this thesis would not have been written.

#### ABSTRACT

In Chapter 1 homogeneous dynamo theory is reviewed Present observational knowledge of astrophysical magnetic fields is summarized, and is shown to provide less support for Schuster's hypothesis than the data presented by Warwick (1971).

In Chapter 2 a review of "mean field electrodynamics" is presented, and the dispersion relation for "wave" mean fields is discussed. A new terminology is suggested for several types of stationary, homogeneous turbulence.

In Chapter 3 it is shown that, to a first approximation, stationary, homogeneous turbulence whose average, properties are invariant under space-time inversion (PT-invariant turbulence) cannot support dynamo action in an incompressible fluid. This result is in direct contradiction to the work of Lerche and Low (1971). However, "mirror-symmetric" turbulence which is not PT-invariant cannot definitely be ruled out as a source of dynamo action.

The decay of "wave" mean fields in the presence of PT-invariant turbulence is studied. It is shown that spatially periodic mean fields can exist only if the correlation tensor of the turbulence satisfies certain conditions. Conditions are also established for validity of the Rädler (1968) expression for "turbulent magnetic diffusivity", when the mean field does not oscillate with time. When the mean

field is oscillatory, Rädler's techniques are not useful.

Numerical results are presented for oscillating mean fields, showing the relationship between mean field frequency and wavelength and the properties of the turbulence. The possibility of a "sporadic helicity" dynamo is discussed.

In Chapter 4 a technique is presented for dealing with nonstationary, inhomogeneous turbulence within the framework of mean field electrodynamics. The technique is applied to the kinematic dynamo problem.

In Chapter 5 temporal variations of magnetic fields are discussed. The " $\alpha^2(r)$ " kinematic dynamo i a spherical shell is studied in detail. It is shown that the dependence of  $\alpha$  on r near the spherical boundary can control the time behaviour of the external magnetic field. Integral properties of the dynamo equations for more general velocity distributions are discussed, and the possibility of "boundary-layer control" is considered in detail. It is found that in the geodynamo, temporal variations of the dipole moment on scales less than  $10^4$  years may be explained by boundary-layer phenomena.

In Chapter 6 the hydromagnetic dynamo problem is studied and the likelihood of "boundary-layer control" in the geodynamo is assessed. It is shown that "dipole wobble" can be explained as an effect of the slow, systematic decrease of the Earth's rate of rotation, if the kinematic viscosity at the core-mantle interface is approximately

1-2 m<sup>2</sup>/sec. Non-periodic variations of the axial dipole moment on the time scale of geomagnetic polarity transitions can also be explained by this model.

The effects of inhomogeneous, locally isotropic, turbulent forces in the Earth's core are considered. The characteristic turbulent length scale and the ratio of the diffusion time on this length scale to the effective turbulent time scale are important parameters. In most cases, a rotation-dependent  $\alpha$ -effect is dominant when the mean magnetic field is small.

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# TABLE OF CONTENTS

<u>Title</u>	Page
1. A GENERAL REVIEW OF DYNAMO THEORY	
1.1 Astrophysical magnetic fields	. 1
1.1.1 Introduction, and summary of observations .	. 1
1.1.2 Dynamo theory and astrophysical magnetic fields	9
1.1.3 Schuster's hypothesis	. 16
1.2 The homogeneous dynamo problem	. 24
1.3 The Kinematic dynamo problem	. 26
1.3.1 The dynamo equations	. 26
1.3.2 The quasi-steady approximation	./28
1.3.3 The magnetic induction equation	. 30
1.4 Solutions to the kinematic dynamo problem	. 31
1.4.1 Requirements on solutions	. 31
1.4.2 Anti-dynamo theorems	، 32 م
1.4.3 Existence of solutions	<b>7</b> 35
1.4.4 "Exact" models.	, 35
1.4.5 Spherical harmonic expansion models	<b>.</b> 35 m
1.4.6 "Sporadic" models	. 36
1.4.7 Asymptotic models	. 37
a. Herzenberg-type models	. 37
b Periodic dynamos	. 37
c. Nearly axisymmetric dynamos	. 38
1 4 8 Moon field many	. 39
	. 39
.5 The hydromagnetic dynamo problem	. 42
1.5.1 The equation of mass conservation	. 42
1.5.2 The Navier-Stokes equation of hydromagnetics	. 43

,		,	
•	<u>Title</u>	,	Page
1.5.3	The hydromagnetic equations in a rotating frame		. 45
	ne full hydromagnetic dynamo proble ermodynamic equations	em ~	. 51
	ne full hydromagnetic dynamo proble undary comditions	em ~	. 53
1.7.1	Electromagnetic boundary condition	ons	. 53
1.7.2	Mechanical boundary conditions .		. 55
1.7.3	Thermal boundary conditions		. 56
	e full hydromagnetic dynamo proble	em -	. 58
1.8.1	Buoyancy forces		. 58
1.8.2	Precessional torques		. 59
1.8.3	Turbulent forces		. 60
1.8.4	More general studies of the hydromagnetic dynamo problem		. 62
1.8.5	Driving forces in the geodynamo		. 66
	e mathematical nature of the dynam	no,	. 712
1.9.1	The kinematic dynamo problem		. 71
1.9.2	The hydromagnetic dynamo problem		. 76
1.10 Su	mmary of Chapter 1		78
2. MEAN	FIELD ELECTRODYNAMICS	· · · · · ·	. 79
2.1 In	troduction		. 79
2.2 Ту	pes of turbulence		., 81
2.2.1	General considerations		. 81
2.2.2	Two-point, two-time correlations	• • • • •	. 87
	×ii		<b>X</b> (
			10

	,	<u>Title</u>	3	Page
;	2.3 Ţ fu	The kinematic Tynamo problem - Green's unction techniques	, ,	91
	2.3.1	The dynamo equations		91
	2.3.2			91
	2.3.3	Higher-order terms		94
2	2.4 T	he kinematic dynamo problem - Fourier ansform techniques	~.	96
	2.4.1	Notation		96
	2.4.2	The fluctuating induction equation		97
*	2.4.3	Solution of the fluctuating induction equation for uniform, time-independent mean fields		
	2.4.4			99
	<b>2.4.</b> 5	Solution of the fluctuating induction equation for "wave" mean fields		102
2	.5 Ev	valuation of $\mathbf{u}^{*}\mathbf{x}\mathbf{B}^{*}$		104
•	2.5.1	The Rädler expansion technique		104,
	2.5.2	Choice of Green's function		105
		Comparison of expansion and Fourier transform techniques	n. er	106
2	2.5.4	First order smoothing, and scaling of terms in the induction equation		107
2	6 So	lution of the mean field induction equation	. 1	112
	1	General considerations	. 1	112
	2.6.2	The mean field dispersion relation	. 1	12
2	2.6.3	An alternative derivation of the mean field dispersion relation	. 1	16
2	.6.4	Symmetry considerations	for-	18
2.	7 The	e mean field hydromagnetic dynamo problem	3	10

1

-	Title	Page
. E	1.2	
2.8 \$	ummary of Chapter 2	120
3. THE	KINEMATIC DYNAMO PROBLEM AND PT-INVARIA	NT
	ULENCE	121
		The state of the s
3.1 H un	elicity, and the maintenance of nearly iform, nearly time-independent mean field	ds 121
3.2 P	Trinvariant turbulence and non-uniform,	
	cillatory mean fields	123
	The spectrum tensor for stationary,	
	homogeneous, isotropic turbulence	123
3,2,2	PT-invariance and helicity	124
•	An anti-dynamo theorem for stationary,	j.
	homogeneous, isotropic turbulence in an	· /
1 1	incompressible fluid	, , 125
3,2,4	Extension of the anti-dynamo theorem -	/ 1
*	PT-invariant turbulence in an incom- pressible fluid	127
3 2 5	Failure of the anti-dynamo theorem for	
21712	PT-invariant turbulence in a compressible	le i
	fluid	128
3,2,6	Reconciliation of the anti-dynamo theorwith the work of Lerche and Low	em 130
3.2.7	The possibility of dynamo action with "mirror-symmetric" turbulence	130
8 11 g		· · · · · · · · · · · · · · · · · · ·
3,3 P7 mea	T-invariant turbulence and decaying an fields	132
3.3.1	The effect of initial conditions	132
9	'Initial condition I = B' independent	
	B	
3.3.3	Initial condition II - B' correlated	with
**************************************		134
3.4 PT fie	P-invariant turbulence, and decaying mean elds - initial condition II	136
3.4.1	The mean field dispersion relation	136
	A STATE OF THE PARTY OF THE PAR	
1 E 1		
/ .		

,

( )	<u>Title</u>	Page
3.4.2	The mean field dispersion relation for isotropic turbulence in an incompressible fluid	136
3.4.3	The nature of the dispersion relation - contrast between oscillatory and non-oscillatory mean fields	. 141
3.5 Di	gression: the properties of stationary, organical organi	143*
3,5.1	General properties	143
	Isotropic turbulence in an incompressible fluid	144
3.5.3	$E(k,\omega)/k^4$ for isotropic turbulence in an incompressible fluid	14′5
	Gaussian isotropic turbulence in an incompressible fluid	. 146
3.5.5	Gaussian-exponential isotropic turbulence in an incompressible fluid	. , 147
* 3.6 Is	otropic turbulence and decaying mean fields tial condition II	. 150
	The nature of the eigenvalue for oscillating mean fields	150
•	Non-oscillatory mean fields - the dispersion relation and the effective magnetic diffusivity	. 151
33,6,3	Insensitivity of the effective diffusivity to initial conditions when $\lambda_{C}^{K}$ is small .	. 153
3.6.4	Comparison of results for small $\lambda$ K with the results of Krause and Rädler	155
3.6.5	The effects of initial conditions and mean field nonuniformity when $\lambda_{C}^{K}$ is not small	<b>. 159</b> ;
3.7 PT- fiel	invariant turbulence and decaying mean $ds$ - initial condition $I$	. 165
	The mean field dispersion relation	. 165
1	The mean field dispersion relation for sotropic turbulence in an incompressible luid	. 165
The house	<b>xv</b>	

Ţitle		Page
1		
3.7.3 Time dependence of the mean field dispersion relation for different of turbulence	types	
3.7.4 The mean field dispersion relatio Gaussian isotropic turbulence -	n for	. 167
non-oscillatory mean fields		. 168
3.8 Isotropic turbulence and decaying, no oscillatory mean fields - comparison initial conditions I and II	on- of	. 173
3.8.1 Relationship between mean field do and turbulent magnetic Reynolds nu effect of mean field initial condi-	mber ~	173
3.8.2 Range of validity of solutions ob- using the Rädler expansion technique	tained	4 176
3.8.3 The mean field decay rate at large		178
3.8.4 Stabilization of the mean field de rate, and loss of energy from the r	ecay	183
3.8.5 Conditions on the turbulence for a decay to be established before sign energy is lost from the mean field	nificant	185
3.9 Isotropic turbulence and decaying mea	an fields ondition I	194
3.9.1 Inappropriateness of the Radler extechnique	mansion	194 :
3.9.2 General statement of the problem	: 	195
3.9.3 Restrictions on the turbulence for meaningful solutions		198
3.9.4 Numerical search procedure		200
3.9.5 The impossibility of slowly-decayi long-period, oscillatory mean field	ng,	202
3.10 Isotropic turbulence and decaying mea which oscillate with time - initial co	n fields ndition	207
3.10.1 General statement of the problem, restrictions on the turbulence for meaningful solutions	and	207

Title	Page
	•
3.10.2 Numerical search procedure	. 209
3.10.3 Behaviour of solutions as functions of $\lambda_{\rm C}/{\rm L}$ , $\tau_{\rm C}/{\rm T}$ , and $R_{\rm m}$	220
3.10.4 The existence of acceptable slowly-decaying, long-period, oscillatory mean fields	
3.11 The kinematic dynamo problem	. 238
3.11.1 The two-dimensional integral technique and turbulence without PT-invariance	. 238
3.11.2 The mean field dispersion relation	. 239
3.11.3 The possibility of a "sporadic helicity" dynamo	241
3.12 Summary of Chapter 3	. 242
4. THE DYNAMO PROBLEM AND INHOMOGENEOUS, NON- STATIONARY TURBULENCE	. 248
4.1 Introduction	248
4.2 Inhomogeneous, nonstationary turbulence a survey of existing techniques	. 250
4.2.1 Locally homogeneous, quasi-stationary random functions - the Kolmogorov structure tensor approach	. 250
4.2.2 The Silverman approach to locally stationary and homogeneous turbulence with smoothly varying mean characteristics	. 251
4.2.3 The Rädler approach to locally stationary and homogeneous turbulence with smoothly varying mean characteristics	. 25/2
	8.
4.3 Inhomogeneous, nonstationary turbulence and the dynamo problem - a successive approximation technique	. 254
4.3.1 Outline of the successive approximation technique	. 254

	Page
ction	. 256
irst	258
ons on indicated in the contract of the contra	. 259
w	. 260
of	. 263
large- velocity	. 263
roximation .	. 265
	267
GNETIC	268
	268
cal	2.60
	268
	276
• • • • • •	281
ic dynamo	283
gnetic	283
	283
	285
	286
	ons on ibility  of large-velocity  coximation  cal  eo- ic dynamo

	<u>Title</u>	Page
5.3	The $\alpha^2(r)$ dynamo in a spherical shell	290
5.3.1	The mean field induction equation and boundary conditions	290
5.3.	2 Separable solutions - the radial equations	<b>29</b> 1
5.3.3	The radial equations in nondimensional form	292
5.3.4	Power series solutions of the radial equations	293
5.3.5	Application of the boundary conditions -	295
\$1 <b>5 . 3 . 6</b>		
5.3.7		301
	Objections to the $\alpha^2(r)$ model for	306
. 1	A	
5.4 T	ntegral properties of the kinematic dynamo	\$ -3
eq	42 m A i i m m —	308
5.4.1	Introduction	308
5.4.2	Multipole representation of the external fields	30 <i>9</i>
5,4,3	Magnetic and electric multipole moments - representation in terms of the internal magnetic and velocity fields	311
5.4.4	Temporal behaviour of the external magnetic dipole moment	3 313
5.4.5	"Boundary-layer control" of the external	314
5.4.6	Simplification of notation	31.7
5.4.7	The "boundary-layer control" approxi-	317
5.5 Th and	ne boundary-layer control approximation the geodyname	321
5.5.1	Time-scale restrictions on boundary-layer	
	control in the geodynamo	21

•	`			
,		Titlé	4	Page
5.5	.2 Temporal vari magnetic dipol	ations of the	e Earth's	322
5.5		nsion of the	approximate	324
5.5.	4 "Dipole wobbl			325
	5 Axial dipole		tions	327
5.5.	6 Limitations o	n the bounda	ry-layer contro	1 ·
5.6	Summary of Chapto	er 5		332
6. ME	AN FIELD ELECTROI	DYNAMICS AND	THE HYDROMAGNET	PIC . 334
6.1	The hydromagnetic	e dynamo prol	blem	334
6.1.	1 The dynamo equ	ations		334
6.1,	2 The neglect of	inertial te	erms	336
6.1.	3. The viscous bo		the state of the s	
	4 The approximat			340
6.2 e	Solution of the a quation in a sphe	pproximate N	Javier-Stokes	343
6.2.	l Preliminary ma	nipulation		343
	2 Boundary-layer			344
6.2.		ion of the a	pproximate	348
6.3 n	emporal behaviou pole moment	r of the ext	ernal magnetic	351
6.3.1	The boundary-la	ayer control	approximation	351
6.3.2				353
6.3.3	Radial forces			357
6.3.4	Azimuthal force reversals	es, dipole w	obble, and	361

## Title

	•
6.4 Effects of an inhomogeneous turbulent force distribution outside the boundary layer in	
the geodynamo	. 371
6.4.1 The fluctuating dynamo equations	. 371
6.4.2 The first-order solution of the fluctuating dynamo equations ,	. 373
6.4.3 Helicity and <u>u'x B'</u> for a locally isotropic force distribution	. 376
6.4.4 The second-order fluctuating equations and their solutions	380
6.4.5 Second-order contributions to u'x B' in the geodynamo	383
6.4.6 The effects of locally isotropic turbulence	
in the geodynamo	396
6.5 Summary of Chapter 6	404
en e	
7. FINAL SUMMARY	406
BIBLIOGRAPHY	411
	*
APPENDIX 1 UNITS AND CONVERSION FACTORS	460
A.1.1 SI units	
A.1.2 Magnetic dipole moments	460
And the state of t	460
APPENDIX 2 MULTIPOLE MOMENTS OF CURRENTS IN A SPHERE	464
A.2.1 The multipole expansion of the external magnetic field	A.S.A.
A.2.2 The magnetic multipole moments of a spherical current distribution	464
A.2.3 Surface terms, and theorems on spherical harmonics	467

	Title	Page
	Expressions for the magnetic multipole moments	. 473
	Electric multipole moments	
, APPENDI	X 3 EVALUATION OF INTEGRALS ASSOCIATED WITH	
( )	INITIAL CONDITION I IN CHAPTER 3	476
·A.3.1	Integrals of section 3.7.4	476
A.3.2	Integrals of section 3,8,5	479
A.3.3	Integrals of section 3.9.2	482
,		
APPENDI	X 4 EVALUATION OF INTEGRALS ASSOCIATED WITH INITIAL CONDITION IF IN CHAPTER 3	485 <sup>9</sup>
A.4.1	The integrals of section 3.10.1	485
A.4.2	The nature of the program	487
A <sub>4</sub> 4.3	The program	491
A.4.4	Gaussian points and weights	511

# LIST OF TABLES

Table	Description	Page
r <sub>l</sub>	Weak astrophysical magnetic fields	4
2	Geomagnetic fields of internal origin	5
<b>' 3</b>	Planetary and lunar magnetic fields	6
4	Solar magnetic fields	7
5	Stellar magnetic fields	8
6	Quantities of interest for magnetic stars	13
7	Field-compression hypothesis, angular momentum, and dipole moment in stellar bodies	14
8	Angular momenta, dipole moments, and surface fields in planetary bodies	1/5
<b>9</b> ,	Anti-dynamo theorems for stationary magnetic fields	,33
10	Anti-dynamo(theorems for general magnetic fields	34
41	Invariance properties of different types of turbulence	90
12	Various types of stationary, homo-	149
13	Geomagnetic field of internal origin:	270
14	Temporal variations of solar magnetic fields	272
15	Temporal variations of other astro- physical magnetic fields	274

Table	Description	•	Page
16	Relationship between $\tau$ and $\lambda_{\rm C}$ implied by (5.63)	<b>5</b> .	305
17	Dependence of integrands on $\widehat{B}$ in expressions for $\widehat{u}^T x \widehat{B}^T$		401
18	Mechanical units		462
19	Electromagnetic units		463

### LIST OF FIGURES

Figure ()	Description	Page
1 1	Re $\theta(\xi,0;p)$ as a function of $\xi$ for	• •
* ,	various p	138
		•
2	θ(ξ <sub>τ</sub> ν;p) as a function of ξ and ν	
	for two values of p	140
_	<i>▶</i>	
3	$9\{[\eta_{eff}/\eta]-1\}/\{R_m^i\}^2$ as a function of	•
•	q when $\lambda_C/L = 0$	158
	$R_m^{l}$ as a function of $[\eta_{eff}/\eta]-1$ for	
	several values of $\lambda_{C}/L$ and q	
V.	(initial condition I)	162
5	${\{R_m^i\}}^2/{\{[n_{eff}/\eta]-1\}}$ as a function of	
	λ /L for several values of q when	r t
	$\eta_{\text{eff}} = 1.1  \eta$	164
•	err	
6 1	$R_{m}'$ as a function of $[\eta_{eff}/\eta]-1$ for	
	$\lambda_{C}/L = 0.3$ and $q = 10$	172
,		
7	Decay of mean field amplitude with	
\	time	180
8	Decay regimes for initial condition I	191
÷ 1,		•
9	$T^*/\tau_C$ as a function of q for	1
	several values of $\lambda_c/L$	193

Figure	Description	o <u>Page</u>
	* <b>&amp;</b>	
10	Integrands of $(3.165a)$ and $(3.165b)$ for	
,	$\lambda_{\rm C}/{\rm L} = 1.6$ and $\tau_{\rm C}/{\rm T} = 3.5 \times 10^{-4}$	<b>C</b> 213
11	Integrands of (3.165a) and (3.165b) for	
	$-\lambda_{\rm C}/L = 0.45$ and $\tau_{\rm C}/T = 3.5 \times 10^{-3}$	214
12	Integrands of (3.165a) and (3.165b) for	
	$\lambda_{\rm C}/L = 0.11$ and $\tau_{\rm C}/T = 3.5 \times 10^{1.2}$	215
<b>.1</b> 3	Integrands of (3.165a) and (3.165b) for	,
	$\lambda_{\rm C}/L = 0.07$ and $\tau_{\rm C}/T = 0.1$	216
14	Integrands of (3.165a) and (3.165b) for	,i
^	$\lambda_{c}/L = 0.053$ and $\tau_{c}/T = 1.0$	217
15	Typical convergence of the n-point	. · · · · · · · · · · · · · · · · · · ·
	Gaussian scheme used to evaluate the	<b>*</b> - :
	integrals in (3.165)	21,9
•	en e	physical and the second
1.6	Solutions of (3.165) - projection	
	onto the $[\lambda_c/L, \tau_c/T]$ plane	∠ <b>225</b> _
1		
17	Solutions of (3.165) - projection	•
	onto the $[\tau_C/T, R_m']$ plane	227
18	Socutions of (3.165) - projection	
	onto the $[\lambda_C/L, R_m^*]$ plane	229
19	Solutions of (3.165) - projection	
· .	onto the [Re $\Omega/\eta K^2$ , (Im $\Omega/\eta K^2$ )-1] plane	231

Figure	Description	Page
20	Solutions of (3.165) - projection onto the $[R_m^*, (\text{Im }\Omega/\eta K^2)-1]$ plane	233
21	Solutions of (3.165) - $(\lambda_C/L)$ and $(R_m^*/q)$ as functions of $(Im \Omega/\eta K^2)-1$	
	in the limit of small $\tau_{\rm C}^{\rm q}\eta {\rm K}^2$	236
22	Reversal rate of the geomagnetic field	
	as a function of time	280
23	Parameters for the $\alpha^2(r)$ dynamo in a spherical shell as functions of	
1	$-r_0 \alpha'' (r_0)/\alpha' (r_0)$	300

### 1. A GENERAL REVIEW OF DYNAMO THEORY

# 1.1 Astrophysical magnetic fields

### 1.1.1 Introduction, and summary of observations

Although large-scale magnetic fields have long been an important feature of both planetary physics and astrophysics, it is only in recent years that significant progress has been made in understanding how these fields are generated and maintained. In part, this improved understanding is due to a marked increase in the amount of observational data available on astrophysical magnetic fields. The fields of interest fall into four broad categories.

This category includes intergalactic, interstellar, and interplanetary magnetic fields. Of these, perhaps the most interesting from a theoretical point of view is the field of order 3-4 x 10<sup>-6</sup> G in the rotating, gaseous disk of the Galaxy.

# b. Planetary magnetic fields (Tables 2 and 3)

This category includes the poloidal surface fields of the Earth (~0.6 G at the magnetic poles) and Jupiter

In this thesis, SI units will be used as a general rule. However, astrophysical magnetic fields will often be quoted in gauss (1  $G = 10^{-4}$  tesla). See Appendix 1 for a summary of the SI system of units.

(10-50 G at the magnetic poles). None of the other planets have been observed to have magnetic fields, but Saturn, Uranus, and Neptune could have undetected fields of the order of a few gauss (see section 1.1.3). Mars, Venus, and Mercury are thought to be "non-magnetic" planets.

### c. Solar magnetic fields (Table 4)

This category includes the general background solar field (of the order of a few gauss), and the much stronger local fields (up to several thousand gauss) observed in magnetically active regions.

### d. Stellar magnetic fields (Table 5)

This dategory includes the fields observed in some bright stars (of order  $10^2$  G); the stronger fields (of order  $10^3$ - $10^4$  G) inferred from spectroscopic observation of the so-called "magnetic stars"; the still stronger fields (of order  $10^7$  G) observed in magnetic white dwarfs; and the extremely strong fields (of order  $10^{12}$  G or higher) inferred from observations of pulsars.

In this thesis we shall be concerned mainly with fields of planetary type, although the techniques employed can be applied to other types of field as well.

It should be noted that the numbers in parentheses in Tables 1-8 refer to a special section of footnotes, to be

found at the end of section 1.1.3, on pages 21-23. These footnotes give references to the literature on astrophysical magnetic field.

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TABLE 1
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Location	Strength (µG=10-10T)	Spatial structure	Possible source(s)
Intergalactic space (1)	<0.02	Disordered	a) "Primeval" fields b) Stretched-out galactic fields
Galactic corona (2)	0,3-1	Unknown	a) Stretched-out galactic fields b) Compressed intergalactic fields
Galactic disk (3)	κ. 	Probably a spiral structure with lines of force directed along the galactic arms. There is a fluctuating component, probably of the same magnitude as the spiral field.	ynam onun yclo tret ield
Supernova remnants (4)	40-300	Unknown	a) Stretched-out pulsar fields b) Compressed interstellar fields
Other galaxies (5)	up to 1000	Unknown	Dynamo action (??)
Quiet interplane- tary space (6)	5000 (at 1 AU)	Spiral structure centered on the Sun, extending out to 30 AU or more, There is a superimposed fluctuating component,	Stretched-out solar fields
	n i		

GEOMAGNETIC FIELDS OF INTERNAL ORIGIN TABLE 2

Location	Strength (G=10-4 T)	Spatial structure	Probable source
Surface (7) dipole field (at magnetic poles non-dipole field	0.6	Mainly dipolar, with dipole axis inclined about 11.5° to axis of rotation at the present time. Field averages to an axial dipole within 2.7 x 104 yr., and to a geocentric axial dipole within 2 x 106 yr. Average field has been an axial dipole for at least 2-3 x 109 yr.	Dynamo action in the fluid core of the Earth. (But see Lyttleton, 1970!)
Core-mantle inter- face poloidal [extra- polation of surface fields (8)] toroidal [estimate (9)]	5-6(?)	Probably mainly poloidal, with the non-dipole field of the same order as or greater than the dipole field.  Small toroidal component due to non-zero conductivity of lower mantle	Dynamo action in the fluid core
Core [various estimates (10)]	50-500	Probably mainly toroidal	Dynamo action in the fluid core

TABLE 3 - PLANETARY AND LUNAR MAGNETIC FIELDS

Location	Strength (G=10-4 T)	Spatial structure	Possible source(s)
Jupiter (11)	·	On the contract of the contrac	201200000000000000000000000000000000000
te) and the		ineld is a centred inclined about	a) Dynam
magnetic poles)	000	tifit to	CORP (S
interior (estimate)	71000	gipe	â
		Observations). Non-dipole   field is much smaller in	here (but
· · · · · · · · · · · · · · · · · · ·	Ġ	proportion than that for the	conductivity is probab-
•		Farth. Interior field is   probably mainly toroidal	
Saturn - surface	\$ 1(?)	d exists	'
		th	7 -
Uranus - gurface			Probably not present(?)
0	\$ (25)	If fields exist, they are probably similar to that of	acti if on
Marke Contraction		4	į
ן אַאַ	<0.001	(Mariner 4 observations)	
Venus - surface (15)	<0.0004	(Venera IV observations)	nt is
Mercury - surface	little or none		interplanetary field.
Lunar surface			
magnetizing field	J. 02-0 05	~	a) Ancient dynamo action
implied by remanent		(Possible sources listed at	b) Long-term immersion in
magnerization (L7)	÷:	right apply to this field!	geomagnetic
	<2 × 10 <sup>-6</sup>		field at some time in
(18)			c) High-velocity meteorid
č			impacts(?)

TABLE 4 - SOLAR MAGNETIC FIELDS

Location	Strength (G= 10-4T)	Spatial structure '	*Possible source(s)
Global fields in photosphere	-		
axial field (19)	. 1-2	Usually	
•		be roughly dipolar within 35° of the poles,	
"sector structure"	€ V '	Variable, Indirect measure-	a) Dynamo action in the solar convection zone
(67)		ments imply a persistent quadrupole moment nartly ob-	
		scured during active portions	b) Deep-seamed magnetic sources"
	•	of the solar cycle. There is also some evidence that the	
		quatorial dipole at tin	, p
Local fields in photosphere (21)	1-5000	variable, filame	Eruption and compression of strong internal fields
Internal fields [theoretical estimates (22)]	several hundred to a thousand	In convection-zone dynamo, theories, internal fields are mainly toroidal, and are confined to the region within	Dyn
	1	0.1R <sub>0</sub> from the solar surface. "Deep-seated field" theory requires a much deeper pene-	"Deep-seated magnetic sources"

TABLE 5 - STELLAR MAGNETIC FIELDS

	Strength (G= 10-4T)	Spatial structure	Possible source(a)
23)		1 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	/ J ) 45 00 0 1 R   0 1
	30-300	Dipolar(?)	Dynamo action in stellar interior (2)
surrace fields (24)	500-1000	Dipolar(?)	Dynamo action in stellar interior (?)
Ap stars (25) surface fields 10	1000-34000	Dipolar, with cinclined to axi (typically ~80°	a) Dynamo action in stellar interior
			b) Cómpressed "fossil" fields
interior fields up (estimated)	up to 10 <sup>10</sup> (?)	Probably ma	
White dwarfs (26) <1	<1-2 x 10 <sup>5</sup>	If fields exist, they may be dipolar.	
Magnetic white dwarfs (27)	,		a) Compressed "fossil" fields
surface fields	-10 <sup>8</sup>	Axisymmetric or inclined dimole(2)	b) Dynamo action(??)
interior fields up (estimated)	up to $10^{12}$ (?)	Probably mainly toroidal	•
Pulsars (28) surface fields 10	1011-1014	Dipolar, with dipole axis inclined to axis of rotation	Compressed "fossil" fields (possibly from magnetic white dwarf stage). Dynamo
<pre>interior fields (estimated)</pre>	>1016(?)	Probably mainly toroidal	action is not possible in present theoretical models since convective fluid
			motions damp out within seconds of neutron star formation,

# 1.1.2 Dynamo theory and astrophysical magnetic fields

The connecting link between the various types of magnetic field mentioned in section 1.1.1 is the presence of a conducting fluid medium - e.g. planetary fluid cores, conducting planetary atmospheres, stellar atmospheres, and the interstellar gas. This observation leads to the conjecture, first advanced by Larmor (1919), that the fields are hydromagnetić in origin. Evidence in support of this conjecture is provided by the fact that some of the fields vary in a complicated way with time. The Earth's magnetic field, for example, has existed in roughly its present form for at least 2.5-2.7 x 10 9 years (McElhinny and Evans, 1968), but archaeo- and palaeomagnetic observations indicate that the field fluctuates on a wide range of time scales, and reverses its polarity at irregular intervals (Bullard, 1968; Braginskii, 1970b, 1971; McElhinny, 1971). These consideran tions effectively rule out any possibility that the geomagnetic field is due to permanent magnetism (Bullard, 1948, 1949; Rikitake, 1966a, p. 13ff.), and make it highly unlikely that the field is due to intrinsic "rotational" magnetism (see section 1.1.3). Attention is therefore focussed on electric currents in the Earth's fluid core as the source of the field. The most likely source of the electromotive force needed to maintain these currents for times long compared with the ohmic decay time  $(10^4-10^5 \text{ years})$  is the motion of cofe material across the geomagnetic lines of

force. The study of this process, in which the currents generated reinforce the magnetic field which gives rise to the driving e.m.f., is known as the "homogeneous dynamo problem".

Not all astrophysical magnetic fields are maintained by "dynamo action". In pulsars (neutron stars), for example, "...most internal motions except for axially symmetric differential rotation are damped out...within a few seconds after [the] neutron star is formed" (Ruderman, 1972). Differential rotation of this type will convert poloidal lines of force into toroidal lines of force, and build up extremely large internal toroidal fields, but the motion cannot regenerate the poloidal field from the toroidal (Elsasser, 1947, 1950). Dynamo action will therefore not occur.

It is generally thought that "...the initial magnetic field of a pulsar is...a compressed fossil field conserving the flux already present in its parent star core before collapse" (Ruderman, 1972). In support of this hypothesis it is argued that the product BR<sup>2</sup> (where B is a typical poloidal magnetic flux density, and R the stellar radius) is approximately the same for magnetic stars, magnetic white dwarfs, and pulsars. The evidence in support of this claim is summarized in the first column of Table 7. Values of BR<sup>2</sup> for Ap stars, magnetic white dwarfs, and pulsars range over three orders of magnitude; however, the ranges for

magnetic white dwarfs and pulsars are very nearly the same. One difficulty with the argument is the scarcity of magnetic white dwarfs. Only four of the more than fifty white dwarfs which have been identified have observable magnetic fields. Any fields present in the "normal" white dwarfs must be less than 1-2 x 10<sup>5</sup> G (Angel and Landstreet, 1970; Preston, 1970; Trimble and Greenstein, 1972). As indicated in Table 7, fields of this size are at least one order of magnitude too small to become pulsar fields under "flux-conserving compression".

It is argued by some workers (e.g. Mestel, 1971) that all large stellar fields are compressed "fossil fields".

However, dynamo models have been proposed for magnetic stars (e.g. Krause, 1971). "Small" stellar fields like that of the Sun, on the other hand, are generally thought to be due to dynamo action because of their extreme complexity and variability. However, some authors (e.g. Piddington, 1972c) feel that dynamo action is an insufficient explanation even for solar magnetic fields.

A similar situation exists with regard to the Galactic magnetic field. One school of thought (e.g. Parker, 1969a, 1971a) claims that the field in the galactic disk is maintained by dynamo action associated with turbulent motion, while another (e.g. Piddington, 1972a,b) argues that the field is more likely to be a compressed "primeval" field.

The remaining class of fields - planetary magnetic fields - is almost universally thought to be generated by dynamo action (see, however, Lyttleton, 1970, and section 1.1.3). In the remainder of this chapter we shall consider the homogeneous dynamo theory as it applies to planetary fields, with particular emphasis on the magnetic field of the Earth.

c .			<b>~</b>	_	
Star	Rotation period	Surface field (G = 10-4T)	R. R.	M/M®	1 (kg-m <sup>2</sup> )
Sun (29)	26d	<b>-1</b>			6 x 10 <sup>4</sup> 6
YCYG (30)	, 2-3d (??)	200	70	10.	В
Sirius (30)	64 (22)	500	2,2	m	
Ap stars (31)	[1.7-2500]a	[1-34]x 10 <sup>3</sup>	[1-4]	[1-5]	
typical values	6.5d	2.5 x 10 <sup>3</sup>	3.2	m	,
White dwarfs (32)	¥ ~	<[1-2]x 10 <sup>5</sup>			
Magnetic white dwarfs (32)	<b>C</b> •	1106-1081	[0,0089-0,013]	[0.65-0,87]	
typical Values		107	0.011	0.76	
Rotating magnetic white dwarfs [one known] (33)	1,34d	107	0.013(2)	[1-4] (?)	
Puffars (34)	[0.03-3.7]s	[0.5-50]x 10 <sup>12</sup>	[2-1]x 10 <sup>-5</sup>	[0.15-2]	[0.7-7]× 1037*
Crab pulsar	0.0338	2 x 10 <sup>12</sup>	1.7 x 10 <sup>-5</sup>	m •	$0.9 \times 10^{37}$

QUANTITIES OF INTEREST FOR MAGNETIC STARS

TABLE 6

M = stellar mass
R, F stellar radius
I = moment of inertia

ubscript "@" refers to values for Sun.

ANGULAR MOMENTUM, FIELD-COMPRESSION HYPOTHESIS,

PODITEC	
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3 MOMENT IN	
DIPOL	
AND	I

	;		
Star	[B/B <sub>0</sub> ][R/R <sub>0</sub> ] <sup>2</sup>	[1/7]	1
Sun		• •	E C C C C C C C C C C C C C C C C C C C
YCYG	980 x 10 <sup>3</sup>	~ 8 × 10 <sup>-3</sup> (2)	7.01
Sirius	2.4 × 10 <sup>3</sup>	6 2 16 3 23	0.11(2)
Ap stars	11-501 < 103	(2) (2)	0.08(?)
typical values	26 x 10 <sup>3</sup>	2 × 30 -3 2 × 30 -3	[1.5 × 10 -2-1]
White dwarfs	<0.02 × 10 <sup>3</sup>		70:0
Magnetic white dwarfs	10.08-181 × 103	-	
typical values	1 × 10 3	~5 x 10 <sup>-4</sup> (?)	(0) (0)
Pulsars (35)	all [0.05-5] x 10 <sup>3</sup>	4-7	
		$\frac{(1.5 \times 10^{-5})}{-1.5 \times 10^{2}}$	$[2 \times 10^{-3} - 2 \times 10^{3}]$
Crab pulsar	0.6 × 10 <sup>3</sup>	1 x 10 <sup>-2</sup>	. 0
			f • • • • • • • • • • • • • • • • • • •

Subscript "0" refers to Sun; subscript "E" to Earth. B = surface flux density M = mass; R = radius; = magnetic dipole moment. J = angular momentum;

 $V_{\rm M}(M/M_{\odot}) (\Omega/\Omega_{\odot})/(B/B_{\odot}) (R/R_{\odot})$  where  $\Omega$  = rotation frequency, I = moment of inertia  $\mathrm{JT}_{\Theta}^{\left(1
ight)}/\mathrm{J}_{\Theta}\mathrm{T}^{\left(1
ight)}\sim\left(\mathrm{I/I}_{\Theta}
ight)\left(\mathrm{\Omega/\Omega}_{\Theta}
ight)/\left(\mathrm{B/B}_{\Theta}
ight)\left(\mathrm{R/R}_{\Theta}
ight)$ 

$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		NE VETTO CAT	OTIC TINE	MISSIER MOMENTS, AND SURFACE FIELDS IN	SURFACE FIEL	S IN PLANETA	PLANETARY BODIES
(6) 1.4 x 10 <sup>3</sup> 7.3 x 10 <sup>4</sup> [0.5-1] x 10 <sup>5</sup> [0.7-1.5] [36-72] (7) 8.5 x 10 <sup>2</sup> 1.2 x 10 <sup>4</sup>	Body	$[R/R_{\rm E}]^3$	J/J.	$/T_{\rm E}^{(1)}$ obs	JT (1) /JET (1)	[B/B <sub>F</sub> ] <sub>obs</sub>	[B/B <sub>P</sub> ]
8.5 x 10 <sup>2</sup> 1.2 x 10 <sup>4</sup>	Jupiter (36)		7.3 x 104	1	[0,7-1,5]	[36-72]	52
8) $4.3 \times 10^{1}$ $3.3 \times 10^{2}$	Saturn (377)	8.5 x 10 <sup>2</sup>	1.2 x 2.04		ı		14
8) $4.3 \times 10^{1}$ $4.0 \times 10^{2}$	Jranus (38)	<u> </u>	3,3 × 10 <sup>2</sup>	,	,	1	6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Neptune (38)	4.3 × 10 <sup>1</sup>	4.0 × 1.0 <sup>2</sup>			1	9
8.8 $\times^{10^{-1}}$ ~ 3 $\times$ 10 <sup>-3</sup> <1 $\times$ 10 <sup>-3</sup> >3 <1 $\times$ 10 <sup>-3</sup> 1.5 $\times$ 10 <sup>-4</sup> 1.5 $\times$ 10 <sup>-1</sup> 3.5 $\times$ 10 <sup>-5</sup> (3 $\times$ 10 <sup>-4</sup> 7.5 $\times$ 10 <sup>-7</sup> (5 $\times$ 10 <sup>-7</sup> (5 $\times$ 10 <sup>-7</sup> (5 $\times$ 10 <sup>-6</sup> (5	arth	-1	, <sub>[</sub> -1	П			-
1.5 x 10 <sup>-1</sup> 3.5 x 10 <sup>-2</sup> <3 x 10 <sup>-4</sup> >120 <2 x 10 <sup>-4</sup> 41) 5.5 x 10 <sup>-1</sup> ~ 9 x 10 <sup>-5</sup>	enus (39)	8.8 × 10 <sup>-1</sup>	m	1	>3	<1 × 10-3	0.03
41) 5.5 x 10 <sup>-1</sup> ~ 9 x 10 <sup>-5</sup> - ;	lars (40)	1.5 x 10-1	3.5 x 10 <sup>-2</sup>	1	>120	<2 × 10-4	*0.2
2.0 x 10 <sup>-2</sup> 4.0 x 10 <sup>-5</sup> <5 x 10 <sup>-8</sup> > >800	dercury (41)	i	~ 9 x 10-5				2 × 10-4
	loon (42)	$2.0 \times 10^{-2}$	4.0 x 10-5	<5 × 10 8	008< -	<3 x 10 6.	2 × 10 -3

refers magum; T(1) = magnetic dipole moment; B = surface
Subscript("E" refers to Earth, Subscript "obs" (I) J = angular momentum; (assumed dipolar). to observed values. netic field R = radius;

 $[B/B_E]_{pred} = value predicted by Schuster's hypothesis = <math>(J/J_E)/(R/R_E)$ 

8.0 x 10<sup>22</sup> A·m<sup>2</sup> 21 T<sub>E</sub>(1)

5.9 x 10<sup>33</sup> St

## 1.1.3 Schuster's hypothesis

must consider the possibility of intrinsic "rotational" magnetic fields. The conjecture that astrophysical fields are a necessary consequence of rotation has been advanced several times in the last 60 years (Schuster, 1972; Wilson, 1923; Blackett, 1947, 1949; Milne, 1950; Papapetrou, 1950; Luchak, 1951; Moroz, 1967; Surdin, 1971; see the discussion in Rikitake, 1966a, p. 18). Interest has persisted despite Blackett's experimental demonstration that the hypothesis in its original form is false (Blackett, 1952). The basic claim is that

$$_{\rm J/T}^{(1)}$$
 = constant

where J is the angular momentum of the body and T<sup>(1)</sup> the magnetic dipole moment. This relationship will be referred to as "Schuster's hypothesis" (Warwick, 1971).

Using Schuster's hypothesis, Blackett (1947) was able to predict surface magnetic fields of 30 G for Jupiter and 3 x 10<sup>6</sup> G for white dwarfs - values which are not unreasonable in the light of recent observational evidence.

Warwick (1971) has examined the relationship between angular momentum and dipole moment in astrophysical bodies, and has concluded that Schuster's hypothesis is not inconsistent with the observational data. He suggests that the Moon is the body most likely to provide a critical test of the hypothesis.

Since only surface fields are directly observable, it is necessary to write Schuster's hypothesis in a modified form. For a dipole magnetic field, the flux density at radius R and magnetic co-latitude  $\theta$  is

$$B(R,\theta) = (\mu/4\pi R^3) T^{(1)} \{1 + 3\cos^2\theta\}^{1/2}$$

where µ is the magnetic permeability. The angular momentum of a body is given by

$$J = I\Omega$$

where  $\Omega$  is the rotation frequency and I the moment of inertia. If it is assumed that  $\mu=\mu_0=\text{constant}$ , and that all magnetic fields are evaluated at the same value of  $\theta$ , Schuster's hypothesis can be rewritten

$$I\Omega/BR^3$$
 = constant

where R is identified as the radius of the body in question. In this form, the hypothesis can be applied directly to the data available for planetary and stellar bodies.

Since Warwick's paper was written, new data have become available, particularly for the Moon (Sharp, Russell, and Coleman, 1973). Furthermore, Warwick uses a value for the dipole moment of Mars which is considerably in excess of the estimate given by Smith, et al. (1965; see Michaux, 1967, p. 51), even though both values are derived from the data provided by Mariner 4. (Warwick's value of the Mars/Earth dipole moment ratio is < 0.01, while that of Smith, et al. is < 0.0003.) The revised evidence to be used as a test

of Schuster's hypothesis is presented in the fourth column of Table 8. The observed values of the angular momentum/dipole moment ratio for planetary bodies span nearly three orders of magnitude. It would therefore appear that Schuster's hypothesis is incorrect. This conclusion is in agreement with Blackett's experimental result (Blackett, 1952).

Values for the angular momentum/dipole moment ratio for stellar bodies are given in the last two columns of Table 7. In most cases (pulsars being the exception) a crude estimate of angular momentum has been obtained by making use of the relationship

$$I \propto MR^2$$
.

M is the mass of the body concerned, and the constant of proportionality depends on the internal density distribution. Assuming that the constant of proportionality in each case is the same as that for the Sun, we may write Schuster's hypothesis as

 $[M/M_{\odot}][\Omega/\Omega_{\odot}]/[B/B_{\odot}][R/R_{\odot}] \sim 1$ 

where the subscript 0 refers to solar values. From the last column of Table 7 it will be seen that when the stellar values of  $[J/T^{(1)}]/[J_E/T_E^{(1)}]$  are added to the list of planetary values given in Table 8, the range spanned increases to nearly 5 orders of magnitude. (N.B. The subscript "E" refers to values for the Earth.)

The possibility remains, however, that Schuster's hypothesis is useful as an empirical relationship between the magnetic fields of bodies in which the physical conditions are not grossly different. Warwick (1971) has drawn attention to the close agreement between the values of for the Earth and Jupiter. Scarf (1972) has used Schuster's hypothesis to predict the magnetic field of Saturn from that observed for Jupiter, and concludes that the field e obtains (a polar field of 2 G, based on Warwick's (1963) value of 10 G for the field of Jupiter) is not inconsistent with radio observations. A further estimate could be made to predict the fields of Uranus and Neptune (~2 G for a 14 G field on Jupiter, and ~7 G for a 50 G field on Jupiter; see Table 8). However, this approach carries with it all the dangers of "geophysical numerology" (Jacobs, 1970a), and should be used with extreme caution.

It is interesting to note that Schuster's hypothesis is not consistent with both the "flux-conserving compression" hypothesis for the evolution of magnetic stars, and the conservation of angular momentum. Assuming both Schuster's hypothesis and the "flux-conservation" hypothesis to be valid, so that J/BR<sup>3</sup> and BR<sup>2</sup> are conserved, we find that J/R must be conserved as well. A stellar contraction would therefore have to be accompanied by a loss of angular momentum proportional to the change in radius. On the other

hand, if we assume both Schuster's hypothesis and the conservation of angular momentum to be valid, we see that  $BR^3$  must be conserved in place of  $BR^2$ . It will be seen from the first column of Table 7 and the values of  $R/R_{\odot}$  given in Table 6 that the spread of values of  $[B/B_{\odot}][R/R_{\odot}]^2$  is much less than that for values of  $[B/B_{\odot}][R/R_{\odot}]^3$ .

#### FOOTNOTES: TABLES 1 TO 8

- (1) Brecher & Blumenthal (1970); Parker (1970a); Kaplan & Pikel'ner (1970, p. 393).
- (2) Ginzburg (1970); Kaplan & Pikel'ner (1970, p./277).
- (3) Pikel'ner (1968); Verschuur (1969); Parker (1969a, 1970a, 1971a, 1972); Jokipii & Parker (1969b); Jokipii & Lerche (1969); Piddington (1972a,b); Michel & Yahil (1973); Moffatt (1973).
- (4) Mustel (1970); Woltjer (1972).
- (5) Parker (1970a).
- T(6) Wilcox (1968); Ness (1968); Jokipii & Parker (1969a); Schatten (1971); Stenflo (1971); Sari & Fisk (1973).
- (7) McElhinny & Evans (1968); Opdyke (1972); Roberts & Soward (1972),
- (8) Lowes (1972); Roberts & Soward (1972).
- (9) The toroidal field was estimated by making use of expressions given by Rochester (1960).
- (10) Bullard & Gellman (1954); Hide (1966a); Braginskii (1971); Roberts & Soward (1972); Busse (1973b).
- (11) Warwick (1963, 1967); Hide (1966b, 1969b, 1971a); Schatten & Ness (1971); Smoluchowski (1971, 1972).
- (12) Smoluchowski (1971, 1972); Scarf (1972); Moffatt (1973).
- (13) Moffatt (1973).
- (14) Smith, et al. (1965); Michaux (1967).
- (15) Koenig, et al. (1967); Van Allen, et al. (1967); Bridge, et al. (1967); Herman, et al. (1971).
- (16) Banks, et al. (1970); Ness & Whang (1971).
- (17) Helsley (197**%)**; Hide (1972); Coleman, Russell, Sharp, & Schubert (1972); Strangway & Sharpe (1973).
- (18) Coleman, Schubert, Russell, & Sharp (1972); Sharp, Russell, & Coleman (1973).

- (19) Parker (1970b); Kopecký (1970); Severny (1971); Stenflo (1972); Piddington (1972c).
- (20) Severny, et al. (1970); Altschuler, et al. (1971); Wilcox & Gonzales (1971); Wilcox (1972); Svalgaard (1973); Patterson (1973); Schulz (1973).
- (21) Weiss (1971a,b); Howard & Stenflo (1972).
- (22) Parker (1970b); Weiss (1971a,b, 1972); Yoshimura (1972); Piddington (1972c); Moffatt (1973).
- (23) Severny (1970, 1971).
- (24) Severny (1970); Weiss (1971b).
- (25) Ledoux & Renson (1966); Preston (1967a,b, 1971a,b);
  Landstreet (1970); Mestel (1967, 1971, 1972 see
  Moffatt 1973); Spiegel (1972 see Moffatt, 1973);
  Mestel & Takhar (1972); Raychaudhuri (1972).
- (26) Angel & Landstreet (1970); Preston (1970); Trimble & Greenstein (1972).
- (27) Kemp (1970); Kemp, et al. (1970); Angel & Landstreet (1971); Landstreet & Angel (1971).
- (28) Ostriker & Gunn (1969); Gunn & Ostriker (1970, 1971); Cameron (1970); Hewish (1970); Ruderman (1972).
- (29) Allen (1963).
- (30) Allen (1963); Severny (1970, 1971).
- (31) Allen (1963); Preston (1967a,b, 1971a); Eggen (1967); Mestel (1967).
- (32) Ostriker (1968); Trimble & Greenstein (1972); Shipman (1972). See note (26) for further references.
- (33) Ostriker & Bodenheimer (1968); Schwartz & Africk (1970); Ostriker (1971).
- (34) Ostriker & Gunn (1969); Ruderman (1972); Greenstein (1972). See note (28) for further references.
- (35), Ruderman (1972).
- (36) Allen (1963). See note (11) for further references.
- (37) Allen (1963). See note (12) for further references.

- (38) Allen (1963); Moffatt (1973).
- (39) Allen (1963); Dyce, et al. (1967); Shapiro (1967); Ash, et al. (1968); Melbourne, et al. (1968); Jurgens (1970); Anderson, et al. (1970). See note (15) for further references.
- (40) Allen (1963); Smith, et al. (1965); Michaux (1967).
- (41) Allen (1963); Dyce, et al. (1967).
- (42) Allen (1963). See note (18) for further references.

#### 1.2 The homogeneous dynamo problem

(5)

Theoretically, the homogeneous dynamo problem involves the solution of a highly complicated system of coupled partial differential equations. The best treatment of the derivation of these equations is that given by P.H. Roberts (1967a). The outline given here is based on his approach.

The equations fall into four major groups, which will be considered separately.

- a. The electrodynamic equations. These include

  Maxwell's equations, the constitutive relations among
  the various electric and magnetic fields, Ohm's Law,
  and the transformation relating the fields observed in
  one reference frame to those observed in another in
  relative motion.
- b. The hydrodynamic equations. These include the equations of conservation of mass and conservation of momentum, and the constitutive equation for the total stress tensor.
- c. The thermodynamic equations. These include the postulate of local thermodynamic equilibrium, the equation of heat conduction, and the constitutive law for the heat conduction vector. When combined with (a) and (b) above, these equations lead to a detailed description of energy flow within the system considered.
- d. The boundary and initial conditions.

been attacked on three levels, corresponding to the first three groups of equations listed above. On the first level we have the kinematic dynamo problem, in which the fluid velocity is specified (independent of the magnetic field), and the electrodynamic equations are considered on their own. On the second level we have the hydromagnetic dynamo problem, in which the driving forces are specified (independent of the velocity and magnetic fields), and the electrodynamic and hydrodynamic equations are considered together. Finally, we have the full hydromagnetic dynamo problem, in which all three groups of equations are taken into consideration. In this thesis, we shall be concerned mainly with the first two levels of attack.

#### 1.3 The kinematic dynamo problem

#### 1.3.1 The dynamo equations

Let us first consider the kinematic dynamo problem.

The form of Maxwell's equations appropriate to a moving conductor is:

$$\operatorname{curl} H = j + \theta u + \partial D/\partial t \qquad (1.1)$$

$$\operatorname{curl} \, \mathbf{E} = - \, \partial \mathbf{B} / \partial \mathbf{t} \tag{1.2}$$

$$div B = 0 ag{1.3}$$

$$div_{\underline{D}} = \theta ag{1.4}$$

where E is the electric field, B the magnetic flux density, D the electric displacement, H the magnetic field, j the electric current density, 0 the charge density, and u the velocity of the medium. We shall assume that the constitutive equations for H and D are isotropic:

$$\mathbf{H} = \mathbf{B}/\mathbf{\mu} \tag{1.5}$$

$$D = \epsilon E$$

where  $\mu$  is the magnetic permeability and  $\epsilon$  the permittivity. In this thesis we shall use SI units (see Appendix 1) and assume that  $\mu = \mu_0 = 4\pi \times 10^{-7} \, \text{H} \cdot \text{m}^{-1}$  everywhere.  $\epsilon$  will be assumed constant for each material considered.

Ohm's Law, which should be valid in a frame moving locally with the medium whenever the particle density is

"sufficiently great" (see the discussion in P.H. Roberts, 1967a, p. 9), is

$$j' = \sigma E' \qquad (1.7)$$

where the conductivity  $\sigma$  is assumed isotropic. Primes are used to denote fields observed in the frame moving with the medium.

The equations relating the fields observed in two frames in relative motion are (Landau and Lifshitz, 1951, \$3-10; P.H. Roberts, 1967a, p. 10)

$$\mathbf{E}' = \mathbf{v}_{\mathbf{u}} \left\{ \mathbf{E} + \mathbf{u} \times \mathbf{B} \right\} + (\mathbf{I} - \mathbf{v}_{\mathbf{u}}) \frac{\mathbf{u} \cdot \mathbf{E}}{\mathbf{u}^2} \mathbf{u}$$
 (1.8)

$$\underline{B}' = \kappa_u \left\{ \underline{B} - \frac{\underline{u} \times \underline{E}}{\underline{c}^2} \right\} + (1 + \kappa_u) \frac{\underline{u} \cdot \underline{B}}{\underline{u}^2} \underline{u} \qquad (1.9)$$

where c is the speed of light, and

6

$$\mathcal{S}_{u} \equiv \left\{1 - \frac{u^{2}}{c^{2}}\right\}^{-\frac{1}{2}} \tag{1.10}$$

Substituting (1.5) and (1.6) into (1.1) and rearranging terms, we have

$$j = \frac{1}{\mu} \text{ curl } \vec{B} - \theta \vec{u} = \epsilon \vec{\partial} \vec{E} / \partial t$$

In the moving system, this equation reduces to

or, making use of (1.7)-(1.9),

$$-\epsilon \frac{9\epsilon}{9} \left\{ \hat{x}^n (\tilde{E} + \tilde{h} \times \tilde{B}) + (1 - \hat{x}^n) \frac{n_3}{\hbar \cdot \tilde{E}} \tilde{n} \right\}$$

$$= \frac{1}{\mu} \operatorname{crul} \left\{ \hat{x}^n \tilde{B} - \hat{x}^n \frac{c_4}{\hbar \times \tilde{E}} + (1 - \hat{x}^n) \frac{n_3}{\hbar \cdot \tilde{B}} \tilde{n} \right\}$$

$$Q \hat{x}^n (\tilde{E} + \tilde{h} \times \tilde{B}) + Q (1 - \hat{x}^n) \frac{n_4}{\hbar \cdot \tilde{E}} \tilde{n}$$

Rearranging terms,

$$+ (1-x^n) \in \frac{9t}{9t} \left[ \frac{n_1}{n_2} \tilde{n} \right] + (1-x^n) \in \frac{9t}{9t} \left[ \frac{n_2}{n_2} \tilde{n} \right] + \left\{ \frac{1}{\mu} \tilde{\Delta} x^n \times \tilde{B} - \frac{1}{\mu} x^n \tilde{\Delta} \times \left( \frac{c_2}{n_2} \right) + \frac{1}{\mu} \tilde{\Delta} \times \left[ (1-x^n) \frac{n_2}{n_2} \tilde{n} \right] + \left\{ \frac{1}{\mu} \tilde{\Delta} x^n \times \tilde{B} - \frac{1}{\mu} x^n \tilde{\Delta} \times \left( \frac{c_2}{n_2} \right) + \frac{1}{\mu} \tilde{\Delta} \times \left[ (1-x^n) \frac{n_2}{n_2} \tilde{n} \right] \right\}$$

$$(1-11)$$

## 1.3.2 The quasi-steady approximation

In the quasi-steady approximation ( H. Roberts, 1967a, pp. 8-11), only the terms in the first set of braces in (1.11) are retained. Justification for this step is obtained by examining the scaling of the various terms. We assume that all the fields vary significantly on a length scale L and a time scale T, and replace space and time derivatives with  $\frac{1}{L}$  and  $\frac{1}{T}$  respectively. Further, we assume that

and that

$$\epsilon \sim \epsilon_0 = (\mu_0 c^2)^{-1}$$

Then, from (1.2),

$$|\underline{E}| \sim |\underline{B}| \cdot (L/T)$$

and the three sets of braces in (1.11) have the ratio

$$(1 + R_{\rm m}) : (L/cT)^{\frac{2}{3}} (1 + R_{\rm m}) : (L/cT)^{\frac{4}{3}} (1)$$

where

$$R_{\rm m} = \mu \sigma \mathbf{u} L = \frac{1}{\eta} \mathbf{u} L \qquad (1.12)$$

is a magnetic Reynolds number for the system, and

$$\eta = 1/\mu\sigma \tag{1.13}$$

is the magnetic diffusivity. If  $(L/cT)^2$  is small compared with unity - i.e. if the electromagnetic and velocity fields change very little in the time it takes light to cross the system - only the first set of terms in (1.11) need be retained, giving the equation

$$\eta \text{curl}$$
,  $B = E + u \times B_{\alpha}$  (1.14)

Similarly, the terms in equation (1.1) have the ratio

$$\{|\underline{B}|/\mu L\}: \{|\underline{j}|\}: \{(\underline{L}/c\underline{T})^{2}[|\underline{B}|/\mu L]\}: \{(\underline{L}/c\underline{T})^{2}[|\underline{B}|/\mu L]\}$$

so that, ignoring terms of order (L/cT)<sup>2</sup>,

$$j = \frac{1}{u} \operatorname{curl} B = \sigma(E + u \times B) \qquad (1.15)$$

Equation (1.15) gives the form of Ohm's Law in the laboratory frame appropriate to the quasi-steady approximation.

#### 1.3.3 The magnetic induction equation

Taking the curl of equation (1.14) and making use of equation (1.2), we obtain the equation

$$\frac{\partial B}{\partial t} + \text{curl}(\eta \text{ curl } B) = 0$$

If  $\eta$  is independent of position, (1.16) becomes

$$\frac{\partial B}{\partial t} - \eta \nabla^2 B = 0$$

(1,16')

(1.16') is generally referred to as the magnetic induction equation.

Equations (1.3) and (1.16), together with the boundary and initial conditions and a specification of the velocity field u, provide a description of the kinematic dynamo problem in its simplest form. More generally, the kinematic dynamo problem involves finding a pair of fields (u, B) which satisfy (1.3), (1.6), the boundary and initial conditions, and certain additional conditions which are described in section 1.4.1.

It should be noted (Krause, 1968a, b; G.O. Roberts, 1970a, b) that equation (1.3) can be regarded as an initial condition. The divergence of (1.16) or (1.16') gives

$$\frac{\partial}{\partial t} [\text{div B}] = 0$$

If  $\text{div } \mathbf{B} = 0$  initially, this equation has the unique solution  $\text{div } \mathbf{B} = 0$  for all time.

#### 1.4 Solutions to the kinematic dynamo problem

# 1.4.1 Requirements on solutions

A "solution" to the kinematic dynamo problem consists of a pair of fields  $(\underline{u}_v \ \underline{B})$  which satisfy the following conditions:

- a. w is an allowable flow (Gibson and Roberts, 1967;

  P.H. Roberts, 1967a, p. 66). In an allowable flow, the velocity gradients are everywhere finite, and the equation of continuity is satisfied everywhere without sources or sinks of mass. It must be possible to define non-singular distributions of body force and density which will generate the flow through the ordinary Navier-Stokes equation, but the flow is not required to satisfy the hydromagnetic Navier-Stokes equation (see section 1.5.2).
- b. B is a field satisfying the magnetic induction equation (1.16), subject to the boundary and initial conditions.
- medium, the magnetic energy stored in V

$$\int_{V} \frac{B^2}{2\mu} dx$$

remains constant, grows with time, or oscillates about a mean value which itself remains constant or grows with time.

d. The total kinetic energy in the system

$$\int_{0}^{\frac{1}{2}} Pu^{2} dr$$

is bounded (Childress, 1968).  $\rho$  is the density of the conducting fluid.

In section 1.9.1, some of the mathematical implications of these equations will be examined in detail.

#### 1.4.2 Anti-dynamo theorems

Numerous anti-dynamo theorems have been proved, placing further explicit restrictions on the nature of u and band to

B. These theorems, which are summarized in Tables (, indicate that magnetic fields with a "simple" structure cannot, in general, be maintained by a dynamo process.

"...appear to be essential for any satisfactory dynamo theory". These features are summarized as follows by Weiss (1971b):

"...first, the velocity cannot be wholly irregular, for 'order does not arise spontaneously out of chaos'; secondly, two separate types of ordered motion should be present; and, thirdly, there should be an adequate dissipative methanism."

These requirements should be kept in mind as we examine the various types of dynamo mechanism which have been proposed.

ANTI-DYNAMO THEOREMS FOR STATIONARY MAGNETIC FIELDS σ TABLE

B) with the following characteristics cannot be solutions to the 1 3B/3t = kinematic dynamo problem, if it is required that Pairs of fields (w,

Vol. 24:20 Lav	מ אינוש	Na forences
₹ Zaracra	₹ Fataman vnat	
Arbitrary	Axisymmetric	Cowling (1933, 1957, 1668)
Arbitrary	Two-dimensional	Cowling (1957); Lortz <sup>( (1968a)</sup>
Arbitrary	Poloidal	see Childress (1968)
Arbitrary	Toroldal	see Childress (1968)
Radial, vanishing at boundary	Arbitrary	Namikawa & Matsushita (1970)

where g is the position vector and T is a scalar field. A poloidal vector field is one which can be represented in the form curl curl Sg, where S is curl Tr Toroidal and poloidal vector fields are solenoidal, by defi-A toroidal vector field is one which can be represented in the form there I is the position vector and I is a scalar field. A poloid a scalar

 $\dot{O}$ 

TABLE 10 - ANTI-DYNAMO THEOREMS FOR GENERAL MAGNETIC FIELDS

Pairs of fields (y, B) with the following characteristics cannot be solutions to the kinematic dynamo problem.

	in the second se	
Velocity y	Flux density B	References
Toroidal (in a sphere)	Arbitrary	Bullard & Gellman (1954); Cowling (1957).
Axisymmetric	Axisymmetric	Backus & Chandrasekhar (1956); Backus (1957); Cowling (1957); Braginskii (1964a).
Pure sin mø or cos mø dependence about axis of B "symmetry"	Nearly axisymmetric	Braginskii (1964b); P.H. Roberts (1967b).
"Slow" (magnetic Reynolds number for mean flow < 1)	Arbitrary	Childress (1968); P.H. Roberts (1967a,b).
"Insufficient rates of strain" ( $\partial u_1/\partial x_j$ too small)	Arbitrary	Backus (1958); Childress (1968).
Arbitrary, in a bounded, simply connected, perfectly conducting medium surrounded by a nonconductor.	Extending into the nonconducting medium	Bondi & Gold (1950); Leorat (1969);

#### 1.4.3 Existence of solutions

It has been shown that solutions to the kinematic dynamo problem do exist. In the decade and a half since the first existence proofs were published (Herzenberg, 1958; Backus, 1958), a large number of successful dynamo models have been developed. Broadly sheaking, these models fall into five main classes, according to the method used in solving the induction equation. These five classes are summarized in sections 1.4.4-1.4.8.

## 1.4.4 "Exact" models

Exact analytical solutions of the kinematic dynamo problem are not common. The most important example in this class is the "helical" dynamo of Lortz (1968b), which operates in an unbounded conductor. The streamlines of u are concentric helices with constant cross-sectional area.

# 1.4.5 Spherical harmonic expansion models

Expansion of u and B in spherical harmonics materially simplifies the equations governing kinematic dynamo action in a sphere. Unfortunately, because of the "interaction" term u x B in the induction equation, B must generally be represented by an infinite set of harmonics even when u has a simple form, so that trunca-

tion difficulties arise. The problem was studied by a number of workers in the late 1940's and early 1950's for the case of a steady magnetic field,  $\partial B/\partial t = 0$  (Elsasser, 1946a,b, 1947; Takeuchi and Shimazu, 1952a,b, 1953, 1954; Bullard and Gellman, 1954). However, no convincing evidence of dynamo action was obtained. Since that time, convergent models have been developed by Gubbins (1972, 1973) and by Roberts and Kumar (1972).

#### 1.4.6 "Sporadic" models

In sporadic models the effects of the terms curl (u x B) and  $\eta V^2 B$  in the induction equation (1.16') are separated by choosing a "sporadic" velocity field (Bade, 1954; Parker, 1955). The dynamo alternates between periods of motion sufficiently rapid and short-lived for diffusion to be neglected, and periods in which the motion is stopped to allow for the "simplification" of spatially complex B-fields by diffusive decay of the higher harmonics. Successful dynamo models have been developed by Backus (1958) and Tverskoy (1966), using motions in a sphere. (See also P.H. Roberts, 1971a.)

Backus (1957) points out that Takeuchi and Shimazu have set too many boundary conditions. It is therefore highly unlikely that their numerical "evidence" for steady dynamo action is meaningful.

### 1.4.7 Asymptotic models

Asymptotic dynamo models are generally characterized by the presence of two different "length" scales. These models fall into three major groups.

- u. varies on a small length scale £, while B has a component varying on a large length scale £. The magnetic Reynolds number/based on the smaller length scale is allowed to approach infinity while the ratio £/L goes to zero and the product  $R_{\rm m}(\ell/L)^3$  remains finite. (Herzenberg, 1958; P.H. Roberts, 1967b, pp. 95-104; Gibson, 1968a,b, 1969; Kropachev, 1964, 1965, 1966; Gailitis, 1970; P.H. Roberts, 1971a.)
- periodic dynamos. In models of this type, w is periodic with a short wavelength &, while B is doubly periodic with both the wavelength & and a much larger wavelength L. The magnetic Reynolds number R<sub>m</sub> based on the shorter wavelength is allowed to approach zero with l/L, while the product R<sub>m</sub><sup>2</sup>(L/L) remains finite. (Childress, 1967a,b,c, 1968, 1969, 1970; G.O. Roberts, 1969, 1970a,b, 1972a).
  - G.O. Roberts (1970a,b) has shown that "nearly all" periodic motions in an unbounded conductor will lead to dynamo action. Furthermore, Childress (1967b, 1968, 1970) has shown that a periodic motion giving dynamo

action in an unbounded conductor retains this property when fitted into a finite spherical volume by means of a "cut-off" function.

- G.O. Roberts (1973; see P.H. Roberts, 1971b) and Gubbins (1972, 1973) have carried out numerical studies of "cellular" dynamos in a sphere for axisymmetric velocity fields u. While the motions considered are not "periodic" in the sense defined above, these models are included here for the sake of illustration.
- Nearly axisymmetric dynamos. In models of this type, u and B are required to tend toward axial symmetry as the magnetic Reynolds number approaches infinity. (Braginskii, 1964a, b, c; Tough, 1967; Tough and Gibson, 1969; Soward, 1971a, 1972a; P.H. Roberts, 1967b, pp. 105-127; P.H. Roberts, 1971a.)

The asymptotic limit used in nearly axisymmetric dynamos can be interpreted in terms of two "length" scales if an "azimuthal length scale" L is defined by means of the ratio

$$\frac{2}{L} \sim \frac{|1 \cdot \nabla u|}{|\nabla u|} \sim \frac{|1 \cdot \nabla B|}{|\nabla B|}$$

 $\ell$  is the length scale of variation of  $\underline{u}$  and  $\underline{B}$  in meridian planes,  $\underline{l}_{\bullet}$  the unit vector in the azimuthal direction, and  $\underline{u}$  and  $\underline{B}$  the magnitudes of  $\underline{u}$  and  $\underline{B}$ . The magnetic Reynolds number  $R_{\underline{m}}$  based on  $\ell$  is

allowed to approach infinity while  $\ell/L$  goes to zero and the product  $R_m \left(\ell/L\right)^2$  remains finite.

Soward (1972a) has pointed out that, for the case of a steady dynamo with closed streamlines, a better interpretation of the asymptotic limit is obtained by requiring that the integral

$$\frac{1}{u} \oint_{C(x)} \frac{dx}{|y|} (y \cdot curly)$$

approach zero as  $R_{\rm m}^{-1}$  when  $R_{\rm m}$  goes to infinity. Here  ${\bf u}$  is a scaling amplitude for the velocity field,  $C({\bf x})$  the contour of a streamline, and  ${\bf x}$  the position vector of points on the streamline. The integral is, in a sense, an average of  ${\bf u}$ -curl  ${\bf u}$  for the flow, and may be considered as a measure of the helicity - a quantity which is very important in turbulent dynamo models (see section 1.4.8).

## 1.4.8 Mean field models,

In mean field dynamo models, w and B are each represented as the sum of a statistical average and a fluctuating part. The average fields w and B are assumed to vary on a length scale L, while the fluctuating fields w and B' (with zero statistical average) are assumed to vary on a length scale l. In this sense the problem is related to the two-scale approach considered in the last section.

The statistical average of Ohm's Law for a moving medium (i.e. the average of equation 1.15) is

$$\overline{j} = \sigma(\overline{E} + \overline{u} \times \overline{B} + \overline{u'} \times \overline{B'})$$
 (1.17)

This equation contains a "new" electromotive force  $\underline{\underline{u}'x}\underline{B}'$ . If this e.m.f. can be represented as a functional of the mean fields  $\underline{\underline{u}}$  and  $\underline{\underline{B}}$ , the mean field kinematic dynamo problem becomes closed. Considerable attention has been focussed on the derivation of simple representations for  $\underline{\underline{u}'x}\underline{B}'$ . Parker (1955) drew attention to the possibility that

$$\overline{\underline{u}' \times \underline{B}'} = \underline{\alpha} \cdot \overline{\underline{B}}$$
 (1.18)

Steenbeck and Krause (1966) have christened this term the  $\alpha$ -effect. Several successful  $\alpha$ -effect dynamos have been studied, both for the case  $\overline{u}=0$  (Krause and Steenbeck, 1967; Steenbeck and Krause, 1966, 1967; Moffatt, 1970a; Leorat, 1969) and for the case  $\overline{u}\neq 0$  (Parker, 1965, 1970a,b,c, 1971a-f; Krause and Steenbeck, 1965; Steenbeck and Frause, 1966, 1967, 1969a,b; Lerche and Parker, 1971, 1972). Models in which  $\overline{u}' \times \overline{B}'$  has a more complicated dependence on  $\overline{u}$  and  $\overline{B}$  than that given by (1.18) have also been studied (Steenbeck, Krause, and Rädler, 1966; Rädler, 1966, 1968a,b, 1969a,b, 1970; Krause and Rädler, 1971; P.H. Roberts, 1971a).

It should be noted that, to a first approximation, a fully isotropic turbulent motion cannot support dynamo action (Gilliland and Aldridge, 1973; Krause and Roberts,

1973; see section 3.2 below). In order for dynamo action to occur, the turbulence must have helicity (Moffatt, 1969) - i.e.

# $\underline{\underline{u} \cdot \text{curl } \underline{u}} \neq 0$

- or be anisotropic with a preferred direction (see, for example, Krause and Rädler, 1971; P.H. Roberts, 1971a).

#### 1.5 The hydromagnetic dynamo problem

Let us now turn from the kinematic dynamo problem to the more complicated hydromagnetic dynamo problem. The magnetic flux density B must still satisfy the induction equation (1.16), subject to boundary and initial conditions, but now the velocity field u must itself be derived from a specified body force distribution by solving the hydrodynamic equations subject to appropriate boundary and initial conditions.

#### 1.5.1 The equation of mass conservation

The first of the hydrodynamic equations to be considered is the equation of conservation of mass

$$\frac{DP}{Dt} = \frac{\partial P}{\partial t} + \underline{u} \cdot \underline{\nabla} P = -P \operatorname{div} \underline{u}$$
 (1.19)

In equation (1.19),

$$\frac{\mathbf{D}}{\mathbf{D}t} = \frac{\partial}{\partial t} + \mathbf{u} \cdot \mathbf{\nabla} \tag{1.20}$$

is the Lagrangian time derivative (i.e. the "material" derivative following the flow), and p is the density of the conducting fluid medium. For a truly incompressible fluid, the left hand side of (1.19) vanishes identically, giving

$$div u = 0$$
 (1.21)

If  $\partial \rho/\partial t$  is identically zero but density gradients are present, (1.19) reduces to

$$\operatorname{div} \, \mathbf{u} = -\frac{1}{\rho} \, \mathbf{u} \cdot \mathbf{v} \, \rho \tag{1.21'}$$

In the full hydromagnetic dynamo problem, Dp/Dt must be evaluated from the thermodynamic equations.

## 1.5.2 The Navier-Stokes equation of hydromagnetics

The second hydrodynamic equation of interest is the equation of conservation of momentum

where  $p_{ij}$  is the total stress tensor, F the applied body force per unit volume, and  $x_i$  a component of the position vector F. The constitutive equation for  $p_{ij}$  can be assumed to have the form (P,H,Roberts,1967a,P,17)

$$P_{ij} = P \delta_{ij} + \Pi_{ij} + M_{ij}$$
 (1.23)

where p is the kinetic pressure,  $\Pi_{ij}$  the viscous stress tensor, and  $m_{ij}$  the electromagnetic stress tensor. For a Newtonian fluid,

$$\Pi_{ij} = P\left\{5 - \frac{2}{3}v\right\} \frac{\partial u_k}{\partial x_k} \delta_{ij} + Pv\left\{\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i}\right\} \qquad (1.24)$$

where v is the kinematic (shear) viscosity and  $\zeta$  the kinematic bulk viscosity. The electromagnetic stress tensor is defined by

$$\frac{\partial}{\partial x_i} m_{ij} = \Theta E_i + (j \times B)_i$$

However, with the scaling used in deriving the induction equation (1.16),  $|\theta_{\rm E}|$  is of order  $({\rm L/cT})^2$  compared with  $|j \times B|$ , so that, in the quasi-steady approximation,

$$\frac{\partial}{\partial x_j} m_{ij} = (j \times B)_i \tag{1.25}$$

From (1.25) and (1.15) it follows that the form of the (electro) magnetic stress tensor is

$$m_{ij} = \frac{1}{\mu} (B_i B_j - \frac{1}{2} B^2 \delta_{ij}) \qquad (1.26)$$

(see P.H. Roberts, 1967a, p. 11). Finally, from (1.23), (1.24), and (1.26),

$$P_{ij} = -\left\{P + \frac{1}{2\mu}B^2 - P(5 - \frac{2}{3}\nu)\operatorname{div}_{\mu}\right\}\delta_{ij} + P\nu\left\{\frac{2\mu_i}{2\pi_j} + \frac{2\mu_i}{2\pi_i}\right\} + \frac{1}{\mu}B_iB_j \qquad (1.27)$$

Substituting (1.27) into (1.22), we obtain the Navier-Stokes equation of hydromagnetics. This equation has two alternative forms (P.H. Roberts, 1967a, p. 17)

$$\rho \frac{Du_{i}}{Dt} = -\frac{\partial}{\partial x_{i}} \left\{ P + \frac{B^{2}}{2\mu} - P(5 - \frac{2}{3}v) div \, u \right\} 
+ \frac{\partial}{\partial x_{j}} \left\{ Pv \left( \frac{\partial u_{i}}{\partial x_{j}} + \frac{\partial u_{j}}{\partial x_{i}} \right) \right\} + \frac{1}{\mu} B_{j} \frac{\partial B_{i}}{\partial x_{j}} + F_{i}$$

$$\rho \frac{Du_{i}}{Dt} = -\frac{\partial}{\partial x_{i}} \left\{ P - P(5 - \frac{2}{3}v) div \, u \right\} + F_{i}$$

$$+ \frac{\partial}{\partial x_{i}} \left\{ Pv \left( \frac{\partial u_{i}}{\partial x_{i}} + \frac{\partial u_{j}}{\partial x_{i}} \right) \right\} + \frac{1}{\mu} \left\{ (curl \, B) \times B \right\}_{i}$$
(1.29)

depending on the form in which the Lorentz force j x B is written. For the incompressible case when (1.21) is valid, (1.28) and (1.29) reduce to

$$D_{\mu}/D_{\mu} = -\frac{1}{P} \nabla \left\{ P + \frac{B^{2}}{2\mu} \right\} + V \nabla^{2} \mu + \frac{1}{P\mu} B \cdot \nabla B + \frac{1}{P} F \qquad (1.30)$$

$$D\underline{u}/Dt = -\frac{1}{P}\underline{\nabla}P + P\nabla^{2}\underline{u} + \frac{1}{P}\underline{u}(\text{curl }\underline{B}) \times \underline{B} + \frac{1}{P}\underline{F}$$
 (1.31)

assuming that  $\nu$  is a constant. Alternatively, if (1.21') is the appropriate form of the mass conservation equation, and  $\nu$  is a constant, the terms involving density gradients in (1.28) and (1.29) can be rewritten as

$$+ \nu \left[ \frac{1}{2} (\vec{n} \cdot \vec{\Delta} b) \vec{\Delta} b + \vec{\Delta} b \cdot \vec{\Delta} \vec{n} + \vec{\Delta} \vec{n} \cdot \vec{\Delta} b \right]$$

$$= \left\{ - \vec{\Delta} \left[ (z + \frac{3}{4} b) \vec{n} \cdot \vec{\Delta} b \right] + b \cdot \Delta_{\sigma} \vec{n} \right.$$

$$\left. \frac{9x!}{9} \left\{ b (z - \frac{3}{4} b) \vec{n} \cdot \vec{\Delta} b \right] + \frac{9x!}{9} \left\{ b \cdot (\frac{9x!}{9n!} + \frac{9x!}{9n!}) \right\}$$

$$(1.35)$$

## 1.5.3 The hydromagnetic equations in a rotating frame

In most cases of interest, we must deal with a rotating conducting fluid. It is therefore useful to transform the hydromagnetic dynamo equations to a rotating frame of reference. The velocity  $\underline{u}$  in the non-rotating frame can be expressed as the sum of a uniform rotation with angular velocity  $\underline{u}$ , and a velocity  $\underline{u}_{rot}$  relative to the rotating frame.

$$\underline{u} = \underline{u}_{rot} + \underline{\Omega} \times \underline{r}$$
 (1.33)

The Lagrangian time derivative (1.20) transforms as

$$\frac{\mathbf{D}}{\mathbf{Dt}} \overset{\mathbf{G}}{\sim} = \left(\frac{\mathbf{D}}{\mathbf{Dt}}\right)_{\mathbf{rot}} \overset{\mathbf{G}}{\sim} + \overset{\mathbf{\Omega}}{\sim} \times \overset{\mathbf{G}}{\sim}$$
 (1.34)

where

$$\left(\frac{D}{Dt}\right)_{rot} \stackrel{G}{\sim} \equiv \left(\frac{\partial}{\partial t}\right)_{rot} \stackrel{G}{\sim} + \stackrel{u}{u}_{rot} \cdot \stackrel{\nabla}{\sim} \stackrel{G}{\sim}$$
 (1.35)

and <u>G</u> is any vector quantity. It follows that the Eulerian time derivative  $\partial/\partial t$  transforms as

$$\frac{\partial}{\partial t}G = \left(\frac{\partial}{\partial t}\right)_{rot}G + \nabla \times \left\{ (\Omega \times r) \times G \right\} - \left(\nabla \cdot G\right)(\Omega \times r) \quad (\hat{1}.36)$$

Applying (1.36) to the induction equation (1.16'), making use of (1.33) we find that the form of the equation is invariant.

$$= \operatorname{curl} \left\{ (\Omega \times \Gamma) \times B \right\} - \eta \nabla^2 B$$

$$= \operatorname{curl} \left\{ (\Omega \times \Gamma) \times B \right\} + (\Omega \times \Gamma) \times B \right\}$$

so that

$$\left\{ \left( \frac{\partial}{\partial t} \right)_{\text{rot}} - \eta \nabla^2 \right\} B = \text{curl} \left\{ \text{urot} \times B \right\} \qquad (1.37)$$

Strictly speaking this invariance holds only if the speed of absolute motion |u| is much less than the speed of light. (See Trocheris, 1949; Backus, 1958; Acheson and Hide, 1973.)

Backus (1958) points out that the corresponding result for the electric field is false. (See Backus, 1956 for the effect on E of a superposed rigid rotation.)

Applying (1.34) to (1.33), we have

$$D\underline{u}/Dt = (D/Dt)_{pol} \underline{u}_{rot} + 2\Omega \times \underline{u}_{rot} + (\partial\Omega/\partial t) \times \underline{r}$$
$$-\frac{1}{2} \nabla \{|\Omega \times \underline{r}|^2\}$$

$$\frac{Du}{Dt} = (D/Dt)_{rot} u_{rot} + 2\Omega \times u_{rot} + (\partial\Omega/\partial t)_{rot} \times r$$

$$- \nabla \left\{ \frac{1}{2} |\Omega \times r|^2 \right\} \qquad (1.38)$$

$$= (D/Dt)_{rot} \dot{u}_{rot} + 2\Omega \times \dot{u}_{rot} + (\partial \Omega/\partial t)_{rot} \times \dot{r}$$

$$+ \Omega \times (\Omega \times \dot{r}) \qquad (1.38')$$

Also, it follows from (1.33) that

$$\nabla \cdot \mathbf{u} = \nabla \cdot \mathbf{u}_{rot} \tag{1.39}$$

$$\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} = \frac{\partial}{\partial x_j} (u_{rot})_i + \frac{\partial}{\partial x_i} (u_{rot})_j \qquad (1.40)$$

while for any scalar field a

$$Da/Dt = (Da/Dt)_{rot}$$
 (1.41)

$$-\frac{\partial a}{\partial t} = \left(\frac{\partial a}{\partial t}\right)_{rot} - \left(\frac{\Omega \times r}{r}\right) \cdot \nabla a \qquad (1.42)$$

The equation of conservation of mass in the rotating frame thus has the same form as (1.19)

$$(DP/Dt)_{rot} = -P \nabla \cdot u_{rot}$$
 (1.43)

while the Navier-Stokes equation (1.28, 1.29) becomes

$$\begin{split}
\dot{f}\left\{\left(\frac{D}{Dt}\right)_{rot} \dot{y}_{rot} + 2\dot{\Omega} \times \dot{y}_{rot} + \left(\frac{\partial \Omega}{\partial t}\right)_{rot} \times \dot{r}\right\}_{i} \\
&= -\frac{\partial}{\partial x_{i}}\left\{p + \frac{B^{2}}{2\mu} - \beta(5 - \frac{2}{3}\nu)\nabla \cdot \dot{y}_{rot} - \frac{1}{2}\beta\Omega \times \dot{r}^{2}\right\} \\
&- \frac{1}{2}(\nabla \beta)_{i} \left[\Omega \times \dot{r}\right]^{2} + \frac{\partial}{\partial x_{j}}\left\{\beta \nu \left(\frac{\partial}{\partial x_{j}}\left[\dot{y}_{rot}\right]_{i} + \frac{\partial}{\partial x_{i}}\left[\dot{y}_{rot}\right]_{j}\right)\right\} \\
&+ \frac{1}{\mu} B_{j} \frac{\partial B_{j}}{\partial x_{i}} + F_{i}
\end{split} \tag{1.44}$$

4.

 $\alpha$ r

$$P\{\left(\frac{P}{Dt}\right)_{rot} \stackrel{\vee}{u}_{rot} + 2\Omega \times \stackrel{\vee}{u}_{rot} + \left(\frac{\partial\Omega}{\partial t}\right)_{rot} \times \stackrel{\vee}{r}\}_{i}$$

$$= -\frac{\partial}{\partial x_{i}} \left\{ P - P(S - \frac{2}{3}V) \stackrel{\vee}{v}_{rot} \right\} - P\Omega \times (\Omega \times \stackrel{\vee}{r})$$

$$+ \frac{\partial}{\partial x_{j}} \left\{ PV\left(\frac{\partial}{\partial x_{j}} \left[ \stackrel{\vee}{u}_{rot} \right]_{i} + \frac{\partial}{\partial x_{i}} \left[ \stackrel{\vee}{u}_{rot} \right]_{j} \right) \right\}$$

$$+ \frac{1}{\mu} \left\{ \left( \text{curl } \stackrel{\vee}{B} \right) \times \stackrel{\vee}{B} \right\}_{i} + F_{i} \qquad (1.44')$$

In this thesis we shall restrict attention to the hydromagnetic dynamo equations in the rotating frame, and drop the subscript "rot". The hydromagnetic dynamo problem is then specified by the equations

$$\{ \frac{\partial}{\partial t} - \eta \nabla^2 \} B = \text{curl} (u \times B)$$
 (1.45)

$$DP/Dt = -P \nabla_{x} u \qquad (1.46)$$

$$\frac{Du}{Dt} + 2\Omega \times u = -\frac{1}{P}\nabla P - \frac{1}{2P} |\Omega \times r|^{2} \nabla P - (\partial\Omega / \partial t) \times r$$

$$+ \nu \{\nabla^{2}u + \nabla \nabla \cdot u\} + \frac{\nu}{P} \{\nabla P \cdot \nabla u + \nabla u \cdot \nabla P\}$$

$$+ \frac{1}{P\mu} B \cdot \nabla B + \frac{1}{P} F \qquad (1.47)$$

$$= -\frac{1}{P} \sum_{\alpha} \left\{ P - P(\zeta - \frac{2}{3} \delta) \sum_{\alpha} \tilde{u} \right\}$$

$$+ \nu \left\{ \nabla_{\alpha} \tilde{u} + \sum_{\alpha} \tilde{u} \right\} + \frac{1}{P} \left\{ \sum_{\alpha} P \cdot \sum_{\alpha} \tilde{u} + \sum_{\alpha} \tilde{u} \cdot \sum_{\alpha} \tilde{u} \right\}$$

$$+ \frac{1}{P} \sum_{\alpha} \left\{ P - P(\zeta - \frac{2}{3} \delta) \sum_{\alpha} \tilde{u} \right\} \times \tilde{u}$$

$$+ \frac{1}{P} \sum_{\alpha} \left\{ P - P(\zeta - \frac{2}{3} \delta) \sum_{\alpha} \tilde{u} \right\} \times \tilde{u}$$

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$$+ \frac{1}{P} \sum_{\alpha} \left\{ P - P(\zeta - \frac{2}{3} \delta) \sum_{\alpha} \tilde{u} \right\} \times \tilde{u}$$

$$+ \frac{1}{P} \sum_{\alpha} \left\{ P - P(\zeta - \frac$$

where v has been assumed constant, and

$$\mathbf{P} = \mathbf{P} + \frac{\mathbf{B}^2}{3\mu} - \mathbf{P}(\mathbf{5} - \frac{2}{3}\mathbf{v})\mathbf{\nabla} \cdot \mathbf{u} - \frac{1}{2}\mathbf{P}\mathbf{I}\mathbf{\Omega} \times \mathbf{r}\mathbf{I}^2$$
 (1.48)

In the simple incompressible case, (1.45)-(1.48) reduce to

This system must be solved for  $\mu$ , B, and  $\rho$  subject to the boundary and initial conditions when F and  $\rho$  are given.

If density gradients are present, but the density distribution does not vary with time, (1.45)-(1.49) reduce to

$$\{D/Dt - \eta \nabla^{2}\} B = B \cdot \nabla u + \frac{1}{P} (u \cdot \nabla P) B$$

$$\nabla \cdot u = -\frac{1}{P} u \cdot \nabla P$$
(1.46b)

$$\begin{array}{lll} D\underline{u}/Dt + 2\Omega \times \underline{u} &= -\frac{1}{P} \nabla P' - (\partial \Omega/\partial t) \times \underline{r} - \frac{1}{2P} I \Omega \times \underline{r} I^2 \nabla P \\ &+ \nu \nabla^2 \underline{u} + \frac{\gamma}{P} \{\frac{1}{P} (\underline{u} \cdot \nabla P) \nabla P + \nabla P \cdot \nabla \underline{u} + \nabla \underline{u} \cdot \nabla P\} \\ &+ \frac{1}{P} \underline{B} \cdot \nabla \underline{B} + \frac{1}{P} \underline{F} \\ &+ \nu \nabla^2 \underline{u} + \frac{\gamma}{P} \{\frac{1}{P} (\underline{u} \cdot \nabla P) \nabla P + \nabla P \cdot \nabla \underline{u} + \nabla \underline{u} \cdot \nabla P\} \\ &+ \nu \nabla^2 \underline{u} + \frac{\gamma}{P} \{\frac{1}{P} (\underline{u} \cdot \nabla P) \nabla P + \nabla P \cdot \nabla \underline{u} + \nabla \underline{u} \cdot \nabla P\} \\ &- (\partial \Omega/\partial t) \times \underline{r} + \frac{1}{P} (\nabla \times \underline{B}) \times \underline{B} \\ &+ \frac{1}{P} \underline{F} \end{array}$$

$$(1.47'b)$$

$$P' = P + \frac{B^2}{3\mu} + (5 + \frac{1}{3}V) \mu - \nu P - \frac{1}{2}P |\Omega \times \Gamma|^2$$
 (1.48b)

This system may be solved for  $\underline{u}$ ,  $\underline{B}$ , and  $\rho$ , subject to the boundary and initial conditions, when  $\underline{F}$  and  $\rho$  are given, or for  $\underline{u}$ ,  $\underline{B}$ , and  $\rho$ , subject to the same conditions, when  $\underline{F}$  and  $\rho$  are specified.

## 1.6 The full hydromagnetic dynamo problem - thermodynamic equations

In most cases of interest, the hydromagnetic dynamo problem is incomplete without consideration of the thermodynamic equations. Two scalar equations are added to the system (1.45)-(1.47), giving nine scalar equations in the nine unknowns [ u , B , p , p , T ], where T is the temperature. The additional equations can be written in the form (P.M. Koherts, 1967a, pp. 12-16, 18-2%)

$$= \nabla_{\alpha} (\lambda \nabla T) + \prod_{ij} \frac{\partial u_i}{\partial x_j} + \frac{1}{\sigma} j^2 + \varepsilon_s$$
 (1.49)

$$DP/Dt = \left\{\frac{1}{a^3} + \frac{\overline{\alpha}^2 T}{c_r}\right\} DP/Dt - \overline{\alpha} P DT/Dt \qquad (1.50)$$

when the system is assumed to be in local thermodynamic equilibrium, and a Fourier Law is assumed to hold for the heat conduction vector. Here  $\lambda$  is the thermal conduction vity,  $\overline{\alpha}$  the volume expansion coefficient,  $c_p$  the specific heat per unit mass at constant pressure,  $\alpha$  the adiabatic speed of sound, and  $\mathbf{E_s}$  the rate, per unit volume, at which sources of heat provide energy within the fluid. In general,  $\lambda$ ,  $\overline{\alpha}$ , and  $\alpha$  are all functions of density, pressure, and temperature. It should be noted that effects due to variations of chemical composition have been negical elected in equation (1.50). This equation is sometimes

replaced by an equation of state, of the form

$$\rho = \rho(T, p; \text{ chemical composition})$$
 (1.50')

(see, for example, Hide, 1969b).

When velocities in the system are small compared with the speed of sound, (1.49) and (1.50) reduce to /

$$DT/Dt = \nabla(\lambda \nabla T) + \prod_{ij} \frac{\partial u_i}{\partial x_i} + \frac{1}{\sigma} j^2 + \epsilon_s \qquad (1.51)$$

$$DP/Dt = \overline{\alpha}PDT/Dt$$
 (1.52)

(P.H. Roberts, 1967a, p. 16). Further simplifications may be made once the scaling of the various terms in the equations is known (see section 6.1). The full hydromagnetic dynamo problem requires equations (1.45)-(1.48) and (1.51)-(1.52) to be solved for [ u , B , p , p , T ] subject to the boundary and initial conditions, once the independent body forces and sources of heat are known.

# 1.7 The full hydromagnetic dynamo problem - boundary conditions

The boundary conditions which must be satisfied by solutions to the full hydromagnetic dynamo problem have been given in some detail by P.H. Roberts (1967a, pp. 22-28). These conditions fall into three major groups, which will be discussed separately in the next three sections.

## 1.7.1 Electromagnetic boundary conditions

The fields E and B must satisfy a total of four independent scalar conditions at any surface of discontinuity of  $\sigma$ ,  $\epsilon$ , or  $\mu$ . These conditions can be written in a number of equivalent forms. Caution must be exercised, however, if the magnetic diffusivity  $\eta = 0$  in any region (see F.H. Roberts, 1967a, pp. 24-26). In this thesis, we shall deal exclusively with the case  $\eta \neq 0$ .

Perhaps the simplest form of the electromagnetic boundary conditions when  $\eta \neq 0$  is

$$\langle \underline{n} \times \underline{B} \rangle = 0$$
 (1.53)  
 $\langle \underline{n} \times \underline{E} \rangle = 0$ 

where n is a unit vector normal to the boundary, and the brackets () denote the *change* in the bracketted quantity as the boundary is crossed. An alternative form of the boundary conditions is

0

$$\langle \Phi \rangle = 0 \tag{1.55}$$

$$\langle \underline{n} \wedge \underline{B} \rangle + 0$$
 (1.56)

$$\langle \mathbf{n} \times \mathbf{B} \rangle = 0 \tag{1.57}$$

where  $\Phi$  is the electromagnetic scalar potential. If  $\stackrel{A}{\sim}$  is the electromagnetic vector potential, then

$$\mathbf{E} = -\nabla \Phi - \partial \mathbf{A}/\partial \mathbf{c} \qquad (1.58)$$

$$\frac{\mathbf{B}}{\mathbf{E}} = \nabla \times \mathbf{A} \tag{1.58'}$$

When the fields E and B vary with time, (1.53) and (1.54) form a complete set of boundary conditions. However, if the fields are time-independent, (1.54) reduces to the single scalar condition (1.55), and the condition (1.56) must be added to give the required number of conditions. Several other conditions can be derived from (1.53) (1.54) or from (1.55) (1.57). For example,

$$\langle \underline{n} \cdot \underline{j} \rangle = 0 \tag{1.59}$$

$$\langle \mathbf{n} \times \mathbf{A} \rangle = 0 \qquad (1.59')$$

(always bearing in mind that  $\eta \neq 0$ ). In general, the magnetic flux density, the tangential electric field, the normal component of electric current density, the scalar potential, and the tangential vector potential are all continuous across a boundary.

An additional condition exists which defines the surface charge density  $\chi$  at the boundary between two

media "1" and "2".

$$\chi = \langle \epsilon \rangle = \langle \epsilon \rangle_2^1$$

where the bracket  $\langle \rangle_2^1$  denotes the amount by which the boundary value of the bracketted quantity in medium I exceeds the boundary value of the quantity in medium 2.

In most cases of interest, we shall assume that the conducting medium is surrounded by a nonconductor which extends to infinity in all directions. The conditions that there be no sources at infinity can them be written

$$|\underline{B}| = O(r^{-3}) \quad \text{as} \quad r \to \infty$$

$$|\underline{E}| = O(r^{-2}) \quad \text{as} \quad r \to \infty$$

$$|\Phi| = O(r^{-1}) \quad \text{as} \quad r \to \infty$$
(1.60)

r is the distance from an origin inside the conducting region.

#### Mechanical boundary conditions 1.7.2

Six independent scalar "mechanical" boundary condi-\*tions must be satisfied. These conditions may be written

$$\langle \underline{n} \cdot \underline{u} \rangle = 0 \tag{1.61}$$

$$\langle \underline{n} \times \underline{u} \rangle = 0$$

$$\langle \underline{n}_{j} p_{ij} \rangle = 0$$
(1.62)
$$(1.63)$$

$$\langle n_{i}p_{ij}\rangle = 0$$
 (1.63)

for a surface of discontinuity separating either two immiscible fluids or a fluid and a solid. For the latter case, if the solid is stationary (1.61) and (1.62) combine to give the condition

$$\underline{u} = 0 \tag{1.64}$$

on the velocity of the fluid at the interface.

It should be noted that the no slip condition (1.62) is an idealization. However, it is widely used because of its simplicity. Strictly speaking, we may only require that the normal component of the fluid velocity vanish at a fluid-solid interface. In this thesis we shall follow standard practice and apply the more stringent condition (1.64).

When the solid boundary is rotating, (1.64) is only satisfied in the rotating frame of reference - i.e.

$$u_{\text{rot}} = 0 \tag{1.64'}$$

at the fluid-solid interface. Following the practice introduced in section 1.5.3, we shall drop the subscript "rot" and use (1.64') in the form (1.64).

The relation (1.63) provides no useful information when the boundary considered is a fluid-solid interface.

The stresses applied by the fluid merely produce elastic strains in the solid.

### 1.7.3 Thermal boundary conditions

Two independent scalar "thermal" boundary conditions arise. These conditions may be written

$$\langle \lambda^{\partial T} \rangle_{\partial n} \rangle = 0 \qquad (1.65)$$

where aT/an represents the normal component of the temperature gradient at the boundary. (1.65) and (1.66) imply that both the normal component of the heat conduction vector and the temperature. The are continuous across the boundary.

## 1.8 The full hydromagnetic dynamo problem - body forces

The full hydromagnetic dynamo problem, as it applies to planetary dynamos like that of the Earth, is defined by equations (1.45)-(1.48), (1.51), and (1.52), and by the boundary conditions (1.53)-(1.54), (1.60), and (1.64)-(1.66). The information required before a solution is possible (even in principle) is a complete description of the initial conditions, the heat sources, and the form of the body force density F. Unfortunately, very little of this information is available, and models must be constructed in any attempt to match the observed behaviour of the system. In addition, the full problem is of such formidable difficulty that simplification of the equations is virtually a necessity. We shall discuss some possible simplifications in sections 1.8.4 and 6.1.

One of the first major problems to be considered is the specification of the body force density. Several possibilities have been considered in the literature. We shall discuss these possibilities in the remainder of this section.

## 1.8.1 Buoyancy forces

The body force density F may well depend largely on variations of the density of the fluid medium. In the Boussinesq approximation (Chandrasek) ar, 1961, p. 16ff.;

deffrence, 1930; Speige! and Veronice, 1960; P.H. Rolerts, 1967a, pp. 194-200) the force density associated with these variations is assumed to be of the Archimedean form

$$\mathbf{E}_{\mathbf{A}} = 0^* \mathbf{g} \qquad (1.67)$$

where q is the acceleration due to gravity, and  $0^*$  is proportional to the excess density.

The case in which the density variations are of thermal origin has been studied by several workers (Chandrasekhar, 1961, Chapters IV and V; Taylor, 1963; Malkus, 1963; Tough and Roberts, 1967; Elayeb and Roberts, 1970; Soward, 1971a, 1972a,b; Roberts and Soward, 1972; Chi Aress, 1972; Busse, 1972b; G.O. Roberts, 1972b).

butions to density variations in the Earth's core from thermal and non-thermal sources, and has concluded that of is due mainly to gravitational separation of lighter elements in the fluid core. He has studied the convection of a two-component fluid, using a generalized form of the dynamo equations. A different model of the same type was suggested by "Urey (1952), fee also Artyushkov (1972).

## 1.8.2 Precessional torques

If the rotating body of fluid is constrained to precess uniformly with angular velocity  $\Omega'$  about its axis of rotation, an extra term appears on the right hand side

of the Naviex-Stokes equation (1.47 or 1.47). In the frame rotating with angular velocity  $\Omega$  , this term has the form

$$+ (\vec{\Omega}_{i} \times \vec{L}) \cdot \vec{\Delta} \vec{R} + \vec{\Omega}_{i} \times \vec{R}$$

$$+ (\vec{\Omega}_{i} \times \vec{L}) \cdot \vec{\Delta} \vec{R} + \vec{\Omega}_{i} \times \vec{R}$$

$$+ (\vec{\Omega}_{i} \times \vec{L}) \cdot \vec{\Delta} \vec{R} + \vec{\Omega}_{i} \times \vec{R}$$

$$(1.68)$$

Malkus (1963, 1968, 1971a,h) has considered the case in which  $\mathbf{F}_{\mathrm{p}}$  is the dominant contribution to the body force density. He uses the approximation

$$\frac{1}{P} \stackrel{\mathcal{F}}{\mathcal{F}} \approx (\Omega' \times \Omega) \times r - \frac{1}{2} \nabla \{ [(2\Omega + \Omega') \times r] - [\Omega' \times r] \}$$
(1.68')

The hydrodynamics of viscous flow in a precessing spheroidal cavity have been studied by a number of authors (Rohdi and Lyttleton, 1953; Stewartson and Roberts, 1963; Koberts and Stewartson, 1964). Busse (1968, 1971) has extended the analysis to the case of a precessing spheroidal shell. The latter geometry is a more appropriate model of the Earth's fluid core because of the presence of the solid inner core. (See also the review by M.O. Rochester, 1973.)

### 1.8.3 Turbulent forces

The mean field approach can be applied to the Navier-Stokes equation (1.47, 1.47') as well as to the induction equation (1.16) (P.H. Roberts, 1971a; Moffatt, 1972). In this approach the body force density £ is separated into a

statistical average and a fluctuating part

$$\mathbf{E} = \widetilde{\mathbf{E}} + \mathbf{E}'$$

The term  $\widehat{\underline{u}'} \times \widehat{\underline{B}'}$  in the "modified" Ohm' Law (1.17) is then evaluated in terms of the mean fields  $\widehat{\underline{u}}$  and  $\widehat{\underline{B}}$ , and the statistical properties of the fluctuating body force density  $\widehat{\underline{Y}}$ 

Moffatt (1972) has considered a model in which  $\mathbf{E}'$  is a homogeneous turbulent field without intrinsic helicity - i.e.  $\frac{\mathbf{F}' \cdot \text{curl } \mathbf{F}'}{\mathbf{F}' \cdot \text{curl } \mathbf{F}'} \equiv 0$ 

However, in order to ensure that the fluctuating velocity field  $\underline{u}^{*}$  does have helicity, he assumes that "...there is some selective mechanism present which leads to a net flux of energy parallel to  $\Omega$  [the angular velocity vector]".

Steenbeck, Krause, and Rädler (1966) have considered a quasi-kinematic dynamo model in which rotation interacts with dradients of density and turbulent intensity to produce an a-effect. However, it has been pointed out that the turbulence spectrum function used by these authors is not physically realizable (Lerche, 1972e).

The dynamo model of Steenbeck, Krause, and Rädler (1966) is not fully hydromagnetic, since they consider only gradients of the intensity of the turbulent velocity field u'. In Chapter 6 we shall consider the effects due to gradients of the intensity of the turbulent force density field F'.



# 1.8.4 More general studies of the hydromagnetic dynamo problem

In addition to the work mentioned above, there have been several more general studies of the hydromagnetic dynamo problem. Children (1968, 1969) has pointed out that any kinematic dynamo can be used as the basis of a self-consistent hydromagnetic dynamo in any dynamical model simply by choosing the body force density in such a way that the momentum balance equation (1.47) is satisfied. However, in more realistic models where the body force density is specified from the start, the choice of a dynamical model will introduce consistency conditions which must be satisfied by F and B.

maylor (1963) has derived a particularly interesting consistency condition which has been used by Thirlby (1973) as the basis of a numerical study of hydromagnetic dynamo action in a sphere. The Taylor condition arises from the magnetogeostrophic approximation to the Navier-Stokes equation (1.47'a) for incompressible flow

$$2\rho\Omega \times u = -\Sigma R + \Sigma \times B + E^{\dagger}$$

$$\nabla \cdot u = 0$$
(1.69)

where p is the dynamic pressure and  $\mathbf{F}^{\dagger}$  is a modified body force density incorporating the terms  $\Omega \mathbf{x}(\Omega \mathbf{x}\mathbf{r})$  and  $(\partial \Omega/\partial t)\mathbf{x}\mathbf{r}$ . Equation (1.69) has been obtained from (1.47'a) by neglecting the inertial term Du/Dt and the viscous term

in comparison with the Carialis term  $2\mathfrak{Q} \times \mathfrak{X}$  . approximation is valid when the Rossby and Ekman numbers for the flow are small compared with unity - i.e.

$$Rey = \mathbf{u}/2\Omega L \ll 1 \tag{1.71}$$

RO 
$$\epsilon$$
  $\mathbf{u}/2\Omega L \ll 1$  (1.71)
$$\epsilon = \sqrt{2\Omega L^2} \ll 1$$
 (1.72)

- and the time scale of velocity variation is much greater than the rotation period - i.e.

$$1/2\Omega T \ll 1 \tag{1.73}$$

Since equation (1.69) is of lower order than equation (1.47'a), viscous boundary layer theory must be applied to satisfy the boundary conditions on u (see section 6.2). The boundary-layer thickness  $\delta$  is of order  $\epsilon^{\prime\prime}$  L . The incompressibility condition (1.70) implies that the solution  $u^1$  to (1,69) must satisfy

$$\mathbf{R} \cdot \mathbf{R}^{1} \sim \epsilon^{4} \mathbf{U}$$
 (1.74)

on the boundary S of the conducting fluid, where U is the average magnitude of  $u^{1}$  on  $S^{*}$ , and n is the unit vector normal to S . If  $\varepsilon <<1$  , it is reasonable to assume that

$$\underline{n} \cdot \underline{u}^1 \sim 0$$
 on S (1.75)

Applying Gauss' Theorem to a cylindrical volume coaxial with  $\Omega$  and bounded at the ends by sections of  $S^*$ we have, from (1.70) and (1.75), that

$$\int_{C} u^{i} \cdot dS = \begin{cases} \nabla \cdot u^{i} dn - \int_{\text{portions}} (n \cdot u^{i}) dS \\ \text{of } S \end{cases}$$

$$= 0 \qquad (1.76)$$

where C is the cylindrical side wall of the volume  $V_{\overline{C}}$  From (1.76) it follows immediately that

$$2\Omega \int_{\mathcal{C}} u^{i} \cdot dS = \int_{\mathcal{C}} (2\Omega \times u^{i})_{\phi} dS = 0 \qquad (1.77)$$

where () represents the azimuthal component. Substituting (1.69) into (1.77) and factoring out the density  $\rho$ , we have

$$\int_{c} (\hat{j} \times \hat{B})_{\phi} ds = \int_{c} (\nabla P - \hat{F}^{\dagger})_{\phi} ds \qquad (1.78)$$

TI

$$(\nabla P - F^{\dagger})_{\phi} = 0 \quad \text{on } C \qquad (1.79)$$

it follows from (1,78) that

$$\int_{C} (j \times B)_{\phi} dS = 0$$
(1.80)

Equation (1.80) is Taylor's consistency condition.

It depends on the assumption that (1.70)-(1.73) and (1.79)

are all valid. For the geodynamo, (1.71) and (1.72) are

certainly true (see section 6.1), and we may certainly

choose meaningful time scales for which (1.73) is satisfied.

The stratification parameter

$$\Delta \rho/\rho$$
 < 0.3

where As represents the change in density over the length

scale 1. On the boundary-layer length scale  $\delta$ , (1.70) is certainly valid, so that (1.75) is a reasonable approximation. Furthermore, the main flow  $u^i$  is predominantly azimuthal, while the density gradient is predominantly radial. It follows that

$$\int_{\mathbf{v}_{c}} \nabla \cdot \mathbf{u}^{i} d\mathbf{v} = -\int_{\mathbf{v}_{c}} \mathbf{u}^{i} \cdot \frac{\nabla P}{P} d\mathbf{v} \approx 0 \qquad (1.82)$$

even though the stratification parameter (1.81) is not much less than unity. The validity of the Taylor condition (1.80) in the geodynamo thus depends mainly on the assumption (1.79). The probability of significant azimuthal body forces in the geodynamo is discussed in Chapter 6, (See also P.H. Roberts, 1971a.)

Yet another interesting approach to the hydromagnetic dynamo problem has been suggested by Busse (1973a). He attacks the problem by treating the Lorentz force term  $\frac{1}{\rho}(\mathbf{j} \times \mathbf{B})$  as a perturbation term in the momentum balance equation. In order for this approach to be valid in the case of the geodynamo, it is necessary for the toroidal field in the fluid core to be much smaller than the values of several hundred gauss (1 G = 10 T) commonly assumed. Busse (1973b) claims that the toroidal field in the core should be less than an order of magnitude greater than the poloidal field.

### 1.8.5 Driving forces in the geodynamo

At the present time, there is no general agreement on the type of body force which is appropriate to the geodynamo (see, for example, Jacobs, 1972h; Malkus, 1972h).

Objections to thermal convection in the outer core have been raised by Higgins and Kennedy (1971) and Kennedy and Higgins (1973), who suggest that the temperature lies close to the melting point of the core material, and that in most of the outer core the melting-point gradient is much less steep than the adiabatic gradient. A temperature distribution of the sort proposed by Kennedy and Higgins (1973) would imply that the outer core is stably stratified, except within 200-300 km. of the outer core-inner core boundary. Thermal convection would therefore be restricted to 3-4% of the volume of the fluid core.

Several arguments have been advanced to counter the proposals of Higgins and Kennedy.

estimate of the melting curve for iron may be incorrect, since it is based solely on consideration of the solid phase. Leppaluoto (1972; see also Verhoogen, 1972), using significant structure theory of the liquid phase, has obtained a revised estimate of the melting curve of iron under core conditions, and finds that both the melting temperature and the melting-point gradient are

greater than those suggested by Higgins and Kennedy (1971). On the other hand, Kennedy and Higgins (1973) argue that significant structure theory may give anomalous results when applied to melting phenomena.

Hirch (1972) has reviewed present knowledge of the melting relations of iron at high pressures, and suggests that "...it appears to be unrealistic to claim that the melting temperature of iron, at core pressures, is known to within 500°.

- estimate of the adiabatic gradient in the outer core may also be incorrect, since it too is based solely on consideration of the solid phase (acobs, 1971a,b, 1972a; Birch, 1972; Kennedy and Magins, 1973; France, 1973). Jacobs (1971a,b, 1972a) and Birch (1972) have suggested that the adiabatic and melting-point curves in the outer core may be nearly coincident. A relation-ship of this sort could lead to a state of marginal stability in the outer core (Jacobs, 1971a,b, 1972a).
- C. Composition. The arguments of Higgins and Kennedy (1971) are based on the properties of pure iron. The presence of a lighter alloying component in the outer core, required by density considerations, may lead to substantial modifications of both the melting-point and the adiabatic gradients (Jacobs, 1971a, b, 1972a;

- Anderson, 1978a, h; Hall and Murthy, 1978; Fisch. 1977;
  Frazer, 1978; Stewart, 1973). Kennedy and Biggins
  (1973) argue, however, that the meagre evidence available on the behaviour of saturation curves at high
  pressures suggests that "...if the adiabatic curve falls on the wrong side of the melting curve of iron, it will be even more on the wrong side of a saturation curve".
- d. Radioactive potassium. If the lighter alloying component in the outer core is mainly sulphur (Murthy and Hall, 1970), much of the radionuclide K<sup>40</sup>, present in the Earth will be located in the outer core. This heat source would provide an estimated 10<sup>12</sup> watts/sec, more than enough to drive thermal convection (Murthy and Hall, 1972; Goettel, 1972; Jacobs, 1972b; Stacey,
- e. "Slurry". Even if the temperature distribution in the outer core does lie along a melting curve with a shallow gradient, it is possible that the core fluid is a slurr; of fine iron particles suspended in an iron-rich liquid. Under certain conditions, a suspension of this type can behave as an adjabatic fluid (Busse, 1972; Elsasser, 1972; Malkus, 1972a). It is likely, however, that the slurry particles would be unstable (Malkus, 1972a; Kennedy and Higgins, 1973). In addition, seismic evidence on attenuation in the outer core seems to cast doubt of the possibility of a slurry (Birch, 1972).

stably stratified against convection, the geodynamo might still be driven by internal wave motions (Bullard and Substitut, 1971, 1973).

A further objection to thermally driven models of the geodynamo arises from consideration of the constraints imposed on heat flux in the core by surface heat-flux measurements. There is some question as to whether the thermal energy available will his sufficient to maintain the magnetic field against ohmic loss. There is also some question (Malkus; 1972b) as to whether the gravitational separation mechanisms proposed by Braginskii (1964d, 1967a) and Wrey (1952) can supply enough energy to drive the geodynamo.

Malkum (1968, 1971a, b, 1972b) and Stacey (1973) claim that there may be just barely enough energy available from precession to drive the geodynamo. However there are substantial objections to several of the arguments used by Malkus in support of the precession-driven geodynamo (Jacobs, Chan, and Frazer, 1972; Jacobs, 1972b; Rochester, 2t al. 1973).

It is difficult to comment on the validity of turbulent force models of the geodynamo without some know-ledge of the mechanism by which the turbulent force is assumed to arise. However, it seems unlikely that

turbulence in the core will be homogeneous. For this reason, the model proposed by Moffatt (1972) seems inappropriate. Furthermore, Moffatt's requirement of a net energy flow parallel to the rotation axis appears unlikely to be met in the geodynamo. The inhomogeneous model proposed in coeff n 6.5 of this thesis may provide a more useful approach.

other forces which may well influence the behaviour of the geomagnetic field. It has been suggested (e.g. Jac ha, 1970h) that a correlation exists between the frequency of field reversals and the time rate of change of the speed of rotation of the Earth. This suggestion implies that the term (30/3t)x r in the Navier-Stokes equation (1.47) may be important. Other forces which may be of interest are those due to oscillations of the Earth's inner core (Won and Kuc, 1973), and those due to roughness of the coremantle interface (Hide and Horai, 1968; Hide, 1969a; Hide and Malin, 1970, 1971a, b, c; Jacobs, 1971b; Ibrahim, 1973).

## 1.9 The mathematical nature of the dynamo problem

## 2.9.1 The kinematic dynamo problem

extremely complicated. However, the problem has several general features which should be noted. Let us first consider the kinematic dynamo problem. Let  $\varepsilon$  represent all space, V a simply-connected volume embedded in  $\varepsilon$ , and so the problem of V. Assume that  $\eta = \infty$  in  $\varepsilon - V$  and  $\eta \neq 0$  in V. The kinematic dynamo problem is then specified by the equations

$$[3/3t - \eta V^2] \underline{B} = \underline{V} \times (\underline{u} \times \underline{B}) \quad \text{in } V \qquad (1.83)$$

$$\underline{V} \times \underline{B} = 0 \quad \text{fin } \epsilon - V \qquad (1.84)$$

$$\nabla B \approx 0 , \qquad \text{in } \epsilon \qquad (1.85)$$

and the boundary and initial conditons

$$r^{3}$$
B bounded, in  $\epsilon$  (1.86)

$$\langle B \rangle \approx 0$$
 on S (1.87)

$$\underline{B}(r,0) = \underline{B}_{O}(r) \qquad (1.88)$$

where u is an allowable flow (see section 1.4.1). It can be shown (Backus, 1958; Childress, 1968) that a solution to the problem (1.83)-(1.88), together with appropriate initial and boundary conditions on E, uniquely determines the solutions to (1.2)-(1.6) and (1.15), provided that the total initial charge on V is known.

The problem can be reduced to one on V alone by noting that B can be represented by a scalar potential

in  $\epsilon = V$  , where

$$v^2 \Psi = 0 \quad \text{in } \epsilon - V \tag{1.89}$$

$$t^2\Psi$$
 bounded in  $\epsilon \sim V$  . (1.90)

If the normal component of the gradient of  $\Psi$  is specified on S, the external problem (1.89) has a unique solution for  $\Psi$ . B is thus uniquely determined in  $A \in \gamma V + S$  by its normal component on S. Because of the continuity condition (1.87) on S, the field in V must satisfy the boundary condition

$$\underline{n} \times \underline{B} = f_S(\underline{n} \cdot \underline{B}) \otimes \underline{n} \times \underline{\nabla}\Psi \quad \text{on } S \qquad (1.91)$$

The problem in V is then a linear differential system in B, elliptic in space and parabolic in time. It should be noted that equation (1.85) can be considered as an initial condition (fee The discussion in section 1.3,3).

A dimensionless velocity u/U can be termed a kinematic dynamo (Childress, 1968) if it satisfies the conditions:

a) The kinetic energy of the system remains below a specified value

$$E_{kin} = \int_{\frac{1}{2}}^{\frac{1}{2}} Pu^2 dN \leq \text{(const.)} \cdot PU^2, t \geq 0$$
 (1.92)

b) There exists a magnetic Reynolds number  $R_{m} = UL/\eta$  less than  $\infty$ , such that the kinematic dynamo problem has at least one solution (B, E) for which the magnetic energy in  $\epsilon$  approaches a positive upper limit as  $t \to \infty$ .

$$\lim_{t\to\infty}\sup\left\{M\equiv\int_{\varepsilon}\frac{B^2}{2\mu}\,dv\right\}>0$$

AF 33

(This condition is somewhat more stringent that the condition suggested in section 1.4.1.)

If u, B, and E are all independent of time, the kinematic dynamo problem reduces to an elliptic system, linear in B. If the equations are written in nondimensional form, the magnetic Reynolds number appears as an eigenvalue, and the dimensionless velocity  $\dot{u}/U$  is a sta-tionary dynamo if and only if the kinematic dynamo problem has an eigenvalue  $R_{\rm m}^{\dagger} \neq \infty$  (Childress, 1968).

In the general kinematic problem, there will be a spectrum of magnetic-energy growth rates for a given velocity u. The largest possible growth rate is given by the difference between the maximum rate at which energy can be supplied by the interaction between the velocity and magnetic fields, and the minimum rate at which energy can be lost by ohmic dissipation. It can be shown (P.H. Roberts, 1967b) that

$$\frac{\partial M}{\partial t} = \frac{\partial}{\partial t} \left[ \frac{B^2}{2\mu} dN \right]$$

$$= \frac{1}{\mu} \int_{0}^{\infty} B_i e_{ij} B_j dN - \int_{0}^{\infty} j^2 / dN \qquad (1.94)$$

where

$$\mathbf{e}_{ij} = \frac{1}{2} \left\{ \frac{\partial \mathbf{u}}{\partial \mathbf{x}_{i}} + \frac{\partial \mathbf{u}}{\partial \mathbf{x}_{i}} \right\} \tag{1.95}$$

is the rate of strain tensor. No energy is lost by radiation in the quasi-steady approximation.

If  $\lambda(\underline{r})$  is the largest real eigenvalue of the symmetric matrix  $e_{ij}$  at the point  $\underline{r}$ , and  $\Lambda$  is the largest value of  $\lambda(\underline{r})$  for points in V+S, then

$$\int_{C} B_{i} e_{ij} B_{j} dw \leq \int_{A} \lambda(\underline{r}) B_{i} B_{i} dw$$

$$\leq \Lambda \int_{C} B^{2} dw \leq \Lambda \int_{E} B^{2} dw$$

$$= 2\mu \Lambda M \qquad (1.96)$$

Similarly, it may be shown (P.H. Roberts, 1967b) that

$$\langle j''_{6} dv \rangle \geq 2CM \qquad (1.97)$$

where C is the smallest possible decay rate for normal modes of the induction equation in a stationary volume V Dimensional arguments show that C is of the form

$$C = (\eta/L^2) \cdot \kappa \qquad (1.98)$$

where  $\kappa = \kappa(V)$ . (For a sphere of radius L,  $\kappa = \pi^2$ .)
Substituting (1.96)-(1.98) into (1.94) we see that

$$\partial M/\partial t \leq 2(\Lambda - C) \cdot M$$
 (1.99)

or  $M(t) \leq M(0) e^{2(\Lambda - C)t}$ 

(1.100)

For dynamo action to occur it is necessary that  $\Lambda \geqslant C$ 

$$\Lambda L^2/\eta \geqslant \kappa$$
 (1.101)

 $\Lambda L^2/n$  may be interpreted as a magnetic Reynolds number, since  $\Lambda$  has the dimensions U/L.

It must be realized that the elliptic equation (1.83) is defined for an ensemble of dimensionless velocities u/u not all of which are dynamos. It is necessary to decide which of these velocities will belong to the class of dynamos, a problem which involves the generally nonlinear correspondence between the existence of an elliptic equation and the nature of its coefficients. This problem is discussed in some detail by Childress (1968, 1970).

properties of the kinematic dynamo problem:

- a) If  $B(\underline{r},t)$  is the solution to the kinematic dynamo problem satisfying the initial condition  $B(\underline{r},0) = B_O(\underline{r})$  then  $-B(\underline{r},t)$  is the solution-satisfying the initial condition  $B(\underline{r},0) = -B_O(\underline{r})$ .
- b) If the volume V is invariant under spatial inversion (r + -r), then the kinematic dynamo problem is invariant under the transformation

c) If (m, , , z) is a system of cylindrical coordinates, the kinematic dynamo problem admits a formal class of solutions satisfying the parity requirements:

$$[B_{\bar{\omega}}, B_{\phi}, E_{z}, u_{z}]$$
 odd in z  
 $[B_{z}, E_{\bar{\omega}}, E_{\phi}, u_{\bar{\omega}}, u_{\phi}]$  even in z (1.103)

The kinematic dynamo equation (1.83) is not self-adjoint. However, Namikawa and Matsushita (1970) have studied the equation in detail and have shown that it becomes self-adjoint for a curl-free velocity under a suitable restriction. Lerche (1972c) has investigated the equations from the Lagrangian point of view, and has derived a variational principle for computing the eigenvalues of the dynamo equations subject to the appropriate boundary conditions. He suggests that this method has decided advantages over other numerical techniques which have been used in investigations of the kinematic dynamo problem.

## 1.9.2 The hydromagnetic dynamo problem

For the hydromagnetic dynamo problem (1.45)-(1.48), the difficulties encountered in the kinematic problem are compounded. We must now solve for u, B, and p, assuming that the body force density F and the fluid density p are given. The implicit nonlinearity introduced by the necessity of determining which of the possible fields E and p lead to dynamo action is severe unless all terms involving Vp are ignored. In addition, the equations are explicitly nonlinear because of the terms u.Vu and

 $\frac{1}{\rho\mu}$  ( $\nabla \times B$ )  $\times B$  in the Navier-Stokes equation, and the term  $\nabla \times (u \times B)$  in the induction equation. Some simplification is obtained if the inertial terms in the Navier Stokes equation are neglected; however, the nonlinear Lorentz force cannot usefully be neglected, since it provides the desired back-reaction of the magnetic field on the flow. The only simplification possible here is to treat the Lorentz force as a perturbation term (Busse, 1973a; see section 1.8.4).

Childress (1968, 1969) has proved an anti-dynamo theorem for the hydromagnetic dynamo problem in the magnetogeostrophic approximation (1.69). The theorem may be stated as follows: if  $u \cdot and B$  are axisymmetric fields, and  $E \equiv 0$ , then  $B = must go to zero as <math>t \rightarrow \infty$ , even if an  $\alpha$ -effect is present.

Childress (1968) has also pointed out certain symmetry properties of the hydromagnetic dynamo problem. If  $(\omega,\phi,z)$  is a system of cylindrical coordinates, the hydromagnetic dynamo problem admits a formal class of solutions satisfying the parity requirements:

$$[F_z, B_{\omega}, B_{\phi}, E_z, u_z]$$
 odd in z  
 $[F_{\omega}, F_{\phi}, B_z, E_{\omega}, E_{\phi}, u_{\omega}, u_{\phi}]$  even in z

(1,,104)

## 1.10 Summary of Chapter 1

This chapter is concerned with dynamo theory and its application to astrophysical magnetic fields. Most of the material presented is taken from the recent literature on the subject. The principal original contributions are to be found in section 1.1, where a detailed summary of present observational knowledge of astrophysical magnetic fields is presented, and an attempt is made to detay nine the validity of the "flux-conserving field compression" hypothesis concerning magnetic star evolution, and Schuster's hypothesis concerning magnetic fields in massive rotating bodies. The data available neither confirm nor disprove the "flux-conserving field compression" hypothesis. Schuster's hypothesis, however, gives erroneous predictions for the dipole fields of the Moon and terrestrial planets other than the Earth.

#### 2. MEAN FIELD ELECTRODYNAMICS

#### 2.1 Introduction

In this thesis we shall be concerned mainly with the "fiean field" approach to the solution of the kinematic and hydromagnetic dynamo problems. This approach has received considerable, attention in recent years, and extensive reviews of the subject have been written by P.H. Roberts (1971a), Krause and Kädler (1971), Parker (1970a,b,c, 1971a-f) and Lerche and Parker (1971, 1972). The East German school (Steenbeck, Krause, Kädler, et al.) have, introduced the term mean field electrodynamics (MFE) to refer to the study of electromagnetic fields in conducting fluids, when the fluids are in turbulent motion.

The standard notation of mean field electrodynamics will be used. (See, for example, P.H. Roberts, 1971a.)

The fields studied are assumed to have random, or "turbulent" components, so that the concept of a statistical ensemble average is appropriate. A given field F (vector or scalar) can be decomposed into an ensemble average (denoted by an overbar) and a random, or fluctuating component (denoted by a prime).

$$F = \overline{F} + F' \qquad (2.1)$$

These components have the following properties:

$$\overline{F'} = 0$$
,  $\overline{\overline{F}} = \overline{F}$ 

$$\overline{F+G} = \overline{F} + \overline{G}$$
,  $\overline{\overline{F}G} = \overline{F} \overline{G}$ ,  $\overline{\overline{F}G'} = 0$ 

80

 $\overline{FG} = \overline{F}G + \overline{F}G$ 

In general, a field F will be both position and time-dependent. We shall denote the position vector by  $\underline{x}$  and the time by t, and write

F := F(x,t)

### 2.2 Types of turbulence

### 2.2.1 General considerations

We shall be dealing with quantities which depend on the joint probability distribution of the values of a field at several points in space and time. Batchelor (1953, p.70) defines

$$\overline{u_{a_{1}}(x_{1},t)u_{a_{2}}(x_{2},t)...u_{a_{m}}(x_{m},t)}$$

$$= \overline{Q}_{a_{1}a_{2}...a_{m}}^{(m)}(x_{1},x_{1},...,x_{n-1},t)$$

as an m-order, n-point product mean value, where  $(\underline{r}_1,\ldots,\underline{r}_{n-1})$ , is a 3(n-1) dimensional vector specifying the configuration formed by those n of the points  $(\underline{x}_1,\ldots,\underline{x}_m)$  which are distinct. We shall extend this definition, and refer to

$$\overline{u_{a_{1}}(\underline{x}_{1},t_{1})u_{a_{2}}(\underline{x}_{2},t_{2})...u_{a_{m}}(\underline{x}_{m},t_{m})} = \overline{Q}_{a_{1}a_{2}...a_{m}}^{(m)}(\underline{x}_{1},t_{1};\underline{r}_{1},...,\underline{r}_{n-1};\tau_{1},...,\tau_{n-1})}$$
(2.2)

as an m-order, n-point, q-time product mean value, where  $(\tau_1, \dots, \tau_{q-1})$  is a (q-1) dimensional vector specifying the configuration formed by those q of the times  $(t_1, \dots, t_m)$  which are distinct.

The invariance properties of the scalar quantity

$$\overline{Q}(\underline{x}_{1}, \underline{t}_{1}; \underline{r}_{1}, \dots, \underline{r}_{n-1}; \underline{l}_{1}, \underline{l}_{2}, \dots, \underline{l}_{m}; \underline{\tau}_{1}, \dots, \underline{\tau}_{q-1})$$

$$(2.2')$$

$$\underline{q}(\underline{x}_{1}, \underline{t}_{1}; \underline{r}_{1}, \dots, \underline{r}_{q-1})$$

$$\underline{q}(\underline{x}_{1}, \underline{t}_{1}; \underline{r}_{1}, \dots, \underline{r}_{q-1}; \underline{\tau}_{1}, \dots, \underline{\tau}_{q-1})$$

where the  $(\frac{1}{2})$  are unit vectors and the Einstein summation convention applies, determine the form of  $\overline{Q}^{(m)}$  alpha  $\frac{1}{4}$ ...am (Robertson, 1940; Batchelor, 1953, pp. 40-45). The invariance properties of interest are those which refer to spatial and temporal translations, rotations, and reflections of the configuration of points and times defining the average, combined with the unit vectors  $(\frac{1}{2})$ . The various types of turbulence can be characterized by their invariance properties, and special terminology has been introduced to describe the simplest types of invariance.

- a. Stationary turbulence.  $\overline{Q}$  is invariant with respect to arbitrary temporal translations of the configuration of times  $(t_1, \dots, t_m)$ . Therefore both  $\overline{Q}$  and  $\overline{Q}_1^{(m)}$  are independent of  $t_1$ .
- b. Homogeneous turbulence.  $\overline{Q}$  is invariant with respect to arbitrary spatial translations of the configuration of points  $(\underline{x}_1,\ldots,\underline{x}_m)$ . Therefore both  $\overline{Q}$  and  $\overline{Q}_{a_1\ldots a_m}^{(m)}$  are independent of  $\underline{x}_1$ .

Once homogeneity is assumed, further conditions on the spatial properties of the turbulence can be introduced.

In each of the next six definitions, the term homogeneous is omitted, although is to be understood.

respect to arbitrary spatial reflections and rigid-body rotations of the configuration  $(\underline{r}_1,\ldots,\underline{r}_{n-1};\underline{l}_1,\ldots,\underline{l}_m)$ . When homogeneity is taken into account, we see that  $\bar{Q}$  is invariant under the extended group of rototranslations in 3-dimensional space (this group includes spatial reflections as part of the rotation group).

Definitions (a)-(c) agree with those given by Batchelor (1953, p. 18 and p. 41): Unfortunately, this terminology is not universally accepted. For example, because it is often convenient to separate the concepts of reflection and rotation invariance, some authors do not include reflection symmetry in their definition of isotropy (e.g. P.H. Raberts, 1971a). The term isotropic, mirrorsymmetric turbulence is then introduced to refer to what Batchelor calls isotropic turbulence (e.g. Krause and # Roberts, 1973). The term statistically steady turbulence provides another example. In some cases (e.g. P.H. Roberts, 1971a) this term is used in place of stationary turbulence, while in others (e.g. Krause and Roberts, 1973), it is used in place of stationary, homogeneous turbulence. In this thesis we shall retain the classical definitions of stationarity, homogeneity, and isotropy. However, we shall

also wise terms taken from elementary particle theory (Fonda and Chirardi, 1970) and crystallography (Shubnikov, 1951) to describe other types of invariance.

### d. "P-invariant" (or "mirror-symmetric") turbulence.

 $\overline{\mathbb{Q}}$  is invariant under spatial inversion, or "reflection in a point" (Shubnikov, 1951) of the configuration  $(\underline{\mathfrak{x}}_{\mathbf{i}};\underline{\mathbb{L}}_{\mathbf{j}})$ . We have used the notation

$$(\underline{x}_i;\underline{1}_j)$$
  $(\underline{x}_1,\ldots,\underline{x}_{n-1};\underline{1}_1,\ldots,\underline{1}_m)$ 

This operation consists of a 180° rotation about some axis, followed by reflection in the plane normal to the axis of rotation. When homogeneity is taken into account,  $\overline{Q}$  is invariant under the group of translations and spatial inversions, but not necessarily invariate under the rotation group or any of its subgroups (other than the identity, of course). The term P=invariance is taken from elementary particle theory (Fonda and Chirardi, 1970, p. 89 and p. 395), with "P" standing for parity.

### e. "R-invariant" (or "pseudo-isotropic") turbulence.

 $\overline{\mathbb{Q}}$  is invariant under rigid-body spatial rotations, but not necessarily invariant under spatial reflections. When homogeneity is taken into account,  $\overline{\mathbb{Q}}$  is invariant under the restricted group of rototranslations (which excludes spatial inversion), but not necessarily invariant under the extended group. Again, the term

- E-invariance is taken from elementary particle theory, though with less justification than the term  $P-[r,\sigma\sigma\rho]=\sigma\rho\rho$ , since we are not considering rotations in four-dimensional space-time. The "R" stands for rotation.
- f. "Skew-isetropic" turbulence. Q is invariant under rigid-body rotations, but changes sign under spatial inversion.
- "Axially-symmetric" (or "axisymmetric") turbulence.  $\overline{Q}$  is invariant under spatial rotations of  $(\underline{r}_i,\underline{l}_j)$  about a given unit vector  $\lambda$ , and invariant under spatial inversion. When homogeneity is taken into account,  $\overline{Q}$  is invariant under the extended group of rototranslations applied to the augmented configuration  $(\lambda,\underline{r}_i,\underline{l}_j)$
- h. "Axially R-invariant" turbulence.  $\overline{Q}$  is invariant under the restricted group of rototranslations applied to the augmented configuration defined in (g), but not necessarily invariant under the extended group of rototranslations.

In a similar fashion, further conditions on the temporal properties of the turbulence can be introduced once stationarity is assumed. i. "T-invariant" turbulence.  $\overline{Q}$  is invariant under the operation of time reversal applied to the times  $(t_1,\ldots,t_m)$ . Thus  $\overline{Q}$  is invariant under the transformation

$$(\tau_1, \ldots, \tau_{q-1}) \rightarrow (-\tau_1, \ldots, -\tau_{q-1})$$

Taking stationarity into account,  $\widehat{Q}$  is invariant under the group of temporal translations and inversions applied to the configuration  $(\tau_k)$ , where

$$(\tau_k) = (\tau_1, \ldots, \tau_{q-1})$$

The term T-invariance is taken from elementary particle theory (Fonda and Chirardi, 1970, pp. 104ff.).

The types of invariance defined in (d)-(h) can of course occur in combination with the type defined in (i). There are also types of invariance which refer to spatial and temporal transformations applied simultaneously to the configuration  $(r_i; l_j; \tau_k)$ . We shall be particularly concerned with

j. "PT-invariant" turbulence.  $\overline{Q}$  is invariant under the combined operations of spatial inversion and time reversal, but not necessarily under either of them separately. Again, the term PT-invariance is taken from elementary particle theory.

The various types of turbulence defined above are listed, with their properties, in Table 11 (see p. 90).

#### 2.2.2 Two-point, two-time correlations

In this thesis we shall be concerned mainly with two-point, two-time correlations. From (2.2),

$$\overline{Q}_{ij}^{(2)}(\underline{x}_1, t_1; \underline{r}, \tau) = \overline{u_i(\underline{x}_1, t_1) u_j(\underline{x}_1 + \underline{r}, t_1 + \tau)}$$

We shall use the standard notation

$$\overline{Q}_{ij}^{(2)}(\underline{x}_{1},t_{1};\underline{r},\tau) = R_{ij}(\underline{x}_{1},t_{1};\underline{r},\tau)$$
 (2.3)

From the definition of the two-point, two-time correlation tensor  $R_{ij}$  we see that

$$R_{ij}(\underline{x}_{1},t_{1};\underline{r},\tau) = R_{ji}(\underline{x}_{1}+\underline{r},t_{1}+\tau;-\underline{r},-\tau) \qquad (2.4)$$

In the case of homogeneous, stationary turbulence, the dependence of  $R_{ij}$  on  $x_1$  and  $t_1$  drops out, and (2.4) becomes

$$R_{ij}(\mathbf{r},\tau) = R_{ji}(-\mathbf{r},-\tau) \qquad (2.4')$$

We also have that

$$\overline{Q}(\underline{r},\underline{l}_1,\underline{l}_2,\hat{\tau}) = (\underline{l}_1)_i (\underline{l}_2)_j R_{ij} (\underline{r},\tau) \qquad (2.5)$$

The operation of spatial inversion is represented by the transformation

$$(\underline{r},\underline{1}_1,\underline{1}_2,\tau) \rightarrow (\underline{-r},-\underline{1}_1,-\underline{1}_2,\tau)$$

Clearly,

$$\widehat{Q}(-\underline{r},-\underline{l}_{1},-\underline{l}_{2},\tau) = (-1)^{2}(\underline{l}_{1})_{1}(\underline{l}_{2})_{j} R_{1j}(-\underline{r},\tau)$$

$$= \widehat{Q}(-\underline{r},\underline{l}_{1},\underline{l}_{2},\tau)$$

It follows immediately that the property of P-invariance implies that

$$R_{ij}(\mathbf{r},\tau) = R_{ij}(-\mathbf{r},\tau)$$
 [P-invariance] (2.6)

Combining this property with (2.4'), we have that

$$R_{ij}(\underline{r},\tau) = R_{ji}(\underline{r},+\tau)$$
 [P-invariance] (2.6')

In a similar fashion, we may show that T-invariance implies

$$R_{ij}(\mathbf{r},\tau) = R_{ij}(\mathbf{r},-\tau) \quad [T-invariance] \quad (2.7)$$

$$R_{ij}(\underline{r},\tau) = R_{ji}(-\underline{r},\tau)$$
 [T-invariance] (2.7')

while PT-invariance implies

$$R_{ij}(\underline{r}, \tau) = R_{ij}(-\underline{r}, -\tau)$$
 [PT-invariance] (2.8)

$$R_{ij}(\underline{r},\tau) = R_{ji}(\underline{r},\tau)$$
 [PT-invariance] (2.8')

It will be noted that while P- and T-invariance combine to give PT-invariance; PT-invariance does not necessarily imply either P-invariance or T-invariance. It will also be noted

that PT-invariance implies symmetry of the tensor  $R_{ij}$  under interchange of its indices. This property will be considered in greater detail in Chapter 3.

INVARIANCE PROPERTIES OF DIFFERENT TYPES OF TURBULENCE TABLE 11

Type of Turbulence	Space Translation	Space	Space	Time	Time	Space-Time
HOMOGENEOUS	invariant				11018197111	IIOT STOAILT
.R-invariant	invariant	invariant	1	1	1	1
P-invariant	invariant		invariant	1	1	,
Isotropic	invariant	invariant	invariant	1		
Skew-isotropic	invariant	invariant	changes	1		
Axisymmetric	invariant	invariant about axis	invariant		-	ı
Axially R-invariant	invarjant	17	1		1	6
STATIONARY				invariant		
T-invariant		1		invariant	invariant	
STATIONARY AND HOMOGENEOUS	invariant	•	(%) 	invariant	^	
PT-invariant	invariant		•	invariant	-	invartant
P-invariant	invariant	•	invariant	invariant	,	
T-invariant	invariant	g page	-	invariant	invariant	1
R-invariant	invariant	invariant	•	invariant	1	ŧ
Isotropic	invariant	invariant	invariant	Invariant	invariant	invariant

\* For two-point, two-time correlations.

**15** 

2.3 The kinematic dynamo problem - Green's function techniques

#### 2.3.1 The dynamo equations

We shall now apply the mean field approach to the kinematic dynamo problem. Writing u and B in the form (2.1), substituting these expressions into the induction equation (1.16'), and separating the average and fluctuating parts of the equation, we obtain the coupled system of equations

$$\left\{ \partial_{\partial t} - \eta \nabla^2 \right\} \overline{B} - \operatorname{curl} \left\{ \overline{u} \times \overline{B} \right\} = \operatorname{curl} \left\{ \overline{u' \times B'} \right\}$$
 (2.9)

where

$$\widehat{\mathbf{B}} = \mathbf{d}i\mathbf{v} \ \mathbf{B}' = \mathbf{O} \tag{2.11}$$

# 2.3.2 The first-order solution to the fluctuating induction equation

As it stands, equation (2.10) cannot be solved directly for B' as a functional of the mean fields  $\overline{B}$ . However, if the second order term in the fluctuating fields

$$\underline{C'} \equiv \underline{u}' \times \underline{B'} - \underline{\underline{u}' \times \underline{B'}}. \tag{2.12}$$

is neglected to a first approximation, (2.10) reduces to

$$\left\{ \frac{\partial}{\partial t} - \eta \nabla^2 \right\} \underline{B}'_o - \operatorname{curl} \left\{ \underline{\overline{u}} \times \underline{B}'_o \right\} = \operatorname{curl} \left\{ \underline{u}' \times \underline{\overline{B}} \right\}$$
 (2.13)

This equation can be solved by Green's function techniques, the right hand side being regarded as a source term (Rädler, 1964, 1968a; Krause, 1968a,b; Krause and Rädler, 1971). The solution is of the form

where  $t_0$  is the initial instant, V the region occupied by the turbulence, and S the boundary surface of V  $\partial/\partial n'$  represents a normal derivative on S. G is a Green's dyadic satisfying

7

In (2.15) and (2.16)  $\frac{1}{x}$  is the idemfactor, or "unity" dyadic (see Morse and Feshbach, 1953, p. 577, while  $\delta(x-x')$  and  $\delta(t-t')$  are Dirac delta functions. In deriving (2.14) use has been made of the boundary condition

$$\underline{\mathbf{u}}'(\underline{\mathbf{x}},\mathsf{t}) = 0, \, \underline{\mathbf{x}} \in S \qquad \qquad (2.18)$$

Boundary conditions must also be specified for  $\frac{B'}{20}$ . For simplicity, we shall assume that

$$B_{O}^{\prime}(x,t) = 0 , x \in S$$
 (2.19)

and

$$\mathcal{L}(\underline{x},t;\underline{x}',t') = 0, \underline{x} \in S \text{ or } \underline{x}' \in S$$
(2.20)

so that the surface term in (2.14) vanishes identically. Finally, as noted in the introduction, the second part of (2.11) is satisfied for all  $t \geqslant t_0$  if \*

$$\operatorname{div} \mathbf{B}_{\mathcal{O}}^{\bullet}(\mathbf{x}, \mathbf{t}_{\mathcal{O}}) = 0 \tag{2.21}$$

From (2.14) we can evaluate the source term  $\overline{u} \times \overline{B}_{O}^{T}$  (2.9) as a functional of  $\overline{B}$ ,  $\overline{u}$ , the statistical properties of  $\underline{u}'$ , and the initial conditions on  $\overline{u}' \overline{B}_{O}^{T}$ . In tensor notation,

$$\begin{cases}
\underline{u}'(\underline{x},t) \times \underline{B}'_{b}(\underline{x},t)\}_{i} \\
= \varepsilon_{ijk} \int_{V} d\underline{x}' \, G_{kl}(\underline{x},t;\underline{x}',t_{o}) \, \underline{u}'_{i}(\underline{x},t) \, \underline{B}'_{o_{k}}(\underline{x}',t_{o}) \\
+ \varepsilon_{ijk} \, \varepsilon_{lmn} \, \varepsilon_{npq} \int_{V} d\underline{x}' \int_{t_{o}}^{t} dt' \, G_{kl}(\underline{x},t;\underline{x}',t') \\
\frac{\underline{a}}{\delta \underline{x}'_{m}} \left\{ R_{jp}(\underline{x},t;\underline{x}',t') \, \overline{B}_{q}(\underline{x}',t') \right\}
\end{cases} (2.22)$$

where  $R_{ij}$  is the two-point, two-time correlation tensor for  $\underline{u}$ ' (see section 2.2.2),

$$R_{ij}(\mathbf{x},t;\mathbf{x}',t') = \overline{u_i'(\mathbf{x},t)} \underline{u_j'(\mathbf{x}',t')}$$
 (2.23)

Clearly, if

$$\overline{u_{i}'(\underline{x},t)} \, \underline{B_{oj}'(\underline{x}',t_{o})} = 0 , \quad \forall \, \underline{x},\underline{x}' \in V , t > t_{o} \quad (2.24)$$

then  $\underline{\underline{u}'x} \underline{\underline{B}'}_0$  depends only on  $\underline{\overline{B}}$  ,  $\underline{\underline{u}}$  , and the statistical properties of  $\underline{u}'$  .

### 2.3.3 <u>Higher-order terms</u>

The full solution to (2.10) may now be developed by iteration (Krause, 1968a,b). We write

$$\frac{B'}{2} = \frac{B'}{2} + \frac{B'}{2} + \frac{B'}{2} + \dots$$
 (2.25)

$$\underline{C}_{n}^{\prime} = \underline{u}^{\prime} \times \underline{B}_{n}^{\prime} - \underline{\underline{u}^{\prime} \times \underline{B}_{n}^{\prime}}$$
 (2.26)

Substituting (2.25) and (2.26) into (2.10), and using (2.14) as the first term in the solution, we have

$$\left\{ \mathcal{H}_{n} - \eta \nabla^{2} \right\} \mathcal{B}_{n}' - \operatorname{curl}\left\{ \mathcal{U} \times \mathcal{B}_{n}' \right\} = \operatorname{curl} \mathcal{C}_{n-1}', \quad n \geqslant 1$$
 (2.27)

u x B can then be evaluated from

$$\underline{\mathbf{u}' \times \mathbf{B}'} = \underline{\mathbf{u}' \times \mathbf{B}'_0} + \underline{\mathbf{u}' \times \mathbf{B}'_1} + \underline{\mathbf{u}' \times \mathbf{B}'_2} + \cdots \qquad (2.28)$$

Writing the solution to (2.27) out explicitly;

$$B'_{n}(x,t) = \int_{0}^{\infty} dx' \, G(x,t,x',t_{0}) \cdot B'_{n}(x',t_{0})$$

$$+ \int_{0}^{\infty} dx' \int_{0}^{\infty} dt' \, G(x,t,x',t') \cdot \text{curl } C'_{n-1}(x',t')$$
(2.29)

so that

"

$$\begin{aligned} & \{u' \times B'_n\}_i = \varepsilon_{ijk} \int_V dx' \, G_{kk}(x,t;x',t_0) \, u'_j(x,t) \, B'_{nk}(x',t_0) \\ & + \varepsilon_{ijk} \, \varepsilon_{kmq} \int_V dx' \int_{t_0}^t dt' \, G'_{kk}(x,t;x',t') \\ & - \frac{\partial}{\partial x'_{im}} \left\{ u'_j(x,t) \, C'_{n-l_0}(x',t') \right\} \end{aligned}$$
(2.30)

Krause (1968a,b) has shown that the iteration process is convergent for all times t and for any choice of  $\underline{u}$ , when V is an infinite domain.

2.4 The kinematic dynamo problem - Fourier transform techniques

#### 2.4.1 Notation

Results similar to those derived in section 2.3 can be obtained by using Fourier-Stieltjes transforms of the fluctuating fields u' and B' (Batchelor, 1953, pp. 28-33; Moffatt, 1970a).

The Fourier-Stieltjes representation of a random vector function f'(x,t) is of the form

$$f'(x,t) = \int_{\mathbb{R}} dF(k,\omega) e^{i\{k\cdot x + \omega t\}}$$
(2.31)

This type of representation is appropriate when the integral

taken over the whole field is not bounded. If f'(x,t) is a stationary, homogeneous random function - i.e. if the two-point, two-time correlation tensor

$$Q_{ij}(\underline{x},t;\underline{x}',t') = \overline{f_i'(\underline{x},t)} f_j'(\underline{x}',t') \qquad (2.32)$$

satisfies the condition

$$Q_{ij}(x,t; x+r, t+\tau) = Q_{ij}(r,\tau)$$
 (2.33)

- then

$$dF_i^*(k,\omega) dF_j(k',\omega')$$

(\_)

$$= \left\{ \frac{1}{(2\pi)^4} \int d\mathbf{r} \int d\mathbf{r} \ Q_{ij}(\mathbf{r}, \mathbf{t}) \ e^{-i\left\{k, \mathbf{r} + \omega \mathbf{t}\right\}} \right\}$$

$$= \chi_{ij}(k,\omega) \delta(k-k') \delta(\omega-\omega') dk dk' d\omega d\omega' \qquad (2.34)$$

The Fourier transform

$$\chi_{ij}(\mathbf{k},\omega) \equiv \frac{1}{(2\pi)^4} \int d\mathbf{r} \int d\mathbf{r} Q_{ij}(\mathbf{r},\tau) e^{-i\{\mathbf{k}\cdot\mathbf{r}+\omega\tau\}}$$
(2.34')

appearing in (2.34) is referred to as the spectrum tensor of f'(x,t).

### 2.4.2 The fluctuating induction equation

The Fourier-Stieltjes representations of u' and B' will be written

$$\underline{u}'(\underline{x},t) = \iint_{\underline{R}} d\underline{z}(\underline{k},\omega) e^{i\{\underline{k},\underline{x}+\omega t\}}$$
(2.35)

$$\mathbf{B}'(\mathbf{x},t) = \iint_{\mathbf{R}} d\mathbf{y}(\mathbf{k},\omega) e^{i\{\mathbf{k}\cdot\mathbf{x}+\omega t\}}$$
(2.36)

following Moffatt (1970a). The expansion (2.25) can now be replaced by the expansion

$$\frac{dy}{2} = \frac{dy}{20} + \frac{dy}{21} + \frac{dy}{22} + \dots$$
 (2.37)

where

$$B'_{n}(x,t) = \int_{\mathbb{R}} \int_{\omega}^{Q} dY_{n}(k,\omega) e^{i\{k\cdot x + \omega t\}}$$
(2.38)

Substituting (2.36) and (2.38) into (2.11),

$$i \underbrace{k \cdot dY}_{i} = i \underbrace{k \cdot dY}_{i} = 0 \qquad (2.39)$$

Before the Fourier transform of (2.10), (2.13), or (2.27) can be obtained, we must define Fourier representations of  $\widetilde{\underline{u}}$  and  $\overline{\underline{B}}$ .

$$\overline{\mathcal{U}}(x,t) = \iint_{K} \widehat{\mathcal{U}}(K,\Omega) e^{i\{K\cdot x + \Omega t\}} dK d\Omega \qquad (2.40)$$

$$\widetilde{B}(x,t) = \iint_{K\Omega} \widetilde{\widetilde{B}}(K,\Omega) e^{i\left[K-x+\Omega t\right]} dK d\Omega \qquad (2.41)$$

Substituting (2.35), (2.38), (2.40), and (2.41) into (2.13) and taking the Fourier transform, we obtain

$$-ik \times \iiint \{\hat{\vec{u}}(\vec{k},\Omega) \times d\vec{\lambda}^{o}(\vec{k}-\vec{k},\vec{n}-\Omega)\} d\vec{k} d\Omega$$

(2.42)

= 
$$i \not k \times \iint \{d\vec{x}(\not k - \not K, \omega - \Omega) \times \frac{\hat{B}}{\hat{B}}(\not k'\Omega)\} d\not k d\Omega$$

This equation must be solved for  $dY_O(k,\omega)$  as a functional of  $dZ(k,\omega)$  and the Fourier transforms of the mean fields, taking into account the initial conditions on B'.

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# 2.4.3 Solution of the fluctuating induction equation for uniform, time-independent mean fields

Equation (2.42) has no simple solution as it stands, because of its complicated dependence on the mean fields. However, if it can be assumed that the mean fields are effectively uniform and time-independent on the length and time scales of the fluctuating fields, we may write

$$\frac{\hat{u}}{\hat{u}}(\underline{K},\Omega) \simeq \frac{\hat{u}}{\hat{u}}(0,0) \delta(\underline{K}) \delta(\Omega) \qquad (2.43)$$

$$\frac{\widehat{\widehat{B}}}{\widehat{B}}(\underline{K},\Omega) \simeq \frac{\widehat{\widehat{B}}}{\widehat{B}}(0,0) \delta(\underline{K}) \delta(\Omega) \qquad (2.44)$$

Under this assumption, (2.42) reduces to

$$\{i\omega + \eta R^2\} dY_0(k,\omega) - ik \times \{\widehat{\mathcal{U}}(0,0) \times dY_0(k,\omega)\}$$

$$= \pi i k \times \{dZ(k,\omega) \times \widehat{\mathcal{B}}(0,0)\} \qquad (2.45)$$

The solution of this equation is

$$d\chi_{o}(\mathbf{k},\omega) = \frac{i\{\mathbf{k},\widehat{\mathbf{k}}(\mathbf{o},o)\,d\mathbf{g}(\mathbf{k},\omega) - \mathbf{k},d\mathbf{g}(\mathbf{k},\omega)\widehat{\mathbf{k}}(\mathbf{o},o)\}}{\{i\omega + \eta\mathbf{k}^{2} + i\mathbf{k}\cdot\widehat{\mathbf{u}}(\mathbf{o},o)\}}$$

$$+ d\chi_{o}'(\mathbf{k})\,\delta(\omega - i\eta\mathbf{k}^{2}) \qquad (2.46)$$

where the term involving  $d\underline{Y}_{O}(k)$  has been added to take the initial conditions into account. We may then write an expression for  $\underline{u} \times \underline{B}$ :

$$\frac{\mathbf{u}' \times \mathbf{B}'_{o}}{\mathbf{u}} = \iiint_{\mathbf{u}} d\mathbf{z}^{*}(\mathbf{k}, \omega) \times d\mathbf{y}_{o}(\mathbf{k}', \omega') e^{i\left\{(\mathbf{k}' - \mathbf{k}) \cdot \mathbf{x} + (\omega - \omega')t\right\}}$$

$$= \iiint_{\mathbf{u}} d\mathbf{z}^{*}(\mathbf{k}, \omega) \times d\mathbf{y}_{o}(\mathbf{k}', \omega) \times d\mathbf{z}(\mathbf{k}', \omega')$$

$$- \mathbf{k}' \cdot d\mathbf{z}(\mathbf{k}', \omega') d\mathbf{z}^{*}(\mathbf{k}, \omega) \times \mathbf{\hat{B}}(o, o) \right\}$$

$$= i\left\{(\mathbf{k}' - \mathbf{k}) \cdot \mathbf{x} + (\omega' - \omega)t\right\}$$

$$+ \iiint_{\mathbf{u}} d\mathbf{z}^{*}(\mathbf{k}, \omega) \times d\mathbf{y}_{o}'(\mathbf{k}') e^{i\left\{(\mathbf{k}' - \mathbf{k}) \cdot \mathbf{x} + (i\eta \mathbf{k}'^{2} - \omega)t\right\}}$$

$$+ \iiint_{\mathbf{k}} d\mathbf{z}^{*}(\mathbf{k}, \omega) \times d\mathbf{y}_{o}'(\mathbf{k}') e^{i\left\{(\mathbf{k}' - \mathbf{k}) \cdot \mathbf{x} + (i\eta \mathbf{k}'^{2} - \omega)t\right\}}$$

Assuming that u' is a stationary, homogeneous random function, and denoting the spectrum tensor of u' by  $\Phi_{ij}(k,\omega)$ , we have from (2.34) that

$$= \Phi_{ij}(k,\omega) \delta(k-k)\delta(\omega-\omega') dkdk'd\omega d\omega' \qquad (2.48)$$

Thus

$$\left\{\overline{\underline{u}' \times \underline{B}'}\right\}_{i} = i \in_{ije} \iint \frac{\left\{k_{m} \underline{\Phi}_{je}(\underline{k}, \omega) \, \widehat{\underline{B}}_{m}(0, 0) - k_{m} \underline{\Phi}_{jm}(\underline{k}, \omega) \, \widehat{\underline{B}}_{e}(0, 0)\right\}}{\left\{i\omega + \eta k^{2} + i \, \underline{k} \cdot \widehat{\underline{\mathcal{D}}}(0, 0)\right\}} d\underline{\underline{k}} d\omega$$

+ 
$$\iiint d\vec{z}^*(\underline{k},\omega) \times d\underline{\gamma}_o'(\underline{k}') e^{i\{(\underline{k}'-\underline{k})\cdot\underline{x} + (i\eta \underline{k}'^2 - \omega)\underline{t}\}}$$

$$\underline{k}\omega\underline{k}'$$
(2.49)

# 2.4.4 Solution of the fluctuating induction equation for nearly uniform, nearly time-independent mean fields

An alternative method of deriving equation (2.49) is to substitute (2.35) and (2.38) directly into (2.13) without using a Fourier representation of  $\overline{u}$  and  $\overline{B}$ . The equation for  $d\underline{Y}_O$  then becomes

clearly indicating that  $d_{\infty}^{Y}$  is really of the form

$$\frac{d\mathbf{Y}}{\partial \mathbf{x}} = \frac{d\mathbf{Y}}{\partial \mathbf{x}} (\mathbf{k}, \mathbf{\omega}; \mathbf{x}, \mathbf{t})$$
 (2.51)

with spatial and temporal variation on the length and time scales of the mean fields. It is also to be expected that dZ will vary on these scales. Thus the fluctuating fields u' and B' will in general be nonstationary, inhomogeneous random functions. In Chapter 4 a method for treating fields of this nature in a more detailed fashion will be described. However, for the present we shall assume that the length and time scales of the fluctuating fields are sufficiently short compared to the length and time scales of the mean fields for u' to be treated as a stationary, homogeneous random function, to a reasonable approximation. This assumption is the underlying feature of the expansion technique

developed by  $R\ddot{a}dler$  (1968a) and others for evaluating the term  $u' \times B'$  (see P.H. Roberts, 1971a; Krause and Rädler, 1971; Moffatt, 1970a).

Neglecting spatial gradients of  $\overline{\underline{u}}$  and  $\overline{\underline{B}}$ , we find that (2.50) reduces to the form (2.45), with

$$\frac{\widehat{\underline{u}}}{\widehat{\underline{u}}}(0,0) \rightarrow \widehat{\underline{u}}$$

$$\frac{\widehat{\underline{g}}}{\widehat{\underline{B}}}(0,0) \rightarrow \widehat{\underline{B}}$$
(2.52)

The result (2.49) then follows directly from the assumption that  $\underline{u}'$  is stationary and homogeneous.

# 2.4.5 Solution of the fluctuating induction equation for "wave" mean fields

The assumption that  $\underline{\underline{u}}$  and  $\underline{\overline{B}}$  are of the form implied by (2.40), (2.41), (2.43), and (2.44) is clearly a gross over-simplification. Among other things, it implies that the energy stored in the mean fields is not finite, and that these fields over all space and time. The assumption is thus strictly applicable only to the unrealistic case of turbulent motion in an infinite fluid, with no boundary conditions implied on  $\underline{\overline{u}}$  or  $\underline{\overline{B}}$ .

If we make the more realistic assumption that the fields  $\overline{u}$  and  $\overline{B}$  go to zero as  $r^{-3}$  in the limit as  $r + \infty$ , the behaviour of the mean field transforms near K = 0 must be (Phillips, 1956)

$$\hat{\vec{F}}(\kappa,\Omega) = \{ \vec{I} - \kappa \kappa / \kappa^2 \} \cdot \hat{\vec{F}}(0,0) \delta(\Omega) + O(\kappa) \qquad (2.53)$$

and (2.45) must be replaced by a much more complicated equation.

On the other hand, if we consider the case of wave mean fields of the type

$$\frac{\widehat{\mathcal{Q}}}{\widehat{\mathcal{Q}}}(\underline{K},\Omega) = \frac{\widehat{\mathcal{Q}}}{\widehat{\mathcal{Q}}}(\underline{K}_1,\Omega_1) \delta(\underline{K}-\underline{K}_1) \delta(\Omega-\Omega_1)$$
(2.54)

$$\frac{\widehat{B}}{\widehat{B}}(\underline{K},\Omega) = \frac{\widehat{B}}{\widehat{B}}(\underline{K}_{O},\Omega_{O}) \delta(\underline{K}-\underline{K}_{O}) \delta(\Omega-\Omega_{O})$$
(2.55)

where

$$\mathbf{K}_{\mathcal{O}} \cdot \frac{\widehat{\mathbf{B}}}{\mathbf{B}} (\mathbf{K}_{\mathcal{O}}, \Omega) = 0 \tag{2.56}$$

equation (2.42) becomes

Here again we meet with the problem of infinite energy in the mean fields, but the spatial and temporal gradients of these fields are non-zero.



### 2.5 Evaluation of u'x B'

#### 2.5.1 The Radler expansion technique

In the Rädler expansion technique (Rädler, 1968a; see Krause and Rädler, 1971)  $\overline{B}$  is expanded in the second integral on the right hand side of equation (2.22), according to

$$\overline{B}(\underline{x}+\underline{r},\underline{t}+\tau) = \overline{B}(\underline{x},\underline{t}) + \underline{r}\cdot\underline{y}\,\overline{B}(\underline{x},\underline{t}) + \tau \frac{\partial}{\partial t}\,\overline{B}(\underline{x},\underline{t}) + \dots$$
(2.58)

The expression for  $\overline{u'x B'}$  becomes

$$\left\{ \begin{array}{ll} \overline{u}' \times \overline{B}'_{o} \right\}_{i} &= \sum_{\mathbf{x}, \mathbf{y}} g_{iq}^{(\mathbf{x}, \mathbf{y})} \frac{\partial^{\kappa_{i} \mathbf{y}} \overline{B}_{q}(\mathbf{x}, \mathbf{t})}{\partial \mathbf{x}_{n_{i}} \dots \partial \mathbf{x}_{n_{k}} \partial \mathbf{t}^{\mathbf{y}}} \\
&+ \varepsilon_{ijk} \int_{\mathbf{y}} d\mathbf{x}' G_{kg}(\mathbf{x}, \mathbf{t}; \mathbf{x}', \mathbf{t}_{o}) \overline{u'_{j}(\mathbf{x}, \mathbf{t})} \overline{B'_{q}(\mathbf{x}', \mathbf{t}_{o})} \\
&\text{where} \\
q_{i, n_{i}, n_{i},$$

$$g_{iq,n_1...n_K}^{(K,\nu)} = -\epsilon_{ijk} \epsilon_{\ell m n} \epsilon_{npq} \cdot \frac{(-i)^{k+\nu}}{k! \nu!}.$$

$$\int_{V} dr \int_{0}^{t-t_0} dr G_{ipq}(x,t; x-r,t-r).$$

$$\cdot \frac{\partial}{\partial r^m} \left\{ R_{jp}(x,t; x+r,t-r) r_{n_i} r_{n_i} \cdots r_{n_k} r^{\nu} \right\} \qquad (2.60)$$

The coefficients (2.60) are then evaluated under a number of assumptions concerning:

- a. the nature of the Green's dyadic Gi;;
- b. the symmetry properties of the turbulence, u'
- c. the nature of the mean flow,  $\overline{\underline{u}}$  .

Once  $\underline{\underline{u}'x} \underline{B}'$  has been evaluated, higher approximations to  $\underline{\underline{u}'x} \underline{B}'$  can be obtained from (2.26)-(2.30). The higher-order terms in (2.28) will involve higher-order velocity correlations. For example,  $\underline{\underline{u}'x} \underline{B}'$  involves three-point, three-time correlations,  $\underline{\underline{u}'x} \underline{B}'$  involves four-point, four-time correlations, and so on.

## 2.5.2 Choice of Green's function

The Green's dyadic most commonly used is that appropriate to an infinite domain for the case  $\overline{u} \equiv 0$ .

$$G_{ij}(x,t;x-r,t-t) = \delta_{ij}G(r,t)$$

$$G(r,t) = (4\pi\eta\tau)^{-3/2}e^{-r^2/4\eta\tau}, \quad t \ge 0$$
(2.61)

The choice of an infinite domain Green's function is justified on the grounds that the turbulence extends over a region large compared with the turbulence correlation length.

Results obtained using (2.61) can be extended to the case  $\bar{u} = \text{constant}$  by transforming to a frame in uniform relative motion (Krause and Rädler, 1971). Green's functions appropriate to several other types of mean flow have also been studied (Krause and Rädler, 1971, pp. 36-37; Rädler, 1964, 1969a; Krause, 1968a,b).

### Comparison of expansion and Fourier transform techniques

The zero-order term obtained from (2,59) may be compared with (2.49) when  $\bar{u} = 0$  and  $G_{ij}$  is given by We have, from (2.59),

$$\{\widetilde{\underline{u}'}\times\widetilde{\underline{B}'_o}\}_i \approx g_{iq}^{(o,o)}\widetilde{\underline{B}}_q + \varepsilon_{ijk}\int_{\underline{a}\underline{x}'} G_{k\ell}(\underline{x},t;\underline{x}',t_o) u_j(\underline{x},t)B'_{o_k}(\underline{x}',t_o)$$

$$\approx \epsilon_{ijl} \epsilon_{lmn} \epsilon_{npq} \int_{all} dr \int_{0}^{t-t_{o}} d\tau (4\pi \eta \tau)^{-\frac{3}{2}} e^{-r^{2}/4\eta \tau}$$

$$\int \int_{\mathbb{R}^{2}} i k_{m} \Phi_{jp}(k,\omega) e^{-i\left\{k,r+\omega\tau\right\}} dk d\omega$$

+ 
$$\epsilon_{ij\ell} \int d\mathbf{r} \left[4\pi\eta(\mathbf{t}-\mathbf{t}_o)\right]^{-\frac{3}{2}} e^{-\mathbf{r}/4}\eta(\mathbf{t}-\mathbf{t}_o)$$
 (2.62)

Space
$$\int \int d\mathbf{r} \left[4\pi\eta(\mathbf{t}-\mathbf{t}_o)\right]^{-\frac{3}{2}} e^{-\mathbf{r}/4}\eta(\mathbf{t}-\mathbf{t}_o)$$

$$= \int \int d\mathbf{r} \left[4\pi\eta(\mathbf{t}-\mathbf{t}_o)\right]^{-\frac{3}{2}} e^{-\mathbf{r}/4}\eta(\mathbf{t}-\mathbf{t}_o)$$

where we have made use of the definitions

$$R_{ij}(\underline{x},t;\underline{x}+\underline{r},t+\tau) = \iint_{\underline{R}\omega} \Phi_{ij}(\underline{k},\omega) e^{i[\underline{k}\cdot\underline{r}+\omega\tau]} d\underline{k}d\omega \qquad (2.63)$$

and (2.35)-(2.38). (2.62) may be simplified by using the identities

$$\int dr e^{-ik \cdot r - r^{2}/4\eta \tau} = (4\pi\eta \tau)^{3/2} e^{-\eta k^{2}\tau}$$
(2.64a)

$$\int_{0}^{\infty} d\mathbf{r} e^{-i\mathbf{k}\cdot\mathbf{r}-\mathbf{r}^{2}/4\eta t} = (4\pi\eta t)^{2/2} e^{-\eta k^{2}t}$$
(2.64a)
$$\int_{0}^{t-t_{0}} e^{-\left[i\omega+\eta k^{2}\right]t} = (i\omega+\eta k^{2})^{-1} \left\{1-e^{-\left(i\omega+\eta k^{2}\right)(t-t_{0})}\right\}$$
(2.64b)

$$\int dr \int dr (4\pi \eta t)^{3/2} e^{-r^2/4\eta r - i(k \cdot r + \omega t)}$$
all space 
$$= (i\omega + \eta k^2)^{-1} \left\{ 1 - e^{-(i\omega + \eta k^2)(t - t_0)} \right\}$$
(2.64c)

From (2.62), (2.64), and (2.46),

$$\left\{ \overline{u' \times B'_{o}} \right\}_{i} \approx \left\{ \varepsilon_{ijk} \varepsilon_{kmn} \varepsilon_{npq} \iint_{\underline{k}\omega} \frac{i k_{m} \overline{a}_{jp}(\underline{k},\omega)}{(i\omega + \eta k^{2})} d\underline{k}d\omega \right\} \overline{B}_{q}$$

$$+ \varepsilon_{ijl} \iiint_{\underline{k}\omega} d\overline{Z'_{j}}(\underline{k},\omega) dY'_{op}(\underline{k'}) e^{i(\underline{k'}-\underline{k}) \cdot \underline{x} - (\eta k'^{2} + i\omega)t}$$

$$\underline{k}\omega\underline{k'}$$
(2.65)

Equation (2.65) is clearly identical to (2.49), with  $\frac{\hat{B}}{B}(0,0)$  replaced by  $\frac{\hat{B}}{B}$ , and  $\frac{\hat{a}}{u}(0,0) \equiv 0$ . This equivalence shows how the uniform, time-independent field assumption in the Fourier transform solution corresponds to the neglect of space and time derivatives in the Rädler expansion technique, when the infinite-domain Green's function (2.61) is used.

# 2.5.4 First order smoothing, and scaling of terms in the induction equation

In most studies to date, it has been assumed that the neglect of C' (see equation 2.12) in the fluctuating induction equation (2.10) is a valid approximation. In other words, it has been assumed that

$$\underline{\underline{u}' \times \underline{B}'} = \underline{\underline{u}' \times \underline{B}'}$$
 (2.66)

Lerche (1971a) has named (2.66) the first order smoothing approximation. The validity of this approximation may be investigated by considering the scaling of terms in the fluctuating part of the induction equation.

Assume that the fluctuating fields  $\underline{u}'$  and  $\underline{B}'$  vary on the scale of the turbulence correlation length,  $\lambda_C$  and correlation time,  $\tau_C$ , while the mean fields  $\underline{u}$  and  $\underline{B}$  vary on the scales L and T. Further, assume that the magnitudes of  $\underline{u}$ ,  $\underline{u}'$ ,  $\underline{B}$ , and  $\underline{B}'$  are  $\overline{u}$ ,  $\underline{u}'$ ,  $\underline{B}$ , and  $\underline{B}'$  are  $\overline{u}$ ,  $\underline{u}'$ ,  $\underline{B}$ , and  $\underline{B}'$  are  $\overline{u}$ ,  $\underline{u}'$ ,  $\underline{B}$ , and  $\underline{B}'$  are  $\overline{u}$ ,  $\underline{u}'$ ,  $\underline{B}$ , and  $\underline{B}'$  are  $\overline{u}$ ,  $\underline{u}'$ ,  $\underline{B}$ , and  $\underline{B}'$  are  $\overline{u}$ ,  $\underline{u}'$ ,  $\underline{B}$ , and  $\underline{B}'$  are  $\underline{u}$ ,  $\underline{u}'$ ,  $\underline{B}$ , and  $\underline{B}'$  are  $\underline{u}$ ,  $\underline{u}'$ ,  $\underline{B}$ , and  $\underline{B}'$  are  $\underline{u}$ ,  $\underline{u}'$ ,  $\underline{B}$ , and  $\underline{B}'$  are  $\underline{u}$ ,  $\underline{u}'$ 

scales as

$$\frac{\mathcal{B}'\eta}{\lambda_{c}^{2}} \left\{ q + 1 + R'_{m} \left( 1 + \frac{\lambda_{c}}{L} \right) \left( \frac{\overline{U}}{U'} + \frac{\overline{B}}{B'} + 1 \right) \right\} \sim 0$$
(2.67)

where

$$R_{m}' = u'\lambda_{c}/\eta \tag{2.68}$$

and

$$f = \lambda_c^2 / \eta \tau_c \qquad (2.69)$$

When  $\overline{\underline{u}} = 0$ , the term 3 in (2.67) drops out, and the equation reduces to

$$\frac{\underline{6}'\eta}{\lambda_{c}^{2}} \left\{ q + 1 + R'_{m} (1 + \lambda_{c/L}) (\overline{8}'_{6}' + 1) \right\} \sim 0$$
(2.70)

If  $\lambda_{C} << L$  , we have

$$\frac{\hat{B}'\eta}{\lambda_{c}^{2}} \left\{ q + 1 + R'_{m} (\hat{B}'_{B'} + 1) \right\} \sim 0$$
(2.70')

First order smoothing corresponds to the neglect of term 6 in (2.67)-(2.70'). There are two limiting cases to be considered (Krause and Rädler, 1971). In the first limiting case,  $q \ll 1$ . The neglect of 6 then implies that

$$B/B \sim R_m \qquad (q \ll 1)$$

and the condition for consistency is

$$R_{m}^{\prime} << 1$$
  $(q << 1)$   $(2.71')$ 

In the second limiting case,  $q \gg 1$ . The neglect of (5) then implies that

$$B'/B \sim R''/q (q \gg 1)$$
 (2.72)

and the condition for consistency is

$$R_{\rm m}' << q \qquad (q >> 1) \qquad (2.72')$$

It should be noted that in deriving (2.72') we have assumed that diffusion is negligible in the fluctuating induction equation. However, a dynamo cannot operate without diffusion (Cowling, 1957, 1965). It follows that if (2.72') is to be valid, diffusion must be significant in the mean field induction equation. If this is not the case, term (2) must be retained in (2.70'), and the condition for (5) to be negligible is again  $R_{\rm m}^+ << 1$ . Bearing this restriction in mind, we may combine the consistency conditions (2.71') and (2.72'), and write

$$R_{\rm m}^* << (1+q)$$
 , (2.72")

The consistency check carried out above can be extended to include the mean field induction equation (2.9). This equation scales as

$$\frac{\partial \overline{B}}{\partial t} - \eta \nabla^2 \overline{B} - \text{curl}(\overline{u} \times \overline{B}) - \text{curl}(\overline{u}' \times \overline{B}') = 0$$

$$(1) \qquad (2) \qquad (3) \qquad (4)$$

$$\frac{\overline{B}\eta}{L^2} \left\{ Q + 1 + R'_m \frac{L}{\lambda_c} (\overline{U}_{u'} + \overline{B}'_{\overline{B}}) \right\} \sim 0 \qquad (2.73)$$

where

$$Q = \frac{L^2}{\eta T}$$
 (2.74)

When  $\overline{u} = 0$ , (2.73) reduces to the condition

$$6/\overline{6} \sim \frac{1}{R_m^2} \frac{\lambda_c}{L} (1+Q) \qquad (2.75)$$

Combining (2.75) with (2.71)-(2.72'), we have

$$(q << 1)$$
  $6/\bar{g} \sim R_m' \sim (\lambda c/L)^{1/2} (1+Q)^{1/2} \ll 1$  (2.76)

$$(q >> 1)$$
  $6/\sqrt{8} \sim R_m/q \sim (\lambda /qL)^{1/2} (1+Q)^{1/2} \ll 1$  (2.76')

These conditions are clearly compatible with the essumption that  $\lambda_C^- << L$  , provided that  $\Omega_-$  is not too large.

### 2.6 Solution of the mean field induction equation

#### 2.6.1 General considerations

When the source term  $\overline{u}$ 'x  $\overline{B}$ ' has been evaluated, it must be substituted into the mean field induction equation (2.9), and (2.9) must then be solved for  $\overline{B}$ . At this stage any assumptions like (2.52) about "uniformity" and "time-independence" of the mean fields are dropped, and  $\overline{u}$  and  $\overline{B}$  are allowed to vary in the expression for  $\overline{u}$ 'x  $\overline{B}$ '. Ideally, the coefficients in an expansion like (2.59) should be allowed to vary as well, to represent any inhomogeneity of  $\underline{u}$ ' required by the boundary conditions or by the Navier-Stokes equation.

### 2.6.2 The mean field dispersion relation

In certain cases, it is possible to keep the solution of the mean field equation consistent with the assumptions made in deriving the expression for  $\overline{u}' \times \overline{B}'$ . For example, if  $\overline{u} = 0$  and  $\overline{B}$  has the wave-like form implied by (2.41) and (2.55), it is possible to derive a dispersion relation for the mean field. This problem has been considered by Lerche (1971a,b), Gilliland and Aldridge (1973), and Krause and Roberts (1973).

Substituting (2.41) and (2.55) to (2.9), and making use of the first order smoothing approximation (2.66),

$$(i\Omega + \eta K^{2}) \hat{\mathbf{B}}(\mathbf{K}, \Omega) e^{i\{\mathbf{K} \cdot \mathbf{x} + \Omega t\}}$$

$$= \operatorname{curl} \{ \underline{\mathbf{u}}' \times \underline{\mathbf{B}}'_{0} \}$$

$$= \operatorname{curl} \{ \underline{\mathbf{u}}' \times \underline{\mathbf{B}}'_{0} \}$$

$$= (2.77)$$
From (2.57), with  $\hat{\mathbf{u}}(\mathbf{K}_{1}, \Omega_{1}) = 0$ ,
$$dY_{0}(\mathbf{k}, \omega) = \{i\omega + \eta \mathbf{k}^{2}\}^{-1} \{ d\mathbf{k}(\mathbf{k} - \mathbf{K}, \omega - \Omega) \times \hat{\mathbf{B}}(\mathbf{K}, \Omega) \}$$

$$+ dY_{0}'(\mathbf{k}) \delta(\omega - i\eta \mathbf{k}^{2})$$
(2.78)

so that

$$\{\underline{u}' \times \underline{B}'_{o}\}_{i} = i \in \operatorname{ijg} \in \operatorname{gmn} \in \operatorname{npg} \widehat{B}_{q}(\underline{K}, \Omega) e^{i\{\underline{K} \cdot \underline{x} + \Omega t\}}.$$

$$\cdot \iint_{\underline{k} \cdot \omega} \frac{(\underline{k} + \underline{K})_{m} \cdot \underline{\Phi}_{jp}(\underline{k}, \omega)}{i(\omega + \Omega) + \eta(\underline{k} + \underline{K})^{2}} d\underline{k} d\omega$$

$$+ i \in \operatorname{ijg} \iiint_{\underline{k} \cdot \omega} dZ_{j}^{*}(\underline{k}, \omega) dY_{og}'(\underline{k}') e^{i(\underline{k}' - \underline{k}) \cdot \underline{x} - (\eta k^{-2} - i\omega)t}$$

$$= \underbrace{\operatorname{idg} \int_{\underline{k} \cdot \omega} dZ_{j}^{*}(\underline{k}, \omega) dY_{og}'(\underline{k}') e^{i(\underline{k}' - \underline{k}) \cdot \underline{x} - (\eta k^{-2} - i\omega)t}}_{\underline{k} \cdot \omega \underline{k}'}$$

$$= \underbrace{\operatorname{idg} \int_{\underline{k} \cdot \omega} dZ_{j}^{*}(\underline{k}, \omega) dY_{og}'(\underline{k}') e^{i(\underline{k}' - \underline{k}) \cdot \underline{x} - (\eta k^{-2} - i\omega)t}}_{\underline{k} \cdot \omega \underline{k}'}$$

$$= \underbrace{\operatorname{idg} \int_{\underline{k} \cdot \omega} dZ_{j}^{*}(\underline{k}, \omega) dY_{og}'(\underline{k}') e^{i(\underline{k}' - \underline{k}) \cdot \underline{x} - (\eta k^{-2} - i\omega)t}}_{\underline{k} \cdot \omega \underline{k}'}$$

$$= \underbrace{\operatorname{idg} \int_{\underline{k} \cdot \omega} dZ_{j}^{*}(\underline{k}, \omega) dY_{og}'(\underline{k}') e^{i(\underline{k}' - \underline{k}) \cdot \underline{x} - (\eta k^{-2} - i\omega)t}}_{\underline{k} \cdot \omega}$$

$$= \underbrace{\operatorname{idg} \int_{\underline{k} \cdot \omega} dZ_{j}^{*}(\underline{k}, \omega) dY_{og}'(\underline{k}') e^{i(\underline{k}' - \underline{k}) \cdot \underline{x} - (\eta k^{-2} - i\omega)t}}_{\underline{k} \cdot \omega}$$

$$= \underbrace{\operatorname{idg} \int_{\underline{k} \cdot \omega} dZ_{j}^{*}(\underline{k}, \omega) dY_{og}'(\underline{k}') e^{i(\underline{k}' - \underline{k}) \cdot \underline{x} - (\eta k^{-2} - i\omega)t}}_{\underline{k} \cdot \omega}$$

$$= \underbrace{\operatorname{idg} \int_{\underline{k} \cdot \omega} dZ_{j}^{*}(\underline{k}, \omega) dY_{og}'(\underline{k}') e^{i(\underline{k}' - \underline{k}) \cdot \underline{x} - (\eta k^{-2} - i\omega)t}}_{\underline{k} \cdot \omega}$$

Substituting (2.79) into (2.77),

$$= -\epsilon_{rsi} \epsilon_{ijk} \iiint (k'-k)_s \frac{dZ_j^*(k,\omega)}{dZ_j^*(k,\omega)} dY_{o_k}^*(k') e^{i(k'-k)\cdot x - i(k'^2 - i\omega)t}$$

$$(2.80)$$

The expression on the right hand side of (2.80) is clearly a decaying function of time, while the expression on the left hand side may grow with time (Im  $\Omega$  < 0) or decay with time (Im  $\Omega$  > 0). If Im  $\Omega$  < 0, after a sufficiently long

time the right hand side of (2.80) will become negligible in comparison to the left hand side, and the form of the mean field  $\overline{\mathbb{B}}$  will be determined by the dispersion relation

$$\left\{ (i\Omega + \eta K^{2}) \delta_{rq} + \epsilon_{rsi} \epsilon_{ijk} \epsilon_{kmn} \epsilon_{npq} K_{s} \right\}$$

$$- \iint_{\mathbb{R}^{\omega}} \frac{(\mathbf{k} + \mathbf{K})_{m} \Phi_{jp}(\mathbf{k}, \omega)}{i(\omega + \Omega) + \eta(\mathbf{k} + \mathbf{K})^{2}} d\mathbf{k} d\omega \right\} \hat{\overline{B}}_{q}(\mathbf{K}, \Omega) = 0$$
(2.81)

Making use of (2.56) and the identities

$$\epsilon_{\text{emp}} \epsilon_{\text{npq}} = \delta_{\text{xp}} \delta_{\text{mq}} - \delta_{\text{xq}} \delta_{\text{mp}}$$
 (2.82a)

$$\epsilon_{ijk} \epsilon_{kmn} \epsilon_{npq} = \epsilon_{ijp} \delta_{mq} - \epsilon_{ijq} \delta_{mp}$$
 (2.82b)

$$\epsilon_{rsi} \epsilon_{ijl} \epsilon_{lmn} \epsilon_{npq} = \delta_{rj} \delta_{sp} \delta_{mq} - \delta_{rp} \delta_{sj} \delta_{mq} - \delta_{rj} \delta_{sq} \delta_{mp}$$

$$+ \delta_{rq} \delta_{sj} \delta_{mp} \qquad (2.82c)$$

we find that (2.81) reduces to

$$\begin{split} & \left\{ i\Omega + \eta K^2 + \iint_{\mathbb{R}^{\omega}} \frac{K_j \, \Phi_{jP}(\underline{k}, \omega)(\underline{k} + \underline{k})_P}{i(\omega + \Omega) + \eta(\underline{k} + \underline{K})^2} \, d\underline{k} d\omega \right\} \, \widehat{\overline{B}}_{r}(\underline{K}, \Omega) \\ & + \left\{ K_S \iint_{\mathbb{R}^{\omega}} \frac{R_F \left[ \Phi_{rS}(\underline{k}, \omega) - \Phi_{Sr}(\underline{k}, \omega) \right]}{i(\omega + \Omega) + \eta(\underline{k} + \underline{K})^2} \, d\underline{k} d\omega \right\} \, \widehat{\overline{B}}_{q}(\underline{K}, \Omega) \end{split}$$

Separating the real and imaginary parts of (2.83), we may write the equation in block matrix form.

$$\begin{pmatrix} a & -b \\ a & a \end{pmatrix} \begin{pmatrix} Re & \hat{B} \\ s & \hat{B} \end{pmatrix} = 0$$

(2.84)

where

$$a = \Re \left[ \prod_{n=1}^{\infty} - \left\{ \operatorname{Im} \Omega - \eta K^2 - \operatorname{Re} \Pi^{(n)} \right\} \right]$$
 (2.85)

$$b = 4m I^{(1)} + \{Re\Omega + 4m I^{(1)}\} I$$
(2.86)

with

$$\hat{\vec{B}}(\vec{K},\Omega) = \Re \hat{\vec{B}}(\vec{K},\Omega) + i \operatorname{Im} \hat{\vec{B}}(\vec{K},\Omega) \qquad (2.87)$$

$$\mathbf{I}^{(i)}(\mathbf{K}, \mathbf{\Omega}) = \iint_{\mathbf{K}\omega} \frac{\mathbf{K}_{j} \Phi_{jp}(\mathbf{k}, \omega)(\mathbf{k} + \mathbf{K})_{p}}{i(\omega + \mathbf{\Omega}) + \eta(\mathbf{k} + \mathbf{K})^{2}} d\mathbf{k} d\omega$$
 (2.88)

$$T_{ij}^{(2)}(\underline{K},\Omega) = \iint_{\underline{K}\omega} \frac{K_{\underline{K}} \{\underline{\Phi}_{i\underline{L}}(\underline{K},\omega) - \underline{\Phi}_{\underline{L}i}(\underline{K},\omega)\}}{i(\omega+\Omega) + \eta(\underline{K}+\underline{K})^2} d\underline{K} d\omega \qquad (2.89)$$

= 
$$2i \text{ K}_2 \iint \frac{\text{k}_j \text{ Im } \Phi_{i,k}(\text{k}_j,\omega)}{i(\omega+\Omega) + \eta(\text{k}_j+\text{k}_j)^2} d\text{k}_j d\omega$$
 (2.89!)

(2.89') follows from (2.89) since  $\Phi_{ij}$  must satisfy the condition of Hermitian symmetry

$$\Phi_{ij}(\underline{k},\omega) = \Phi_{ji}^{*}(\underline{k},\omega) \qquad (2.89")$$

as a consequence of (2.4') and the equation of the type (2.34') which relates  $\phi_{ij}$  to  $R_{ij}$ .

(Equation (2.84) has a non-trivial solution only if

$$\det \begin{pmatrix} a & -b \\ b & a \end{pmatrix} = 0 \tag{2.90}$$

Because of the form of the block matrix, (2.90) may be rewritten in the equivalent form

$$\det^{2}\begin{pmatrix} a & -b \\ b & a \end{pmatrix} = \det\begin{pmatrix} a & -b \\ b & a \end{pmatrix} \det\begin{pmatrix} a & b \\ -b & a \end{pmatrix}$$

$$= \operatorname{at} \begin{pmatrix} \left[ aa + bb \right] & \left[ ab - ba \right] \\ \left[ ba - ab \right] & \left[ aa + bb \right] \end{pmatrix}$$

$$= \det \left( \frac{\left[ aa + bb \right]}{\left[ 4m I^{(2)} + Re I^{(2)} \right]} \left[ Re I^{(2)} \right] m I^{(2)} - 4m I^{(2)} Re I^{(2)} \right)$$

$$\left[ 4m I^{(2)} Re I^{(2)} - Re I^{(2)} \right] \left[ aa + bb \right]$$

# 2.6.3 An alternative derivation of the mean field dispersion relation

The results (2.84)-(2.91) may be compared with the results obtained using the Rädler approximation technique in the first order smoothing approximation. The assumption that the initial conditions have had time to "die out" is equivalent to ignoring the second term in (2.59) and setting the upper limit of the time integration in (2.60) equal to infinity. Then, making use of (2.61) and (2.63),

$$\left\{\overline{\underline{u}' \times \underline{B}'_{o}}\right\}_{i} = \sum_{K, \nu} g_{iq}^{(K, \nu)} \frac{\partial^{K+\nu}}{\partial x_{n_{i}} \cdots \partial x_{n_{K}} \partial t^{\nu}} \overline{B}_{q}(\underline{x}, t)$$
 (2.92)

where

$$g(\mathbf{K}, \mathbf{V}) = \frac{(-1)^{K+V+1}}{K! \, \mathbf{V}!} \in_{ije} \in_{imn} \in_{npg}$$

$$\int_{ign} \Phi_{ip}(\mathbf{k}, \omega) \, d\mathbf{k} \, d\omega \int_{ign} d\mathbf{r} \, \left(4\pi \eta \tau\right)^{-3/2} e^{-r^{3/4}\eta \tau}.$$

$$\int_{ign} \Phi_{ip}(\mathbf{k}, \omega) \, d\mathbf{k} \, d\omega \int_{ign} d\mathbf{r} \, \left(4\pi \eta \tau\right)^{-3/2} e^{-r^{3/4}\eta \tau}.$$

$$\int_{ign} \left\{ r_{n_{i}} r_{n_{K}} \tau^{V} e^{-i(\mathbf{k}\cdot\mathbf{r}+\omega\tau)} \right\} \qquad (2.93)$$

The assumption, used in deriving (2.92), that term-by-term integration is valid in (2.22) implies that the series on the right hand side of (2.92) may be Fourier transformed term by term to give a convergent Fourier representation (see, for example, Whittaker and Watson, 1927, p. 78). Thus, making use of (2.41),

$$\left\{ \overline{\mu'x} \, \underline{B}'_{o} \right\}_{i} = \iint_{K\Omega} dK d\Omega \, e^{i\{\underline{K} \cdot X + \Omega t\}} \, \hat{\overline{B}}_{q}(\underline{K}, \Omega) \cdot \\
 \cdot \sum_{KP} g^{(K,P)}_{iqn_{i} \cdots n_{K}} \, i^{K+P} \, \Omega^{P} K_{n_{i}} \cdots K_{n_{K}}$$

so that, taking the Fourier transform,

$$\widehat{\{\underline{u}' \times \underline{B}'_{o}\}_{i}} = \widehat{\underline{B}}_{q}(\underline{K}, \Omega) \sum_{K, p} g_{iqn, \dots n_{K}}^{(K, p)} i^{K+p} \Omega^{p} K_{n_{i}} \dots K_{n_{K}}$$
(2.94)

The Fourier transform of the mean' field induction equation (2.9) is then

$$\{i\Omega + \eta K^2\} \hat{\vec{B}}_r = i \epsilon_{rsi} K_s \{\hat{\vec{u}}' \times \hat{\vec{B}}'_o\}_i$$

= 
$$i \in_{rsi} K_s \widehat{\overline{B}}_q \sum_{K,V} g_{iqn_1...n_K}^{(K,V)} i^{K+V} \Omega^V K_{n_1}...K_{n_K}$$
 (2.95)

$$\approx i \, \epsilon_{rsi} \, K_{s} \, \widehat{\widehat{B}}_{q} \, \Big\{ g_{iq}^{(o,o)} + i \, g_{iqn_{1}}^{(i,o)} \, K_{n_{1}} + i \, g_{iq}^{(o,i)} \, \Omega \\ - g_{iqn_{1}n_{2}}^{(2,o)} \, K_{n_{1}} K_{n_{2}} - g_{iqn_{1}}^{(i,i)} \, \Omega K_{n_{1}} \\ - g_{iq}^{(o,2)} \, \Omega^{2} + \dots \Big\}$$

$$(2.95')$$

retaining only the first few terms on the right hand side.

Taking real and imaginary parts of (2.95'), and noting that the  $\mathbf{gign}_{\mathbf{K}}$  are purely real, by definition, we obtain an equation equivalent to (2.84). In this equation,  $\mathbf{I}^{(1)}$  and  $\mathbf{I}^{(2)}$  are expressed as power series expansions of (2.88) and (2.89) about  $(\mathbf{K}, \mathbf{\Omega}) = (0,0)$ , integrated term by term.

#### 2.6.4 Symmetry considerations

If the spectrum tensor of the turbulence is symmetric under interchange of indices,

$$\Phi_{ij}(\underline{k},\omega) = \Phi_{ji}(\underline{k},\omega)$$
 (2.96)

(i.e.  $\Phi_{ij}$  is purely real, because of equation 2.89"), then  $I^{(2)}$  vanishes identically, and (2.85)-(2.91) reduce to the equations

$$\int_{\mathbf{m}} \mathbf{\Omega} - \eta \, \mathbf{K}^2 - \Re \mathbf{I}^{(1)} = 0 \qquad (2.97)$$

$$\Re \Omega + \Im I^{(1)} = 0 \tag{2.98}$$

We shall consider these equations in detail in Chapter 3.

### 2.7 The mean field hydromagnetic dynamo problem

The techniques of mean field electrodynamics which have been outlined in this chapter can also be applied to the hydromagnetic dynamo problem (Moffatt, 1972). We shall examine this application in Chapter 6.

#### 2.8 Summary of Chapter 2

This chapter is concerned with mean field electrodynamics and its application to the kinematic dynamo
problem. Most of the material presented is taken from the
recent literature on the subject; however, several original
contributions appear.

In section 2.2 a new terminology, related to that used in other disciplines, is proposed for several types of stationary, homogeneous turbulence with particular invariance properties.

In section 2.5 a comparison is presented of the results obtained using Fourier transform and Green's function techniques in the mean field electrodynamic approach to the dynamo problem.

Finally, in section 2.6 the mean field dispersion relation for wave mean fields is cast in a novel determinantal form.

- THE KINEMATIC DYNAMO PROBLEM AND PT-INVARIANT TURBULENCE
- 3.1 Helicity, and the maintenance of nearly uniform, nearly time-independent mean fields

As noted in section 1.4.1, a solution to the kinematic dynamo problem consists of a pair of fields  $(\underline{u}, \underline{B})$  such that  $\underline{u}$  is "allowable",  $\underline{B}$  satisfies the induction equation, and the mean magnetic energy stored in the conducting fluid grows with time or remains constant. In the MFE approach, it is the energy associated with the mean field  $\underline{B}$  which is required to grow (or remain constant), and the question to be asked is: what restrictions must be placed on the fluctuating velocity field  $\underline{u}'$  to ensure that dynamo action will occur? An important restriction of this type has been proposed by Krause (1968a),  $R\ddot{a}dler$  (1968a), and Moffatt (1970a), who point out that perhaps the simplest method of ensuring that dynamo action can occur when  $\tilde{u} = 0$  is to require that

$$\overline{\underline{u}' \cdot \text{curl } \underline{u}'} \neq 0 \tag{3.1}$$

This quantity has been given the name helicity by Moffatt (1969). Its effect is seen most clearly by making use of the Fourier-Stieltjes representation (2.35) for u' to obtain (Moffatt, 1970a)

$$\underline{\mathbf{y}'.\operatorname{Curl}\underline{\mathbf{y}'}} = i \in ijl \iint_{\mathbb{R}^{\omega}} \mathbf{k}_{i} \Phi_{jl}(\mathbf{k},\omega) \, d\mathbf{k} \, d\omega \qquad \qquad (3.2)$$

If the mean field  $\widetilde{\underline{B}}$  is virtually uniform and time-independent on the length and time scales of the turbulence, we have from (2.65) that

$$\{\underline{\underline{u}' \times \underline{B}'_{o}}\}_{i} \approx i \in ijk \in kmn} \in \sup_{n \neq q} \iint_{\underline{k}\omega} \frac{k_{m} \underline{B}_{q} \underline{\Phi}_{jp}(\underline{k},\omega)}{i\omega + \eta k^{2}} d\underline{k} d\omega$$
 (3.3)

where the effects of initial conditions have been neglected.

Also, assuming that the fluid is incompressible,

$$k_{\mathbf{i}} \Phi_{\mathbf{i} \dot{\mathbf{j}}} (\mathbf{k}, \mathbf{\omega}) = 0 = k_{\mathbf{j}} \Phi_{\mathbf{i} \dot{\mathbf{j}}} (\mathbf{k}, \mathbf{\omega})$$
 (3.4)

(Batchelor, 1953, p. 27). Substituting (3.4) into (3.3), and making us of (2.82a),

$$\{\overline{\underline{u}' \times \underline{B}'_o}\}_i = i \in ij_{\underline{I}} \iint_{\underline{R}\omega} \frac{\underline{k_q} \overline{B_q} \Phi_{j\underline{e}}(\underline{k},\omega)}{i\omega + \eta k^2} d\underline{k} d\omega \qquad (3.5)$$

Clearly, if u'x B' is not to vanish, we must require

 $f_{F_{I}}^{1}$ 

But, from (3.2) and the nature of the spectrum tensor, (3.6) is equivalent to (3.1) - i.e. in order for a turbulent velocity field u' to be able to maintain a magnetic field B which is early uniform and time-independent on the length and time scales of the turbulence, u' must have helicity.' (This derivation, of course, is only valid in the first order smoothing approximation.)

- 3.2 PT-invariant turbulence and nonuniform, oscillatory mean fields
- 3.2.1 The spectrum tensor for stationary, homogeneous, isotropic turbulence

It has recently been suggested by Lerche (1971a,b,d, 1972b,d) and Lerche and Low (1971) that helicity is not required when  $\overline{B}$  is nonuniform and time-dependent on the length and time scales of the turbulence. These authors consider the case of stationary, homogeneous, isotropic turbulence, for which the spectrum tensor  $\Phi_{ij}$  has the simple form (Batchelor, 1953, p. 49)

$$\Phi_{ij}(k,\omega) = \frac{E(k,\omega)}{4\pi k^4} \{k^2 \delta_{ij} - k_i k_j\}$$
(3.7)

In (3.7), which is valid for incompressible flow,  $E(k,\omega)$  denotes the energy spectrum function of the turbulence. This function represents the density of contributions to the kinetic energy of the fluid in  $(k,\omega)$  space, and

$$\int_{-\infty}^{\infty} d\mathbf{k} \ E(\mathbf{k}, \omega) = \frac{1}{2} \overline{u'_i(\mathbf{x}, t) u'_i(\mathbf{x}, t)}$$
 (3.8)

is the total kinetic energy per unit mass of the fluid. Consequently,  $E(k, \omega)$  can never be negative.

It can be shown (Batchelor, 1953, pp. 39-40, 51) that  $E(k,\omega)$  has the form

$$F(\mathbf{k},\omega) = C(\omega) \mathbf{k}^4 + O(\mathbf{k}^6)$$
 (3.9)

near k = 0.

#### 3.2.2 PT-invariance and helicity

Since the spectrum tansor (3.7) is symmetric, it cannot satisfy (3.6) - i.e. stationary, homogeneous, isotropic turbulence has no helicity. This lack of helicity is a general property of PT-invariant turbulence (see section 2.2). As was shown in equations (2.4'), (2.8), and (2.8'), the correlation tensor for PT-invariant turbulence satisfies

$$R_{ij}(\underline{r},\tau) = R_{ji}(-\underline{r},-\tau) \qquad (3.10)$$

$$R_{ij}(\mathbf{r},\tau) = R_{ij}(-\mathbf{r},-\tau) \qquad (3.11)$$

$$R_{ij}(\underline{r},\tau) = R_{ji}(\underline{r},\tau) \tag{3.12}$$

It follows immediately from (3.12) and the definition of the spectrum tensor  $\phi_{ij}$  that

$$\Phi_{ij}(\underline{k},\omega) = \Phi_{ji}(\underline{k},\omega) \qquad (3.13)$$

Since  $\Phi_{ij}$  must also satisfy the condition of Hermitian symmetry

$$\Phi_{ij}(\underline{k},\omega) = \Phi_{ji}(\underline{k},\omega) \qquad (3.13')$$

as a consequence of (3.10), the spectrum tensor for PTinvariant turbulence is purely real. The converse is also
true: turbulence for which the spectrum tensor is purely
real is necessarily PT-invariant.

### 3.2.3 An anti-dynamo theorem for stationary, homogeneous, isotropic turbulence in an incompressible fluid

PT-invariant turbulence of the type (3.11) cannot maintain a nearly uniform  $\overline{\underline{B}}$ . However, it is still possible that the turbulence might maintain a field of the form

$$\overline{B}(x,t) = \overline{B}(x,\Omega) e^{i\{x,x+\Omega t\}}$$
(3.14)

for a suitable choice of  $(\underline{K},\Omega)$ . The necessary condition for the maintenance of this field is that  $(\underline{K},\Omega)$  satisfy the dispersion relation (2.97)-(2.98) with Im  $\Omega < 0$ . Rewriting the dispersion relation for the case of stationary, homogeneous, isotropic turbulence, making use of (2.88), (3.4), and (3.10), we have

$$\text{Im}\,\Omega - \eta K^2 \stackrel{\circ}{=} \text{Re}\, \Gamma^{(1)}(K,\Omega)$$
 (3.15)

$$\Re \Omega = - \operatorname{Im} \mathbf{I}^{(0)}(\mathbf{K}, \Omega)$$
 (3.16)

where

$$\mathbf{I}^{(0)}(\mathbf{K},\Omega) = \mathbf{K}_{j} \mathbf{K}_{p} \iint \frac{\mathbf{E}(\mathbf{R},\omega)}{4\pi \mathbf{R}^{4}} \frac{\left\{\mathbf{R}^{4}\delta_{jp} - \mathbf{k}_{j}\mathbf{k}_{p}\right\}}{\left\{i(\omega+\Omega) + \eta(\mathbf{R}+\mathbf{R}^{3})^{2}\right\}} d\mathbf{k} d\omega \quad (3.17)$$

Taking K to define the z-axis in k-space, so that  $k \cdot K = kK\cos\theta$ ,

$$K_{j}K_{p}\{k^{2}\delta_{jp}-k_{j}k_{p}\}=(kK)^{2}-(k_{j}K_{p})^{2}=(kK)^{2}\sin^{2}\theta$$
 (3.18)

and (3.17) becomes

$$I^{(i)}(\kappa,\Omega)$$

$$= \frac{1}{2}K^{2}\int_{-\infty}^{+\infty} d\omega \int_{0}^{\infty} E(\mathbf{k}, \omega) d\mathbf{k} \int_{0}^{\pi} \frac{\sin^{3}\theta d\theta}{i(\omega+\Omega) + \eta(\mathbf{k}^{2}+K^{2}+2\mathbf{k}K\cos\theta)}$$

$$= \frac{1}{4}K^{7}\int_{-\infty}^{\infty} d\left(\frac{\omega}{\eta K^{2}}\right) \int_{0}^{\infty} d\left(\frac{\mathbf{k}}{K}\right) \frac{E(\mathbf{k}, \omega)}{\mathbf{k}^{4}} \Theta\left\{\frac{\mathbf{k}}{K}, \frac{\omega+\Re\Omega}{\eta K^{2}}; \Im \frac{\Omega}{\eta K^{2}}\right\} (3.19)$$

where

1

$$\Theta(\xi,\nu;p) = 2\xi^4 \int_0^{\pi} \frac{\sin^3\theta \,d\theta}{(1+\xi^2+2\xi\cos\theta-p)+i\nu}$$
 (3.20)

It is clear from (3.15) that Im  $\Omega \le 0$  if and only if Re I<sup>(1)</sup>  $\le \neg \eta K^2$ . But, from (3.19), Re I<sup>(1)</sup> can only be negative if Re  $\theta < 0$  for at least <u>some</u> values of its arguments, since  $E(k,\omega)$  is everywhere positive. From (3.20) we see that

$$\Re(Y, V; p) = 2Y^4 \int_0^{\pi} \frac{(1+Y^2+2Y\cos\theta-p)}{(1+Y^2+2Y\cos\theta-p)^2+v^2} \sin^3\theta d\theta$$

$$> 2 \int_{0}^{4} \int_{0}^{4} \frac{\{(i-1)^{2} - p\} \sin^{3}\theta}{(1+j^{2}+2j\cos\theta-p)^{2}+v^{2}} d\theta$$
 (3.21)

Thus, when p<0, corresponding to  ${\rm Im}\ \Omega<0$  in (3.19), Re  $\theta(\xi,\nu;p)$  is a non-negative function of  $\xi$  and  $\nu$ . It follows that Re I<sup>(1)</sup> can never be negative when  ${\rm Im}\ \Omega<0$ . We have therefore proved that stationary, homogeneous, isotropic turbulence in an incompressible fluid cannot support a growing magnetic field of the type (3.14), within the framework of the first order smoothing approximation. An alternative proof of this statement has been

given by Krause and Roberts (1973).

#### Extension of the anti-dynamo theorem | PT-invariant turbulence in an incompressible fluid

We may extend the proof given above to show that in an incompressible fluid, a growing magnetic field of the form (3.14) cannot be supported by any stationary, homogeneous turbulence which is PT-invariant. Turbulence of this sort will have a spectrum tensor which satisfies both (3.13) and the condition of Hermitian symmetry

$$\Phi_{ij}(\underline{k},\omega) = \Phi_{ji}^{\star}(\underline{k},\omega) , \qquad (3.22)$$

As noted above, the spectrum tensor must therefore be purely real. From (3.15) we see again that Im  $\Omega \leqslant 0$ if and only, if Re  $exttt{T}^{(1)}$  , defined by (2.88), is less than or equal to  $-\eta K^2$ . But, from (2.88), (3.4) and the condition that  $\Phi_{ip}(k,\omega)$  is real,

$$Re I^{(i)}(K,\Omega) = K_i K_p \iint \frac{\Phi_{ip}(k,\omega) \{\eta(k+K)^2 - 4m\Omega\}}{(\omega + Re\Omega)^2 + \{\eta(k+K)^2 - 4m\Omega\}^2} dkd\omega \quad (3.23)$$

This integral can be negative when  $\operatorname{Im} \Omega \leqslant 0$  only if

$$-K_{1}K_{p}\Phi_{1p}(\underline{k},\omega) < 0$$
 (3.24)

for some range of  $(k,\omega)$ . However, by Bochner's Theorem (see Krause and Roberts, 1973; Batchelor, 1953, p. 25),

the quadratic form

$$\Phi = X_{j}X_{p}^{*} \Phi_{jp}(\underline{k},\omega)$$
 (3.25)

must be non-negative for any choice of the complex vector X, if  $\phi_{jp}$  is the spectrum tensor of a continuous, stationary, homogeneous random process. Thus (3.24) cannot be satisfied for any choice of  $(k,\omega)$  and the proof is complete.

### 3.2.5 Failure of the anti-dynamo theorem for PT-invariant in a compressible fluid •

The proof cannot be extended to the case of stationary, homogeneous, PT-invariant turbulence in a compressible fluid. To see this, we may note that, by virtue of (3.13) and (3.22), the spectrum tensor is still purely real in the compressible case. Thus (2.88) gives

$$Re \ T^{(1)}(K,\Omega) = \iint \frac{K_j(K_p + K_p) \mathcal{D}_{jp}(K,\omega) \{\eta(K_p + K)^2 - Jm\Omega\}}{(\omega + Re\Omega)^2 + \{\eta(K_p + K)^2 - Jm\Omega\}^2} dKd\omega \quad (3.26)$$

and Re I (1) can be negative for Im  $\Omega \leq 0$  only if

$$K_{j}(K_{p}+k_{p})\Phi_{jp}(\underline{k},\omega)<0 \qquad (3.27)$$

for some range of  $(k,\omega)$ . From (3.13),

$$k_j K_p \Phi_{jp} = k_p K_j \Phi_{jp}$$
 (3.28)

for PT-invariant turbulence. Therefore,

$$K_{j}(K_{p}+R_{p}) \Phi_{jp} = \frac{1}{2} \{ (K_{j}+R_{j})(K_{p}+R_{p}) + K_{j}(K_{p}-R_{j})R_{p} \} \Phi_{jp}$$
 (3.29)

By Bochner's Theorem (3.25), each of the three quadratic forms on the right hand side of (3.29) is non-negative. However, the minus sign attached to the last term is sufficient to allow the right hand side to become negative. Consider, for example, the case  $\phi_{jp} = \phi \circ \delta_{jp}$ , where  $\phi \circ > 0$ . In this case, (3.29) becomes

 $K_{j}(K_{p}+k_{p})\Phi_{jp} = K_{j}(K_{p}+k_{p})\Phi^{*}\delta_{jp} = \Phi^{*}K\cdot\{K+k\}$  (3,30) It is clear from (3.30) that if  $k\cdot K < 0$  and  $|k\cdot K| > |K|^{2}$  equation (3.27) will be satisfied. It follows that it may be possible for stationary, homogeneous, PT-invariant turbulence in a compressible fluid to support a magnetic field of the form (3.14), within the framework of the first order smoothing approximation. However, Krause and Roberts (1973) show that stationary, homogeneous, isotropic turbulence in a compressible fluid cannot support dynamo action in the

$$q \equiv \lambda_c^2/\eta \tau_c >> 1 \qquad (3.31)$$

where  $\lambda_{C}$  and  $\tau_{C}$  are the correlation length and time of the turbulence.

case when

## 3.2.6 Reconciliation of the anti-dynamo theorem with the work of Lerche and Low

The theorem proved in sections 3.2.3 and 3.2.4 is in direct contradiction to the work of Lerche and Low (1971), who suggest that stationary homogeneous, isotropic turbulence in an incompressible fluid can lead to dynamo action for a mean field  $\overline{B}$  of the form (3.14), within the framework of first order smoothing. The discrepancy between the two results lies in the fact that the correlation tensor used by Lerche and Low does not satisfy Bochner's Theorem. In fact, their correlation tensor corresponds to a spectrum tensor of the form (3.7) in which the energy spectrum function  $E(k,\omega)$  has negative values for some choices of  $(k,\omega)$ . Such a choice of  $E(k,\omega)$  is clearly unphysical.

Krause (1972a) and Krause and Roberts (1973) give a more detailed discussion of the work of Lerche (1971a-f, 1972a-d) and Lerche and Low (1971), in which attention is drawn to the discrepancy mentioned here and to several other inconsistencies.

### 3.2.7 The possibility of dynamo action with "mirror-symmetric" turbulence

It has frequently been stated in the literature that "mirror-symmetric" turbulence cannot support dynamo action (e.g. Moffatt, 1970a). This statement is usually supported

12

by considering the case of isotropic turbulence (3.7). However, as noted in Table 11, isotropy implies PTinvariance, and, as proved in the last few sections, it is the property of PT-invariance that leads to the impossibility of dynamo action (at least under certain conditions). The anti-dynamo theorem proved in sections 3.2.3 and 3.2.4 cannot be extended to the case of P-invariance (or "mirror symmetry"), since there is no general requirement that the spectrum tensor of P-invariant turbulence be symmetric under interchange of indices. It is therefore possible that some types of "mirror-symmetric" turbulence in an incompressible fluid can produce dynamo action, even within the framework of first order smoothing. The only types of P-invariant turbulence which might be able to do so are those whose average properties are not invariant under time reversal i.e. the turbulence must not be T-invariant. Furthermore, as noted above, the turbulence must not be isotropic.

#### 3.3 PT-invariant turbulence and decaying mean fields

#### 3.3.1 The effect of initial conditions

case of PT-invariant turbulence in more detail, attention being given to mean fields of the type (3.14) which decay with time (i.e. Im  $\Omega > 0$ ). Under these circumstances it is no longer possible to neglect the effect of initial conditions on B', and the term on the right hand side of (2.80) must be retained. When the turbulence is PT-invariant, so that (3.13) holds, (2.80) reduces to

$$\left\{i\Omega + \eta K^2 + I^{(i)}(\underline{K},\Omega)\right\} \widehat{\widehat{B}}_{r}(\underline{K},\Omega) e^{i\left\{\underline{K}\cdot\underline{X} + \Omega t\right\}}$$

$$= -\epsilon_{rsi} \epsilon_{ijk} \iiint (\underline{R}' - \underline{R})_s d\overline{Z}_j^*(\underline{R}, \omega) dY'_{o_k}(\underline{R}')$$

$$= \epsilon_{rsi} \epsilon_{ijk} \iiint (\underline{R}' - \underline{R})_s d\overline{Z}_j^*(\underline{R}, \omega) dY'_{o_k}(\underline{R}')$$

$$= \epsilon_{rsi} \epsilon_{ijk} \iiint (\underline{R}' - \underline{R})_s d\overline{Z}_j^*(\underline{R}, \omega) dY'_{o_k}(\underline{R}')$$

$$= \epsilon_{rsi} \epsilon_{ijk} \iiint (\underline{R}' - \underline{R})_s d\overline{Z}_j^*(\underline{R}, \omega) dY'_{o_k}(\underline{R}')$$

$$= \epsilon_{rsi} \epsilon_{ijk} \iiint (\underline{R}' - \underline{R})_s d\overline{Z}_j^*(\underline{R}, \omega) dY'_{o_k}(\underline{R}')$$

$$= \epsilon_{rsi} \epsilon_{ijk} \iiint (\underline{R}' - \underline{R})_s d\overline{Z}_j^*(\underline{R}, \omega) dY'_{o_k}(\underline{R}')$$

$$= \epsilon_{rsi} \epsilon_{ijk} \iiint (\underline{R}' - \underline{R})_s d\overline{Z}_j^*(\underline{R}, \omega) dY'_{o_k}(\underline{R}')$$

$$= \epsilon_{rsi} \epsilon_{ijk} \iiint (\underline{R}' - \underline{R})_s d\overline{Z}_j^*(\underline{R}, \omega) dY'_{o_k}(\underline{R}')$$

$$= \epsilon_{rsi} \epsilon_{ijk} \iiint (\underline{R}' - \underline{R})_s d\overline{Z}_j^*(\underline{R}, \omega) dY'_{o_k}(\underline{R}')$$

$$= \epsilon_{rsi} \epsilon_{ijk} \iiint (\underline{R}' - \underline{R})_s d\overline{Z}_j^*(\underline{R}, \omega) dY'_{o_k}(\underline{R}')$$

The term on the right hand side of (3.32) is not in a useful form. An alternative expression may be obtained by starting from the Green's function representation (2.22), with  $\overline{u} = 0$  and  $G_{ij}$  defined by (2.61). Substituting the Fourier representations (2.63) and (3.14) for  $R_{ij}$  and  $\overline{B}$  in this equation, and making use of (3.13) we obtain

$$\begin{split} &\left\{i\Omega+\eta\,K^2+\,\,\mathbf{I}^{(i)}(\underline{K},\Omega)\right\} \widehat{\overline{B}}_{r}(\underline{K},\Omega)\,\,e^{i\left\{\underline{K}\cdot\underline{x}+\Omega t\right\}} \\ &=-\varepsilon_{rsi}\varepsilon_{ijk}\left\{K_{s}\,\widehat{\overline{B}}_{k}\,\,e^{i\left\{\underline{K}\cdot\underline{x}+\Omega t\right\}}\,\,. \\ &\cdot \iint_{\underline{K}\,\omega} \frac{(\underline{k}+\underline{K})_{p}\,\underline{\Phi}_{jp}(\underline{k},\omega)}{i(\omega+\Omega)+\eta(\underline{k}+\underline{K})^{2}}\,\,e^{-\left[i(\omega+\Omega)+\eta(\underline{k}+\underline{K})^{2}\right](t-t_{o})}\,\,d\underline{k}\,d\omega \\ &-\int_{all\,\,space} \frac{-r^{2}/4\eta(t-t_{o})}{2\pi}\left[4\pi\eta(t-t_{o})\right]^{-3/2}\,. \\ &\cdot \frac{\partial}{\partial x_{s}}\left[u'_{j}(\underline{x},t)\,B'_{op}(\underline{x}-\underline{r},t_{o})\right]\,\,\right\} \end{aligned} \eqno(3.33)$$

3.3)2 Initial condition I - B' independent of  $\overline{B}$ 

We may now consider the effect of various initial conditions on the form of the dispersion relation. If

$$\overline{u'_{j}(x,t) B'_{o_{k}}(x',t_{o})} = O \qquad (3,34)$$

or, less restrictively, if

$$u'_{i}(x,t) B'_{ox}(x',t_{o}) = f_{ik}(x'-x;t,t_{o})$$
 (3.34').

equation (3.33) reduces to

$$i\Omega + \eta K^{2} = -K_{i} \iint \frac{(\underline{k} + \underline{K})_{p} \Phi_{ip}(\underline{k}, \omega)}{i(\omega + \Omega) + \eta(\underline{k} + \underline{K})^{2}} \cdot \left\{ 1 - e^{[i(\omega + \Omega) + \eta(\underline{k} + \underline{K})^{2}](t - t_{o})} \right\} d\underline{k} d\omega \qquad (3.35)$$

or

$$i\Omega + \eta K^{2}$$

$$= -K_{j} \int_{0}^{t-t_{o}} e^{-i\Omega \tau} d\tau \int_{\mathbb{R}} (\underline{R} + \underline{K})_{p} \hat{R}_{jp}(\underline{R}; \tau) e^{-\eta (\underline{R} + \underline{K})^{2\tau}} d\underline{R}$$
(3.35)

where  $R_{ij}(\c k; au)$  is the spatial Fourier transform of the correlation tensor  $R_{ij}$  , defined by

$$R_{ij}(\mathbf{r},\tau) = \int \hat{R}_{ij}(\mathbf{k};\tau) e^{i\mathbf{k}\cdot\mathbf{r}} d\mathbf{k}$$
 (3.36)

The "dispersion relation" (3.35) or (3.35') is clearly time-dependent. If Im  $\Omega>0$  , values of k such that

$$\eta \left( \underline{k} + \underline{K} \right)^2 < Im \Omega$$
 (3.37)

will provide contributions to the integral on the right hand side of (3.35') which do not tend to zero as  $(t-t_0)$  goes to infinity.

### 3.3.3 Initial condition $II = \mathbf{B}'$ correlated with $\overline{\mathbf{B}}$

A second possible initial condition is that the right hand side of (3.32) or (3.33) should vanish. This condition is satisfied if

$$\frac{dZ_{j}^{*}(\underline{R},\omega)dY_{o_{k}}^{\prime}(\underline{R}^{\prime})}{dZ_{j}^{*}(\underline{R},\omega)} = \sum_{j,k} (\underline{R},\omega) \delta(\underline{R}-\underline{R}^{\prime}) d\underline{R} d\underline{R}^{\prime}d\omega \qquad (3.38)$$

or

$$\left\{\operatorname{curl}\left(\underline{\mathbf{u}}'\times\underline{\mathbf{B}}'_{o}\right)\right\}\left(\underline{\mathbf{x}},\mathbf{t}_{o}\right)=-\widehat{\underline{\mathbf{B}}}_{r}(\underline{\mathbf{x}},\Omega)\,e^{i\left\{\underline{\mathbf{x}}\cdot\underline{\mathbf{x}}+\Omega\mathbf{t}_{o}\right\}}\,\mathbf{I}^{(i)}(\underline{\mathbf{x}},\Omega) \qquad (3.38')$$

or

$$\overline{u_j'(x,t)\,B_{o_{\chi}}'(x_j',t_o)} = -i\,\widehat{\overline{B}}_{\chi}(\underline{\kappa},\Omega)\,e^{i\{\underline{\kappa}\cdot\underline{x}+\Omega\,t\}}.$$

$$\int \int \frac{(\underline{R} + \underline{K})_p \, \underline{\Phi}_{jp}(\underline{k}, \omega)}{i(\omega + \Omega) + \eta(\underline{R} + \underline{K})^2} .$$

(3.38")

implying that the fluctuating fields  $\underline{u}'$  and  $\underline{B}'$  are correlated even at time  $t=t_0$ , and that  $\underline{B}'$  is always proportional to  $|\overline{B}|$ . Under these circumstances, the dispersion relation (3.15)-(3.16) is valid for all  $\Omega$ .

3.4 PT-invariant turbulence and decaying mean fields - initial condition II

#### 3.4.1 The mean field dispersion relation

Let us first examine the case when initial condition [1] (3.38) applies. The dispersion relation is, rewriting (3.15) and (3.16),

$$i\Omega + \eta K^2 + I^{(i)}(K,\Omega) = 0$$
 (3.39)

where

$$\mathbf{I}^{(i)}(\mathbf{K}, \Omega) \equiv \iint_{\mathbf{R}\omega} \frac{\mathbf{K}_{j} \, \mathbf{P}_{jp}(\mathbf{k}, \omega) (\mathbf{k} + \mathbf{K})_{p}}{i(\omega + \Omega) + \eta (\mathbf{k} + \mathbf{K})^{2}} \, d\mathbf{k} \, d\omega \qquad (3.40)$$

When Im  $\Omega \geqslant 0$  , there is a pole on the integration contour in (3.40), at ,

$$\dot{\omega} = -\Omega + i \eta (R + K)^2 \qquad (3.41)$$

and the integral must be defined in terms of a Cauchy principal value.

### 3.4.2 The mean field dispersion relation for isotropic. turbulence in an incompressible fluid

When the turbulence is isotropic and the fluid is incompressible, the spectrum tensor is given by (3.7) and the integral (3.40) may be written in the form (3.19). We may then discuss the behaviour of the integral in terms of

the function  $\theta(\xi,\nu;p)$  defined th (3.20). For all p<1 Re  $\theta^{\nu}$  is a non-negative function of  $\xi$  and  $\nu$ , going to zero along the line  $\xi=0$ . In addition, Re  $\theta$  is an even function of  $\nu$ , tending monotonically to zero as  $|\nu| + \infty$ . The behaviour of Re  $\theta$  with  $\xi$  is indicated in Figure 1, where the function is plotted against  $\xi$  for  $\nu=0$ , for several typical values of p. From this behaviour it is clear that the dispersion relation (3.39) has no solutions for Im  $\Omega < \eta K^2$ , since Re I (1) is positive definite in this region, while the real part of (3.39) requires that

$$\tilde{J}_{m}\Omega - \eta K^{2} = \Re I^{(i)}(K,\Omega)$$
 (3.15)

Solutions will occur, however, when Im  $\Omega > \eta K^2$ , since now the left hand side of (3.15) is positive, while the right hand side can assume positive or negative values, according to the choice of  $(K,\Omega)$ .

The real and imaginary parts of  $\theta$  are

$$\Re\Theta(\xi, \nu; p) = 2\xi^4 \int_0^{\pi} \frac{(1+\xi^2+2\xi\cos\theta-p)\sin^3\theta}{(1+\xi^2+2\xi\cos\theta-p)^2+\nu^2} d\theta$$
 (3.42)

$$\int_{m} \Theta(\xi, \nu; p) = -2\nu \xi^{4} \int_{0}^{\pi} \frac{\sin^{3}\theta}{(1+\xi^{2}+2\xi\cos\theta-p)^{2}+\nu^{2}} d\theta$$
 (3.43)

These functions are plotted against  $\xi$  and  $\nu$  for typical values of p > 1 in Figure 2.

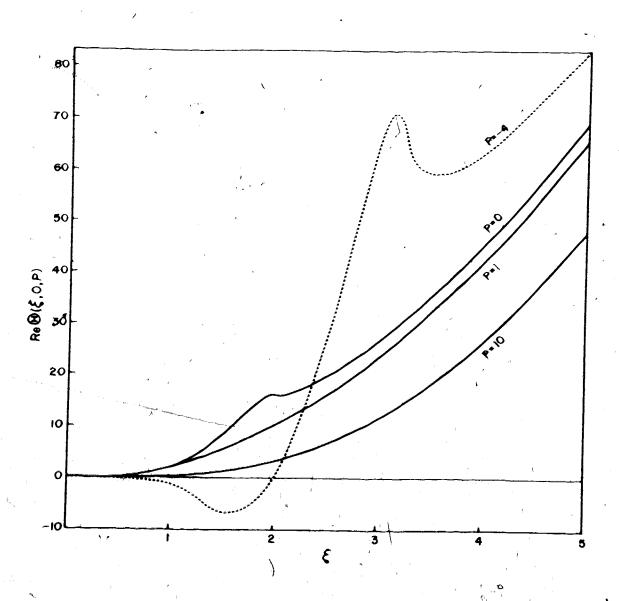
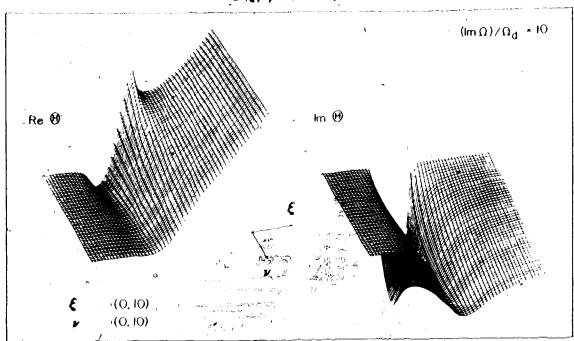


Figure 1. Re  $\theta(\xi,0;p)$  as a function of  $\xi$  for various p.

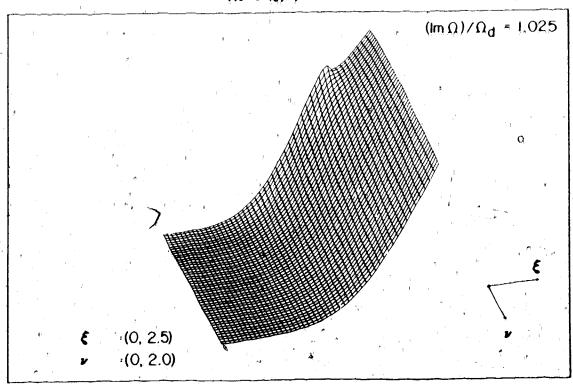
Figure 2.  $\theta(\xi, \nu; p)$  as a function of  $\xi$  and  $\nu$  for two values of p.

In the plots shown, p has been replaced by  $(\operatorname{Im}\Omega)/\Omega_{\rm d}$ , where  $\Omega_{\rm d}\equiv\eta K^2$ . In the upper plot, Re  $\theta$  and Im  $\theta$  are plotted against  $\xi$  and  $\nu$  for  $\rho=10$ , while in the lower plot, Re  $\theta$  is plotted against  $\xi$  and  $\nu$  for  $\rho=1.025$ .





### Re $\Theta\left(\xi,\nu,\operatorname{Im}\Omega/\Omega\mathrm{d}\right)$



From (3.19),

$$I^{(i)}(\underline{K},\Omega)$$

$$= \frac{1}{4} K^7 \int_{-\infty}^{\infty} dv \int_{-\infty}^{\infty} dv \int_{-\infty}^{\infty} \frac{1}{(K\xi)^4} E(K\xi, \eta K^2 v + \Re\Omega) \Theta(\xi, v, 4m \frac{\Omega}{\eta K^2})$$
(3.44)

Since  $E(k,\omega)$  is purely real, Re I<sup>(1)</sup> is determined by Re 0, while Im I<sup>(1)</sup> is determined by Im  $\blacksquare$ 

## 3.4.3 The nature of the dispersion relation - contrast between oscillatory and non-oscillatory mean fields

Since Im  $\theta$  is an odd function of  $\nu$ , while  $E'(k,\omega)$  is by definition an even function of  $\omega$ , it follows from (3.44) that Im  $I^{(1)} \equiv 0$  whenever  $\text{Re }\Omega = 0$  In this case, the imaginary part of (3.39),

$$\Re \Omega = - \operatorname{Im} \operatorname{I}^{(i)}(\underline{K}, \Omega)$$
 (3.16)

is satisfied identically. When Re  $\Omega \neq 0$ , however, (3.16) is no longer trivially satisfied, and (3.15) and (3.16) may be considered as an eigenvalue problem. If we define

$$A \cdot \hat{h}(k,\omega) = E(k,\omega)/k^4$$
,  $\hat{h}(0,0) = 1$  (3.45)

and let

$$P = 1 + \frac{i\Omega}{nK^2}$$
 (3.46)

(3.39) can be written in the form

$$A\begin{pmatrix} Re P \\ Im P \end{pmatrix} = \frac{\eta}{AK^5}\begin{pmatrix} Re P \\ Im P \end{pmatrix}$$
(3.47)

where  $\mathbf{A}$  is a complex-valued integral operator. The parameter  $\eta/\Delta K^5$  may then be considered as an eigenvalue for the problem (3.47).

Solutions to the dispersion relation (3.39) are thus of two types – those with Re  $\Omega=0$ , and those with Re  $\Omega\neq 0$ . In the limit as Re  $\Omega \to 0$ , solutions of the second type may form a discrete subset of the set of solutions of the first type.

### 3.5 Digression: the properties of stationary, homogeneous, isotropic turbulence

#### 3.5.1 General properties

Before continuing with a more detailed study of the solutions of the mean field dispersion relation, let us consider the significance of the function (3.45). For isotropic turbulence, the correlation tensor is of the form

$$R_{ij}(x,\tau) = F(x,\tau) r_{i}r_{j} + G(x,\tau) \delta_{ij} \qquad (3.48)$$

(Batchelor, 1953, p. 45ff.), and we may define longitudinal and transverse correlation functions  $f(r,\tau)$  and  $g(r,\tau)$  such that

$$u_{\rm cp}^2$$
  $f(r,\tau) \equiv u_{\rm cp}(x,t) u_{\rm cp}(x+r,t+\tau) = r^2 F(r,\tau) + G(r,\tau)$  (3.49)

$$u_{(m)}^{2} g(r,t) \equiv u_{(m)}(x,t) u_{(n)}(x+r,t+r) = G(r,t)$$
 (3.50)

 $u_{(p)}$  and  $u_{(n)}$  denote velocity components parallel and normal respectively to the vector separation  $\underline{r}$  (Batchelor, 1953, p. 46), and

$$u_{(p)}^2 \equiv u_{(n)}^2 \equiv \frac{1}{3} u_i'(x,t) u_i'(x,t) \equiv \frac{1}{3} u^2$$
 (3.51)

The Fourier transforms of  $R_{ij}$  , f , and g are

$$\hat{R}_{ij}(\underline{k},\omega) = \Phi_{ij}(\underline{k},\omega) = -\frac{\partial^2 \hat{F}(\underline{k},\omega)}{\partial k_i \partial k_j} + \hat{G}(\underline{k},\omega) \delta_{ij}$$

$$= -\frac{1}{R} \frac{\partial}{\partial k} \left\{ \frac{1}{R} \frac{\partial \hat{F}}{\partial k} \right\} k_i k_j + \left\{ \hat{G} - \frac{1}{R} \frac{\partial \hat{F}}{\partial k} \right\} \delta_{ij} \qquad (3.52)$$

$$\frac{1}{3}\overline{u^{2}} \hat{f}(\mathbf{R},\omega) = -\nabla_{\mathbf{R}}^{2} \hat{f}(\mathbf{R},\omega) + \hat{\mathbf{G}}(\mathbf{R},\omega)$$

$$= -\frac{1}{\mathbf{R}^{2}} \frac{\partial}{\partial \mathbf{R}} \left\{ \mathbf{R}^{2} \frac{\partial \hat{\mathbf{F}}}{\partial \mathbf{R}} \right\} + \hat{\mathbf{G}}$$
(3.53)

$$\frac{1}{3}\overline{u^2}\,\hat{g}\left(\mathbf{k},\omega\right) = \hat{G}\left(\mathbf{k},\omega\right) \tag{3.54}$$

#### 3.5.2 Isotropic turbulence in an incompressible fluid

For incompressible flow, the spectrum tensor  $\Phi_{ij}$  must satisfy (3.4), so that

$$-k\frac{\partial}{\partial k}\left\{\frac{1}{k}\frac{\partial \hat{F}}{\partial R}\right\} + \left\{\hat{G} - \frac{1}{k}\frac{\partial \hat{F}}{\partial R}\right\} = -\frac{\partial^2 \hat{F}}{\partial R^2} + \hat{G} = 0$$

giving

$$\hat{\mathbf{G}}(\mathbf{k},\omega) = \frac{\partial^2}{\partial \mathbf{k}^2}, \hat{\mathbf{F}}(\mathbf{k},\omega)$$
 (3.55)

From (3,52) and (3,55),

$$\frac{1}{3}u^2 \, \hat{f}(R,\omega) = -\frac{2}{R} \frac{\partial}{\partial R} \hat{f}(R,\omega)$$

so that, for incompressible flow,

$$\frac{1}{R} \frac{\partial \hat{F}}{\partial R} = -\frac{1}{G} u^{2} \hat{f} , (3.56)$$

$$\hat{G} = \frac{1}{3} u^{2} \hat{g} = \frac{\partial^{2} \hat{F}}{\partial R^{2}} = -\frac{1}{G} u^{2} \frac{\partial}{\partial R} (R \hat{f}) , (3.57)$$

$$\Phi_{ij} = \frac{1}{G} u^{2} \frac{1}{R} \frac{\partial \hat{F}}{\partial R} R_{i} R_{j} + \left\{ -\frac{1}{G} u^{2} \frac{\partial}{\partial R} (R \hat{f}) + \frac{1}{G} u^{2} \hat{f} \right\} \delta_{ij}$$

$$= -\frac{1}{G} u^{2} \frac{1}{R} \frac{\partial \hat{F}}{\partial R} \left\{ R^{2} \delta_{ij} - R_{i} R_{j} \right\} , (3.58)$$

13

# 3.5.3 $E(k,\omega)/k^4$ for isotropic turbulence in an incompressible fluid

From (3.7), the energy spectrum function  $E(k,\omega)$  is given by

$$E(k,\omega) = 2\pi k^2 \Phi_{ij}(k,\omega) \qquad (3.59)$$

Thus, by (3.58) and (3.59),

$$E(\mathbf{k},\omega) = -\frac{2\pi}{3} \overline{\mathbf{u}^2} \, \mathbf{k}^3 \, \frac{\partial}{\partial \mathbf{k}} \, \hat{\mathbf{f}}(\mathbf{k},\omega) \tag{3.60}$$

The function (3,45) can therefore be represented as

$$A_{1}\hat{h}(k,\omega) \equiv E(k,\omega)/k^{4} = -\frac{2\pi}{3}\overline{u^{2}}\frac{1}{k}\frac{\partial}{\partial k}\hat{f}(k,\omega)$$
(3.61)

where

$$A = \left\{ \frac{E(k,\omega)}{k^4} \right\}_{k=0=\omega} = -\frac{2\pi}{3} \overline{u^2} \left\{ \frac{1}{k} \frac{\partial}{\partial k} \hat{f}(k,\omega) \right\}_{k=0=\omega}$$
(3.62)

From the definition of the Fourier transform,  $\hat{f}(k,\omega)$  is given by

$$\hat{f}(k,\omega) = \frac{1}{(2\pi)^4} \int_{-\infty}^{\infty} d\tau \int_{-\infty}^{\infty} dr f(r,\tau) e^{-i\left\{\frac{k}{2}, r + \omega\tau\right\}}$$

$$= \frac{2}{(2\pi)^3} \int_{-\infty}^{\infty} d\tau e^{-i\omega\tau} \int_{0}^{\infty} dr r^2 f(r,\tau) \frac{\sin kr}{kr}$$
(3.63)

Thus

$$E(R,\omega)/k^{4} = -\frac{2}{3(2\pi)^{3}} \overline{u^{2}} \int_{-\infty}^{\infty} e^{-i\omega \tau} d\tau \cdot \int_{0}^{\infty} r^{4} f(r,\tau) \frac{1}{(kr)^{2}} \left\{ \cos kr - \frac{\sin kr}{kr} \right\} dr \quad (3.64)$$

The oscillatory factor in the integrand of (3.64) may be expanded in a Taylor series about kr = 0.

$$\frac{1}{(kr)^2} \left\{ \cos kr - \frac{\sin kr}{kr} \right\} = -\frac{1}{3} \left\{ 1 - \frac{(kr)^2}{10} + \cdots \right\}$$
 (3.65)

Substituting (3.65) into (3.64), and taking the limit  $k \to 0$  ,  $\omega \to 0$  , we have, from (3.62), that

$$A = \left\{ \frac{E(\mathbf{r}, \omega)}{k^4} \right\}_{\mathbf{R} = 0 = \omega} = \frac{2}{9(2\pi)^2} \overline{u^2} \int_{-\infty}^{\infty} d\tau \int_{\mathbf{r}}^{\infty} r^4 f(\mathbf{r}, \tau) d\mathbf{r}$$
(3.66)

## 3.5.4 Gaussian isotropic turbulence in an incompressible fluid

The expressions (3.64) and (3.66) may be used to evaluate  $E/k^4$ ,  $\hbar$ , and A for any desired type of isotropic turbulence. Consider first the case when the longitudinal correlation function is Gaussian, so that

$$f(r,\tau) = e^{-\frac{1}{2} \{r^2/\lambda_c^2 + \tau^2/\tau_c^2\}}$$
 (3.67)

 $\lambda_{_{\mbox{\scriptsize C}}}$  and  $\tau_{_{\mbox{\scriptsize C}}}$  are the correlation length and correlation time of the turbulence.

Substituting (3.67) into (3.64) and (3.66), we obtain

$$E(R,\omega)/R^4 = \frac{1}{6\pi} \overline{u^2} \lambda_c^5 \tau_c e^{-\frac{1}{2} \{(\lambda_c R)^2 + (\tau_c \omega)^2\}}$$

$$A = \frac{1}{6\pi} \overline{u^2} \lambda_c^5 \tau_c$$
(3.69)

(See Gradshteyn and Ryzhik, 1965, equations 3.952.4, 3.952.1, and 3.461.2 for the integral formulae used in obtaining 3.68 and 3.69.) From (3.68), (3.69), (3.45), and (3.63),

$$\hat{h}(k,\omega) = e^{-\frac{1}{2}\{(\lambda_c k)^2 + (\tau_c \omega)^2\}} = \frac{(2\pi)^2}{\lambda_c^3 \tau_c} \hat{f}(k,\omega)$$
 (3.70)

### 3.5.5 Gaussian-exponential isotropic turbulence in an incompressible fluid

As a second example, consider the case in which the longitudinal correlation function is Gaussian in space and exponential in time.

$$f(r,\tau) = e^{-r_{/2}^2 \lambda_c^2} - \frac{|\tau|}{\tau_c}$$
 (3.71)

From (3.64), (3.66), and (3.71),

$$E(k,\omega)/k^4 = \frac{1}{6\pi} \sqrt{\frac{2}{\pi}} \frac{1}{u^2} \lambda_c^5 \tau_c \frac{e^{-\frac{1}{2}(\lambda_c k)^2}}{1 + (\tau_c \omega)^2}$$
(3.72)

$$A = \frac{1}{6\pi} \sqrt{\frac{2}{\pi}} u^2 \lambda_c^5 t_c$$
 (3.73)

(See Gradshteyn and Ryzhik, 1965, equations 3.952.4, 3.952.1, 3.461.2, and 3.310.) From (3.72); (3.73), (3.45), and (3.63),

$$\hat{h}(k,\omega) = \frac{1}{1 + (r_c\omega)^2} e^{-\frac{1}{2}(\lambda_c k)^2} = \frac{(2\pi)^2 \sqrt{\pi/2}}{\lambda_c^2 \tau_c} \hat{f}(k,\omega)$$
 (3.74)

The correlation functions (3.67) and (3.71) have been used fairly widely in the literature. (See, for example, P.H. Roberts, 1971a; Krause and Rädler, 1971.)
The results obtained in (3.68)-(3.70) and (3.72)-(3.74) are summarized in Table 12, p. 149; along with similar results for "exponential-Gaussian" and "exponential" isotropic turbulence.

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Turbulence	f(r, t)	ች(አ,ቈ)	U	f(x,w)/f <sub>o</sub>	0 6 6 6
Gaussian	e-1[r3/2 + r3/2;}	e-#{(nxc)+(wrc)}	-15	ۍ (ه.ک) ۲	(2n) <sup>3</sup>
Gaussian- exponential	e-{r/2x +1=1/e.}	e-4(R),3		B(R, E)	(2m) <sup>2</sup> (4/4)
Exponentiage. Gaussian	Exponenti e-{"/\c + \c^2\z\c ?\ \cappa = \ \cappa \cappa \cdots \	e-4(ωτ.)² {1 + (κλ.)² }³	4 E	[1+(K).7] h(k,w) 4	4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Exponential	e-{"/x. + IT//e.}	1 {1+60€;}}[1+6R\\) <sup>3</sup> ] <sup>3</sup>	8 3ft \$	{ 1+ (R), } \( (a, (a))	12

Fourier transform of longitudinal correlation function = longitudinal correlation function £(0,0)

 $E(k,\omega) = \text{energy spectrum function} = c \cdot (u^2) \frac{5}{c^2} \cdot \hat{h}(k,\omega) \cdot x^4$ 

[See equations (3.59)-(3.66) and (3.75)-(3.76),]

- 3.6 <u>Isotropic turbulence and decaying mean fields</u> initial condition *II*
- 3.6.1 The nature of the eigenvalue for oscillating mean fields

We may now use (3.69) and (3.73) to determine the nature of the "eigenvalue"  $\eta/\Delta K^5$  in (3.47) for the cases of "Gaussian" and "Gaussian-exponential" turbulence. Comparing the two equations, we see that

$$AK^{5}/\eta = C \cdot \frac{u^{2}\lambda_{c}^{5}\tau_{c}}{\eta} \cdot K^{5} = C \cdot \left\{\frac{u^{2}\lambda_{c}^{2}}{\eta^{2}}\right\} (\lambda_{c}K)^{5} (\eta\tau_{c}/\lambda_{c}^{2})$$

$$= C \cdot \left\{(R'_{m})^{2}/q\right\} (\lambda_{c}K)^{5}$$

$$= C \cdot (R'_{m})^{2} (\lambda_{c}K)^{3} (\eta K^{2}\tau_{c}) \qquad (3.75)$$

where we have made use of the definitions (2.68) and (2.69), and the identification

$$u' = \sqrt{\overline{u^2}}$$
 (3.76)

C is a constant determined by the form of  $f(r,\tau)$ .

It may be seen from Table 12 that (3.75) is a general expression applying to any type of stationary, homogeneous, isotropic turbulence. Values of C are given in the table for "Gaussian", "Gaussian-exponential", "exponential-Gaussian", and "exponential" turbulence.

The quantity  $\lambda_{C}K$  in (3.75) can be interpreted as a ratio of length scales. The wavelength of the mean field

is

$$L = 2\pi/K \tag{3.77}$$

so that

$$\lambda_{C}K = 2\pi \cdot (\lambda_{C}/L) \tag{3.78}$$

Similarly, the quantity  $\eta K^2 \tau_C$  can be interpreted as a ratio of time scales. In the absence of turbulence, the mean field  $\overline{\underline{B}}$  will decay as  $\exp\{-\eta K^2 t\}$ , so that the mean field decay time is

$$T_{d} = 1/\eta K^2 \tag{3.79}$$

Therefore,

$$\eta K^2 \tau_c = \tau_c / T_d \qquad (3.80)$$

and the eigenvalue n/AK5 can be expressed as

$$(\eta/AK^5)^{-1} = (2\pi)^3 \cdot C \cdot (R_m^*)^2 \cdot (\lambda_C/L)^3 \cdot (\tau_C/T_d)$$

## 3.6.2 Non-oscillatory mean fields - the dispersion relation and the effective magnetic diffusivity

We may now examine the solutions of (3.39) more closely. Consider first the case in which  $\text{Re }\Omega=0$ . Then by (3.15), (3.44), (3.45), and (3.75) the mean field dispersion relation has the form

$$\Im m \frac{\Omega}{\eta K^2} - 1 \tag{3.83}$$

= 
$$\frac{1}{4} C \frac{(R_m')^2}{q} (\lambda_c K)^5 \int_{-\infty}^{\infty} d\nu \int_{0}^{\infty} d\vec{r} \hat{h}(K\vec{r}, \eta K^2 \nu) \operatorname{Re} \Theta\{\vec{r}, \nu; \operatorname{Im} \frac{\Omega}{\eta K^2}\}$$

The parameter Im  $\Omega/\eta K^2$  may be interpreted in terms of an effective magnetic diffusivity,  $\eta_{\mbox{eff}}$ . When no turbulence is present, the solution of (3.83) is

$$\operatorname{Im} \Omega = \operatorname{\gamma} K^2 \tag{3.84}$$

and the mean field decays as  $\exp[-\eta K^2 t]^2$ . When there is turbulence present, the mean field decays more rapidly, with the exponential factor now being  $\exp[-Im\Omega \cdot t]$ . We may therefore define

$$J_{m}\Omega \equiv \eta_{eff} K^2$$
 (3.85)

by analogy with (3,84), so that

$$\int_{M} \Omega / \eta K^{2} = \eta eff / \eta \qquad (3.86)$$

Equation (3.83) may be rewritten in the form

$$(R'_{m})^{2} = \frac{4q}{C \cdot (\lambda_{c}K)^{5}} \left\{ \operatorname{Peff}_{\eta} - 1 \right\} \left\{ \int_{-\infty}^{\infty} dv \left[ d\xi \, \hat{h}(K\xi, \eta K^{2}V) \cdot \right] \right\} \left\{ \left[ -\infty \right] \left[ -\infty \right] \left[ -\infty \right] \left[ -\infty \right] \right\} \left[ -\infty \right] \left[ -\infty \right]$$

specifying the magnetic Reynolds number of the turbulence,  $R_m^{\prime}$ , as a function of  $\eta_{\mbox{eff}}/\eta$ , q,  $\lambda_{\mbox{c}} K$ , and  $\eta K^2 \tau_{\mbox{c}}$ . In principle, (3.87) can be inverted to give  $\eta_{\mbox{eff}}/\eta$  as a function of  $R_m^{\prime}$ , q,  $\lambda_{\mbox{c}} K$ , and  $\eta K^2 \tau_{\mbox{c}}$ .

69.

### 3.6.3 Insensitivity of the effective diffusivity to initial conditions when $\lambda_{C}K$ is small

In order to establish a correspondence between (3.83) and the results obtained using the Rädler expansion technique, we must investigate the limiting behaviour of (3.83) as  $\lambda_{\rm C} K \neq 0$ . Making a change of variable in the integral,

$$\frac{4}{C(R_m')^2} \left\{ \operatorname{Peff}_{\eta}^{\Lambda} - 1 \right\}$$

$$= (\lambda_c K)^2 \int d\nu \int \hat{h} \left\{ \bar{t}_{\lambda_c}, \nu_{\tau_c} \right\} \operatorname{Re} \left\{ \bar{t}_{\lambda_c K}, \nu_{\eta K^2 \tau_c}, \operatorname{Peff}_{\eta} \right\} d\xi$$
(3.88)

From (3.42) and Figures 1 and 2 we can see that the dominant contribution to the integral in (3.88) will come from the values of Re 0 ( $\xi$ , $\nu$ ;p) at large  $\xi$ , since Re 0  $\leftrightarrow \infty$  as  $\xi \leftrightarrow \infty$ . From (3.42) we have

$$Re \Theta \{ \frac{3}{\lambda_{cK}} \frac{\sqrt{\eta K^{2} \tau_{c}}; p \} = Re \Theta \{ \frac{3}{\lambda_{cK}}, \frac{9}{\eta (\lambda_{cK})^{2}}; p \}$$

$$= \frac{2 f^{4}}{(\lambda_{cK})^{2}} \int_{0}^{\pi} \frac{f^{2} + 2(\lambda_{cK}) f \cos \theta + (\lambda_{cK})^{2} (I-p)}{[f^{2} + 2(\lambda_{cK}) f \cos \theta + (\lambda_{cK})^{2} (I-p)]^{2} + [\sqrt{\eta}]^{2}} \sin^{3}\theta d\theta$$
(3.89)

Expanding the integrand in (3.89) as a power series in  $\lambda_{\rm C} {\rm K}$  and integrating term by term,

$$= \frac{8}{3(\lambda_{c}K)^{2}} \frac{\xi^{4} + (\nu q)^{2}}{\{\xi^{4} + (\nu q)^{2}\}} - \left\{1 + \frac{(\lambda_{c}K)^{2}}{\xi^{2}[\xi^{4} + (\nu q)^{2}]} \left[\frac{1}{5}\xi^{4}(3\xi^{4} - \nu^{2}q^{2}) + (p-1)\xi^{8} - \nu^{4}q^{4}\right]\right\}$$

$$+ \dots \} \qquad (3.90)$$

Substituting (3.90) into (3.88) and dropping terms of order  $(\lambda_c K)^{\frac{2}{2}}$ ,

$$\left\{ \frac{\text{Teff}}{\eta - 1} = \frac{2C(R_m')^2}{3} \int_{-\infty}^{\infty} d\nu \int_{-\infty}^{\infty} \frac{F^c}{F^4 + (\nu q)^2} \hat{h}(F/\lambda_c, \nu/\tau_c) dF + O\{(\lambda_c K)^2\} \right\}$$
(3.91)

Equation (3.91) shows that when  $(\lambda_{\rm C} {\rm K})^2$  is small the effective diffusivity is independent of the properties of the mean field, and depends only on the properties of the turbulence. The equation can be shown to be identical to the result obtained by Krause and Radler (1971, equations 7.85, 7.39a, 7.43b), using initial condition I (6.34) rather than initial condition II (3.38). The effective diffusivity is therefore also independent of the initial conditions on B' when  $(\lambda_{\rm C} {\rm K})^2$  is small.

3.6.4 Comparison of results for small  $\lambda_{C}K$  with the results of Krause and Kädler

Applying (3.91) to turbulence of the Gaussian type (3.67)-(3.70), we obtain

$$\begin{cases} \eta_{eff}/\eta - 1 \end{cases} = \frac{(R'_m)^2}{9\pi} \int_{-\infty}^{\infty} dv \int_{-\overline{K}^4 + (Vq)^2}^{\overline{K}^4 + (Vq)^2} e^{-\frac{1}{2}(\xi^2 + V^2)} d\xi + \mathcal{O}(\lambda_c^2 K^2)$$

$$= \frac{(R'_m)^2}{9} \sqrt{\frac{2}{\pi}} \int_{0}^{\infty} e^{-(qt)^2/2} dt \int_{0}^{\overline{K}^4 + (Vq)^2} d\xi + \mathcal{O}(\lambda_c^2 K^2)$$

$$= \frac{1}{3} (R'_m)^2 \int_{0}^{\infty} e^{-(qt)^2/2} \frac{dt}{(2t+i)^{5/2}} + \mathcal{O}(\lambda_c^2 K^2)$$
 (3.92)

making use of a number of standard integral formulae

(Gradshteyn and Ryphik, 1965, equations 3,466.1, 8,252.6,
and 3,461.2).

Similarly, for turbulence of the Gaussian-exponential type (3.71)-(3.74),

(Gradshteyn and Ryzhik, 1965, equations 3.264.2 and 3.461.2)

The final expressions in (3.92) and (3.93) have been written in a form closely similar to that used by Krause and Kädler (1971, pp. 67-70) to facilitate comparison. In Figure 3,  $9[(\eta_{eff}/\eta)-1]/R_m'$  has been plotted as a function of q for  $\lambda_c K = 0$ , making use of (3.92) and (3.93). The upper curve corresponds to (3.92) and the lower curve to (3.93).

It should be noted that equation 7.34, p. 69 of

Krause and Kädler (1971) is in error. For Gaussian turbulence, the expression should read

$$\beta^{(\lambda\nu)} = \frac{\lambda_c^{2\lambda} \tau_c^{\nu+1}}{3 \cdot 2^{\lambda} \cdot \lambda! \nu!} (8/2)^{5/2} \int_{0}^{\infty} \frac{x^{\nu+\lambda} e^{-x^{\nu}/2}}{(x+8/2)^{\lambda+5/2}} dx \qquad (3.94)$$

while for Gaussian-exponential turbulence,

$$\beta^{(\lambda V)} = \frac{\lambda_c^{2\lambda} \tau_c^{V+1}}{3 \cdot 2^{\lambda} \cdot \lambda! V!} \left( \frac{q}{2} \right)^{\frac{q}{2}} \int_{-\infty}^{\infty} \frac{x^{V+\lambda} e^{-x}}{(x+q/2)^{\lambda+\frac{q}{2}}} dx$$
 (3.95)

The  $\beta^{(\chi_V)}$  are coefficients in an expansion of the dispersion relation (3.33) for initial condition I.

$$(\Omega + \eta K^2 = -u^2 K^2 \sum_{\nu,\lambda=0}^{\infty} (-1)^{\nu+\lambda} \beta^{(\lambda\nu)} (i\Omega)^{\nu} K^{2\lambda}$$
(3.96)

Thus, to a first approximation when  $Re \Omega = 0$ 

$$\eta_{eff}/\eta - 1 = \frac{\overline{u^2}}{\eta} \beta^{(oo)} + \dots$$
 (3.96')

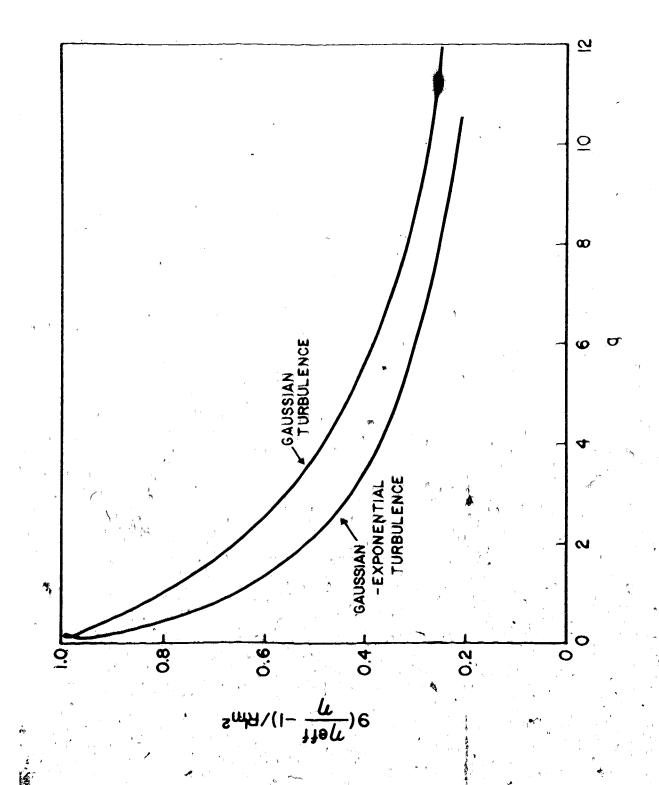
and this equation may be compared with (3.92) and (3.93).

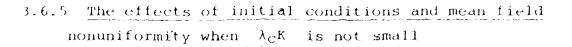
Figure 3.  $9\{[n_{eff}/n]-1\}/\{R_m^*\}^2$  as a function of q when  $\lambda_c AL = 0$ .

Upper curve: Gaussian turbulence

(see equation 3,92)

Lower curve: Gaussian-exponential turbulence (see equation 3.93)







When  $(\lambda_C K)^2$  is not small, the properties of the mean field  $\overline{B}$  and the initial conditions on B' have significant effects on the solutions of the dispersion relation (3.83). These effects are illustrated by the curves in Figures 4 and 5.

In Figure 4 the magnetic Reynolds number  $R_m$  is shown as a function of  $[(\eta_{\rm eff}/\eta)-1]$  for Gaussian turbulence, for several values of  ${\bf q}$  and  $\lambda_{\rm c}{\bf K}$ . It is interesting to note that the dispersion relation (3.83) has no solutions when  $[(\eta_{\rm eff}/\eta)-1]$  is greater than a critical value which depends mainly on  $\lambda_{\rm c}{\bf K}$ . The reason for this behaviour is immediately evident from equations (3.83) and (3.42), and from Figures 1 and 2. Re  $0(\xi,\nu;\eta_{\rm eff}/\eta)$  is negative for  $\xi < \sqrt{(\eta_{\rm eff}/\eta)-1}$ . Thus if  $\lambda_{\rm c}{\bf K}$  is large enough for  $h({\bf K}\xi,\eta{\bf K}^2\nu)$  to be effectively zero at values of  $\xi > \sqrt{(\eta_{\rm eff}/\eta)-1}$ , the right hand side of (3.83) will be negative, making a solution impossible.

In Figure 5 the function  $R_m^{\prime 2}/\{(\eta_{eR}/\eta)-1\}$  is plotted against,  $\lambda_C/L = \lambda_C K/2\pi$  for various q when  $\eta_{eff}/\eta = 1.1$ . The upper curves correspond to the initial condition (3.38) (initial condition II), and the turbulence considered i Gaussian. Gaussian-exponential turbulence will have quatatively the same behaviour, but the values of the intercepts at  $\lambda_C K = 0$  will have a different dependence on q.

This difference is clearly illustrated in Figure 3.

The lower curves in Figure 5 correspond to the initial condition (3.34) (initial condition 1), which will be considered in the next section.

Figure 4. R as a function of  $[n_{eff}/n]-1$  for several values of  $\lambda_c/L$  and q. (Initial condition  $I_r$ )

The plot shows values for Gaussian turbulence, determined from equation (3.87) with  $\hat{h}(k,\omega)$  given by equation (3.70).

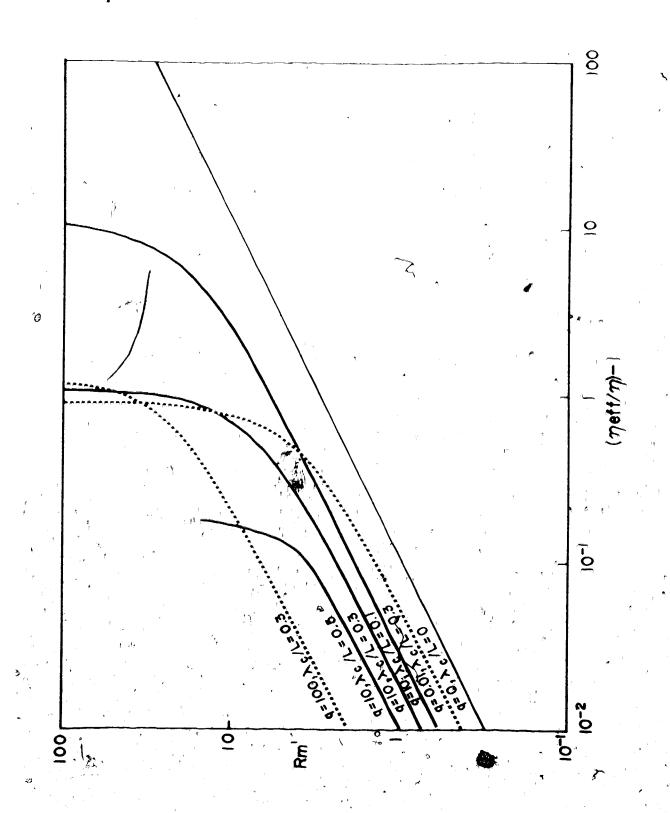
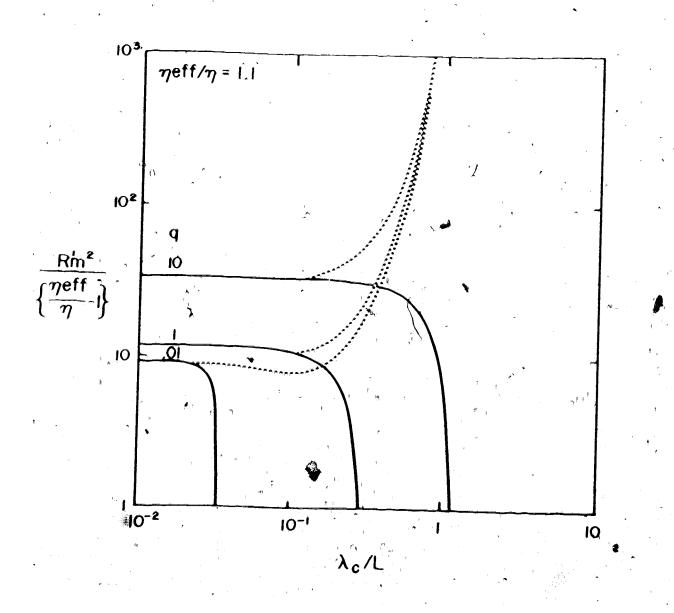


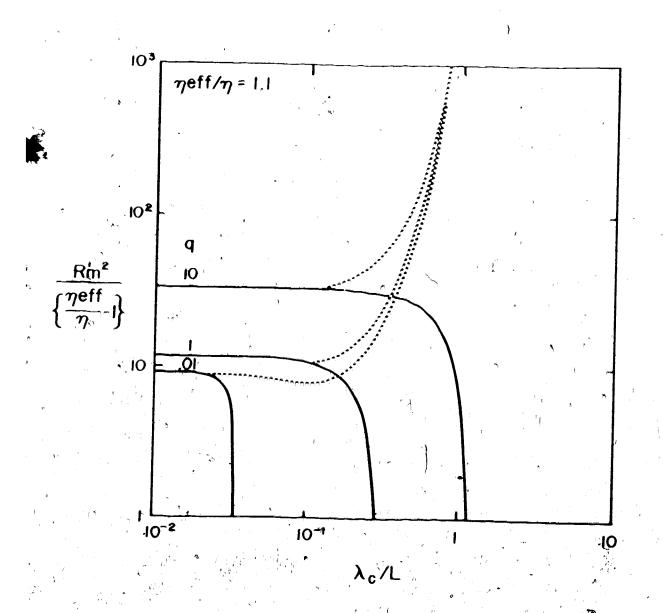
Figure 5.  $\{R_m^i\}^2/\{[\eta_{eff}/\eta]-1\}$  as a function of  $\lambda_c/L$  for several values of q when  $\eta_{eff}=1.1$   $\eta$ .

The plot shows values for Gaussian turbulence, determined from equation (3.87) with  $\hat{h}(k,\omega)$  given by equation (3.70).

Solid curves: initial condition I

Dashed curves: initial condition II





- 3.7 PT-invariant turbulence and decaying mean fields initial condition I
- 3.7.1 The mean field dispersion relation

Let us now consider the solution of the dispersion relation (3.35), corresponding to the initial condition (3.34) (initial condition I) on  $B^{+}$ . As noted above, this solution does not differ significantly from the solution (3.91) corresponding to initial condition II, when  $(\lambda_{C}K)^{2}$  is small. From (3.35) we see that the choice of initial condition has removed the pole (3.41) which occurs on the integration contour in (3.40). The dispersion relation is best written in the form (3.35')

$$i\Omega + \eta K^2 = -K_j \int_0^{t-t_0} e^{-i\Omega \tau} d\tau \int_{\mathbf{R}} (\mathbf{R} + \mathbf{K})_p \, \hat{\mathbf{R}}_{jp}(\mathbf{R}_i \tau) \, e^{-\eta (\mathbf{R} + \mathbf{K})^2 \tau} d\mathbf{R}$$
 (3.35')

It may be noted that the spatial Fourier transforms of the quantities  $R_{ij}$ , f, and g bear the same relationship to one another as do the full Fourier transforms (3.51)(3.53).

## 3.7.2 The mean field dispersion relation for isotropic turbulence in an incompressible fluid

For homogeneous, stationary, isotropic turbulence in an incompressible fluid, (3.35') reduces to

For turbulence with a Gaussian spatial correlation, like (3.67) and (3.71),

$$\hat{f}(k;\tau) = \frac{\lambda_c^3}{(2\pi)^{3/2}} e^{-(\lambda_c k)^2/2} + (\tau)$$

$$k \frac{\partial \hat{f}(k;\tau)}{\partial k} = -\frac{\lambda_c^5}{(2\pi)^{3/2}} k^2 e^{-(\lambda_c k)^2/2} + (\tau)$$
(3.98)

so that (3.97) becomes

$$i\Omega + \eta K^{2} = -\frac{u^{2}\lambda_{c}^{5}}{3}K^{2}\int_{c}^{t-t_{o}} e^{-\left\{i\Omega + \frac{\eta(\lambda_{c}K)^{2}}{\lambda_{c}^{2} + 2\eta t}\right\}t} \frac{\psi(t) dt}{\eta t^{3}}$$
(3.99)

after some reduction. A similar dispersion relation was developed by Lerche (1971a,b) and Lerche and Low (1971), in the limit as  $(t-t_0) + \infty$ .

## 3.7.3 Time dependence of the mean field dispersion relation for different types of turbulence

Taking the derivative of the right hand side of. (3.99) with respect to time, we see that

$$\frac{\partial}{\partial t} \left\{ i\Omega + \eta K^{2} \right\} = \frac{1}{3} \overline{u^{2}} \lambda_{c}^{5} K^{2} e^{-\left\{ i\Omega + \frac{\eta (\lambda_{c} K)^{2}}{\lambda_{c}^{2} + 2\eta (t-t_{o})} \right\} (t-t_{o})} \frac{\psi (t-t_{o})}{\left\{ \lambda_{c}^{2} + 2\eta (t-t_{o}) \right\}^{5/2}}$$

$$(t-t_{o}) + \infty - \frac{1}{3} \overline{u^{2}} \lambda_{c}^{5} K^{2} e^{-i\Omega (t-t_{o})} \frac{\psi (t-t_{o})}{\left\{ 2\eta (t-t_{o}) \right\}^{5/2}}$$
(3.100)

Clearly, (3.100) will diverge as  $(t-t_0) \rightarrow \infty$  unless

$$\lim_{t\to\infty} e^{\int dm \Omega(t-t_0)} \Psi(t-t_0) (t-t_0)^{-5/2} = 0$$
 (3.101)

For turbulence with a Gaussian time correlation, (3.67), (the condition (3.101) is satisfied for all values of  $\text{Im }\Omega$ ; however, for turbulence with an exponential time correlation, (3.71), condition (3.101) is only satisfied if

$$\tau_{c} \operatorname{sm} \Omega \leq 1$$
 (3.102)

For turbulence with a power-law time correlation, (3.101) is never satisfied when  $\text{Im }\Omega=\text{constant}>0$ , and the dispersion relation (3.99) has no meaning.

The time dependence of the dispersion relation (3.99) can be regarded as: an indication of the way in which the turbulence works to "build" a fluctuating field B' of

the form required by the induction equation, at the expense of the mean field  $\overline{\,{\, {\widetilde{\! E }}}}$  . If the memory of the turbulence is "too long" - as in the case of a power-law correlation - the effect of the initial, inappropriate field  $B'(x,t_0)_{t_0}$  will persist, and make it impossible for the turbulence to maintain even a decaying mean field of the type (3.14). However, if the memory of the turbulence îs "short" - as with a Gaussian time correlation - the effects of the initial, inappropriate B'-field will die away rapidly enough for the dispersion relation (3.99) to stabilize. Gaussian turbulence (3.67), this stabilization will take place fairly quickly - typically after a few correlation times. We shall therefore restrict attention in what follows to the case of Gaussian turbulence.

The mean field dispersion relation for Gaussian isotropic turbulence - non-oscillatory mean fields

For Gaussian turbulence (3,67), the time correlation function is

$$\Psi(\tau) = e^{-\tau^2/2\tau_c^2}$$
 (3.102)

and the dispersion relation (3.99) becomes

$$i\Omega + \eta K^{2} = -\frac{1}{3} \overline{u^{2}} \lambda_{c}^{5} K^{2} \int_{0}^{t-t_{0}} e^{-\tau^{2}/2\tau_{c}^{2}} - \left\{ i\Omega + \frac{\eta (\lambda_{c} K)^{2}}{\lambda_{c}^{2} + 2\eta \tau} \right\} \tau \frac{d\tau}{\left\{ \lambda_{c}^{2} + 2\eta \tau \right\}^{5/2}}$$
(3.103)

(3.103)

Equation (3.103) can be written in a number of alternative forms by making appropriate changes of variable. The most useful of these forms are:

$$i\Omega/\eta \kappa^{2} + i$$

$$= -\frac{1}{3} (R'_{m})^{2} \int_{0}^{\frac{(t-t_{0})}{8^{T_{K}}}} e^{-\frac{1}{2}q^{2}x^{2} - (\lambda_{c}K)^{2}} \left\{ \frac{i\Omega}{\eta K^{2}} + \frac{1}{1+2x} \right\} \times \frac{dx}{(1+2x)^{5/2}}$$

$$= -\frac{1}{3} \frac{(R'_{m})^{2}}{q} \int_{0}^{\frac{(t-t_{0})}{T_{c}}} e^{-\frac{1}{2}x^{2} - (\eta K^{2}t_{c})} \left\{ \frac{i\Omega}{\eta K^{2}} + \frac{1}{1+2x/q} \right\} \times \frac{dx}{(1+2x/q)^{5/2}}$$
(3.103")

When  $Re'\Omega = 0$ , these equations reduce to:

$$\int_{0}^{\infty} \frac{\Omega}{\eta K^{2}} = \frac{1}{3} (R_{m}^{1})^{2} \int_{0}^{\frac{(t-t_{0})}{q \cdot t_{0}}} e^{-\frac{1}{2} q^{2} x^{2} + (\lambda_{c} K)^{2} \left\{ \int_{0}^{\infty} \frac{\Omega}{\eta K^{2}} - \frac{1}{1+2x} \right\} x} \frac{dx}{(1+2x)^{5/2}}$$

$$= \frac{1}{3} \frac{(R_{m}^{1})^{2}}{q} \int_{0}^{\frac{(t-t_{0})}{q \cdot t_{0}}} e^{-\frac{1}{2} x^{2} + \frac{(\lambda_{c} K)^{2}}{q} \left\{ \int_{0}^{\infty} \frac{\Omega}{\eta K^{2}} - \frac{1}{1+2x/q} \right\} x} \frac{dx}{(1+2x/q)^{5/2}}$$
(3,104')

It will be noted that (3.103)-(3.104') are integral equations for  $\Omega(t-t_0)$ . When,  $\lambda_C K=0$  the integrands no longer depend on  $\Omega(t-t_0)$  and in the limit  $(t-t_0)+\infty$  (3.104) reduces to the form (3.92) specified by the Rädler expansion (3.96). When  $\lambda_C K \neq 0$ , on the other hand, Im  $\Omega/\eta K^2$  satisfies the inequality

$$(R_m^2)^2 J_1 \le 9m \frac{\Omega}{\eta \kappa^2} - 1 \le (R_m^2)^2 J_2$$
 (3.105)

where

$$J_{1}(q, \lambda_{c}K; T)$$

$$= \frac{1}{3} \int_{0}^{T/q\tau_{c}} e^{-\frac{1}{2}q^{2}x^{2} + (\lambda_{c}K)^{2} \left\{ \frac{2x^{2}}{1+2x} \right\}} \frac{dx}{(1+2x)^{2}/2}$$
(3.106)

$$J_{2}(q, \lambda_{c}K; T)$$

$$= \frac{1}{3} \int_{0}^{T/q\tau_{c}} e^{-\frac{1}{2}q^{2}x^{2} + (\lambda_{c}K)^{2} \left\{ \frac{d}{dx} \frac{\Omega(T)}{\eta K^{2}} - \frac{1}{1+2x} \right\} x} \frac{dx}{(1+2x)^{5/2}}$$

(3.106) and (3.107) have been obtained by setting Im  $\Omega/\eta K^2 = 1$  and Im  $\Omega/\eta K^2 = [Im \Omega/\eta K^2]_{t=t_0+T}$ 

respectively on the right hand side of equation (3.104).

It follows from (3.104) and (3.105) that

$$\frac{\left\{g_{m}\Omega_{\eta K^{2}}^{2}-1\right\}}{J_{2}(q,\lambda_{c}K;T)} \leq \left(R_{m}^{\prime}\right)^{2} \leq \frac{\left\{g_{m}\Omega_{\eta K^{2}}^{2}-1\right\}}{J_{i}(q,\lambda_{c}K;T)}$$
(3.108)

$$\frac{\left\{\eta_{\text{eff}/\eta}-1\right\}}{J_{2}(q_{1}\lambda_{c}K;\omega)} \leq \left(R'_{m}\right)^{2} \leq \frac{\left\{\eta_{\text{eff}/\eta}-1\right\}}{J_{i}(q_{1}\lambda_{c}K;\omega)} \tag{3.108!}$$

The two sides of the inequality (3.108') are plotted in Figure 6 for particular values of  $\lambda_{C}K$  and q. In (3.108') we have used the definition

$$\eta_{eff}/\eta \equiv \lim_{(t-t_0)\to\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} d\eta \kappa^2$$
 (3.109)

Figure 6.  $R_m^*$  as a function of  $[\eta_{eff}^*/\eta]-1$  for  $\lambda_C/L=0.3$  and q=10.

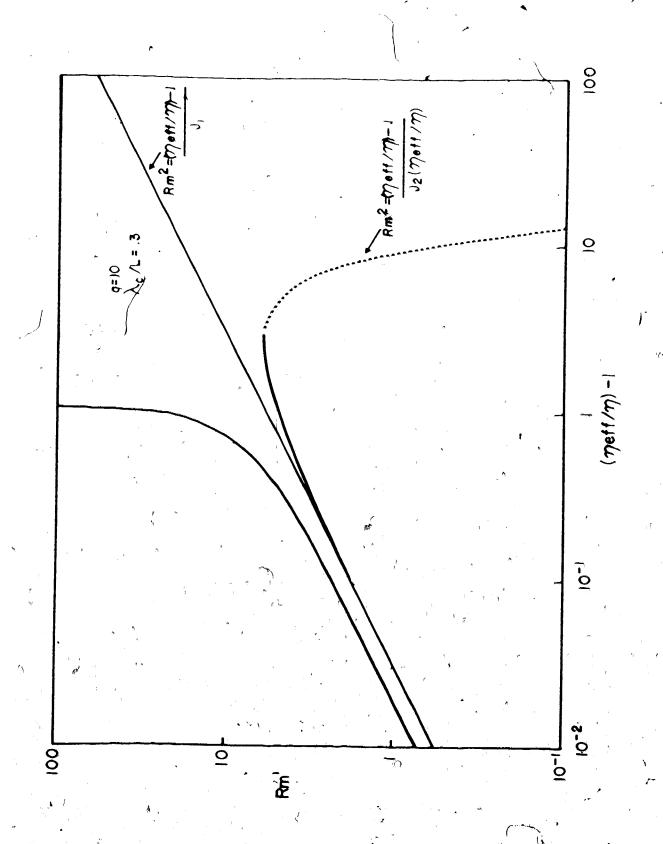
The plot shows values for Gaussian turbulence.

Lowermost curve:  $\{R_{m}^{i}\}^{2} = \{[n_{eff}/n]-1\}/J_{2}$ (see left hand side of 3.108')

Middle curve:  ${R_m^i}^2 = {[n_{eff}/n]-1}/J_1$ (see right hand side of 3.108')

Uppermost curve:  $R_{m}^{*}$  determined from equation (3.87) with  $\hat{h}(k,\omega)$  given by equation (3.70).

The two lower curves correspond to initial condition *I*, while the uppermost curve corresponds to initial condition *II*.



- 3.8 Isotropic turbulence and decaying, non-oscillatory mean fields + comparison of initial conditions I and II
- 3.8.1 Relationship between mean field decay rate and turbulent magnetic Reynolds number effect of mean field initial conditions

From Figure 6 it can be seen that the true value of  $R_{\rm m}^*$  is closely approximated by both sides of the inequality (3.108'), up to fairly large values of the ratio  $\eta_{\rm eff}/\eta$ . (This ratio may be taken as a measure of the mean field decay rate, by virtue of [3.79] and [3.86].) Moreover, the solutions for the two initial conditions, I and II, do not differ greatly when  $(\eta_{\rm eff}/\eta)-1$  is small, even for the comparatively large value of  $\lambda_{\rm c}K$  considered  $[\lambda_{\rm c}/L=0.3]$ .

The most striking difference between the lowest curve in Figure 6, which corresponds to the left hand side of (3.108'), and the other two curves, which correspond to the right hand side of (3.108') and to (3.87), is the occurrence of a maximum in the plot of  $R_{\rm m}$  against  $(\eta_{\rm eff}/\eta)-1$ . This behaviour is due to the nonlinear dependence of  $J_2(q,\lambda_{\rm c}K;\infty)$  on  $\eta_{\rm eff}/\eta$ . When  $\frac{(\lambda_{\rm c}K)^2}{q} \frac{\eta_{\rm eff}}{q}$  is small,  $J_2$  is independent of  $\eta_{\rm eff}/\eta$ . However, when  $\frac{(\lambda_{\rm c}K)^2}{q} \frac{\eta_{\rm eff}}{q}$  is large,  $J_2$  has a roughly exponential dependence on  $\eta_{\rm eff}/\eta$ , causing a rapid decrease in the value of  $R_{\rm m}^*$  given by the left hand side of (3.108').

It'may be seen from (3.105) that points on the curve

beyond the maximum are of no interest. If we assume for the moment that  $\operatorname{Im} \Omega(T)/\eta K_{\cdot}^{2}$  is defined as a function of  $T=t-t_{0}$  by the right hand side of (3.105), and the problem is regarded as one of switching on a fully developed turbulent velocity field at time T=0 and observing the subsequent behaviour of a mean field  $\overline{B}$  present in the fluid at the initial instant, we see that the decay rate of the mean field at large T depends on the initial decay rate,

$$(\mathfrak{I}_{m}\Omega)_{o} \equiv \mathfrak{I}_{m}\Omega(\tau)|_{\tau=t-t_{o}=0}$$
 (3.110)

Expanding (3.107) as a power series in T about T = 0,

$$g_{m}\Omega^{(T)}/_{\eta \kappa^{2}} - 1 = \frac{(R'_{m})^{2}}{3q\tau_{c}} \left\{ e^{(A_{c}K)^{2}(T/q\tau_{c})(g_{m}\Omega)}/_{\eta \kappa^{2}} \right\}_{T=0} + \dots$$
 (3.111)

we see that only two initial decay rates are possible:

$$(4m\Omega)_{o} = \eta K^{2}$$

$$(4m\Omega)_{o} = \infty$$

$$(3,112a)$$

$$(3,112b)$$

The first of these values corresponds to a mean field decaying at the normal diffusive rate in a stationary conductor. The second, on the other hand, is completely unphysical. Detailed numerical study shows that points to the right of the maximum on the lowermost curve in Figure 6 correspond to the unphysical condition, so that these points may be disregarded. (See Appendix 3, section A.3.1 for details of numerical techniques.)

Since the mean field initial conditions (3.112) apply to equation (3.104) as well as to the right hand side of (3.105), it is to be expected that a true plot of  $R_{\rm m}^{\rm r}$  against  $(\eta_{\rm eff}^{\rm r}/\eta)-1$  will also exhibit a maximum of the type shown in Figure 6. Further justification for this statement can be obtained by examining the derivatives of (3.104) and (3.105) with respect to  $(R_{\rm m}^{\rm r})^2$ . From (3.105) we have

$$\frac{\partial}{\partial (R_{m}^{\prime 2})} \left\{ \int_{0}^{\infty} \frac{\Omega}{\eta_{K^{2}}} \right\} = \frac{\left\{ \int_{0}^{\infty} \frac{\Omega}{\eta_{K^{2}}} - 1 \right\}}{(R_{m}^{\prime})^{2}} 
= \frac{\left\{ \int_{0}^{\infty} \frac{\Omega}{\eta_{K^{2}}} - 1 \right\}}{(R_{m}^{\prime})^{2}} 
- \left\{ 1 - \frac{1}{3} (R_{m}^{\prime})^{2} (\lambda_{c} K)^{2} \int_{0}^{T/q} \tau_{c} e^{-\frac{1}{2} q^{2} x^{2} + (\lambda_{c} K)^{2}} \left\{ \int_{0}^{\infty} \frac{\Omega}{\eta_{K^{2}}} - \frac{1}{1 + 2x} \right\} \times \frac{dx}{(1 + 2x)^{4/2}} \right\}^{-1}$$

while from (3.104),

$$\frac{\partial}{\partial (R_{m}^{\prime 2})} \left\{ \int_{\eta K^{2}}^{\eta} \left\{ \int_{\eta K^{2}}^{\eta} \left( \int_{\eta$$

The right hand side of (3.113) can be made to go to infinity by choosing  $\left(R_{m}^{\prime}\right)^{2}$  sufficiently large. Similarly, in

(3.114) The ratio of derivatives in the integrand runs from 0 to I as x spans the range of integration, so that the integral will be finite for all  $(R_m^i)^2$  and of the same general character as the integral in (3.113). The right hand side of (3.114) can therefore also be made to go to infinity by choosing  $(R_m^i)^2$  sufficiently large. As might be expected from the inequality (3.105), the maximum for (3.104) will occur at a larger value of  $R_m^i$  than the maximum of the curve plotted in Figure 6.

When the unphysical solutions of (3.104) and (3.105) are neglected - i.e. when points to the right of the maximum in the plot of  $R_{\rm m}^{\prime}$  against  $(\eta_{\rm eff}/\eta)-1$  are ignored, we have cut-off values of both  $\eta_{\rm eff}/\eta$  and  $R_{\rm m}^{\prime}$ , beyond which no useful solutions occur. This behaviour may be contrasted with that of the uppermost curve in Figure 6, which corresponds to initial condition II. In this curve there is a cut-off only in  $\eta_{\rm eff}/\eta$ 

## 3.8.2 Range of validity of solutions obtained using the Rädler expansion technique

It is interesting to note that the relationship  $\kappa$  between  $(R_{m}^{\prime})^{2}$  and  $(\eta_{eff}/\eta)-1$  in Figure 6 remains linear nearly all the way out to the cut-off point. This indicates that the approximate solution (3.92), derived with the aid of the Rädler expansion technique, is useful over a wide

range of parameters. From (3.104') we see that the first term in the expansion may be expected to provide a good approximation as long as the increasing exponential factor in the integrand is negligibly different from unity over the range in which the Gaussian factor  $e^{-x^2/2}$  has a significant amplitude. Imposing the condition that the increasing exponential differ from unity by less than 5%, and assuming that the Gaussian factor is effectively zero when x = 2, we obtain a condition for validity of the first term in the Rädler expansion:

$$(\eta K^2 \tau_c) \left\{ 4m \frac{\Omega}{\eta K^2} - (1+4/q)^{-1} \right\} = \frac{(\lambda_c K)^2}{q} \left\{ 4m \frac{\Omega}{\eta K^2} - (1+4/q)^{-1} \right\} \leq 0.025 \quad (3.115)$$

When this condition is not satisfied, higher-order terms in the expansion must be retained.

Taking limiting values of q in (3.115), we obtain the conditions

$$(q+0) \frac{(\lambda_c \kappa)^2}{q} \int_{m} \frac{\Omega}{\eta \kappa^2} = \tau_e^2 \int_{m} \Omega \lesssim 0.025 \qquad (3.115'')$$

$$(q + \omega) \frac{(\Omega_c K)^2}{q} \left\{ \int_{m} \frac{\Omega}{\eta K^2} - 1 \right\} = \tau_c \left\{ \int_{m} \Omega - \eta K^2 \right\} \lesssim 0.025$$
 (3.  $15''$ )

for the first term of the Rädler expansion to be a valid approximation. Figure 5 indicates that (3.115") is applicable even for values of q as low as 0.01.

The condition (3.115) clearly applies only to the case of turbulence with a Gaussian time correlation. If the time correlation falls off more slowly, the first term of the Radler expansion will be valid over a much narrower

range of parameters.

#### 3.8.3 The mean field decay rate at large times

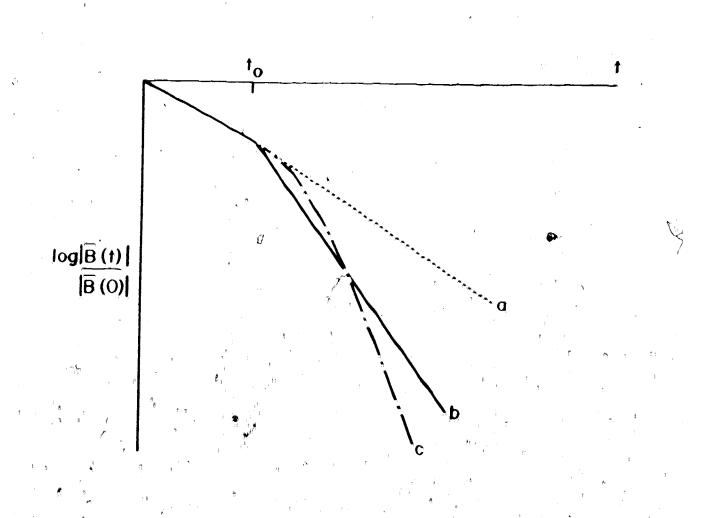
The curves of Figure 5 illustrate a second major difference between solutions corresponding to initial condition 1 and those corresponding to initial condition 11. It is apparent that for large values of  $\lambda_{\rm C} K$ , initial condition 1 leads to a more rapid decay rate of the mean field at large times than does initial condition 11. This behaviour is illustrated schematically in Figure 7. Curve "a" corresponds to a mean field decaying in the absence of turbulence: Curve "b" corresponds to the case in which u' and B' are switched on together at time  $t=t_0$  in a correlated manner. Curve "c" corresponds to the case in which u' is switched on at the initial instant and B' is allowed to develop.

It is clear from the slope discontinuity in Figure ? that the initial condition for curve "b" (i.e. initial condition II) is somewhat unphysical. However, the behaviour of curve "c" (initial condition I) is also open to question. The reason for the difference between the slopes of the two curves at large times can be seen from a comparison of equations (3.35) and (3.39), rewritten in the form

Decay of mean field amplitude with time.

- (a) No turbulence
- (b) Isotropic turbulence, with  $|\underline{\mathbf{u}}' \mathbf{x} | \underline{\mathbf{B}}' |_{t=t_0} \neq 0$ (c) Isotropic turbulence, with  $|\underline{\mathbf{u}}' \mathbf{x} | \underline{\mathbf{B}}' |_{t=t_0} = 0$

Curve (c) corresponds to initial condition I, and curve (b) corresponds to initial condition II.



$$i\Omega +^{A}\eta K^{2} + I^{(i)} =$$

$$= -\int_{\mathbb{R}} d\mathbf{k} \int_{-\infty}^{\infty} d\mathbf{r} K_{j}(\mathbf{k} + \mathbf{k})_{p} \hat{R}_{jp}(\mathbf{k}_{i}\mathbf{r}) e^{\{i\Omega + \eta(\mathbf{k} + \mathbf{k})^{2}\}\mathbf{r}}$$

$$\eta(\mathbf{k} + \mathbf{k})^{2} \leq \int_{m}^{\infty} \Omega \qquad (3.116a)$$

$$i\Omega + \eta K^2 + I^{(i)} = O \qquad (3.116b)$$

The right hand side of (3.116a) represents the limiting value of the time-dependent term in (3.35) as  $(t-t_0) \neq \infty$ .

Clearly, the form of the spectrum tensor  $R_{jp}(k,\tau)$  for small values of k will be crucial to the evaluation of the right hand side of (3.116a). Unfortunately, it is at just these values of k that our assumptions about the nature of the turbulence are most likely to be in error. For example, the assumption of isotropy at infinite separations will never be satisfied in a real, finite fluid. This difficulty does not arise in the evaluation of the integral  $T^{(1)}$ , which is dominated by contributions from values of |k| near  $2\pi/\lambda_{C}$ 

For Gaussian turbulence in an incompressible fluid, (3.116a) reduces to

$$i\Omega + \eta K^{2} + I^{(1)} =$$

$$= -\frac{1}{12\eta} u^{2} \lambda_{c}^{5} \tau_{c} K^{2} \int dk \ k^{2} e^{-(\lambda_{c} K)^{2}/2} \sin^{2}\theta \ e^{\frac{1}{2} \tau_{c}^{2} \left[ \frac{d}{d} m \Omega - \eta (k + K)^{2} \right]^{2}}$$

$$\eta (k + K)^{2} \leq \frac{d}{dm} \Omega$$

when Re  $\Omega$  = 0 . If  $\tau_{C}$  Im  $\Omega$  << 1 , the second exponential factor can be set equal to unity over the entire range of

integration, and the equation becomes

$$i\Omega + \eta K^{2} + I^{(1)} \approx$$

$$\approx -\frac{1}{6} u^{2} \lambda_{c}^{5} \tau_{c} K^{2} \iint R^{4} e^{(\lambda_{c}K)^{2}/2} \sin^{3}\theta \, dk \, d\theta$$

$$\eta(k^{2} + K^{2} + 2kK\cos\theta) \lesssim 4m\Omega$$

$$\lesssim \frac{2}{9} u^{2} \lambda_{c}^{5} \tau_{c} K^{2} \int \sqrt{24m\Omega/\eta} k^{4} e^{-(\lambda_{c}R)^{2}/2} \, dk$$

$$\lesssim \frac{2}{9} (R_{m}^{\prime})^{2} q^{3/2} (\eta K^{2}) \int \sqrt{2\tau_{c}4m\Omega} t^{4} e^{-Qt^{2}/2} \, dt \qquad (3.117)$$

In order for the two initial conditions I and II to lead to the same result for this type of turbulence, we must therefore have.

$$T^{(1)} \gg \frac{2}{3} (R_m^2)^2 q^{3/2} (\eta R^2) \int_0^{2\tau_c 4m\Omega} t^4 e^{-8t^2/2} dt$$
 (3.118a)

and  $\tau_{\star} \leq \Omega \leq 1$  (3.118b)

The inequality (3.118a) is satisfied automatically when q is small, but it is not necessarily satisfied when q is large. It is apparent from (3.117) that the right hand side, which represents the difference between the two dispersion relations, is determined by the behaviour of the spectrum tensor at small values of |k| whenever

This condition is very likely to be satisfied - particularly

when (3.118b) is true and the first term in the Rädler expansion is a valid approximation.

On general grounds, we expect there to be less energy in the turbulence at small values of 'k than is implied by the use of the spectrum tensor (3.7), which is isotropic at k = 0. The right hand side of (3.116a) is therefore likely to be smaller than the value obtained using (3.7) - for example, the right hand side of (3.117) is probably an overestimate. It therefore appears that the slope of curve "c" (Figure 7) at large times may well be inaccurate when it differs markedly from the slope of curve "b".

### 3.8.4 Stabilization of the mean field decay rate, and loss of energy from the mean field

The initial, time-dependent portion of curve "c" in Figure ? is undoubtedly more realistic than the abrupt slope discontinuity shown in curve "b". It is only sensible to discuss the stabilized dispension relation if the energy lost from the mean field during the time-dependent part of the decay is small. If  $T_1$  is defined to be the time after which the mean field decay rate has reached its stabilized value, and  $T_2$  is the time it takes the mean field amplitude to decay to 1/e of its value at time  $t = t_0$ , we may write

$$\frac{\mathcal{E}(T)}{\mathcal{E}_{o}} = \frac{\text{mean field energy density at } t = t_{o} + T}{\text{mean field energy density at } t = t_{o}}$$

$$= e^{-2 \int_{m} \Omega(T) \cdot T}$$

$$= \frac{\mathcal{E}(T_{o})}{\mathcal{E}_{o}} = \frac{\mathcal{E}(T_{o})}{\mathcal{E}_{o}} e^{-2 \int_{m} \Omega(T_{o})(T-T_{o})}, \quad T > T_{o}$$

$$= \frac{\mathcal{E}(T_{o})}{\mathcal{E}_{o}} = e^{-2}$$

$$= e^{-2}$$

$$= \frac{\mathcal{E}(T_{o})}{\mathcal{E}_{o}} = e^{-2}$$

When  $T_2 > T_1$  we have, from (3.120)-(3.122),

$$e^{-2} = \left\{ \frac{\mathcal{E}(T_i)}{\mathcal{E}_o} \right\} e^{-2 \operatorname{sim} \Omega(T_i) \cdot (T_2 - T_i)}$$

$$= \left\{ \frac{\mathcal{E}(T_i)}{\mathcal{E}_o} \right\} e^{-2 \operatorname{sim} \Omega(T_i) \cdot T_i \cdot (T_2 / T_i)}$$

$$= \left\{ \frac{\mathcal{E}(T_i)}{\mathcal{E}_o} \right\}^{T_2 / T_i}$$

Therefore

$$\mathcal{E}(T_i)/\varepsilon_o = e^{-2T_i/T_2} \qquad (3.123)$$

It follows from (3.123) that if  $T_1 = T_2$ , only 13.5% of the original mean field energy is left by the time the dispersion relation stabilizes. We must therefore require that  $T_1 << T_2$  if we wish to study the decay of the mean field solely in terms of the stabilized dispersion. For example, if  $T_1 < 0.05 T_2$ , no more than 10% of the initial energy will be lost during the time-dependent portion of the decay.

We may study the restriction imposed by the condition  $T_1 \le T_2$  for the case of Gaussian turbulence in an incompressible fluid by examining the behaviour of solutions of (3.104). Results obtained in this way should be qualitatively valid despite the reservations mentioned above concerning the behaviour of solutions of this equation at large times. In order to simplify the discussion, we shall replace (3.104) with the right hand side of the inequality (3.105), since, as noted above, the results obtained using these two equations are not substantially different over most of the allowed range of  $\text{Im } \Omega/\eta \text{K}^2$ .

# 3.8.5 Conditions on the turbulence for stable decay to be established before significant energy is lost from the mean field

We shall first derive a necessary condition on  $(\lambda_c K)^2/q$  for  $T_1$  to be less than  $T_2$ . From either (3.104) or (3.105) we see that  $T_1$  is determined by the requirement that the integrand on the right hand side be effectively zero - i.e.

$$-\frac{1}{2}q^{2}x^{2} + (\lambda_{c}K)^{2}\left\{ 3m\frac{\Omega}{\eta K^{2}} - \frac{5}{1+2x} \right\} x - \frac{5}{2}\ln(1+2x)$$

$$< -N , \forall x > x, \qquad (3.124)$$

where  $x = T/q\tau_c$ ,  $x_1 = T_1/q\tau_c$ , and N is a positive

number for which  $e^{-N}$  is fairly small (say N=2). The requirement  $T_1 < T_2$  is satisfied if  $x_1 < x_2$ , where, by (3.120) and (3.122),

$$x_{\lambda} = \frac{T_{2}}{q \tau_{c}} = \left\{ q \tau_{c} \int_{m} \Omega \right\}^{-1} = \left\{ (\lambda_{c} K)^{2} \int_{m} \Omega / \eta K^{2} \right\}^{-1}$$
 (3.125)

In the limit  $q+\infty$  , (3.124) is satisfied for all  $x>x_1=\sqrt{2N}/q$  , so that the condition  $x_1< x_2$  implies that

$$\frac{(\lambda_c K)^2}{9} \int m \frac{\Omega}{7K^2} < \frac{1}{\sqrt{2N}} < 1$$

But  $\operatorname{Im} \Omega/\eta K^2 \ge 1$ . Hence a necessary condition for  $T_1 < T_2$  is

$$\frac{(\lambda_c \kappa)^2}{q} = \eta \kappa^2 \tau_c \ll 1 \tag{3.126}$$

Similarly, when  $q \neq 0$  (3.124) can only be satisfied if x is sufficiently large for the first two terms on the left hand side to give a negative contribution - i.e.

$$x_i > 2 \frac{(\lambda_c \kappa)^2}{g^2} g_m \frac{\Omega}{\eta \kappa^2}$$
(3.127)

From (3.125), (3.127), and the condition that  ${\rm Im}~\Omega/\eta K^2 > 1$  (3.126) again gives a necessary condition for  ${\rm T}_1 < {\rm T}_2$ . (3.126) may therefore be taken as a necessary condition on  $(\lambda_c K)^2/q$  for all values of q.

Numerical study of (3.104), or, to a reasonable approximation, of the right hand side of (3.105), leads to more precise conditions on the form of the turbulence for

$$T_1 < T_2$$
. Figure 8 shows a plot of 
$$\left\{ R'_m/_{g} \right\}_{T_1 = T_2} = \left\{ \sqrt{\overline{u^2}} \ t_c/_{\lambda_c} \right\}_{T_1 = T_2}$$

obtained from (3.105) as a function of  $\lambda_{\rm C}/{\rm L}$  for several values of q. At points to the right of each curve,  $T_1 > T_2$  and the mean field decay rate is effectively time-dependent throughout the decay. In plotting these curves we have determined  $T_1$  by assuming the time-dependence of  $T_1$  to be effectively linear during the time-dependent portion of the decay. From (3.104) or (3.105), we see that

$$\left\{\frac{\partial}{\partial t} \int_{\Gamma} m \frac{\Omega}{\gamma K^2}\right\}_{T=0} = \frac{\left(R_m'\right)^2}{3q\tau_c}$$

Thus, making use of the initial condition (3.112a) on  $\overline{\mathbb{B}}$ ,

$$\int_{\eta K^{2}} \frac{\Omega}{\eta K^{2}} \approx \frac{\left(\int_{\eta K^{2}} \Omega\right)_{0}}{\eta K^{2}} + \frac{\left(R'_{m}\right)^{2}}{3q \tau_{c}} + \dots$$

$$\approx 1 + \frac{\left(R'_{m}\right)^{2}}{3q} \left(\frac{T}{\tau_{c}}\right) + \dots$$
(3.128)

Using (3.128) we may write, approximately,

$$\left(R_m'/q\right)^2 \approx \frac{3\left\{\int_m \left(\Omega/\eta \kappa^2\right) - 1\right\}}{q\left(T/\tau_c\right)}$$
(3.129)

The value of  $T_1$  is then determined by equating  $\left\{\frac{R_m(T_0)_2}{2}\right\}^2$  defined by (3.129), with the value of  $\left\{\frac{R_m}{2}\right\}^2$  obtained from the right hand side of (3.105) in the limit  $T + \infty$ , where  $T \equiv (t-t_0)$ .

$$(T_i/\tau_c) = q \int_0^\infty e^{-\frac{1}{2}q^2x^2} + q\tau_c \{ Im\Omega(T_i) - \frac{\eta K^2}{1+2x} \} x \frac{dx}{(1+2x)^{5/2}}$$
(3.130)

From (3.125) the value of  $T_2$  is given by

$$\left(T_2/\tau_c\right) = \left\{\tau_c \int_{m} \Omega(\tau_2)\right\}^{-1} = \frac{9}{(\lambda_c \kappa)^2 \int_{m} \Omega(\tau_2)/\eta \kappa^2}$$
(3.131)

The condition  $T_1 \le T_2$  then implies that

Equation (3.132) may be solved numerically or graphically for  $(T^*/\tau_C)$  .

Equations (3.129), (3.131), and (3.132) lead to the identification

$${R'_{m}/q}_{T^{*}}^{2} = \frac{3{9/(\lambda_{c}K)^{2} - (T''/\tau_{c})}}{9(T''/\tau_{c})^{2}}$$
(3.134)

From (3.134) it is clear that  $[R_m'/q]_T^*$  is real only if

$$-\frac{(\lambda_c K)^2}{9} \leqslant (T^9/t_c)^{-1}$$
 (3.135)

Thus, in a plot of  $[R_{\rm m}'/q]_{\rm T}^*$  against  $\lambda_{\rm C}^{\rm K}$  for a fixed value of q, there will be a critical value of  $\lambda_{\rm C}^{\rm K}$  beyond which no solutions exist. This behaviour is illustrated in Figure 8. As q approaches zero, it is clear from (3.126) that  $\lambda_{\rm C}^{\rm K}$  must also go to zero. It follows that when q

is small, it is only appropriate to discuss the decay of the mean field in terms of the stabilized decay rate if  $\lambda_c K$  is also small. In the limit as  $q \to \infty$ , the solution of (3.132) gives

$$T_{i}/\tau_{c} \leq \left(T^{*}/\tau_{c}\right)_{q=\infty} = 2.0 \tag{3.136}$$

so that, from (3.133) and (3.134),

$$\lim_{q \to \infty} \frac{4m\Omega(T^*)}{\eta K^2} = \frac{2q}{(\lambda_c K)^2} = \frac{8}{2\pi^2(\lambda_c/L)^2}$$
 (3.137)

$$\lim_{q \to \infty} \left( \frac{R'_m}{q} \right)_{T^*}^2 = \frac{3}{4(\lambda_c K)^2} = \frac{3}{4\pi (\lambda_c / L)}^2 \qquad (3.138)$$

Solutions of (3.132) are shown in Figure 9, where  $(T^*/\tau_c)$  is plotted as a function of q for several values of  $\lambda_c/L$ . It is clear from (3.132) that the largest values of  $T^*/\tau_c$  occur in the limit  $q + \infty$ , so that, from (3.136), stabilization of the dispersion relation must take place in less than two correlation times if  $T_{1c}$  is to be less than  $T_2$ . At low values of q, stabilization must take place more rapidly, as indicated in Figure 9.

It should be noted that in all plots,  $\lambda_{\rm C}/{\rm L}$  is restricted to values less than unity. A situation in which the wavelength of the mean field was shorter than the correlation length of the turbulence (i.e.  $\lambda_{\rm C}/{\rm Ir} > 1$ ), would clearly have little physical significance.

The program used to calculate  $T^*/_{C}$  and  $[R'_{m}/q]_{T^*}$  is listed in Appendix 3, section A.3.2.

#### Figure 8. Decay regimes for initial condition I.

The plot shows  $[R_m'/q]_{T_1=T_2}$  as a function of  $\lambda_C/L$  for several values of q . For each q , decay is effectively time-dependent at all times for points to the right of the curve.

Values plotted are determined from equation (3.134).

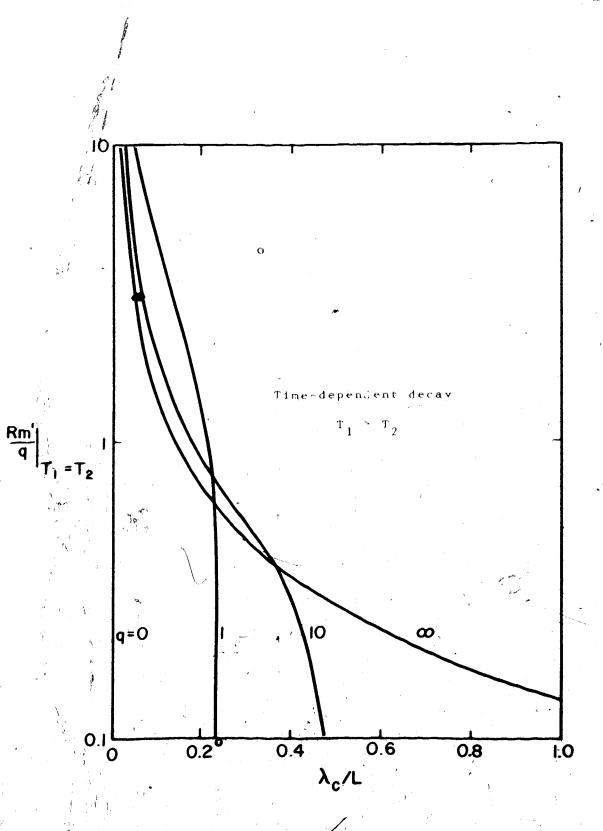
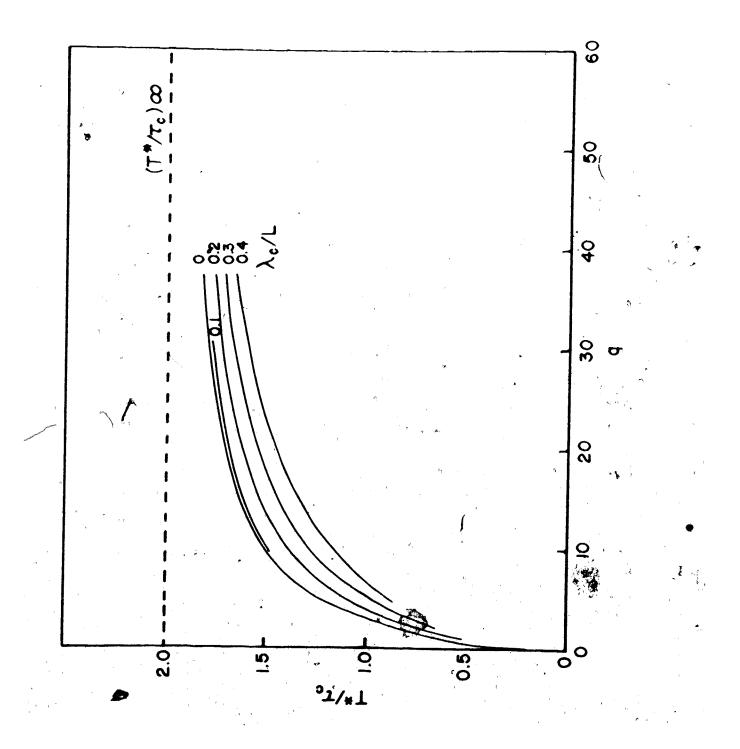


Figure 9.  $T^*/\tau_C$  as a function of q for several values of  $\lambda_C/L$  .

Values plotted represent numerical solutions of equation (3.132).



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## 3.9 Isotropic turbulence and decaying mean fields which oscillate with tame - initial condition I

#### 3.9.1 Inappropriateness of the Radler expansion technique

We shall now turn our attention to the case in which the decaying mean field oscillates with time - i.e. Re  $\Omega \neq 0$ . It is not immediately obvious that either (3.35) or (3.39) has solutions of this type. The Rädler expansion (3.96), which corresponds to (3.35) is of no use in studying the problem, as may be seen by taking the first few terms of the expansion and separating the real and imaginary parts.

$$\int_{m} \Omega - \eta K^{2} = \overline{u^{2}} K^{2} \{ \beta^{(00)} - \dot{\beta}^{(10)} K^{2} + \beta^{(01)} \int_{m} \Omega + \dots \}^{4} + \beta^{3} \cdot (3, 139a)$$

$$Re \Omega = Re \Omega \{ \overline{u^{2}} K^{2} \} \{ \beta^{(01)} - \beta^{(11)} K^{2} + \beta^{(02)} \int_{m} \Omega + \dots \} (3, 139b)$$

If  $\Re \Omega = 0$ , (3.139b) is identically satisfied, and (3.139a) is a meaningful equation of the form

$$O(\epsilon) = O(\epsilon) \cdot u^2 \left\{ 1 + O(\epsilon) + u^2 \right\}$$
 (3.140a)

where  $\epsilon$  is assumed to be small. However, when Re  $\Omega \neq 0$  (3.139b) is of the form

$$1 = O(\epsilon) \cdot \overline{u^2} \{ 1 + O(\epsilon) + ... \}$$
 (3.140b)

and is clearly incompatible with (3.140a) under the assumption that ( is small. We must therefore study the problem in terms of the unexpanded equations, taking note

of their eigenvalue nature, discussed above in section 3.4.3. -

#### 3.9.2 General statement of the problem

Consider first equation (3.35), associated with initial condition I on B'. For the reasons set out above in section 3.7.3, we shall restrict ourselves to the case of Gaussian turbulence (3.67), for which (3.35) reduces to (3.103). Separating the real and imaginary parts of (3.103),

$$\int_{m} \left\{ \Omega(T) / \eta \kappa^{2} \right\} - 1 = \left( R'_{m} \right)^{2} \int_{R} \left( q_{i} \lambda_{c} \kappa_{i} T / \tau_{c} \right) \qquad (3.141a)$$

$$Re\{\Omega(T)/\eta K^2\} = -(R'_m)^2 J_T(q, \lambda_c K, T/\tau_c) \qquad (3.141b)$$

where

$$J_{R}(q, \lambda_{c}K; T/\tau_{c}) \equiv \frac{1}{3} \int_{0}^{T/q} e^{-\frac{1}{2}q^{2}x^{2} + (\lambda_{c}K)^{2}} \left\{ \frac{dm}{\eta K^{2}} - \frac{1}{1+2x} \right\} x .$$

$$\cdot \cos \left\{ (\lambda_{c}K)^{2} \operatorname{Re} \frac{\Omega}{\eta K^{2}} x \right\} \frac{dx}{(1+2x)^{5/2}}$$

$$J_{T}(q, \lambda_{c}K; T/\tau_{c}) \equiv \equiv \frac{1}{3} \int_{0}^{T/q} \frac{\tau_{c}}{e^{-\frac{1}{2}q^{2}x^{2}} + (\lambda_{c}K)^{2}} \left\{ \frac{dm}{\eta K^{2}} - \frac{1}{(1+2x)^{5/2}} \right\} x .$$

$$\cdot \sin \left\{ (\lambda_{c}K)^{2} \operatorname{Re} \frac{\Omega}{\eta K^{2}} x \right\} \frac{dx}{(1+2x)^{5/2}}$$
(3.142b)

Once again, it must be stressed that (3.142a,b) are integral equations. To a first approximation, they may be replaced by

$$\int_{\mathbb{R}} \left\{ \Omega(T) / \eta_{K} \right\} = \left( R_{m} \right)^{2} \int_{2R} \left( q_{s}, \lambda_{cK} \right) \left( T / \tau_{c} \right)$$
 (3.143a)

$$\Re\left\{\Omega(T)/\eta \kappa^{2}\right\} = -(R'_{m})^{2} J_{2T}(q, \lambda_{c} \kappa_{c} T/\tau_{c}) \qquad (3.143b)$$

where

$$J_{2R}(q, \lambda_{c}K; T/\tau_{c}) = \frac{1}{3} \int_{0}^{T/qT_{c}} e^{-\frac{1}{2}q^{2}x^{2} + (\lambda_{c}K)^{2} \left\{ \int_{0}^{T} \frac{\Omega(T)}{\eta K^{2}} - \frac{1}{1+2x} \right\} x} dx$$

$$\cdot \cos \left\{ (\lambda_{c}K)^{2} \operatorname{Re} \frac{\Omega(T)}{\eta K^{2}} x \right\} \frac{dx}{(1+2x)^{\frac{2}{2}/2}}$$
(3.144a)

$$J_{2T}(q, \lambda_c K; T/\tau_c) \equiv \frac{1}{3} \int_{0}^{T/q^{2}c} e^{-\frac{1}{2}q^{2}x^{2} + (\lambda_c K)^{2}} \left\{ \int_{0}^{T} \frac{\Omega(T)}{\eta K^{2}} - \frac{1}{1+2x} \right\} x.$$

$$Sin \left\{ (\lambda_c K)^{2} \operatorname{Re} \frac{\Omega(T)}{\eta K^{2}} x \right\} \frac{dx}{(1+2x)^{\frac{2}{2}}}$$
(3.144b)

and solutions may be sought in the limit as  $T + \infty$ . As discussed above in section 3.8.4, the parameters of the turbulence must be chosen in such a way that  $T_1 << T_2$  if the solutions of (3.143a,b) are to have any physical significance.

Dr. K.D. Aldridge and the present author have developed a numerical program which evaluates the integrals  ${\bf J}_{2R}$  and  ${\bf J}_{2I}$  by a Simpson's Rule, technique, and calculates the dispersion function

$$D = 1 - \frac{\Re \{\Omega/\eta K^2\}}{4m \{\Omega/\eta K^2\} - 1} \cdot \frac{J_{2R}(q, \lambda_c K; \omega)}{J_{2I}(q, \lambda_c K; \omega)}$$
(3.145)

D must vanish for a solution of (3.143a,b) with Re  $\Omega \neq 0$  to exist. When this condition is satisfied, the eigenvalue for the problem may be calculated from

$$(R'_m)^2 = -\frac{Re\{\Omega/\eta \kappa^2\}}{J_{2I}(q, \lambda_c \kappa; \omega)}$$
(3.146)

### 3.9.3 Restrictions on the turbulence for meaningful solutions

In order for the problem to have meaningful solutions, the parameters of the turbulence must satisfy a number of conditions, which are summarized here for convenience.

$$\lambda_{c/L} < 1$$
 ,  $\tau_{c/T} < 1$  (3.147a,b)

$$\tau_{c}\eta K^{2} = (\lambda_{c}K)^{2}/q \ll 1 \qquad (3.148)$$

$$\left\{R_{m}^{\prime}/q\right\} \leftarrow \left\{R_{m}^{\prime}/q\right\}_{T^{\pm}} \left(q, \lambda_{c/L}\right) \tag{3.149a}$$

$$\{\lambda_{c}/L\} < \{\lambda_{c}/L\}_{T^{*}}(q, R'_{m}/q) \qquad (3.149b)$$

$$R_{m} < 1 + q \qquad (3.150)$$

In (3.147), L and T are the wavelength and period of the mean field  $\overline{\mathbb{B}}$ . (3.148) and (3.149) are the conditions derived in section 3.8.5 for  $T_1$   $T_2$ , and the functions referred to in (3.149) are plotted in Figure 8. (3.150) is the condition derived in section 2.5.4 for the first order smoothing approximation to be consistent.

First order smoothing also implies that

$$\operatorname{Im}\Omega/\eta K^2 \geqslant 1$$
 (3.151)

when the turbulence is PT-invariant, as proved in section 3.2. This condition may be combined with (3.147)-(3.150)

to derive further restrictions on the parameters of the mean field.

From (3.147b) and (3.148) we have

or, writing  $T_d = 1/\eta K^2$ ,

$$\tau_{\rm c} \ll \sqrt{\tau \cdot \tau_{\rm d}}$$
 (3.152')

Similarly, from (3.151) we have

$$T_2/\tau_c < \mathcal{V}(\lambda_c K)^2 \qquad (3.153)$$

The effective range of the arguments of the sine and cosine terms in (3.144a,b) is limited by

$$(\lambda_c K)^2 \Re \{\Omega/\eta K^2\} \propto \langle (\lambda_c K)^2 \Re \{\Omega/\eta K^2\} \times \langle 2\pi T_i/\tau_c \rangle \langle 2\pi \{T^4/\tau_c\} (q_i, \lambda_c K) \rangle \langle 4\pi \rangle$$

$$(3.154)$$

where  $(T^*/\tau_C)$  is the function plotted in Figure 9.

#### 3.9.4 Numerical search procedure

A numerical search has failed to reveal any long-period oscillatory solutions of (3.143a,b) which satisfy (3.147) and (3.148). Asymptotic evaluation of the integrals  $J_{2R}$  and  $J_{2I}$  indicates that oscillatory solutions do exist when  $(\lambda_{C}K)^{2} >> 1$ , but the program used was unable to check the existence of solutions in this range because of the extremely large values attained by the exponential factors in the integrands in (3.143).

The procedure used in the numerical search was briefly as follows.

- a) Trial values of Im  $\Omega/\eta K^2$  and Re  $\Omega/\eta K^2$  were chosen.
- b) A value of q was assumed.
- c) The integrals  $J_{2R}$  and  $J_{2I}$ , and the dispersion function D were calculated for a range of values of  $\lambda_{C}K$  satisfying (3.147a), (3.148), and (3.152).
- d) The calculated values of D were checked for changes of sign or trends toward zero.
- Further values of  $\lambda_{C}^{K}$  were chosen in accordance with the results of step (d), until the conditions (3.147a), (3.148), and (3.152) could no longer be satisfied.

f) The process was repeated for new values of  $\, {\rm q}$  , and for new trial values of  $\, {\rm Im} \, \, \Omega/\eta K^2$  and  $\, {\rm Re} \, \, \Omega/\eta K^2$  .

As the trial values of Re  $\Omega/\eta K^2$  chosen were kept fairly small (in general, much less than unity), the entire range of Re  $\Omega/\eta K^2$  permitted by (3.152) was not explored at large values of q. It is therefore possible that acceptable oscillatory solutions to (3.143) do exist when both q and Re  $\Omega/\eta K^2$  are large. The assumption of small Re  $\Omega/\eta K^2$ , which implies that the period sought is long compared with the mean field decay time, was made in order to restrict consideration to small departures from the case Re  $\Omega=0$ .

See Appendix 3, section A.3.3 for details of the numerical techniques used in evaluating the integrals  ${\rm J}_{2R}$  and  ${\rm J}_{2T}$  .

### 3.9.5 The impossibility of slowly-decaying, long-period, oscillatory mean fields

It may be demonstrated directly that (3.143) has no oscillatory solutions when

$$\frac{\left(\lambda_{c}K\right)^{2}}{q}\left|1+i\frac{\Omega}{\eta K^{2}}\right|\ll 1$$

The equations (3:143) may be rewritten in the form

$$\Gamma = \frac{(R'_m)^2}{3q} \int_0^\infty e^{-\frac{1}{2}y^2 + \pi \Gamma y} + \frac{2yy^2}{q+2y} \frac{dy}{(1+2y/q)^{5/2}}$$
(3.155)

where

$$\Gamma = -\left\{1 + i\frac{\Omega}{\eta K^2}\right\} = \left\{4m\frac{\Omega}{\eta K^2} - 1\right\} - iRe\frac{\Omega}{\eta K^2}$$
 (3.156)

$$\Upsilon = (\lambda_c K)^2/q \qquad (3.157)$$

The integrand in (3.155) may be expanded as a Taylor series in  $\gamma\Gamma$  about  $\gamma\Gamma=0$ , and integrated term by term to give

$$\Gamma = \frac{(R'_m)^2}{3q} \sum_{n=0}^{\infty} \frac{1}{n!} a_n (r\Gamma)^n$$
 (3.158)

where

$$a_n \equiv \int_0^\infty y^n e^{-\frac{1}{2}y^2 + \frac{2xy^2}{q+2y}} \frac{dy}{(1+2y/q)^{5/2}}$$
 (3.159)

The series in (3.158) converges absolutely for all values of  $\gamma\Gamma$  by d'Alembert's ratio test (Whittaker and Watson, 1927, p. 22).

Equation (3.158) will clearly have no complex solutions for  $\Gamma$  as long as  $|\gamma\Gamma|$  is small enough for the quadratic term on the right hand side to be ignored. This condition may be written

$$|\gamma\Gamma| \ll 2a_1/a_2 \tag{3.161}$$

When q is large, (3.161) may be replaced by

$$(q \rightarrow \infty) \qquad |\gamma\Gamma| \ll 2\sqrt{2/\pi} \qquad (3.161')$$

and when q is small, (3.161) becomes approximately

$$(q \rightarrow 0) \qquad |\gamma\Gamma|^{\frac{1}{2}} << 2/(3\sqrt{q}) \qquad (3.161")$$

It would appear, therefore, that complex solutions will be found most readily when q is large. In this limit,

$$\lim_{q \to \infty} a_{2n} = \int_{0}^{\infty} y^{2n} e^{-\frac{1}{2}y^{2}} dy = \frac{(2n)!}{2^{n} n!} \sqrt{\frac{\pi}{2}}$$

$$\lim_{q \to \infty} a_{2n+1} = \int_{0}^{\infty} y^{2n+1} e^{-\frac{1}{2}y^{2}} dy = 2^{n} n!$$

When the quadratic term in (3.158) is retained, the solution is

$$\Gamma = \frac{1}{Ya_2} \left\{ \frac{1}{Y(R'_m)^2} - a_1 \pm \sqrt{\left[\frac{3q}{Y(R'_m)^2} - a_1\right]^2 - 2a_0a_2} \right\}$$
 (3.162)

I will be complex if

$$2a_0a_2 > \left\{\frac{3q}{7(R'm)^2} - a_1\right\}^2 \tag{3.163}$$

or, taking the limit of large q,

$$\left(\frac{3 + \infty}{4}\right) \left\{\frac{(\lambda_{c} \kappa) R_{m}^{\prime}}{4}\right\}^{2} > \frac{3}{1 + \sqrt{\pi}}$$
(3.163')

(3.163') may be compared with the condition (3.138), which must be satisfied if  $T_1$  is to be less than  $T_2$ .

$$\left(\frac{1}{4}\right)^{2} < \frac{3}{4} \qquad (3.138')$$

Clearly, the two conditions are incompatible, indicating that no acceptable oscillatory solutions to (3.143) are to be found when  $|\gamma\Gamma|$  is small enough for the cubic term in (3.158) to be neglected - i.e. when

$$|\gamma\Gamma| \ll 3a_2/a_3$$

In the limit of large q , this condition becomes

$$|\gamma\Gamma| << 3\sqrt{\pi}/2\sqrt{2} \approx 2$$
From (3.156) and (3.157),
$$|\nabla\Gamma| = |\nabla\Gamma| = \frac{(\Lambda_c \kappa)^2}{4} \left\{ \left( 4m \frac{\Omega}{\eta \kappa^2} - 1 \right)^2 + \left( Re \frac{\Omega}{\eta \kappa^2} \right) \right\}^{\frac{1}{2}}$$

Thus  $|\gamma\Gamma| \ll 2$  only if

$$\frac{(\lambda_c K)^2}{9} \operatorname{Re} \frac{\Omega}{\eta K^2} = \tau_c \operatorname{Re} \Omega \ll 2$$

and

$$\frac{\left(\lambda_{c}K\right)^{2}}{q}\left\{g_{m}\frac{\Omega}{\eta K^{2}}-1\right\} = \tau_{c}\left\{g_{m}\Omega-\eta K^{2}\right\} \ll 2$$

But, by (3.148),

$$\gamma = \eta \tau_c K^2 << 1$$

It follows that  $|\gamma\Gamma| << 2$  only if the period of the mean field

$$T = 2\pi/\text{Re }\Omega$$

and the effective decay time

$$T_d^{eff} \equiv 1/Im \Omega$$

satisfy the conditions

$$\tau_{_{\rm C}}/{
m T}$$
 << 1/ $\pi$  ,  $\tau_{_{\rm C}}/{
m T_{\rm d}^{\rm eff}}$  << 2

We may therefore state that (3.143) has no acceptable oscillatory solutions for which both the period and the effective decay time of the mean field are long compared with the correlation time of the turbulence.

By (3.147b),  $\tau_{_{\hbox{\scriptsize C}}}/T<1$  . In the limit as  $q\to\infty$  we must also require that  $T_{_{\hbox{\scriptsize d}}}^{\hbox{\scriptsize eff}}$  satisfy

$$T_d^{eff} \equiv T_2 > T_1 \sim 2T_C$$

- i.e. when q is large,  $\tau_{\rm C}/T_{\rm d}^{\rm eff}$  is typically less than  $\frac{1}{2}$ . It follows therefore, that the only range in which acceptable solutions to (3.143) may possibly occur is that in which

$$(q + \infty) \qquad (1/\pi) \leq \tau_c/T < 1$$

This condition confirms the numerical result that the only range in which solutions may possibly lie is that for which both q and Re  $\Omega/\eta K^2$  are relatively "large".

- 3.10 Isotropic turbulence and decaying mean fields which oscillate with time initial condition II.
- 3.10.1 General statement of the problem, and restrictions on the turbulence for meaningful solutions

We shall now consider equation (3.39), associæted with initial condition II on B'. For Gaussian turbulence, (3.67), equation (3.39) reduces to

$$-\left\{1+i\frac{\Omega}{\eta K^{2}}\right\}^{2} = \frac{1}{\eta K^{2}} I^{(i)}(K,\Omega) =$$

$$\left(\frac{(\lambda_{c}K)^{5}}{24\pi} \frac{(R_{m}^{\prime})^{2}}{q} \int_{-\infty}^{\infty} \int_{0}^{\infty} dY e^{-\frac{1}{2}\left\{(\lambda_{c}KF)^{2}+(\eta K^{2}\tau_{c})^{2}(V+Re\frac{\Omega}{\eta K^{2}})^{2}\right\}} -\Theta\left(F,V;\int_{m} \frac{\Omega}{\eta K^{2}}\right) \qquad (3.164)$$

Separating the real and imaginary parts of (3.164),

$$\left\{ \operatorname{Im} \frac{\Omega}{\eta K^{2}} - 1 \right\} = \frac{1}{\eta K^{2}} \operatorname{Re} I^{(1)}(K,\Omega) =$$

$$= \frac{(\lambda_{c}K)^{5}}{24\pi} \frac{(R_{m}^{\prime\prime})^{2}}{q} \int_{-\infty}^{\infty} d\gamma \int_{0}^{\infty} d\zeta e^{-\frac{1}{2}\left\{(\lambda_{c}K\zeta)^{2} + (\eta K^{2}\tau_{c})^{2}(v + \operatorname{Re} \frac{\Omega}{\eta K^{2}})^{2}\right\}} \cdot \operatorname{Re} \Theta(\zeta, \gamma; \operatorname{Im} \frac{\Omega}{\eta K^{2}}) \qquad (3.165a)$$

$$\left\{ \operatorname{Re} \frac{\Omega}{\eta K^{2}} \right\} = -\frac{1}{\eta K^{2}} \operatorname{Im} I^{\Omega}(K,\Omega) = \\
= -\frac{(\lambda_{c}K)^{5}}{24\pi} \frac{(R_{m}^{\prime})^{2}}{q} \int_{0}^{\infty} dv \int_{0}^{\infty} d\xi e^{-\frac{1}{2}\left[(\lambda_{c}K\xi)^{2} + (\eta K^{2}\tau_{c})^{2}(v^{2} + Re\frac{\Omega}{\eta K^{2}})^{2}\right]} \\
\cdot \operatorname{Im} \Theta(\xi, v; \operatorname{Im} \frac{\Omega}{\eta K^{2}}) \quad (3.165b)$$

where Re  $\theta$  and Im  $\theta$  are defined in (3.42) and (3.43).

solutions, the parameters of the turbulence and the mean field must satisfy a number of conditions, as was the case for solutions corresponding to initial condition I (see section 3.9.3). The conditions (3.147), (3.150), (3.151), and the right hand side of (3.152) apply to solutions of (3.165), as they did to solutions of (3.143). However, because of the assumption that u' and B' are correlated initially, solutions to (3.165) need not necessarily satisfy the conditions (3.148) and (3.149).

Dr. K.D. Aldridge and the present author have developed a numerical program which evaluates the two-dimensional integrals in (3.165) by means of an n-point Gaussian scheme, and calculates the dispersion function

$$D = 1 + \frac{\Re(\Omega/\eta \kappa^2)}{\left\{ \Im(\Omega/\eta \kappa^2) - 1 \right\}} \frac{\Re(\Gamma^{(1)})}{\Im(\Gamma^{(2)})}$$

As for the dispersion function defined in (3.145), D must vanish for a solution of (3.165) with Re  $\Omega \neq 0$  sto exist. When this condition is satisfied, the eigenvalues for the problem may be calculated from

$$\frac{(\Lambda_c K)^2}{24\pi} \frac{(Rm)}{q} = \frac{-Re(\Omega/\eta K^2)}{-Re(\Omega/\eta K^2)}$$

$$= \frac{-Re(\Omega/\eta K^2)}{\int_0^\infty d\vec{r} e^{-\frac{1}{2}\{(\Lambda_c K\vec{r})^2 + (\eta K^2 t_c)^2(\vec{v} + Re\frac{\Omega}{\eta K^2})^2\}} dm \Theta(\vec{r}, \vec{v}; dm \frac{\Omega}{\eta K^2})}$$

#### 3.10.2 Numerical search procedure

parameters of the turbulence for *initial condition II*, numerical solutions to (3.165) can be obtained relatively easily. The numerical search procedure used is outlined below.

- a) Trial values of  $\text{Im }\Omega/\eta K^2$  and  $\text{Re }\Omega/\eta K^2$  were chosen.
  - b) A value of  $(\lambda_C K)^2/q$  was assumed.
  - c) The integrals in (3.165) and the dispersion function D were calculated for a range of values of  $\lambda_{\rm C} K$  satisfying the condition (2.147a).
  - d) The calculated values of D were examined for changes of sign, and further values of  $\lambda_C K$  were used if necessary to locate a sign change.
  - e) An iterative interpolation technique was used to determine the values of  $\lambda_c K$  and  $R_m^*$  corresponding to the solution point.
  - f) The process was repeated for new values of  $(\lambda_c K)^2/q$  and for new trial values of Im  $\Omega/\eta K^2$  and Re  $\Omega/\eta K^2$  .

Solutions were obtained for both large and small values of the parameter  $|\Gamma|$ , defined in (3.156).

The numerical integration was carried out with a fair degree of precision. Typical examples of the functions integrated are shown in Figures 10-14. The surfaces plotted correspond to  $\operatorname{Im} \Omega/\eta K^2 = 1.025$  and  $\operatorname{Re} \Omega/\eta K^2 = 0.001$  for several different values of  $(\lambda_{\rm c} K)^2/q$  marked by dots on the appropriate solution curve in Figure 16. The functions involving Re 0 (Figures 10a, 11a, 12a, 13a, and 14a) were integrated in three sections:

- a)  $\xi < \sqrt{(\text{Im }\Omega/\eta K^2)-1}$ , for which Re 0 < 0
- b)  $\sqrt{(\text{Im }\Omega/\eta K^2)-1} < \xi < \xi^*$ , where  $\xi^*$  was chosen in such a way that the integration spanned the first peak in the integrand, but stopped short of the second peak (if one existed)
- c)  $\xi > \xi^*$ , spanning the second peak.

On the other hand, the functions involving Im  $\theta$  (Figures 10b, 11b, 12b, 13b, and 14b) were integrated in a straightforward manner, since these functions have only a single peak. In each integration, limiting values of  $\xi$  and  $\nu$ , if not already specified by "section" boundaries, were chosen by requiring the absolute value of the integrand to fall below a specified fraction of the value at or near the peak.

The integration scheme has been tested for convergence with respect to both the choice of the specified fraction defining the integration limits, and the number of Gaussian points used. Typical results of the second test are shown in Figure 15. In view of these results, most of the integrations were carried out with an 8x8 grid for each of the three integrations involving Re θ, and a 12x12 or 16x16 grid for the single integration involving Im 0. A further check on the accuracy of the integration was provided by preliminary calculations in which the ξ and ν integrations were carried out using a 10-point Laguerre and a 10-point Hermite polynomial technique, respectively (see, for example, Abramowitz and Stegun, 1964, \$25.4.45 and \$25.4.46). The results of the Hermite-Laguerre integration were in good agreement with those obtained later using the Gaussian scheme (see, for example, Abramowitz and Stegun, 1964, \$25.4.30).

betails of the program used for the Gaussian.

integration scheme are given in Appendix 4.

Figures 10-14. Integrands of (3.165a) and (3.165b) for several values of  $\lambda_c/L$  and  $\tau_c/T$ .

In each figure, plot (a) shows

while plot (b) shows

### $J_{m}\Theta\{Y,v;J_{m}\Omega/\eta K^{2}\},e^{-\frac{1}{2}\{(\lambda_{c}KY)^{2}+(\eta K^{2}\tau_{c})^{2}(v+Re}\Omega/\eta K^{2})^{2}\}$

These quantities are plotted as functions of  $\xi$  and  $\nu$  for fixed values of  $\mbox{Im}~\Omega/\eta\mbox{K}^2$  ,  $\mbox{Re}~\Omega/\eta\mbox{K}^2$  ,  $\mbox{$\lambda_{\rm C}$K}$  , and  $\mbox{$\eta \mbox{K}^2$\tau}_{\rm C}$  . In the figures,

$$\frac{\lambda_{c}/L}{\tau_{c}/T} = \frac{\lambda_{c}K/2\pi}{\eta K^{2}\tau_{c}/2\pi}$$

$$\frac{\Omega_{d}}{\sigma} = \eta K^{2}$$

Figure 10: 
$$\lambda_{C}/L = 1.6$$
  $\tau_{C}/T = 3.5 \times 10^{-4}$ 

Figure 11:  $\lambda_{C}/L = 0.45$   $\tau_{C}/T = 3.5 \times 10^{-3}$ 

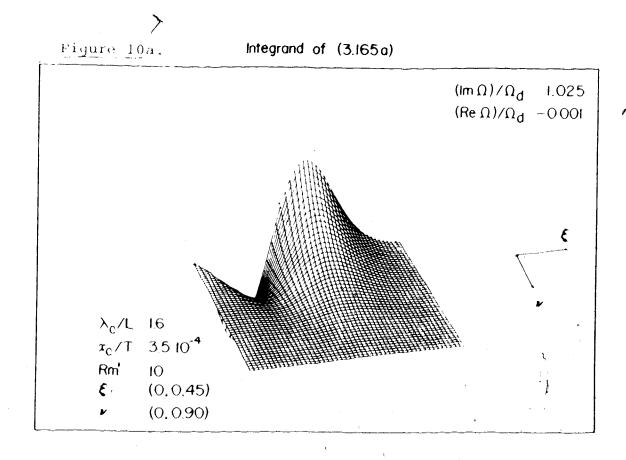
Figure 12:  $\lambda_{C}/L = 0.11$   $\tau_{C}/T = 3.5 \times 10^{-2}$ 

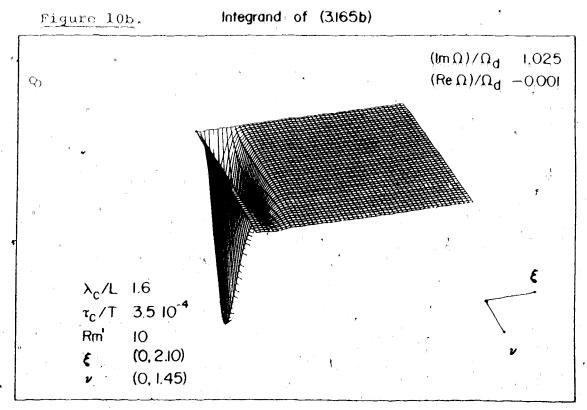
Figure 13:  $\lambda_{C}/L = 0.07$   $\tau_{C}/T = 0.1$ 

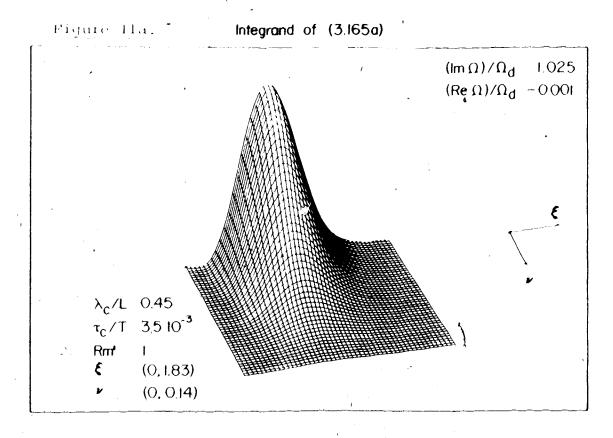
Figure 14:  $\lambda_{C}/L = 0.053$   $\tau_{C}/T = 1.0$ 

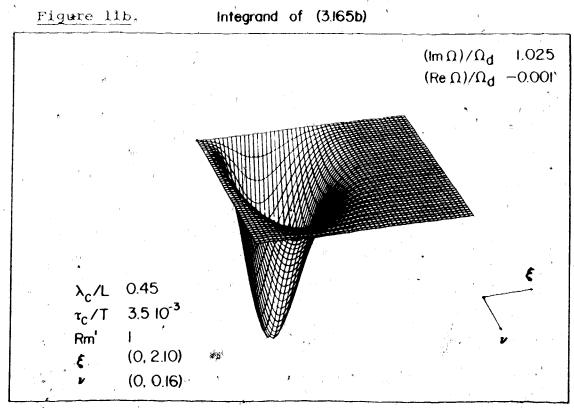
These values are taken from the fourth curve in Figure 16. In each case,

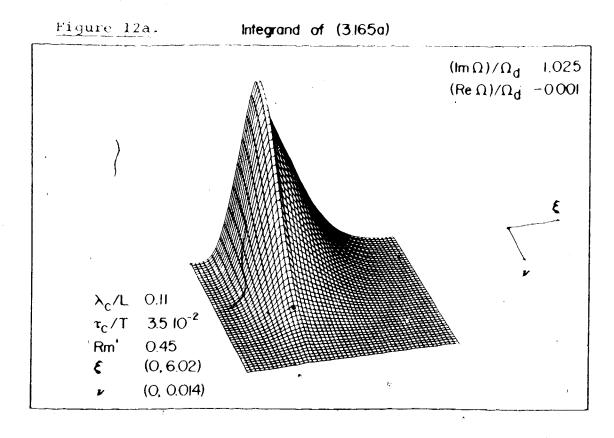
Im 
$$\Omega/\Omega_d = 1.025$$
 | Re  $\Omega/\Omega_d$  = 0.001

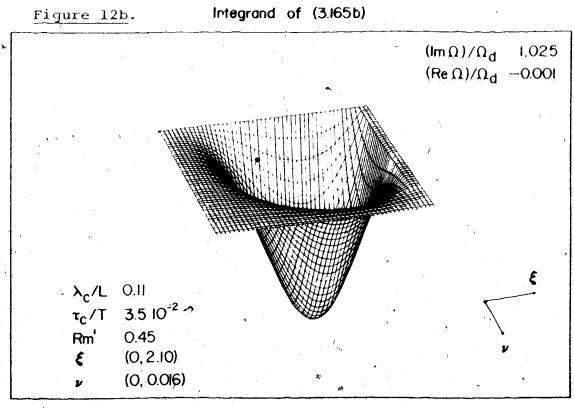


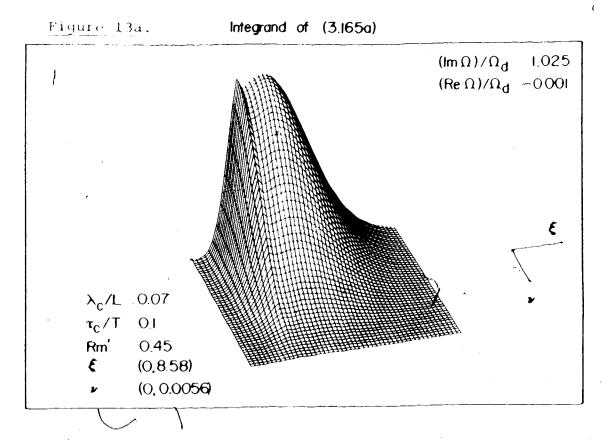




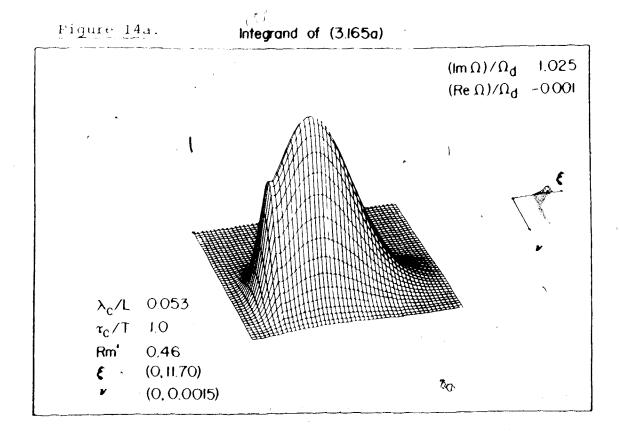








| No. | Integrand of (3.165b) |  $(Im Ω)/Ω_d$  | 1.025 |  $(Re Ω)/Ω_d$  | -0.001 |  $(Re Ω)/Ω_d$  | -0.001



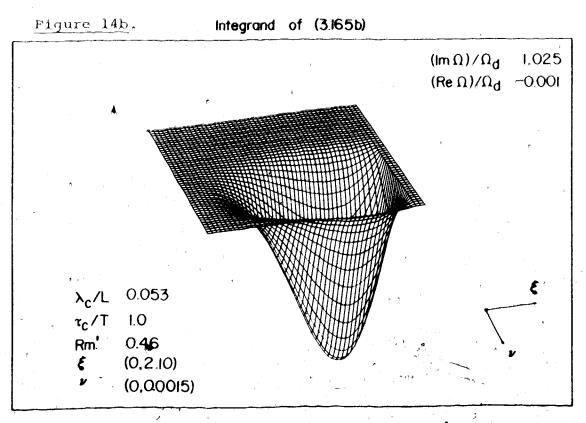
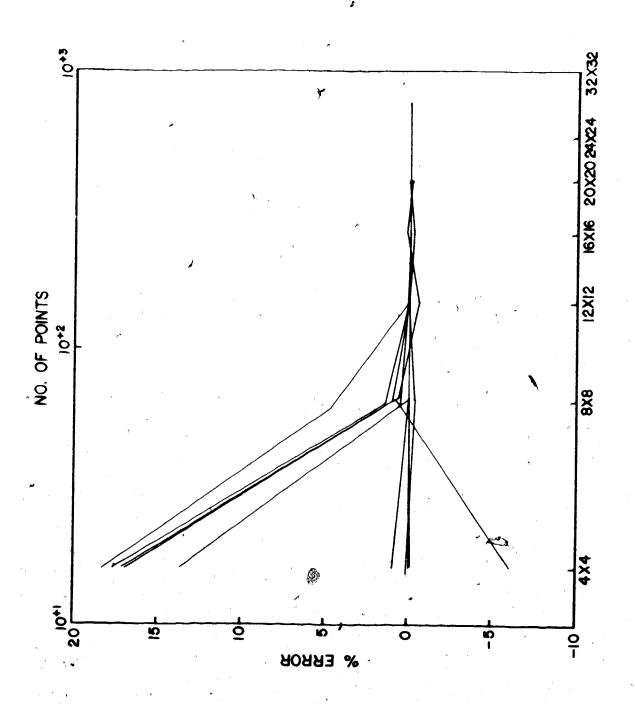


Figure 15. Typical convergence of the n-point Gaussian scheme used to evaluate the integrals in (3.165).

The plot shows percentage difference from the limiting value as a function of the number of integration points used. The upper scale shows number of points; the lower scale shows grid size.



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# 3.10.3 Behaviour of solutions as functions of $\lambda_C/L$ , $\tau_C/T$ , and $R_m$ .

Typical results of the calculations are shown in Figures 16-19. The solutions to (3.165) may be thought of as a pair of functions

Im 
$$\Omega/\eta K^2 = \text{Im } \Omega/\eta K^2 \left[ \lambda_C/L, \tau_C/T, R_m^* \right]$$
Re  $\Omega/\eta K^2$  Re  $\Omega/\eta K^2 \left[ \lambda_C/L, \tau_C/T, R_m^* \right]$ 

The equations

$$Im \Omega/\eta K^2 \approx constant = c_1$$

Re 
$$\Omega/\eta K^2 = constant = C_2$$

then define a curve representing the intersection of two surfaces in the space  $[\lambda_C/L, \tau_C/T, R_m']$ . Figures 16-18 show projections of this curve onto the three coordinate planes  $[\lambda_C/L, \tau_C/T]$ ,  $[\tau_C/T, R_m']$ , and  $[\lambda_C/L, R_m']$  for a fixed value of  $C_2$  and several different values of  $C_1$  corresponding to roughly equal logarithmic spacing of the values of  $(\text{Im }\Omega/\eta K^2)-1$ . On most of the plots,  $\lambda_C/L$  and  $\tau_C/T$  are restricted to values less than unity, in accordance with the conditions (3.147a,b).

The projection onto the  $[\lambda_{\rm C}/{\rm L},\,\tau_{\rm C}/{\rm T}]$  plane, shown in Figure 16, indicates that the value of  $\lambda_{\rm C}/{\rm L}$  corresponding to an oscillatory solution of (3.165) is more or less independent of  $\tau_{\rm C}/{\rm T}$  when  $\tau_{\rm C}/{\rm T}$  is small (i.e. when

 $[(\lambda_C K)^2/q] \cdot \text{Re}(\Omega/\eta K^2) \text{ is large, } \geq 1.9 \text{ ). As } \text{Im}(\Omega/\eta K^2)$  increases, solutions are found at progressively lower values of  $\lambda_C/L$ . On the other hand, Figure 17, which shows the projection onto the  $[\tau_C/T, R_m']$  plane, indicates that as  $\text{Im}(\Omega/\eta K^2)$  increases, so must  $R_m'$ . In addition, for each value of  $\text{Re}(\Omega/\eta K^2)$ ,  $R_m'$  reaches a minimum at  $\tau_C/T \geq 0.3$  when  $(\text{Im} \Omega/\eta K^2) \cdot 1 \approx \text{Re}(\Omega/\eta K^2)$ . The value of  $R_m'$  at this minimum decreases with  $\text{Re}(\Omega/\eta K^2)$ , as may be seen from Figure 19.

Figure 17 also indicates that at a given value of  $\text{Re}\,(\Omega/\eta K^2)$  , no solutions to (3.165) exist when

$$R_{m}^{\prime} < (R_{m}^{\prime})_{C} [\tau_{C}/T; \operatorname{Re}(\Omega/\eta K^{2})]$$
or  $\tau_{C}/T < (\tau_{C}/T)_{C} [R_{m}^{\prime}; \operatorname{Re}(\Omega/\eta K^{2})]$ 
(3.168)

where the functions  $(R_m^*)_C$  and  $(\tau_C/T)_C$  are defined by the lower envelope of the plotted curves when  $\tau_C/T < 0.3$ , and by the minimum in  $R'_m$  when  $\tau_C/T \geq 0.3$ . As might be expected from the way in which  $\lambda_C/L$  and  $\tau_C/T$  are interrelated, (3.168) is equivalent to the statements that there exist no solutions to (3.165) at a given value of  $Re(\Omega/\eta K^2)$  when

$$R_{m}^{\prime} < (R_{m}^{\prime})_{c} [\lambda_{c}/L; \operatorname{Re}(\Omega/\eta K^{2})]$$
or  $\lambda_{c}/L < (\lambda_{c}/L)_{c} [R_{m}^{\prime}; \operatorname{Re}(\Omega/\eta K^{2})]$ 
(3.169)

where  $(R_{m}^{r})_{c}$  and  $(\lambda_{c}/L)_{c}$  are defined by the dotted

cateoff curve in Figure 18.

Figure 18, which shows the projection of the solution curves onto the  $[\lambda_C/L]$ ,  $R_m^*$  plane, gives a clear illustration of the existence of a minimum in  $R_m'$  for a given value of  $Re(\Omega/\eta K^2)$ . For the value chosen in the plot  $[Re(\Omega/\eta K^2)] = 0.001$  the minimum in  $R_m^*$  occurs at  $\lambda_C/L \approx 0.25$ . The same result is obtained at different values of  $Re(\Omega/\eta K^2)$ , over a fairly wide range, as may be seen from Figure 19.

As  $\mathrm{Re}(\Omega/\eta K^2)$  is varied, the cut-off curve in Figure 18 retains its general shape, and the minimum stays at the same value of  $\lambda_{\mathrm{C}}/\mathrm{L}$ . In addition, the curves of constant  $\mathrm{Im}(\Omega/\eta K^2)$  do not alter greatly. The cut-off merely moves down in  $\mathrm{R}_{\mathrm{m}}^{\star}$  with decreasing  $\mathrm{Re}(\Omega/\eta K^2)$ , allowing the curves of constant  $\mathrm{Im}(\Omega/\eta K^2)$  to extend further toward the left of the diagram.

Figure 19 is a plot of curves of constant  $R_{\rm m}^{\prime}$  and curves of constant  $\lambda_{\rm c}/L$  as functions of  $({\rm Im}~\Omega/\eta K^2)-1$  and  ${\rm Re}~(\Omega/\eta K^2)$  at a fixed value of  $(\lambda_{\rm c} K)^2/q$ . The only curve of constant  $\lambda_{\rm c}/L$  shown is the one which passes through the points corresponding to the minimum  $R_{\rm m}^{\prime}$  for each value of  ${\rm Re}~(\Omega/\eta K^2)$ . Other curves of constant  $\lambda_{\rm c}/L$  run roughly parallel to the one shown, with  $\lambda_{\rm c}/L$  increasing foward lower values of  $({\rm Im}~\Omega/\eta K^2)-1$ .

Figure 20 is a plot of curves of constant  $\text{Re}(\Omega/\eta K^2)$  and curves of constant  $\lambda_C/L$  as functions of  $(\text{Im} \Omega/\eta K^2)-1$ 

and  $R_{\rm in}^{\prime}$  at the same fixed value of  $(\lambda_{\rm c} {\rm K})^2/{\rm q}$  as in Figure 19  $[(\lambda_{\rm c} {\rm K})^2/{\rm q}=30]$ . Only two curves of constant  $\lambda_{\rm c}/{\rm L}$  are shown - those for  $\lambda_{\rm c}/{\rm L}=0$  and  $\lambda_{\rm c}/{\rm L}=1$ . Because of condition (3.147a), all acceptable solutions will lie between these two curves.

It is interesting to compare Figure~20 with Figure~4. Clearly, when  $\lambda_{\rm C}/{\rm L}=0$  and  ${\rm Re}(\Omega/\eta{\rm K}^2)=0$ , the relation—ship between  $R_{\rm m}^{\rm i}$  and  $({\rm Im}~\Omega/\eta{\rm K}^2)-{\rm l}$  is the same on both plots—at least for  $R_{\rm m}^{\rm i}$  greater than the minimum shown on Figure~20. However, at larger values of  $\lambda_{\rm C}/{\rm L}$ , Figure~20 gives only a single pair of values  $[R_{\rm m}^{\rm i}; ({\rm Im}~\Omega/\eta{\rm K}^2)-{\rm l}]$  for each value of  $\lambda_{\rm C}/{\rm L}$ , in contrast to the infinite range of values shown in Figure~4. Figure~20 thus shows how the solutions of the eigenvalue problem for oscillatory mean fields form a discrete subset of the solutions for non-oscillatory mean fields in the limit  ${\rm Re}~\Omega + 0$ , as suggested in section 3.4.3.

Figure 20 clearly illustrates the existence of a minimum in  $R_{m}^{\prime}$  as  ${\rm Im}\,(\Omega/\eta K^{2})$  is varied and  ${\rm Re}\,(\Omega/\eta K^{2})$  is held constant. It is apparent that the value of  $R_{m}^{\prime}$  at the minimum increases monotonically with  ${\rm Re}\,(\Omega/\eta K^{2})$ . From Figure 17 it may also be seen that the minimum value of  $R_{m}^{\prime}$  increases monotonically as  $(\lambda_{C}K)^{2}/q$  decreases. The slope of the envelope curve in Figure 17 shows that, for  $T_{C}/T<0.3$ ,

$$(R_{\rm m}^{\prime})_{\rm min}^2 \propto (\tau_{\rm c}/T)^{-1}$$

Figure 16. Solutions of (3.165) ~ projection onto the  $[\lambda_c/L, \tau_c/T]$  plane.

Each curve shown is the projection onto the  $[\lambda_C/L, \tau_C/T]$  plane of a curve in  $[\lambda_C/L, \tau_C/T, R_m^*]$  space defined by the interpretation of the two surfaces

Im  $\Omega/\eta K^2$  = constant =  $C_1$ Re  $\Omega/\eta K^2$  = constant =  $C_2$ 

Curves are plotted for several different values of  $C_1$  at a fixed value of  $C_2$ . In the diagram,  $\Omega_d \equiv \eta K^2$ 

The dots on the fourth curve  $[C_1 = 1.025]$ , indicate the values of  $\lambda_C/L$  and  $\tau_C/T$  used in plotting the surfaces shown in Figures 10-14.

Projections onto the two remaining coordinate planes are shown in Figures 17 and 18.

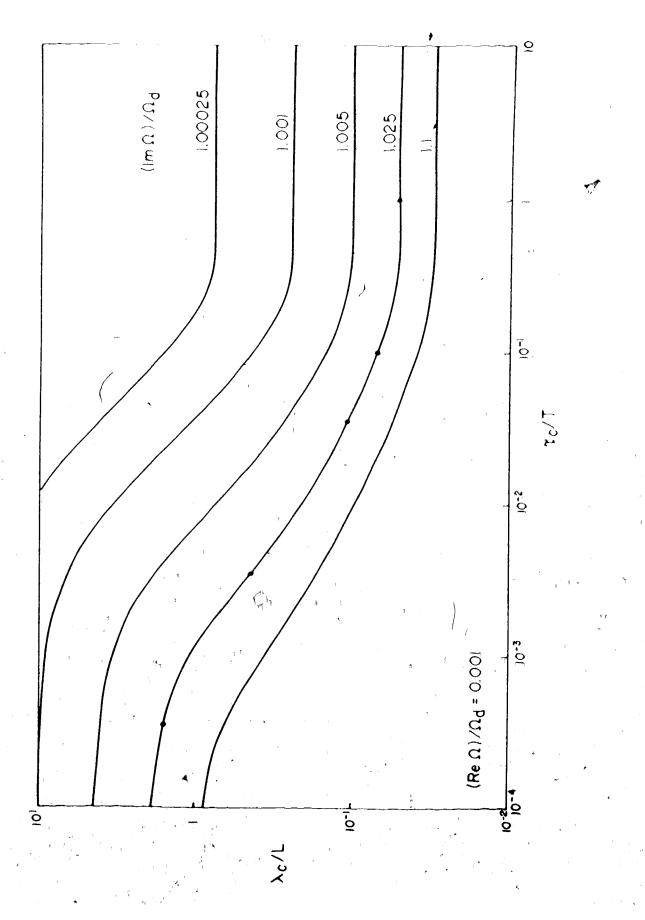


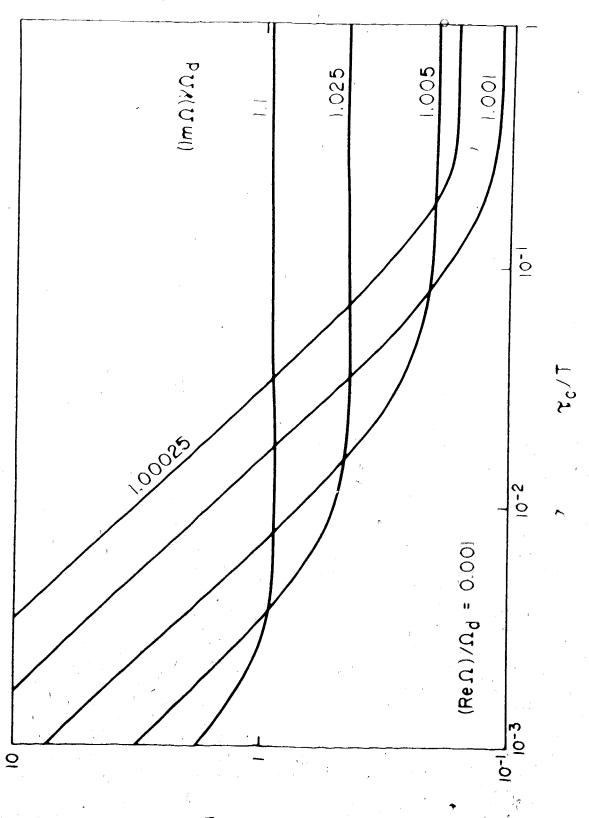
Figure 17. Solutions of (3.165) - projection onto the  $[\tau_{\text{C}}/T, R_{\text{m}}^{*}]$  plane.

Each curve shown is the projection onto the  $[\tau_C/T, R_m^*]$  plane of a curve in  $[\lambda_C/L, \tau_C/T, R_m^*]$  space defined by the intersection of the two surfaces

Im 
$$\Omega/\eta K^2 = \text{constant} = C_1$$
  
Re  $\Omega/\eta K^2 = \text{constant} = C_2$ 

Curves are plotted for several different values of  $\rm C_1$  at a fixed value of  $\rm C_2$  . In the diagram,  $\Omega_d \equiv \eta K^2$  ,

Projections onto the two remaining coordinate planes are shown in Figures 16 and 18.



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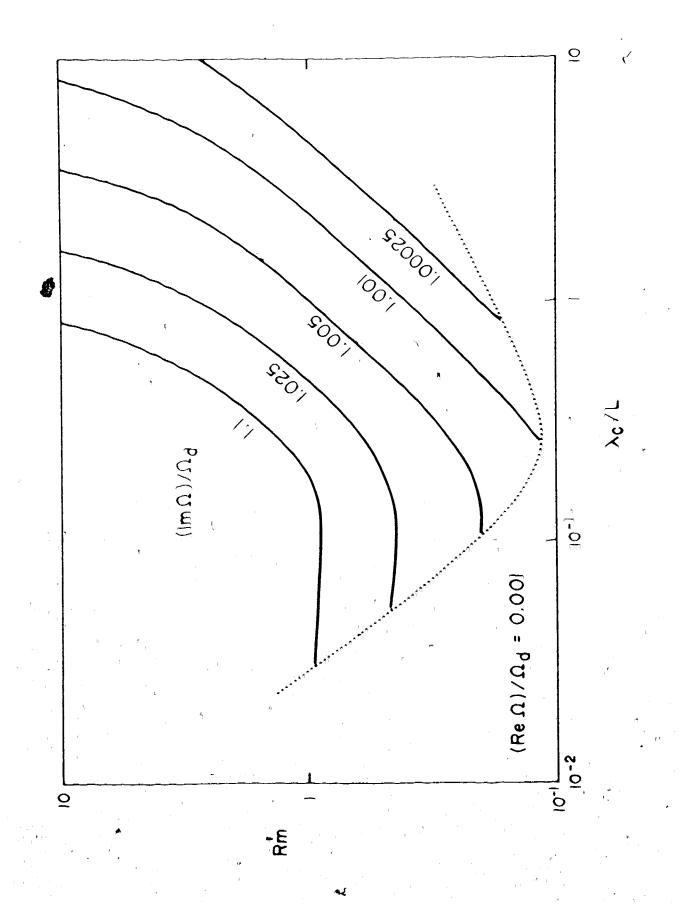
Figure 18. Solutions of (3.165) ~ projection onto the  $[\lambda_c/L, R_m^*]$  plane.

Each curve shown is the projection onto the  $[\lambda_C/L, R_m^i]$  plane of a curve in  $[\lambda_C/L, \tau_C/T, R_m^i]$  space defined by the intersection of the two surfaces

Im 
$$\Omega/\eta K^2$$
 = constant =  $C_1$   
Re  $\Omega/\eta K^2$  = constant =  $C_2$ 

Curves are plotted for several different values of  $C_1$  at a fixed value of  $C_2$ . In the diagram,  $\Omega_d = \eta K^2$ 

Projections onto the two remaining coordinate planes are shown in Figures 16 and 17.



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Figure 19. Solutions of (3.165) - projection onto the [Re  $\Omega/\eta K^2$ , (Im  $\Omega/\eta K^2$ )-1] plane.

Each of the solid curves is the projection onto the [Re  $\Omega/\eta K^2$ , (Im  $\Omega/\eta K^2$ )-1] plane of the intersection of two surfaces



$$R_{m}' = constant = C_{1}'$$

$$\tau_{C} \eta K^{2} = constant = C_{2}'$$

Curves are plotted for several different values of  $C_1^i$  at a fixed value of  $C_2^i$ . In the diagram,  $\Omega_d \equiv \eta K^2$ .

The dotted curve is the projection onto the same plane of the intersection of the two surfaces

$$\lambda_{\rm C}/L = {\rm constant} = C_3'$$

$$\tau_{\rm C} \eta K^2 = {\rm constant} = C_2'$$

C'\_3 is chosen in such a way that the curve passes through the points corresponding to the minimum value of R'\_m at each value of Re  $\Omega/\eta K^2$ . Curves for other values of C'\_3 run roughly parallel to the dotted curve, with C'\_3 increasing toward lower values of (Im  $\Omega/\eta K^2$ )-1.

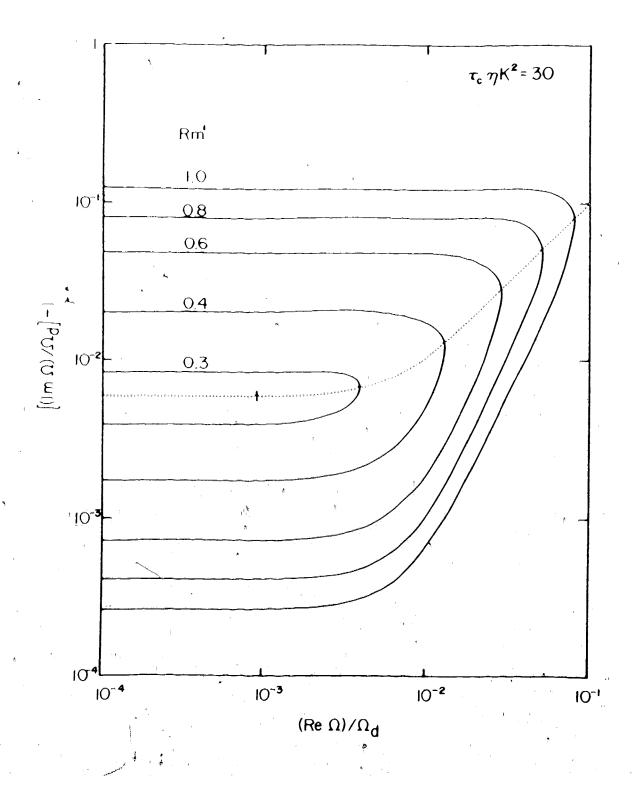


Figure 20. Solutions of (3.165) - projection onto the  $[R_m^+, ^{\ \ \ \ }(Im\ \Omega/\eta K^2)-1]$  plane.

Each of the solid curves is the projection onto the  $[R_m^*, (\text{Im }\Omega/\eta K^2)-1]$  plane of the intersection of two surfaces

1

Re 
$$\Omega/\eta K^2$$
 = constant =  $C_2$   
 $\tau_C \eta K^2$  = constant =  $C_2$ 

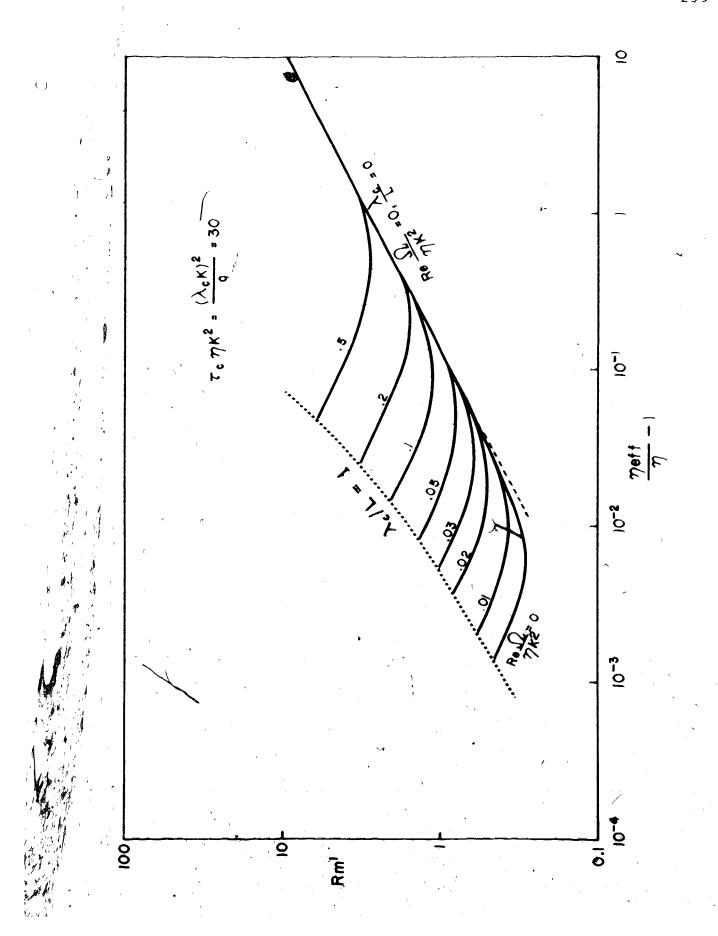
Curves are plotted for several different values of  $C_2$  at the value of  $C_2^{\dagger}$  used in Figure 19 [i.e.  $C_2^{\dagger} = 30$ ]. In the diagram,  $(\eta/\eta_{\rm eff})$  has been written in place of Im  $\Omega/\eta K^2$  (see section 3.6.2, equation 3.86).

The dotted curves are the projections onto the same plane of the intersection of the surfaces

$$\lambda_{\rm C}/L = {\rm constant} = {\rm C}_3'$$

$$\tau_{\rm C}\eta {\rm K}^2 = {\rm constant} = {\rm C}_2'$$

, for  $C_2' = 30$  and  $C_3' = 0, 1$ .



# 3.10.4 The existence of acceptable slowly-decaying, long-period, oscillatory mean fields

Although initial condition II does not lead to a restriction like (3.148) on  $(\lambda_C K)^2/q$ , it is of interest to see whether such a condition can be satisfied. From Figures 16 and 17 we see that

$$R_{m}^{\prime} = \beta_{1} \left[ \operatorname{Im} \left( \Omega / \eta K^{2} \right), \operatorname{Re} \left( \Omega / \eta K^{2} \right) \right] / \tau_{c} \eta K^{2}$$
 (3.171)

$$\lambda_{C}^{K} \rightarrow \beta_{2} [\text{Im}(\Omega/\eta K^{2}), \text{Re}(\Omega/\eta K^{2})]$$
 (3.172)

when  $(\lambda_c K)^2/q = \eta \tau_c K^2 \ll 1$ . Therefore

$$\frac{l_{im}}{(\lambda_{cK})^{2}/q} = \frac{l_{im}}{(\lambda_{cK})^{2}/q} \left\{ \frac{R'_{m}}{(\lambda_{cK})^{2}} \frac{(\tau_{c\eta}K^{2})}{(\lambda_{cK})^{2}} \right\}$$

$$= \frac{\beta_{i}}{\beta_{a}^{2}} \left[ \int_{m} \Omega/\eta K^{2}, \operatorname{Re} \Omega/\eta K^{2} \right] \qquad (3.173)$$

This limit will give the smallest possible value of R'/q for given values of  $Im(\Omega/\eta K^2)$  and  $Re(\Omega/\eta K^2)$ .

Figure 21 shows how  $R_m^*/q$  and  $\lambda_c/L$  depend on  ${\rm Im}\,(\Omega/\eta K^2) \quad {\rm and} \quad {\rm Re}\,(\Omega/\eta K^2) \quad {\rm when} \quad \eta \tau_c K^2 \quad {\rm is \ small.} \quad {\rm For} \quad \eta \tau_c K^2 \lesssim 5 \times 10^{-4} \ , \ {\rm and} \quad {\rm Re}\,(\Omega/\eta K^2) \lesssim 100 \ ,$ 

$$\lambda_c/L \approx 0.35 \{ (\text{Im } \Omega/\eta K^2) - 1 \}^{-1/2}$$
 (3.174a)

$$R_{\rm m}/q \approx 0.78 \{ (\text{Im } \Omega/\eta k^2) - 1 \}^{-1/2}$$
 (3.174b)

so that

$$(\lambda_{c}^{K}) (R_{m}^{\prime}/q) = 2\pi (\lambda_{c}^{\prime}/L) (R_{m}^{\prime}/q) \approx 1.7$$
 (3.175)

In general, there is very little dependence on  $\operatorname{Re}(\Omega/\eta K^2)$  .

It may be seen from Figure~21 that the condition (3.148) can in fact be satisfied by solutions to (3.165) which also satisfy (3.147) and (3.150). In other words, there exist solutions to (3.165) for which

- a) the wavelength is long compared with the correlation length of the turbulence  $[\lambda_{\hat{c}}/L < 1]$
- b) the decay time is long compared with the correlation time of the turbulence  $[\tau_{\rm c}/T_{
  m d}$  << 1 i.e.  $\eta\tau_{
  m c}K^2$  << 1]
- c) the first order smoothing approximation is valid  $[R_m^* < q \text{ , for } q \text{ large}]$
- d) the period is long compared with the correlation time of the turbulence  $[\tau_c/T << 1$  this condition holds since the solutions depend very little on  $\text{Re}(\Omega/\eta K^2)$ ]

The range in which solutions of this type can occur is very limited, as may be seen from Figure 21. Clearly, for the conditions (a)-(d) all to be satisfied, we must have  $1.13 \leq \text{Im}(\Omega/\eta K^2) \leq 2.6$ .

It is never possible to satisfy (3.148) and (3.150) simultaneously when q is small. In this limit, (3.150) requires that  $R_{\rm m}' << 1$ , while (3.148) requires that  $q/\left(\lambda_{\rm C}K\right)^2 >> 1$ . But, for a given value of  ${\rm Re}\left(\Omega/\eta K^2\right)$ , (3.170) implies that

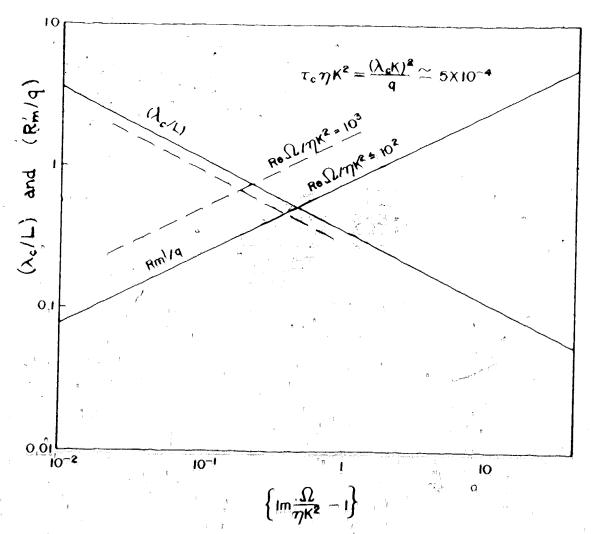


Figure 21. Solutions of (3.165) -  $(\lambda_c/L)$  and  $(R_m/q)$  as functions of  $(\text{Im }\Omega/\eta K^2)-1$  in the limit of small  $\tau_c\eta K^2$ .

The solid curves show the behaviour of  $(\lambda_{_{\bf C}}/L)$  and  $(R_m'/q)$  when Re  $\Omega/\eta K^2 < 10^2$ . At larger values of Re  $\Omega/\eta K^2$ ,  $(\lambda_{_{\bf C}}/L)$  and  $(R_m'/q)$  depend on both Re  $\Omega/\eta K^2$  and Im  $\Omega/\eta K^2$ , as indicated by the dashed curves [Re  $\Omega/\eta K^2$  10 $^3$ ].

$$(R'_m)_{min}^2 \propto \frac{(T/\tau_c)}{Re \Omega/\eta \kappa^2} \propto \frac{q}{(\lambda_c \kappa)^2}$$
 (3.176)

It may be seen from Figure 17 that the constant of proportionality on the right hand side of (3.176) is approximately 12.4. Hence, in the limit as  $q \neq 0$  but  $q/\left(\lambda_c K\right)^2$  remains large,

$$Iq \to 0; q/(\lambda_c K)^2 largel R_m >> \sqrt{12.4} = 3.5$$
 (3.177)

in contradiction to (3.150).

### 3.11 The kinematic dynamo problem

# 3.11.1 The two-dimensional integral technique and turbulence without PT-invariance

For the case of decaying mean fields, it has been found that the two-dimensional integration scheme used in treating initial condition II is generally easier to handle than the one-dimensional scheme used in dealing with initial condition I. Although the principal difficulty encountered with the one-dimensional integration will not earise in the case of growing mean fields, it may well be that the two-dimensional technique is better suited to a general study of dynamo action in turbulent fluids.

The irregular behaviour exhibited by the function Re O, when the mean field is rapidly decaying  $[\operatorname{Im}(\Omega/nK^2) > 1]$  is not present when the mean field is growing or slowly decaying  $[\operatorname{Im}(\Omega/nK^2) < 1]$ , as may be seen from Figure 1. It remains to be shown that the evaluation of the integral  $I_{ij}^{(2)}$  defined in (2.89) can be carried out easily by the two-dimensional integration technique when helicity is present.

The simplest possible case of turbulence which is not PT-invariant is described by the spectrum tensor (Batchelor, 1953, p. 43; Moffatt, 1970a)

$$\bar{\Phi}_{ij} = \frac{E(k,\omega)}{4\pi k^4} \left\{ k^2 \delta_{ij} - k_i k_j \right\} + i \epsilon_{ij\ell} \frac{F(k,\omega)}{8\pi k^4} k_\ell \qquad (3.178)$$

From (3.178) and (2.89'),

$$I_{ij}^{(2)} = i \epsilon_{igm} K_{2} \iint \frac{F(k_{i}\omega)}{4\pi k^{4}} \frac{k_{j} k_{m}}{i(\omega+\Omega) + \eta(k_{j}+k_{j})^{2}} dkd\omega \qquad (3.179)$$

Taking K to define the z-axis in k-space, as was done in (3.18),

$$T_{ij}^{(2)} = \frac{i}{8} \epsilon_{ijj} K_{j} \int_{-\infty}^{\infty} d\omega \int_{0}^{\infty} dk \frac{F(k_{i}\omega)}{k^{4}} \cdot 2k^{4} \cdot \int_{0}^{\pi} \frac{\sin^{3}\theta d\theta}{i(\omega + \Omega) + \eta(k^{2} + K^{2} + 2kK\cos\theta)}$$

= 
$$\frac{i}{8} \epsilon_{i\beta j} K_{\beta} K^{5} \int_{-\infty}^{\infty} dv \int_{0}^{\infty} d\xi \frac{F(K\xi, \eta K^{2}v + \Re\Omega)}{(K\xi)^{4}} \Theta(\xi, v; 4m\frac{\Omega}{\eta K^{2}})$$

(3,180)

It follows, therefore, that the integrals to be evaluated are of precisely the same form as those already treated in the case of PT-invariant turbulence.

### 3,11,2 The mean field dispersion relation

If we define

$$\mathbf{I}^{(2)} \equiv \frac{1}{8} \mathbf{K}^5 \int_{-\infty}^{\infty} d\mathbf{r} \int_{-\infty}^{\infty} d\mathbf{r} \frac{F(\mathbf{K}_{\mathbf{r}}^{\mathbf{r}}, \mathbf{\eta} \mathbf{K}^2 \mathbf{v} + \Re \Omega)}{(\mathbf{K}_{\mathbf{r}}^{\mathbf{r}})^4} \Theta(\mathbf{r}, \mathbf{v}; \mathbf{f}_m \frac{\Omega}{\mathbf{\eta} \mathbf{K}^2})$$
(3.181)

then, from (3.180),

$$\mathbf{I}_{ij}^{(2)} = -i \, \epsilon_{ijk} \, \mathbf{K}_{k} \, \mathbf{I}^{(2)}(\mathbf{K}, \Omega) \qquad (3.182)$$

and

$$\left\{ \text{Re } \underline{\mathbf{I}}^{(2)} \text{ Im } \underline{\mathbf{I}}^{(2)} \right\}_{ij} = \left\{ \text{Im } \underline{\mathbf{I}}^{(2)} \text{ Re } \underline{\mathbf{I}}^{(2)} \right\}_{ij}$$

$$= -\epsilon_{ijm} \epsilon_{mnj} \, \kappa_{j} \, \kappa_{n} \, \text{Re } \underline{\mathbf{I}}^{(2)} \, \text{Im } \underline{\mathbf{I}}^{(2)}$$

$$= \left\{ \kappa^{2} \delta_{ij} - \kappa_{i} \, \kappa_{j} \right\} \, \text{Re } \underline{\mathbf{I}}^{(2)} \, \text{Im } \underline{\mathbf{I}}^{(2)}$$

$$= \left\{ \kappa^{2} \delta_{ij} - \kappa_{i} \, \kappa_{j} \right\} \, \text{Re } \underline{\mathbf{I}}^{(2)} \, \text{Im } \underline{\mathbf{I}}^{(2)}$$

$$(3.183) \, \underline{\mathbf{S}}^{(2)}$$

Substituting (3.183) into (2.91), we see that the dispersion relation for the mean field is

$$\det \left( \begin{array}{c} aa + bb \\ a & b \end{array} \right) = O \tag{3.184}$$

where

$$a_{ij} = -4m \left\{ \epsilon_{ijk} K_k \mathbf{I}^{(2)} + \delta_{ij} \left[ \Omega - i\eta K^2 - i \mathbf{I}^{(3)} \right] \right\}$$
(3.185a)

$$b_{ij} = \Re\left\{ \epsilon_{ijk} \kappa_k \mathbf{I}^{(2)} + \delta_{ij} \left[ \Omega - i\eta \kappa^3 - i\mathbf{I}^{(i)} \right] \right\}$$
 (3.185b)

When (3.185) is substituted into (3.184) and the determinant is expanded, the dispersion relation is found to have three roots, specified by

$$i\Omega + \eta K^2 + I^{(i)} = O, \qquad (3.186a)$$

$$i\Omega + \eta K^2 + I^{(1)} = \mp K I^{(2)}$$
 (3.186b,c)

As pointed out by Moffatt (1970a), these roots correspond to normal decay (3.186a), enhanced decay (3.186b), and netarded decay (or growth) (3.186c). (3.186c), the equation which leads to growing wave solutions, and hence to dynamo action, corresponds to the lower sign in (3.186b,c).

### 3.11.3 The possibility of a "sporadic helicity" dynamo

Consideration of the growing wave solutions of (3.186c) leads to a situation in which decaying wave solutions corresponding to initial condition II may be important. A nonstationary kinematic dynamo of the speradic type discussed in section 1.4.6 can be constructed by allowing the helicity of the turbulence to vary with time. The helicity is initially "turned on" for a period long enough to allow the effects of initial conditions to die away: The growing wave solutions to (3.186c) can then be followed as  $F(k,\omega)$ , and hence  $I^{(2)}$ , is allowed to vary slowly with time. When  $I^{(2)}$  goes to zero, equation (3.186c) reduces to equation (3.39), corresponding to initial condition II. The mean field will then decay in the manner described above in section 3.10, until such time as the fielicity is "turned on" again.

#### 3.12 Summary of Chapter 3

This chapter is concerned with the effects of PT-invariant turbulence on large scale magnetic fields. Much of the work described was carried out jointly by the present author and Dr. K.D. Aldridge (Gilliland and Aldridge, 1973).

In section 3.2 it is proved that stationary, homogeneous turbulence whose average properties are invariant under space-time inversion (PT-invariant turbulence) cannot support dynamo action in an incompressible fluid, in the first order smoothing approximation (see section 2.5.4 for a definition of first order smoothing). This result is a generalization of a theorem due to Krause and Roberts (1973). It directly contradicts the work of Lerche and Low (1971).

Sections 3,3,3,10 present a detailed study of the decay of wave mean fields in the presence of PT-invariant turbulence. Two initial conditions are studied:

- It the initial turbulent component of the magnetic field is not correlated with the turbulent velocity -i.e.  $u'_j(x,t)B'_k(x',t_0) = 0$  for all choices of (x,x',t). (A less restrictive condition which leads to the same result is described in section 3.3.2.)
- II: the initial turbulent component of the magnetic field is correlated with the turbulent velocity in

such a way that  $\operatorname{curl}\left[\begin{array}{ccc} \widetilde{\mathbf{u}}' \times \widetilde{\mathbf{B}}' \end{array}\right] \left(\underline{\mathbf{x}}, \mathbf{t}_{O}\right) \propto \widetilde{\widetilde{\mathbf{B}}}\left(\underline{\mathbf{x}}, \mathbf{t}_{O}\right)$  for all choices of  $\underline{\mathbf{x}}$ . (See section 3.3.3.)

In the first order smoothing approximation, spatially periodic mean magnetic fields can exist in an infinite turbulent medium only if the two-point, two-time correlation tensor of the turbulence falls off at least exponentially with time displacement  $\tau$ . If the correlation tensor has an exponential dependence on  $\tau$ , spatially periodic mean fields can/exist only if the correlation time of the turbulence,  $\tau_{\rm c}$ , is shorter than the effective decay time of the mean field,  $\tau_{\rm d}^{\rm eff} = [\eta_{\rm eff}^{\rm K^2}]^{-1}$ .  $\eta_{\rm eff}^{\rm f}$  is the turbulent magnetic diffusivity, and K the wave number of the mean magnetic field. (See section 3.7.3.)

In sections 3.6-3.10, isotropic Gaussian turbulence is studied as an example of turbulence in which the correlation tensor falls off more rapidly with  $\tau$  than  $\exp\left[-\left|\tau\right|/\tau_{\rm C}\right]$ . Several restrictions on the parameters of the mean field and the turbulence arise.

a) When initial condition I applies, spatially periodic mean fields can exist only if  $\tau_{\rm c}$  is shorter than  $\beta T_{\rm d}^{\rm eff}$ , where  $\beta = \beta (\tau_{\rm c}/T_{\rm d}; \lambda_{\rm c}/L)$ .  $T_{\rm d}$  is the natural decay time of the mean field in the absence of turbulence,  $\lambda_{\rm c}$  the correlation length of the turbulence, and L the wavelength of the mean field.

Furthermore, spatially periodic mean fields can

exist only if the magnetic Reynolds number of the turbulence,  $R_m^*$ , is less than a critical value,  $\binom{R_m^*}{C} = \binom{T_d}{C} + \binom{T_d}{C$ 

- b) When initial condition II applies, spatially period mean fields can exist only if  $\tau_C \leq \beta' T_d^{eff}$ , where  $\beta' = \beta' [\lambda_C/L]$ . There is no restriction on .  $R_m' \leq [See\ section\ 3.6.5.]$
- The effective magnetic diffusivity,  $\eta_{\rm eff}$ , normally depends on the parameters of the turbulence  $[\tau_{\rm c}, \lambda_{\rm c}]$ ,  $R_{\rm m}^{\prime}]$ , the relationship between the turbulence and the mean field  $[\tau_{\rm c}/T_{\rm d}, \lambda_{\rm c}/L]$ , and the initial conditions [I, II]. However, both the dependence on the r properties of the mean field and the dependence on initial conditions are weak, and disappear entirely in certain circumstances.
- and ii. the diffusion time on the length scale of the turbulence,  $(\lambda_c^2/\eta)$  << the effective diffusion time on the length scale of the mean field,  $(L^2/\eta_{\rm eff})$ .
  - e) When initial condition I applies, neff is

independent of the properties of the mean field if [section 3, 8, 2]

$$\begin{split} &\tau_{c} < 0.025 \ T_{d}^{eff} \ , \quad [\lambda_{c}^{2}/\eta < 0.01 \ \tau_{c}] \\ &\tau_{c} < 0.025 \ [T_{d}^{eff}]/[T_{d}^{-}T_{d}^{eff}] \ , \quad [\lambda_{c}^{2}/\eta > 0.01 \ \tau_{c}] \end{split}$$

f) When initial coefficient applies,  $\eta_{\rm eff}$  changes with time, stabilizing at a limiting value  $[\eta_{\rm eff}]^{*}$  after a time  $T_1$ .  $[\eta_{\rm eff}]^{*}$  can be used to describe the decay of the mean field provided that  $T_1 \ll T_{\rm d}^{\rm eff}$  [ner section 3.8.4 for a more precise statement of this (condition).

The condition on  $T_1$  can be translated into a condition on the parameters of the turbulence and the mean field [see section 3.8.5 and Figure 8]. In general,  $T_1$  must be less than two correlation times [much less, if  $\lambda_C^2/\eta << \tau_C$ ] for  $[\eta_{eff}]^*$  to be a meaningful parameter.

g) When initial condition II applies,  $\eta_{\rm eff}$  is independent of the properties of the mean field if  $\lambda_{\rm C}$  << 0.16 L [see section 3.6.3].

Restrictions (d)-(g) can be interpreted as restrictions on the usefulness of the  $R\ddot{a}dler\ expansion$  (3.96) as a representation of  $u'x\ B'$ . The Rädler expansion is

obtained using initial condition I, and only the first term of the expansion is independent of the properties of the mean field.

It should be noted that the Rädler expansion is not useful when the mean field oscillates with time [section 3.9.1]. For this reason, the validity of Krause and Rädler's expression for the "turbulent conductivity" appropriate to an oscillatory, decaying mean field (Krause and Rädler, 1971, pp. 70-71) is open to question.

Sections 3.9 and 3.10 present a study of the behaviour of decaying mean fields, periodic in space and oscillatory in time, in the presence of Gaussian turbulence. It is shown [sections 3.9.4 and 3.9.5] that if initial condition I applies, no mean fields of this type with

$$\{(\tau_{c}/\tau_{d}^{eff})^{2} + (\tau_{c}/\tau)^{2}\}^{1/2} \ll 1$$

can exist unless  $(\tau_C/T)$  is identically zero. T is the oscillation period of the mean field.

On the other hand, if initial condition II applies, spatially periodic, oscillatory mean fields for which  $\tau_{\rm C} << {\rm T}$  can exist. (Initial condition II does not lead to the requirement that  $\tau_{\rm C} << {\rm T}_{\rm d}^{\rm eff}$ .) The behaviour of these fields is described in section 3.10.3. If the condition  $\tau_{\rm C} << {\rm T}_{\rm d}$  is imposed on solutions obtained using initial condition II, it is found that turbulence for which

 $\lambda_{\rm c}^2/\eta << \tau_{\rm c}$  cannot support spatially periodic, oscillatory mean fields of the required type [section 3.10.4].

In section 3.11 the effect of relaxing the condition of PT-invariance on the turbulence is investigated. It is found that the mean field dispersion relation for this problem, while somewhat more complicated than the one studied earlier in the chapter, still involves only integrals of the type studied in section 3.10. It is suggested that the numerical techniques used in section 3.10 may well provide the most convenient method for investigating dynamo action generated by non-PT-invariant turbulence. The possibility of a dynamo with sporadic helicity is also discussed [section 3.11.3].

4. THE DYNAMO PROBLEM AND INHOMOGENEOUS, NONSTATIONARY TURBULENCE

#### 4.1 Introduction

As pointed out in the last chapter, the assumption of stationary, homogeneous turbulence is a gross oversimplification in a real, finite fluid. One of the principal difficulties lies in the fact that no boundary conditions can be applied to turbulence of this sort. In a dynamo like the geodynamo, where boundary conditions are important, it will clearly be necessary to consider inhomogeneous turbulence. Furthermore, if the time behaviour of the mean magnetic field is to be described with any degree of accuracy, the turbulence will have to be nonstationary, particularly in the hydromagnetic dynamo problem.

The principal effect of introducing nonstationary, inhomogeneous turbulence into mean field electrodynamics is to make  $\underline{\underline{u}}$ 'x  $\underline{\underline{B}}$ ' depend explicitly on position and time, as well as on the mean fields  $\underline{\underline{u}}$  and  $\underline{\underline{B}}$ . When  $\underline{\underline{B}}$  is a growing function of time, equation (2.22) gives

after a time sufficiently long for the effects of initial conditions on  $\underline{B}$ ! to have died out. Clearly, the effects of nonstationarity and inhomogeneity of the turbulence are represented by the dependence of the correlation tensor  $R_{ip}(\underline{x},t;\underline{x}',t')$  on each of its arguments separately

We may therefore introduce nonstationarity and inhomogeneity into the kinematic dynamo problem fairly simply by choosing suitable forms for the tentor  $R_{jp}$  [in the first order smoothing approximation], and for higher-order correlation tensors [when equations (2.25)-(2.30) are taken into account].

- 4.2 Inhomogeneous, nonstationary turbulence a survey of existing techniques
- 4.2.1 Locally homogeneous, quasi-stationary random functions the *Kolmogorov* structure tensor approach

One of the most commonly used approaches to the study of inhomogeneous, nonstationary turbulence is that introduced by Kolmogorov ([84]a,b). In this approach, a random field u'(x,t) is said to be locally homogeneous and quasi-stationary in a region G if the distribution functions of the difference

$$u_{\underline{1}}^{\bullet}(\underline{x}+\underline{r}, t+\tau) - u_{\underline{1}}^{\bullet}(\underline{x},t)$$
 (4.2)

are inveriant for all choices of (x,t) in G. In other words, the difference (4.2) can be considered as a stationary, homogeneous random function in G. (See, for example, Tatarski, 1961, p. 19ff; Yaglom, 1962, p. 93; Panchev, 1971, p. 149.)

The principal quantity of interest in this approach is the structure tensor,

$$D_{ij}(\mathbf{r},\tau) \equiv \left\{ u_i(\mathbf{x}+\mathbf{r},t+\tau) - u_i(\mathbf{x},t) \right\} \left\{ u_i(\mathbf{x}+\mathbf{r},t+\tau) - u_j(\mathbf{x},t) \right\}$$

$$(4,3)$$

which is related to the correlation tensor by the equation

$$D_{ij}(\underline{r},t) = R_{ij}(\underline{x}+\underline{r},t+\tau)\underline{x}+\underline{r},t+\tau) + R_{ij}(\underline{x},t;\underline{x},t)$$

$$- R_{ij}(\underline{x},t;\underline{x}+\underline{r},t+\tau) - R_{ii}(\underline{x},t;\underline{x}+\underline{r},t+\tau)$$

(4.3')

As may be seen from equation (4.3'), the structure tensor approach does not provide a direct method for evaluating the correlation tensor  $R_{ij}$ . The approach is therefore not immediately useful in mean field electrodynamics.

# 4.2.2 The Silverman approach to locally stationary and homogeneous turbulence with smoothly varying mean characteristics

Probably the simplest approximation to the correlation tensor of a nonstationary, inhomogeneous random process is that suggested by Silverman (1967; see also Tatarski, 1961, pp. 53-55). In this approach, the average properties of the turbulent field are assumed to vary smoothly over large length and time scales.

In Silverman's terminology, a random field wi(x,t) is said to be locally stationary and homogeneous if its correlation tensor can be written as

$$R_{ij}(x,t,x',t') = \overline{u_i(x',t')u_j'(x,t)}$$

$$= f\left\{\frac{x+x'}{2}, \frac{t+t'}{2}\right\} r_{ij}(x'-x,t'-t) \qquad (4.4)$$

It is clear from (4.4) that the Silverman approach will not permit boundary conditions on u' to be applied exactly, because of the way in which the "amplitude" f is

defined. Because of this restriction, the Silverman approach has only limited application in mean field electrodynamics.

# 4.2.3 The Rädler approach to locally stationary and homogeneous turbulence with smoothly varying mean characteristics

The principal difficulty encountered in the Silverman approach can be overcome by means of a Taylor series
approach due to Krause and Rädler (1971) and Kädler (1972;
see also P.M. Roberts, 1971a). In this approach it is
assumed that the correlation tensor has the form

$$R_{ij}(x,t;x+r,t+\tau) =$$

= 
$$u'^{2}(x,t) m_{ij}^{(i)}(r,\tau) + \tau \frac{\partial}{\partial t} u'^{2}(x,t) m_{ij}^{(i)}(r,\tau) + r \cdot \left[\sum_{i=1}^{n} u'^{2}(x,t)\right] f^{(i)}(r,\tau)$$
  
+  $r \cdot \sum_{i=1}^{n} u'^{2}(x,t) m_{ij}^{(i)}(r,\tau) + r \cdot \left[\sum_{i=1}^{n} u'^{2}(x,t)\right] f^{(i)}(r,\tau)$   
+  $r \cdot \left[\sum_{i=1}^{n} u'^{2}(x,t)\right] f^{(i)}(r,\tau) + r \cdot \left[\sum_{i=1}^{n} u'^{2}(x,t)\right] f^{(i)}(r,\tau)$   
(4.5)

where

$$u'^{2}(x+r,t+r) = u'^{2}(x,t) + r \nabla u'^{2}(x,t) + r \frac{\partial}{\partial t} u'^{2}(x,t)$$

$$+ \cdots \qquad (4.6)$$

General symmetry considerations are then used to determine the form of the tensors  $m_{ij}^{(0)}$ ,  $m_{ij}^{(11)}$ , and  $m_{ij}^{(12)}$ . This method is very useful when dealing with the kinematic

dynamo problem, but it is not well suited to the study of the more general hydromagnetic dynamo problem.

kädler (1972) has derived a general expression for the correlation tensor of a turbulent velocity field in which all deviations from homogeneity and isotropy can be described in terms of the gradient of the turbulence intensity.

## Inhomogeneous, nonstationary turbulence and the dynamo problem - a successive approximation technique

#### 4.3.1 Outline of the successive approximation technique

Another method for dealing with inhomogeneous, nonstationary turbulence can be suggested which will be applicable to the hydromagnetic dynamo problem. This method involves treating the large scale variations of both the mean fields and the turbulence by means of a виссевы ve approximation technique. As an illustration, we shall apply the technique here to the kinematic dynamo problem. Later, in Chapter 6, we shall use the technique. in an investigation of the hydromagnetic dynamo problem.

We shall assume that the fluctuating fields y' and can be represented by Fourier-Stieltjes integrals of the type

$$u'_{i}(x,t) = \iint_{\mathbb{R}^{\omega}} U_{ij}(x,t;k,\omega) dZ_{j}(k,\omega) e^{i\int_{\mathbb{R}^{\infty}} x + \omega t} dx_{j}(x,t) dx_{j}(x,t;k,\omega) dX_{j}(k,\omega) e^{i\int_{\mathbb{R}^{\infty}} x + \omega t} dx_{j}(k,\omega) dX_{j}(k,\omega) dX_{j}(k,\omega) e^{i\int_{\mathbb{R}^{\infty}} x + \omega t} dx_{j}(k,\omega) dX_{j}($$

$$B'_{i}(x,t) = \iint_{\mathbb{R}^{\omega}} \beta_{ij}(x,t;k,\omega) \, d\gamma_{j}(k,\omega) \, e^{i \{k,x+\omega\tau\}}$$
 (4.7b)

where the tensors  $U_{ij}(x,t;k,\omega)$  and  $\beta_{ij}(x,t;k,\omega)$  vary with position and time on scales large compared with the correlation length and time of the turbulence.

The representations (4.7a,b) may now be substituted into the fluctuating induction equation (2.10) In the irst order smoothing approximation, (2.10) reduces to

W

(2.13). A successive-approximation solution to (2.13) may be sought in the form

$$d\underline{z}(\underline{k},\omega) = d\underline{z}^{(0)}(\underline{k},\omega) + d\underline{z}^{(1)}(\underline{k},\omega) + \dots \qquad (4.8a)$$

$$d\underline{Y}(\underline{k},\omega) = d\underline{Y}^{(0)}(\underline{k},\omega) + d\underline{Y}^{(1)}(\underline{k},\omega) + \dots \qquad (4.8b)$$

with the zero-order approximation being obtained by neglecting the large-scale variations of all quantities in (2.13). B' must of course satisfy the divergence condition (2.11). For simplicity, the flow will be assumed incompressible, so that u' satisfies (1.21).

At each stage in the successive approximation, the large scale variations of all fields (and their derivatives) must be ignored to ensure that dZ and dY, defined by (4.8), remain functions of k and  $\omega$  alone. Under this assumption, we may make use of equation (2.48)

$$dZ_{i}^{\alpha}(k,\omega) dZ_{j}(k,\omega) = \Phi_{ij}(k,\omega) \delta(k-k') \delta(\omega-\omega') dk dk' d\omega d\omega' \qquad (4,9)$$

to obtain the expansion

$$\phi_{ij}(\mathbf{k},\omega) = \phi_{ij}^{(oo)}(\mathbf{k},\omega) + \phi_{ij}^{(oi)}(\mathbf{k},\omega) + \phi_{ij}^{(oo)}(\mathbf{k},\omega) + \dots \quad (4,10)$$

where

d Z (m) \* (κ,ω) d Z (n)(κ,ω')

=  $\Phi_{ij}^{(mn)}(k,\omega) \delta(k-k') \delta(\omega-\omega') dk dk' d\omega d\omega'$ 

(4.11)

### + 4.3.2 Solution of the fluctuating induction equation

Writing out the first few terms of the successive approximation solution in detail, we have, from (1.21) and (2.11),

$$(k - U - dZ^{\omega}) = 0$$

$$(4.12a)$$

$$i \not k \cdot v \cdot d \not z^{(n)} \stackrel{?}{=} - v \cdot v \cdot d \not z^{(n-1)}$$
,  $n > 1$  (4.12b)

$$(4.13a)$$

$$i \not R \cdot \beta \cdot d \uparrow^{(n)} = - \nabla \cdot \beta \cdot d \uparrow^{(n-1)}$$
,  $n \ge 1$  (4.13b)

The simplest way of satisfying these equations is to assume

$$\nabla \cdot \mathbf{U} = \mathbf{0} \tag{4.14}$$

$$\nabla_{a}\beta_{a} = 0$$
 (4.15)

so that

$$(k, y) \cdot dz^{(n)} = 0$$
  $\forall n$   $(4.16)$ 

$$i \mathbf{k} \cdot \mathbf{\beta} \cdot \mathbf{d} \mathbf{Y}^{(n)} = \mathbf{0} \quad , \quad \forall \mathbf{n} \quad (4.17)$$

(4.14)-(4.17) are useful in the kinematic dynamo problem. However, in the hydromagnetic dynamo problem, the full equations (4.12)-(4.13) must be retained (see section 6.4.4).

The solution to (2.13) may now be written

$$\beta \cdot d\gamma^{(o)} = \frac{i(\underline{R} \cdot \overline{\underline{B}})}{i\omega + \eta R^2 + i(\underline{R} \cdot \overline{\underline{\omega}})} \quad \underline{\underline{U}} \cdot dZ^{(o)}$$
(4.18a)

$$\beta \cdot d\chi_{(i)} = \frac{1}{i\omega + i\omega_{3} + i(\vec{k} \cdot \vec{m})} \left\{ i(\vec{k} \cdot \vec{B}) \vec{n} \cdot d\vec{x}_{(i)} + \vec{B} \cdot \vec{\Delta} \vec{n} \cdot d\vec{x}_{(i)} \right\}$$

$$-\vec{n} \cdot \vec{\Delta} \vec{b} \cdot d\vec{\lambda}_{(i)} - \frac{3}{3} \cdot (\vec{b} \cdot d\vec{\lambda}_{(i)}) \cdot \vec{\Delta} \vec{n}$$

$$-\vec{n} \cdot \vec{\Delta} \vec{b} \cdot d\vec{\lambda}_{(i)} - \frac{3}{3} \cdot (\vec{b} \cdot d\vec{\lambda}_{(i)}) \cdot \vec{\Delta} \vec{n}$$

$$+ 3i \eta \vec{k} \cdot \vec{\Delta} \vec{b} \cdot d\vec{\lambda}_{(i)} - \frac{3}{3} \cdot (\vec{b} \cdot d\vec{\lambda}_{(i)}) \cdot \vec{\Delta} \vec{n}$$

$$+ 3i \eta \vec{k} \cdot \vec{\Delta} \vec{b} \cdot d\vec{\lambda}_{(i)} - \frac{3}{3} \cdot (\vec{b} \cdot d\vec{\lambda}_{(i)}) \cdot \vec{\Delta} \vec{n}$$

$$+ 3i \eta \vec{k} \cdot \vec{\Delta} \vec{b} \cdot d\vec{\lambda}_{(i)} - \frac{3}{3} \cdot (\vec{b} \cdot d\vec{\lambda}_{(i)}) \cdot \vec{\Delta} \vec{n}$$

$$+ 3i \eta \vec{k} \cdot \vec{\Delta} \vec{b} \cdot d\vec{\lambda}_{(i)} - \frac{3}{3} \cdot (\vec{b} \cdot d\vec{\lambda}_{(i)}) \cdot \vec{\Delta} \vec{n}$$

$$+ 3i \eta \vec{k} \cdot \vec{\Delta} \vec{b} \cdot d\vec{\lambda}_{(i)} - \frac{3}{3} \cdot (\vec{b} \cdot d\vec{\lambda}_{(i)}) \cdot \vec{\Delta} \vec{n}$$

$$\beta_{1} d \chi^{(m)} = \frac{1}{i\omega + \eta k^{2} + i(\underline{k}, \overline{\underline{u}})} \left\{ i(\underline{k}, \overline{\underline{B}}) \underline{v} \cdot d \underline{\chi}^{(m)} + \overline{\underline{B}} \cdot \underline{v} \underline{v} \cdot d \underline{\chi}^{(m-1)} - (\underline{v} \cdot d \underline{\chi}^{(m-1)}) \cdot \underline{v} \overline{\underline{u}} \right.$$

$$\left. - \underline{u} \cdot \underline{v} \underline{\beta}_{1} \cdot d \chi^{(m-1)} - \frac{\partial}{\partial t} (\underline{\beta}_{1} \cdot d \chi^{(m-1)}) \cdot \underline{v} \underline{u} \right.$$

$$\left. + 2i \eta \underline{k} \cdot \underline{v} \underline{\beta}_{2} \cdot d \chi^{(m)} + \eta \underline{v}^{2} \underline{\beta}_{1} \cdot d \chi^{(m-2)} \right\} (\lambda_{1}, 18c)$$

These expressions may now be used to obtain further expressions for  $\overline{\underline{u}' \times B'}$ .

# 4.3.3 Calculation of y'x B' in the first order smoothing approximation

The value of  $\frac{1}{2} \times \frac{B^T}{20}$  appropriate to the first order, smoothing approximation may now be obtained in the form of a series. Making use of (4.11),

$$\underline{\underline{u}' \times \underline{B}'_{o}} = \Re \iiint \underbrace{\underline{\underline{U}^{\bullet} \cdot d\underline{Z}^{\bullet}(\underline{k}, \omega) \times \underline{\beta} \cdot d\underline{Y}(\underline{k}'\omega')}_{\underline{\underline{k}} \cdot \underline{\underline{k}}', \underline{\underline{w}} \cdot \underline{\underline{w}}$$

$$+ \underset{k\omega}{\mathbb{Z}_{(i)}} + \underset{k\omega}{\mathbb{Z}_{(i)}} \times \left( k, \omega \right) \times$$

so that

+ 
$$U_{np} \frac{\partial \overline{u}_{e}}{\partial x_{n}} \cdot \frac{(\Phi_{mp}^{(\infty)})}{(i\omega + \eta k^{2} + i k \cdot \overline{u})} + \dots$$

$$-\left[\overline{u}_{n}\frac{\partial}{\partial x_{n}}+\frac{\partial}{\partial t}-2i\eta R_{n}\frac{\partial}{\partial x_{n}}\right]\frac{i(\underline{k},\overline{\underline{B}})U_{\underline{k}}}{(i\omega+\eta R^{2}+i\underline{k},\overline{\underline{\mu}})}$$

(4.19')

£ 2

4.3.4 Introduction of boundary conditions on the turbulent velocity - the possibility of a scalar velocity amplitude

The final step in the solution is to assume that  $U_{ij}$ ,  $\overline{B}$ , and  $\overline{u}$  are all functions of  $(\underline{x},t)$  in (4.19'). It will then be possible to satisfy any desired boundary conditions on  $\underline{u}'$  by adjusting the form of  $U_{ij}$ . It is of course clear that for the kinematic dynamo problem, the expansions (4.8a)—and (4.10) are unnecessary. In addition, the complex tensor  $U_{ij}$  may be replaced with a real scalar velocity amplificated function  $U(\underline{x},t)$ . Equation (4.19') then simplifies to

$$\begin{split} & \{\overline{u'} \times B'_{o}\}_{i} = \Re \left[ \varepsilon_{ijk} U(\underline{x}, t) \right\} \left( i U \overline{B}_{g} \iint_{\underline{u} \omega} \frac{\aleph_{q} \phi_{ik}(\underline{y}, \omega)}{(i\omega + \eta \aleph^{2} + i \underline{y}, \underline{u})} d\underline{x} d\omega \\ & + i U \overline{B}_{g} \frac{\partial \overline{u}_{k}}{\partial x_{n}} \iint_{\underline{u} \omega} \frac{\aleph_{q} \phi_{jn}}{(i\omega + \eta \aleph^{2} + i \underline{y}, \underline{u})} d\underline{x} d\omega \\ & + \overline{B}_{n} \frac{\partial U}{\partial x_{n}} \iint_{\underline{u} \omega} \frac{\phi_{jk} d\underline{x} d\omega}{(i\omega + \eta \aleph^{2} + i \underline{y}, \underline{u})} - U \frac{\partial \overline{B}_{k}}{\partial x_{n}} \iint_{\underline{u} \omega} \frac{\phi_{jn} d\underline{y} d\omega}{(i\omega + \eta \aleph^{2} + i \underline{y}, \underline{u})} \\ & - i \left(\overline{u}_{n} \frac{\partial}{\partial x_{n}} + \frac{\partial}{\partial t}\right) \left(U \overline{B}_{q}\right) \iint_{\underline{u} \omega} \frac{\aleph_{q} \phi_{jk}}{(i\omega + \eta \aleph^{2} + i \underline{y}, \underline{u})^{2}} d\underline{y} d\omega \\ & - U \overline{B}_{q} \left(\overline{u}_{n} \frac{\partial}{\partial x_{n}} + \frac{\partial}{\partial t}\right) \overline{u}_{r} \iint_{\underline{u} \omega} \frac{\aleph_{q} \aleph_{n} \Re_{jk}}{(i\omega + \eta \aleph^{2} + i \underline{y}, \underline{u})^{2}} d\underline{y} d\omega \\ & - 2 \eta \frac{\partial}{\partial x_{n}} \left(U \overline{B}_{q}\right) \iint_{\underline{u} \omega} \frac{\aleph_{q} \aleph_{n} \varphi_{jk}}{(i\omega + \eta \aleph^{2} + i \underline{y}, \underline{u})^{2}} d\underline{y} d\omega \\ & + 2 i \eta U \overline{B}_{q} \frac{\partial \overline{u}_{r}}{\partial x_{n}} \iint_{\underline{u} \omega} \frac{\aleph_{q} \aleph_{n} \aleph_{r} \phi_{jk}}{(i\omega + \eta \aleph^{2} + i \underline{y}, \underline{u})^{3}} d\underline{y} d\omega \\ & + 2 i \eta U \overline{B}_{q} \frac{\partial \overline{u}_{r}}{\partial x_{n}} \iint_{\underline{u} \omega} \frac{\aleph_{q} \aleph_{n} \aleph_{r} \varphi_{jk}}{(i\omega + \eta \aleph^{2} + i \underline{y}, \underline{u})^{3}} d\underline{y} d\omega \\ & + 2 i \eta U \overline{B}_{q} \frac{\partial \overline{u}_{r}}{\partial x_{n}} \iint_{\underline{u} \omega} \frac{\aleph_{q} \aleph_{n} \aleph_{r} \varphi_{jk}}{(i\omega + \eta \aleph^{2} + i \underline{y}, \underline{u})^{3}} d\underline{y} d\omega \\ & + 2 i \eta U \overline{B}_{q} \frac{\partial \overline{u}_{r}}{\partial x_{n}} \iint_{\underline{u} \omega} \frac{\aleph_{q} \aleph_{n} \aleph_{r} \varphi_{jk}}{(i\omega + \eta \aleph^{2} + i \underline{y}, \underline{u})^{3}} d\underline{y} d\omega \end{aligned}$$

However, the more complicated expressions in (4.19') will be required later on, when we consider the hydromagnetic dynamo problem (see section 6.4).

## 4.3.5 $u' \times B'_0$ for purely turbulent flow

When the mean velocity  $\widetilde{u}$  and its gradient can be neglected, (4.20) reduces to

$$\left\{ \underline{u}' \times \underline{B}'_{o} \right\}_{i} = \Re \left\{ \hat{e}_{ijk} \cup \left\{ i \cup \underline{B}_{g} \iint \frac{R_{g} \Phi_{jk}}{(i\omega + \eta R^{2})} dR d\omega \right. \right.$$

$$+ \left[ \underline{B}_{n} \frac{\partial U}{\partial x_{n}} \iint \frac{\Phi_{jk}}{(i\omega + \eta R^{2})} dR d\omega \right. - \left. U \frac{\partial \underline{B}_{k}}{\partial x_{n}} \iint \frac{\Phi_{jn}}{(i\omega + \eta R^{2})} dR d\omega \right.$$

$$- \left. i \frac{\partial}{\partial t} \left( U \underline{B}_{g} \right) \right\} \iint \frac{R_{g} \Phi_{jk}}{(i\omega + \eta R^{2})^{2}} dR d\omega$$

$$= 2 \eta \frac{\partial}{\partial x_{n}} \left( U \underline{B}_{g} \right) \iint \frac{R_{g} R_{n} \Phi_{jk}}{(i\omega + \eta R^{2})^{2}} dR d\omega + \sum_{k=1}^{n} \left\{ (A_{n} \otimes 1) \right\}$$

If the turbulence is locally PT-invariant - i.e. if u' can be represented in the form (4.7a), where dZ satisfies (4.9), and  $\phi_{ij}$  is the spectrum tensor of a PT-invariant process - then  $\phi_{ij}$  is real, and

$$\phi_{ij}(k,\omega) = \phi_{ji}(k,\omega)$$

by (3.22). In this case, all but one of the terms in (4.21) drop out, and the equation reduces to

$$\left\{ \underbrace{\mathbf{u}' \times \mathbf{B}'_{o}}_{i} \right\}_{i} = \Re \left\{ -U^{2} \underbrace{\mathbf{e}_{ijk}}_{ijk} \frac{\partial \overline{\mathbf{B}}_{k}}{\partial x_{n}} \iint_{\mathbf{R}\omega} \frac{\phi_{jn}}{(i\omega + \eta k^{2})} d\mathbf{k} d\omega \right\}$$

$$= -U^{2} \underbrace{\mathbf{e}_{ijk}}_{\partial x_{n}} \frac{\partial \overline{\mathbf{B}}_{k}}{\partial x_{n}} \iint_{\mathbf{R}\omega} \frac{\eta k^{2} \phi_{jn}}{(\omega^{2} + \eta^{2} k^{4})} d\mathbf{k} d\omega \qquad (4.22)$$

Equation (4.22) may be rewritten in the form,

$$\overline{\underline{\mathbf{u}'} \times \underline{\mathbf{B}'_{\bullet}}} = -\eta \left( \underbrace{\mathbf{A} \cdot \underline{\nabla}}_{\sim} \right) \times \overline{\underline{\mathbf{B}}}$$
(4,22')

where the tensor  $\Lambda_{ij}$  is defined as

$$\Lambda_{ij} = U^2 \iint \frac{\mathbf{k}^2 \phi_{ij}}{(\omega^2 + \eta^2 \mathbf{k}^4)} d\mathbf{k} d\omega \qquad (4.22")$$

Since  $\phi_{ij}$  is symmetric under interchange of indices, by the assumption of PT-invariance,  $\Lambda_{ij}$  must also be symmetric under interchange of indices. Furthermore, since the diagonal elements of  $\phi_{ij}$  must be separately nonnegative if Bochner's Theorem is to be satisfied (Batchelor, 1953, p. 27),  $\Lambda_{ij}$  must also have non-negative diagonal elements.

For the particular case in which  $\phi_{ij}$  is the spectrum tensor of a homogeneous, stationary, isotropic process, we have, from (3.7)

$$\Phi_{ij} = \frac{\mathcal{E}(\mathbf{k}, \omega)}{4\pi \mathbf{k}^4} \left\{ \mathbf{k}^2 \delta_{ij} - \mathbf{k}_i \mathbf{k}_j \right\}$$
(4.23)

where  $\varepsilon(k,\omega)$  is a non-negative function. Equations (4.22") and (4.22") then become

$$\widehat{\underline{u}' \times \underline{8}'_{o}} = -\eta \Lambda \underline{\nabla} \times \overline{\underline{B}} = \frac{1}{\sigma} \Lambda \overline{\underline{\flat}}$$

$$\Lambda_{ij} = \Lambda \delta_{ij}$$

$$(4.24')$$

$$\Lambda \equiv \frac{2}{3}U^2 \frac{1}{\eta^2 \lambda_c^3 \tau_c} \int_{-\infty}^{\infty} d\nu \int_{0}^{\infty} d\xi \frac{\xi^2 \mathcal{E}(\xi / \lambda_c, \nu / \tau_c)}{\xi^4 + (g\nu)^2} \qquad (4.24^{\circ})$$

where  $\lambda_{\rm C}$  and  $\tau_{\rm C}$  are to be interpreted as the correlation length and time, q is the parameter defined in (2.69), and  $\xi_{\rm C}$  and v are dimensionless. Substituting (4.24) into the modified Ohm's Law, (1.17), we obtain

$$\underline{\tilde{J}} = \sigma_{\underline{T}} \underline{\tilde{E}}$$
 (4.25)

where  $\sigma_{\mathbf{T}}$  is the turbulent conductivity, defined by

$$\sigma_{\mathbf{T}} = \sigma \left[ 1 + \Lambda \right]^{-1} \qquad (4.26)$$

Since A is non-negative, the only effect of locally isotropic turbulence of the type-considered here is to cause a decrease in the effective (turbulent) conductivity. This result is in agreement with the conclusion of Sweet (1950) that isotropic turbulence must increase the rate of diffusive decay of a nearly uniform magnetic field.

(See section 3.1.)

The results of the last paragraph make it clear that if a scalar velocity amplitude U is assumed, the introduction of inhomogeneity and nonstationarity in the turbulence does nothing to remove the need for asymmetry

in the local spectrum tensor,  $\phi_{ij}$ , if dynamo action is to be obtained.

## 4.3.6 Comparison of results with those of Chapter 3

The expression (4.26) for the turbulent conductivity can be compared with the expression obtained for the effective diffusivity,  $\eta_{eff}$ , in (3.91). Writing

$$\epsilon(k,\omega) = C \cdot \lambda_C^5 \tau_C \cdot k^4 \cdot \hat{h}(k,\omega)$$
 (4.27)

in agreement with (3.45) and (2.75), and rearranging terms in (4.24"), we obtain

$$(\eta_{eff}/\eta) - 1 = \frac{2}{3} C \left(\frac{U\lambda_{e}^{3}}{\eta}\right)^{3} \int_{0}^{\infty} dv \int_{0}^{\infty} \frac{\xi^{4} + (v_{g}^{2})^{2}}{\xi^{4} + (v_{g}^{2})^{2}} \hat{h}(\xi_{\lambda_{e}}, \frac{1}{2}, v_{e}^{2}) d\xi$$
 (4.28)

Equation (4.28) is identical to (3.91), apart from the fact that U is now a function of position and time. This agreement provides a useful check on the validity of the successive approximation technique used in deriving (4.26),

# 4.3.7 Introduction of helicity through large variations of the turbulent velocity

The correlation tensor used in the approach leading to equation (4.19) is of the form

$$R_{ij}(z,t;z+r,t+r)$$

$$= \iiint_{\mathbb{R}} U_{\mathcal{G}}^{*}(\underline{x},t;\underline{k},\omega) U_{jm}(\underline{x}+\underline{r},t+t;\underline{k}',\omega') d\underline{Z}_{k}^{*}(\underline{k},\omega) d\underline{Z}_{m}(\underline{k}',\omega') - e^{i\frac{1}{2}(\underline{k}'-\underline{k})\cdot\underline{x}} + (\omega^{2}-\omega)t + \underline{k}'\cdot\underline{r} + \omega'\tau$$

$$= \iint_{\mathbb{R}^{\omega}} U_{ik}^{\Phi}(x,t;k,\omega) U_{jm}(x+r,t+r;k,\omega) \phi_{km}(k,\omega) e^{i[k\cdot r+\omega\tau]} dkd\omega$$
(4.29)

If the assumption concerning a scalar velocity amplitude, used in deriving (4.20), is made, (4.29) reduces to

$$R_{ij}(x,t;x+r,t+r) = U(x,t)U(x+r,t+r)M_{ij}(r,t) \qquad (4.30)$$

where

$$m_{ij}(\mathbf{r},\tau) = \iint_{\mathbf{R}\omega} \Phi_{ij}(\mathbf{k},\omega) e^{i\{\mathbf{k}\cdot\mathbf{r}+\omega\tau\}} d\mathbf{k} d\omega$$
 (4.31)

When (4.30) is used, the spectrum tensor is of the form

$$\Phi_{ij}(\underline{k}, \omega) = U^2 \Phi_{ij}(\underline{k}, \omega) \qquad (4.32)$$

where the large-scale variations of U have been ignored in writing the arguments of  $\phi_{ij}$ . Since the symmetry properties of  $\phi_{ij}$  in (4.32) are just those of  $\phi_{ij}$ , it is not to be expected, in this approximation, that large-scale variations in U will materially affect the symmetry requirements on  $\phi_{ij}$  for dynamo action to occur.

When (4.29) is used, on the other hand, the spectrum tensor is of the form

$$\Phi_{ij}(k,\omega) = U_{ik}^{*}(k,\omega)U_{jm}(k,\omega) \phi_{km}(k,\omega) \qquad (4.33)$$

when the large-scale variations of  $U_{ij}$  are ignored. In (4.33) the symmetry properties of  $\Phi_{ij}$  depend on both those of  $\phi_{lm}$  and those of  $U_{il}U_{jm}$ , so that  $\Phi_{ij}$  may have an asymmetric component even when  $\Phi_{ij}$  does not. Helicity may therefore arise from either small-scale or large-scale variations of  $u^i$ . (See section 6.4.6 for further discussion of this point.)

# 4.3.8 Comparison of the successive approximation technique with Rädler's approach

We may now identify the principal difference between the successive approximation technique suggested in this thesis and the approach of Rädler (1972) and Krause and Rädler (1971), described in section 4.2.3.

Krause and Rädler obtain helicity which is related to the large-scale variations of use by assuming Rij to have the specific form (4.5). They then choose the coefficients  $m_{ij}^{(0)}$ ,  $m_{ij}^{(11)}$ , and  $m_{ij}^{(12)}$  to represent correlation tensors of stationary, homogeneous, isotropic processes, with the form (3.48), so that all the helicity effects arise from the large-scale variations. In the successive approximation technique used here, we introduce the effects of large-scale variations through the tensor

without making any a priori assumptions about the form of  $R_{ij}$ . The successive approximation technique allows  $\overline{u}$   $\overline{x}$   $\overline{B}$  to be derived from the hydromagnetic dynamo equations in a much more general form than is possible with the method of Krause and Rädler. This topic will be studied in more detail in section 6.4.

#### 4.4 , Summary of Chapter 4

This chapter is concerned with nonstationary, inhomogeneous turbulence and its treatment within the framework of mean field electrodynamics.

A successive approximation technique is proposed, and is applied to the kinematic dynamo problem. Some of the results obtained are compared with expressions derived in Chapter 3.

The possibility of introducing helicity through large-scale variations of the turbulent velocity distribution is discussed, and the successive approximation technique is compared with the approach suggested by Rädler (1972).

#### 5. TEMPORAL BEHAVIOUR OF ASTROPHYSICAL MAGNETIC FIELDS

#### 5.1 Introduction

#### 5,1.1 Temporal variations of astrophysical magnetic fields

As was noted in section 1.1.2, many astrophysical magnetic fields vary in a complicated way with time.

These variations are summarized for a number of fields in Tables 13, 14, and 15.

variations listed in Tables 14 and 15 can be explained in terms of stellar or planetary rotation. If the magnetic field of a rotating body is not symmetric about the axis of rotation, the field must vary periodically when viewed from the Earth. The simplest possible case of this type is that in which the magnetic field is predominantly dipolar, and the magnetic dipole axis is inclined to the axis of rotation. This oblique rotator model is clearly applicable to planetary fields like those of the Earth and Jupiter. It has also been applied with considerable success to stellar magnetic fields (see, for example, Mestel, 1967, 1971, 1972; Preston, 1967a,b, 1971a,b; Landstreet, 1970; Mestel and Takhar, 1972).

The oblique rotator model does not, however, provide a unique explanation for the periodic variations of stellar magnetic fields. An alternative model has been proposed by

Krause (1971, 1972b,c), in which the stellar field is assumed to be nondipolar, and symmetric under reflection in the equatorial plane. This equator-symmetric rotator model takes into account the fact that in some dynamo models including an a-effect (Stix, 1971; Roberts and Stix, 1972; Krause, 1972c; Moffatt, 1973) non-axisymmetric mean fields are more easily excited than axisymmetric mean fields.

TABLE 13 - GEOMAGNETIC FIELD	LD OF INTERNAL ORIGIN; Time scale	TEMPOR
17 Pe Or Variación	ars)	Comments
SECULAR VARIATION OF NONDIPOLE FIELD		
"High frequency" oscillations [1]	, < 100	,
"Medium frequency," oscillations [2]	100-5000	compileated spectrum of Variations
"Westward drift" [3]	~ 2000	
CHANGES IN ENERGY DISTRIBUTION		ast 120v the net ener
Dipole-nondipole energy transfer [4]	2000	has been v
Changes in transfer rate [5]	٦ ١٥٥	le-nondipole (bercent of
Changes in total energy [5]	103-104	over the last 1500
		average loss rate has been much higher ( $\sim 0.138/y$ ), [5]
SECULAR VARIATION OF DIPOLE FIELD		
Dipole "wobble" (eastward drift) [6]	1200-1800	Various estimates
'Field strength oscillation [7]	0006 ~	ental fre
POLARITY REVERSALS		
Change in field direction [8,9,10]	1000-4000	(8): intensity time scale ≥ 10x direction time scale
Change in intensity [8,9]	3000-10,000	scales t
Interval between reversals [11]	0.03-30 x 106	
Long-term periodicity(?) [12]	75 x 10 <sup>6</sup>	ation L qalactic
	250 x 10 <sup>6</sup>	1
	700 × 10 <sup>6</sup>	

#### FOOTNOTES TO TABLE 13

- [1] Braginskii (1964d, 1970a,b, 1971, 1972); Currie (1968); Acheson & Hide (1973).
- [2] Braginskii (1964b, 1967b, 1970b, 1971, 1972); Hide (1966a); Rikitake (1966b); Malkus (1967b, 1971a); Stewartson (1967, 1971); Gans (1971); Hide & Stewartson (1972); Soward (1972a); Roberts & Soward (1972); Acheson & Hide (1973),
- [3] For early references see Jacobs (1963, pp. 70-76), Rikitake (1966a, p. 83 and p. 109). See also Pudovkin & Valuyeva (1967, 1972); Yukutake (1968a,b, 1972); James (1968, 1970, 1971); Honkura & Rikitake (1972); Roberts & Soward (1972); Moffatt (1973).
- [4] McDonald & Gunst (1968); Verosub & Cox (1971); Cox (1972); Jin (1973).
- [5] Verosub & Cox (1971),.
- [6] Kawai & Hirooka (1967); Kovacheva (1969); Márton (1970); Cox (1972). Šee also Jacobs (1971c); Pudovkin & Valuyeva (1972).
- [7] Smith (1967); Braginskii (1970b, 1971, 1972); Cox (1972).
- [8] Dunn, et al. (1971).
- [9] Kent, et al. (1973).
- [10] Harrison & Somayajulu (1966); Bullard (1968); Creer & Ispir (1970); Cox (1972).
- [11] Bullard (1968); Heirtzler, et al. (1968); Helsley & Steiner (1969); McElhinny (1971); Vogt, et al. (1972); Helsley (1972a); Blakely & Cox (1972b); Stewart & Irving (1973); Reid (1973).
- [12] Crain, et al. (1969); Crain & Crain (1970); Ulrych (1972).

Variations associated with velocity [10] solar cycle period is "lly, individual "cycles" of activity overlap. been definitely The length of each cycle is 13y [9] Active photospheric field rotates question as to the dipole reversals [] Although the generally accepted 1°/day faster than solar atmosequator is  $\sim 27d$  , while that, at the poles is  $\sim 34d$  [4]. Atmospheric rotation period at solar atmosphere Magnetic cycle period ~22y rotates with atmosphere phere [4], while sector Comments SOLAR MAGNETIC FIELDS has not There is some regularity of Periodicity established fields in TEMPORAL VARIATIONS OF scale 80-100y 30g 25d 27d 10-15m 20-24h 80٧ ع حرار ځ Time Reversal of characteristic polarity 8 FILAMENTARY STRUCTURE VARIATIONS Reversal of axial dipole field Latitude migration of zones of maximum activity [6] Sector structure activity [12] Equatorial active regions [4] 2 of variation Supergranular structure Giant cell structure [3] 80-YEAR CYCLE VARIATIONS Granular structure [1] SOLAR CYCLE VARJATIONS Sunspot activity [11] DIFFERENTIAL ROTATION TABLE Sector structure [5] of spot zones [7] Type

#### FOOTNOTES TO TABLE 14

- [1] Parker (1970b); Mehltretter (1971); Harvey (1971); Weiss (1971a, 1972).
- [2] Parker (1970b); Howard, (1971a,b); Weiss (1971a, 1972).
- [3] 'Howard (1971a,b); Weiss (1971a, 1972).
- [4] Dupree & Henze (1972).
- [5] Severny, et al. (1970); Wilcox & Gonzales (1971); Svalgaard (1973).
- [6] Parker (1970b); Stenflo (1972).
- [7] Stenflo (1972),
- [8] Severny (1971, 1972); Stenflo (1972). ,
- [9] de Jager (1959); see also 'Gilliland (1967, p. 159).
- [10] \*Stenflo (1972).
- [11] Kopecky (1970).
- [12] Patterson (1973).

TABLE 15 -	TEMPORAL VARI	VARIATIONS OF OTHER ASTROPHYSICAL MAGNETIC FIELDS
Location of field	Time scale of variation	Nature and explanation of variation
Jupiter	9h 55m	Periodic variation. Explained in terms of the oblique rotator model, with dipole axis inclined 11° to axis of rotation. [1]
Magnetic stars	1.7-2500 d typicallu	All vary, and many show periodic variation. About 50% exhibit polarity reversals. [2]
	5-9 2	can be explained in terms of stel the oblique rotator model [3], the
α. <del>1</del> 4.5	, <u>1</u>	inationary of inagnetic stars have their dipole axis inclined ~80° to rotation axis, though some have inclinations ~0° [4]. Alternatively, the equator symmetric rotator model [5] may apply.
	•	tuations and certain other fe ciated with wave processes [6
Magnetic white dwarfs	(1.34d)-	Only one of the four magnetic white dwarfs observed to date exhibits periodic variation [7]. Variation is explained in terms of the oblique rotator model.
Pulsars	0.03-3.7 s most cases, 0.5-1 s	All vary in a rapid periodic fashion. Periodic variations are explained in terms of the oblique rotaton model [8].
		Glitches (sudden jumps in frequency) are also observed, with "lifetimes" $4-7$ d (Crab pulsar) and $1.2$ y (Vela). Several explanations have been proposed [9].

#### FOOTNOTES TO TABLE 15

- [1] Warwick (1967); Hide (1971a); \$chatten & Ness (1971).
- [2] Ledoux & Renson (1966); Preston (1967a,b, 1971b).
- [3] Mestel (1967, 1971, 1972); Mestel & Takhar (1972); Moffatt (1973).
- [4] Preston (1967b, 1971b); Landstreet (1970).
- [5] Krause (1971).
- [6] Severny (1971).
- [7] Landstreet & Angel (1971).
- [8] Ruderman (1972).
- [9] Ruderman (1972).

#### 5.1.2 Polarity reversals

As may be seen from Tables 13-15, the magnetic fields of the Earth, the Sun, and some magnetic stars all exhibit polarity reversals. In the case of magnetic stars, these reversals are readily explained in terms of either the oblique rotator model or the equator-symmetric rotator model. However, these models cannot be applied to the magnetic fields of the Earth and the Sun.

Reversals of the solar and geomagnetic fields differ considerably in character. The background solar field appears to reverse in a quasi-periodic fashion related to the 22-year magnetic solar cycle. The changeover from one polarity to the other is not always smooth for example, the field is sometimes quadrupolar rather than dipolar during a reversal. [Recent observations (Stenflo, 1972) suggest that irregularities of this nature are more common and of longer duration than would be expected on the simple "periodic reversal" model. 1. The geodynamo, on the other hand, reverses in a highly irregular fashion - so irregular that geomagnetic reversals are often modelled as a nonstationary random process (Cox, 1968, 1969, 1970, 1971; Surdin, 1968; Nagata, 1969 Crain and Crain, 1970; Crain, 1971; Naidu, 1971; Kono, 1972; Blakely and Cox, 1972a; Phillips, et al., 1972).

The frequency of geomagnetic reversals is plotted as a function of time in Figure 22. The smooth, dashed curve has been obtained from the work of McElhinny (1971), who plots the percentage of polarity measurements that are "mixed" (i.e. both "normal" and "reversed" polarities in the same rock unit) as a function of time. As shown in Figure 22, the most recent portions of McElhinny's curve can be fitted quite well to detailed reversal frequency measurements if the curve is considered as a logarithmic plot of frequency vs. time. The curve is clearly a very crude approximation, but it serves to illustrate the non-stationary character of the reversal process.

The detailed results of Heirtzler, et al. (1968), and of Helsley and Steiner (1969), plotted on the right in Figure 22, indicate that changes in the reversal frequency are likely to be disgontinuous on the time scale shown. There appear to be sudden jumps in the frequency of reversals at 50 m.y.b.p. (million years before present), and at 72 m.y.b.p.

Other results, not plotted in Figure 22, indicate that the nonstationary character of the reversal process has persisted over much longer times than those indicated. Reid (1972) and Stewart and Irving (1973) have found that reversal rates in the Precambrian varied in much the same way as those plotted for the Phanerozoic (i.e. the entire

period shown in Figure 22). Reid (1972) reports a variation of the reversal rate from 0.4/m.y. to 1.1/m.y. over a 60 m.y. interval at roughly 1800 m.y.b.p. Stewart and Irving (1973) report reversal frequencies less than 0.1/m.y. at 990 m.y.b.p., and greater than 1/m.y. at 790 m.y.b.p.

Since Figure 22 was plotted, two papers have been discovered which indicate that the peak shown in the Jurassic and Triassic is somewhat too low. Vogt, Einwich, and Johnson (1972) report 41 reversals between 150 and 135 m.y.b.p., giving an average reversal rate of 2.7/m.y. in the late Jurassic. Helsley (1972a) reports that at least 23 reversals occurred during the Triassic, giving an average reversal rate > 0.7/m.y. between 225 and 190 m.y.b.p.

Detailed study of more recent palaeomagnetic data indicates that the time between reversals varies widely - from  $\sqrt{3} \times 10^4$  years to as long as 3 x  $10^7$  years (Bullard, 1968; Heirtzler, et al., 1968; Blakely and Cox, 1972b; Moffatt, 1973). During the last few million years, reversals have occurred at intervals of roughly 2-3 x  $10^5$  years.

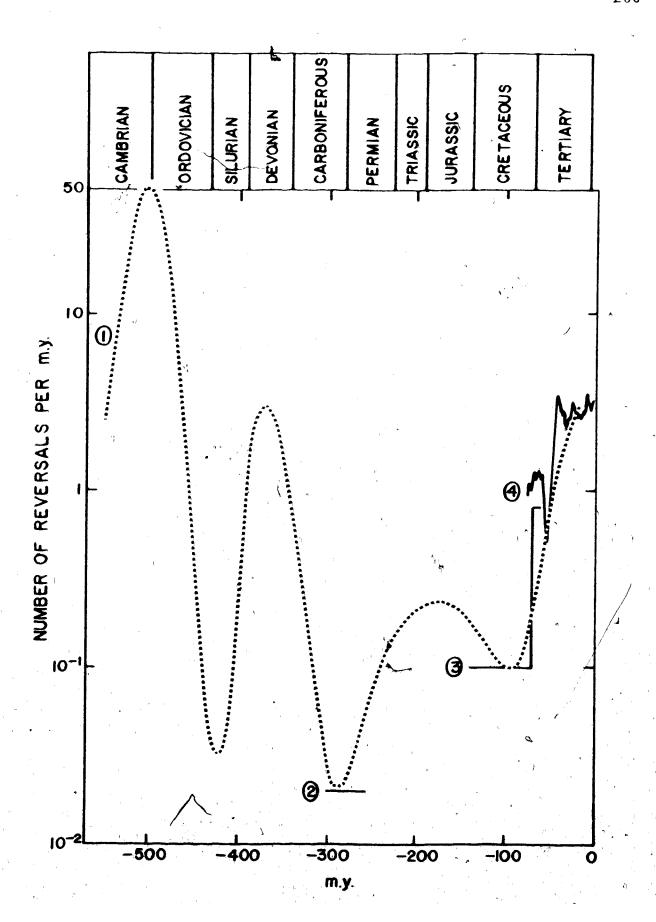
The behaviour of the geomagnetic field during a polarity reversal has received considerable attention in recent years. Dunn, et al. (1971), in a study of a reversal at 15 m.y.b.p., find that the field intensity decreased by a factor of 10 before any change in field direction occurred, and did not return to normal until after the directional change was completed. The directional

Figure 22. Reversal rate of the geomagnetic field as a function of time.

- (1) Curve derived from the work of McElhinny (1971). McElhinny's plot of percentage of "mixed" polarity measurements vs. time is interpreted, to a crude approximation, as a logarithmic plot of reversal rate vs. time.
- (2) Kiaman Magnetic Interval approximately one reversal in 50 m.y.
- (3) Results of Helsley and Steiner (1969).
- (4) Results of Heirtzler, et al. (1968), obtained from sea-floor anomaly patterns.

  (Plot shows a 10 m.y. average taken every 1 m.y.)

As pointed out on p. 278, the work of Vogt, Einwich, and Johnson (1972) and of Helsley (1972a) indicates that the peak shown in the Jurassic and Triassic is perhaps an order of magnitude too low.



change is estimated to have taken 1-4 x 10<sup>3</sup> years, while the intensity change is estimated to have taken 10<sup>4</sup> years. Similarly, Watson and Larson (1972) suggest that "major dipole instabilities" (e.g. reduction of the dipole intensity by 80%) occur prior to reversals. On the other hand, Kent, et al. (1973), in a detailed study of two reversals, find that the change in field direction took the same time as the change in field intensity in each case (3800 y for one reversal, and 3500 y for the other).

Recent work suggests that "...the field during a [polarity] transition is not a geocentric dipole tightly coupled to the mantle" (Hillhouse, et al., 1972). Large variations in magnetic inclination and declination, as well as a decrease in field intensity, occur during a reversal (Kent, et al., 1973).

## 5.1.3 The oscillation spectrum of the geomagnetic field

As may be seen from Table 13, the geomagnetic field varies with time on many scales besides that of polarity reversals. It is frequently helpful to consider an bscillation spectrum of geomagnetic variations (Cox and Doell, 1964; Jacobs, 1970b; Braginskii, 1970b, 1971, 1972). Bnaginskii (1970b, 1971, 1972) divides this "spectrum" into three major categories:

- a. the fundamental frequency, characteristic of dipole field strength oscillations, with period  $^{9}$  x  $10^{3}$  years (see footnote [7], Table 13);
- b. medium frequency oscillations, with periods in the range 100-5000 years (typically ~10<sup>3</sup> years, with peaks in the spectrum close to the period of westward drift of the nondipole field);
- C. high frequency oscillations, with periods < 100 years (see footnote [1], Table 13).

The theoretical treatment of these oscillations is highly complicated. Braginskii (1970b, 1971, 1972) suggests that the existence of a fundamental frequency is a consequence of the two-stage nature of the dynamo process, in which a weak poloidal field leads to the generation of a strong toroidal field, and the toroidal field is responsible for the regeneration of the poloidal field. Medium frequency oscillations are associated with the so-called "MAC-waves" (i.e. Magnetic-Archimedean-Coriolis waves) in the Earth's fluid core (see the references in footnote [2], Table 13). Finally, high frequency oscillations are linked to torsional magnetohydrodynamic oscillations and turbulent pulsations in the core (see the references in footnote [1]. Table 13).

#### 5.2 Reversals and the mean field kinematic dynamo problem

#### 5.2.1 Dynamo models for solar and geomagnetic reversals

In the last few years, a number of reasonably successful dynamo models have been developed to account for the temporal variation of the solar magnetic field (Gilman, 1968, 1969a,b; Leighton, 1969; Steenbeck and Krause, 1969a; Parker, 1970h; Deinzer and Stix, 1971; Stix, 1971; Roberts and Stix, 1972; Stix, 1972; Lerche and Parker, 1972). However, the problem of the long-term temporal variation of the geomagnetic field has proved much less tractable. Some progress has been made by Parker (1969b) and by Levy (1972a,b,c), who have carried out kinematic investigations of geomagnetic reversals. The model suggested by Levy (1972a,b,c) is of particular interest because of its relative mathematical simplicity. However, like most kinematic models, it suffers from the disadvantage that its velocity distribution may well be a very poor representation of the distribution actually present in the Earth's fluid core.

#### 5.2.2 The mean field induction equation

Let us first consider the mean field kinematic dynamo problem as it applies to the Earth. It is convenient to separate the magnetic field into its toroidal and poloidal parts

$$\mathbf{B} = \operatorname{curl} \mathbf{T_r} + \operatorname{curl} \operatorname{curl} \mathbf{S_r}$$
 (5.1)

where  $\underline{r}$  is the position vector, and  $T(\underline{r},t)$  and  $S(\underline{r},t)$  are scalar fields (see the footnote to Table 9, p. 33, and P.H. Roberts, 1967a, pp. 80-82).

Using spherical polar coordinates  $[r,\theta,\phi]$ , and assuming that T and S are functions only of  $[r,\theta,t]$ , we may rewrite (5.1) in the form

$$\overline{B} = -\frac{\partial T}{\partial \theta} \underline{1}_{\phi} - \text{curl} \left\{ \frac{\partial S}{\partial \theta} \underline{1}_{\phi} \right\}$$

$$\equiv B \underline{1}_{\phi} + \text{curl} \left\{ A \underline{1}_{\phi} \right\} \tag{5.2}$$

where  $\frac{1}{2\phi}$  is the unit vector in the azimuthal direction. We shall also assume that the mean field induction equation has the form

$$\left\{\frac{\partial}{\partial t} - \eta \nabla^2\right\} \overline{B} = \text{curl}\left\{\overline{u} \times \overline{B} + \alpha \overline{B}\right\} \qquad (5.3)$$

where an  $\alpha$ -effect term  $\alpha \overline{B}$  has been substituted for the fluctuating e.m.f.  $\overline{u}' \times \overline{B}''$  (see the discussion in section 1.4.8).

5.2.3 The 
$$\alpha^2$$
 dynamo

5.2.3 The  $\alpha^2$  dynamo . If, in (5.3), we make the further assumptions that  $\overline{\underline{u}}$  and  $\alpha$  are functions only of  $[r, \theta, t]$  , and that

$$\overline{u} = u_{10}^{1} + curl\{a_{10}^{1}\}$$
(5.4)

, equations (5.2), (5.3), and (5.4) can be combined to give

$$\left\{\frac{\partial}{\partial t} - \eta \Delta_i\right\} A = \tag{5.5a}$$

= 
$$\alpha B + \frac{1}{r^2 \sin \theta} \left\{ \frac{\partial}{\partial r} (ra) \frac{\partial}{\partial \theta} (A \sin \theta) + \frac{\partial}{\partial \theta} (a \sin \theta) \frac{\partial}{\partial r} (rA) \right\}_{(p)}$$

$$\begin{cases}
\frac{\partial}{\partial t} - \eta \Delta_{i} \right\} B = \frac{1}{r^{2}} \frac{\partial}{\partial \theta} \left\{ \alpha \frac{\partial}{\partial \theta} (A \sin \theta) \right\}$$

$$= -\frac{1}{r} \frac{\partial}{\partial r} \left\{ \alpha \frac{\partial}{\partial r} (rA) \right\} - \frac{1}{r^{2}} \frac{\partial}{\partial \theta} \left\{ \alpha \frac{\partial}{\partial \theta} (A \sin \theta) \right\}$$

$$+ \left\{ \frac{1}{r^{2}} \frac{\partial}{\partial \theta} - \frac{\cot \theta}{r} \frac{\partial}{\partial r} \right\} (aB - uA)$$

$$+ \frac{1}{r} \left\{ \frac{\partial u}{\partial r} \frac{\partial A}{\partial \theta} - \frac{\partial u}{\partial \theta} \frac{\partial A}{\partial r} - \frac{\partial B}{\partial r} \frac{\partial a}{\partial \theta} + \frac{\partial B}{\partial \theta} \frac{\partial a}{\partial r} \right\}$$

where

$$\Delta_1 \equiv \left\{ \text{div.grad} - \frac{1}{r^2 \sin^2 \theta} \right\} = \left\{ \nabla^2 - \frac{1}{r^2 \sin^2 \theta} \right\}$$
 (5.6)

If  $\overline{u} = 0$ , equations (5.5a,b) reduce to

$$\left\{\frac{\partial}{\partial t} - \eta \Delta_{i}\right\} A = \alpha B \tag{5.7a}$$

$$\left\{\frac{\partial}{\partial t} - \eta \Delta_i\right\} B = -\frac{1}{r} \left\{\alpha \frac{\partial}{\partial r} (rA)\right\} - \frac{1}{r^2} \frac{\partial}{\partial \theta} \left\{\alpha \frac{\partial}{\partial \theta} (A \sin \theta)\right\}$$
(5.7b)

giving the equations of the so-called  $\alpha^2$  dynamo (Krause and Steenbeck, 1967; P.H. Roberts, 1971a; Soward, 1972a; Roberts and Stîx, 1972).

Equation (5.7a) represents the generation of poloidal field (represented by A) from toroidal field (represented by B), while equation (5.7b) represents the generation of toroidal field from poloidal. The name " $\alpha^2$  dynamo" derives from the fact that in the  $\omega$ -stage process described by equations (5.7a,b) the operation of each stage depends on the fact that  $\alpha \neq 0$ .

### 5.2.4 The waw dynamo

If, in equation (5.4) a=0, and if the terms involving  $\alpha$  in equation (5.5b) can be ignored in comparison with the terms involving u, equations (5.5a,b) reduce

$$\left\{\frac{\partial}{\partial t} - \eta \Delta_{i}\right\} A = \alpha B \tag{5.8a}$$

$$\left\{\frac{\partial}{\partial t} - \eta \Delta_{i}\right\} B = \frac{\cot \theta}{r} \frac{\partial}{\partial r} (uA) - \frac{1}{r^{2}} \frac{\partial}{\partial \theta} (uA)$$

$$+ \frac{1}{r} \left\{\frac{\partial u}{\partial r} \frac{\partial A}{\partial \theta} - \frac{\partial u}{\partial \theta} \frac{\partial A}{\partial r}\right\}$$
(5.8b)

giving the equations of the so-called aw' dynamo (Steenbeck and Krause, 1966; Soward, 1972a). The dynamo equations (5.8a,b), and generalizations of them, have been

studied by many authors, including Parker (1955, 1970a,c, 1971c), Braginskii (1964a,b,c), Krause and Steenbeck (1965), Steenbeck and Krause (1967, 1969a,b), Krause and Rädler (1971), and Roberts and Stix (1972).

u is often assumed to have the form of a "modified" rigid body rotation

 $u = \omega r \sin \theta$ 

where  $\omega = \omega(r, \theta)$ . Under this assumption, equations (5.8a,b) reduce to

$$\left\{\frac{\partial}{\partial t} - \eta \Delta_{i}\right\} A = \alpha B \qquad (5.8a')$$

$$\left\{\frac{\partial}{\partial t} - \eta \Delta_{i}\right\} B = \frac{1}{4} \cdot \left\{ \nabla \omega \times \nabla (Arsin\theta) \right\}$$
 (5.8b')

If, in addition,  $\omega$  is independent of  $^{\circ}\theta$  , the equations reduce further to

$$\left\{\frac{\partial}{\partial t} - \eta \Delta_{i}\right\} A = \alpha B \qquad (5.8a'')$$

$$\left\{\frac{\partial}{\partial t} - \eta \Delta_{i}\right\} B = \omega' \frac{\partial}{\partial \theta} \left(A \sin \theta\right) \tag{5.8b"}$$

where  $\omega' \equiv \omega'(r) = d\omega/dr$ .

The reason for the name " $\alpha\omega$ ' dynamo" is clear from equations (5.8a") and (5.8b"). In the two-stage process described by the equations, the first stage (generation of poloidal field from toroidal) operates only if  $\alpha \neq 0$ , while the second stage (generation of toroidal field from

poloidal) operates only if  $\omega' \neq 0$ 

### 5.2.5 The Levy model for geomagnetic reversals

The model studied by Levy (1972a,b,c) is of the  $\alpha\omega'$  type, with

$$\mathbf{u} = \{\omega r \sin \theta\} \mathbf{H}(r_{e} - r) \tag{5.9}$$

where H(x) is the Heaviside unit function, equal to unity for x > 0 and zero for x < 0. Levy (1972a,b), like Parker (1969b), represents  $\alpha$  as a pair of axisymmetric  $\delta$ -function rings, symmetrically placed above and below the equatorial plane. This model can be taken to represent two rings of cells of cyclonic convection.

Levy (1972b) studies field reversals by using a sporadic model in which "bursts" of shear (i.e. δ-functions in time) of the form (5.9) alternate with bursts of cyclonic convection at various latitudes. Two kinematic reversal schemes are discussed. In the first, it is shown that "...a strong burst of cyclonic convection at high latitudes will reverse the dipole field", while in the second it is shown that "...if the geomagnetic dynamo has a region of reverse toroidal flux in the core, then a strong burst of cyclonic convection in that region will also reverse the dipole field" (Levy, 1972c).

Levy (1972c) examines the second kinematic reversal

represents two or three pairs of rings of cyclonic convection, and shows that stationary solutions of the dynamo equations exist in which extensive regions of reverse toroidal flux occur. It is estimated that in these solutions, a fluctuation of 20-30% in the distribution of cells of cyclonic convection can lead to a polarity reversal.

## 5.3 The $\alpha^2(r)$ dynamo in a spherical shell

## 5.3.1 The mean field induction equation and boundary conditions

In order to test the possibility of an  $\alpha^2$  dynamo model for geomagnetic reversals, let us consider equations (5.6a,b) in the case when  $\alpha$  depends only on r. Under this assumption, the equations reduce to

$$\left\{\frac{\partial}{\partial t} - \eta \nabla^2\right\} S = \alpha T$$

$$\left\{\frac{\partial}{\partial t} - \eta \nabla^2\right\} T = -\alpha \nabla^2 S - \frac{\alpha'}{r} \frac{\partial}{\partial r} (rS)$$
(5.10a)
(5.10b)

where T and S are the scalar fields defined in (5.1) and (5.2), and  $\alpha' = \alpha'(r) = d\alpha/dr$ . Equations (5.10a,b) will be assumed valid in the spherical shell  $r \leqslant r \leqslant r_0$ , bounded by a nonconducting medium in  $r > r_0$ . In r < r the mean velocity  $\overline{u}$  may be nonzero, and equations (5.8a,b) may hold in this region in place of equations (5.10a,b).

The boundary conditions to be satisfied by the mean magnetic field are

$$\langle S \rangle = \langle T \rangle = \langle \partial S / \partial r \rangle = 0 , r = r_0$$

$$\langle S \rangle = \langle T \rangle = \langle \partial S / \partial r \rangle = \langle \partial T / \partial r \rangle = 0 , r = r_0^{*}$$

$$\langle S \rangle = \langle T \rangle = \langle \partial S / \partial r \rangle = \langle \partial T / \partial r \rangle = 0 , r = r_0^{*}$$

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$$\langle S \rangle = \langle T \rangle = \langle \partial S / \partial r \rangle = 0 , r = r_0$$

$$\langle S \rangle = \langle T \rangle = \langle \partial S / \partial r \rangle = 0 , r = r_0$$

$$\langle S \rangle = \langle T \rangle = \langle D \rangle = \langle D \rangle = 0$$

$$\langle S \rangle = \langle T \rangle = \langle D \rangle = \langle D \rangle = \langle D \rangle = 0$$

$$\langle S \rangle = \langle T \rangle = \langle D \rangle$$

$$\begin{cases} S & \text{nonsingular as } r \to 0 \\ T \to 0 & \text{as } r \to 0 \end{cases}$$
 (5.14)

The velocity field will be assumed to satisfy the boundary conditions

$$\alpha = 0$$
,  $r \ge r_0$  (5.15a)  
 $\langle \alpha \rangle = \langle \alpha' \rangle = \langle \overline{\mu} \rangle = \langle \overline{\mu} \rangle = 0$ ,  $r = r^{m}$  (5.15b)

## 5.3.2 Separable solutions - the radial equations

In the region  $r \le r \le r$  the equations (5.10a,b) have separable solutions of the form

$$S = \sum_{n=1}^{\infty} S_n^*(r) P_n(\cos \theta) e^{-\sigma_n t}$$
 (5.16a)

$$T = \sum_{n=1}^{\infty} T_n(r) P_n(\cos \theta) e^{-\sigma_n t}$$
 (5.16b)

where the padial functions  $S_{n}(r)$  and  $T_{n}(r)$  satisfy the equations

$$\left\{\sigma_{n} - \eta \left[\frac{d^{2}}{dr^{2}} - \frac{n(n+1)}{r^{2}}\right]\right\} (rS_{n}) = \alpha \cdot (rT_{n}) \qquad (5.17a)$$

$$\left\{\sigma_{n} - \eta \left[\frac{d^{2}}{dr^{2}} - \frac{n(n+1)}{r^{2}}\right]\right\} (rT_{n}) = -\alpha \left[\frac{d^{2}}{dr^{2}} - \frac{n(n+1)}{r^{2}}\right] (rS_{n}) - \alpha' \frac{d}{dr} (rS_{n})$$

and the  $P_n(\cos\theta)$  are Legendre polynomials in  $\cos\theta$  . In the region  $r>r_0$  the conditions (5.13) lead

to solutions of the form

$$\hat{S}_{n}(r) = C_{n} r^{-(n+1)}$$
 (5.18a)

$$\hat{T}_{n}(r) = 0 \tag{5.18b}$$

#### 5.3.3 The radial equations in nondimensional form

In order to reduce the equations (5.17a,b) to a nondimensional form, we shall define

$$z = 1 - (\gamma/r_o) \tag{5.19}$$

$$\chi \equiv (rS_n)/r_oS_n(r_o)$$
 (5.20a)

$$\Upsilon \equiv (rT_n)/S_n(r_0) \tag{5.20b}$$

$$\gamma = \sigma_n r_0^2 / \eta \tag{5.21}$$

$$R = r_0 \alpha(r) / \eta \qquad (5.22)$$

We shall also use the notation

$$N \equiv {}^{\prime}n(n+1) \tag{5.23}$$

Substituting (5.19)-(5.23) into equations (5.17a,b), we obtain the nondimensional equations

$$\left\{ \frac{d^2}{dz^2} - \left[ \frac{1}{2} \right] \right\} X = -RY \qquad (5.24a)$$

$$\left\{\frac{d^2}{dz^2} - \left(\frac{d^2}{dz^2} - \frac{N}{(1-z)^2}\right)X + \frac{dR}{dz}\frac{dX}{dz}\right\}$$

$$= R\left\{\frac{d^2}{dz^2} - \frac{N}{(1-z)^2}\right\}X + \frac{dR}{dz}\frac{dX}{dz}$$

These equations are valid in the interval  $0 \le z \le z^*$ , where

$$z^* = 1 - (r^*/r_0)$$
 (5.25)

#### 5.3.4 Power series solutions of the radial equations

Since the problem is kinematic, the function R(z) may be specified in any way which gives an allowable flow. We shall assume that R(z) has a power series representation in  $z \leqslant z^*$ .

$$R(z) = \sum_{m=0}^{\infty} R_m z^m \qquad (5.26)$$

The solutions to  $(5.24a_{\nu}b)$  may also be expressed as power series in  $z \leqslant z^*$ .

$$X(z) = \sum_{m=0}^{\infty} X_m z^m$$
 (5.27a)

$$Y(z) = \sum_{m=0}^{\infty} Y_m z^m \qquad (5.27b)$$

Substituting (5.26) and (5.27) into (5.24), and

equating coefficients of powers of z , we find that

$$(k+2)(k+1) \times_{k+2} - N \sum_{k=0}^{k} (k-l+1) \times_{k} - Y \times_{k} =$$

$$= - \sum_{k=0}^{k} R_{k-k} Y_{k}$$
(5.28a)

$$(k+2)k+1)Y_{k+2} - N\sum_{\ell=0}^{k} (k-\ell+1)Y_{\ell} - YY_{k} = (5.28b)$$

$$= \sum_{\ell=0}^{k} (\ell+2)(\ell+1)R_{k-\ell}X_{\ell+2} - N\sum_{\ell=0}^{k} (k-\ell+1)\sum_{t=0}^{\ell} R_{\ell-t}X_{t}$$

$$+ \sum_{\ell=0}^{k} (k-\ell+1)(k+1)R_{k-\ell+1}X_{\ell+1}$$

The mean field and velocity boundary conditions at z = 0 give

$$X_0 = 1 \qquad , \qquad X_1 = \eta \qquad (5.29)$$

$$Y_{o} = 0 \tag{5.30}$$

$$R_{o} = 0 \tag{5.31}$$

Thus, from (5.28a,b),

$$X_2 = \frac{1}{2}(N+T)$$
 (5.32)

$$X_3 = \frac{1}{6} \{ N(n+2) + r \}$$
 (5.33)

$$X_4 = \frac{1}{12} \left\{ N(3+2n) + \frac{1}{2} (N+1)^2 - R_1 Y_1 \right\}$$
 (5.34)

$$X_{5} = \frac{1}{20} \left\{ N(4+3n) + N(N+v(1+\frac{n+2}{6})) + \frac{1}{6}v(N+v) - R_{1}Y_{2} - R_{2}Y_{1} \right\}$$
(5.35)

and

$$Y_{2} = \frac{n}{2}R_{1}$$

$$Y_{3} = \frac{1}{6}\{(N+V)Y_{1} + (N+2V)R_{1} + 2nR_{2}\}$$

$$Y_{4} = \frac{1}{12}\{2NY_{1} + \left[\frac{n}{2}(V-N) - 2N + \frac{3}{2}N(n+2) + \frac{3}{2}V\right]R_{1} + (2N+3V)R_{2} + 3nR_{3}\}$$

$$Y_{5} = \frac{1}{20}\{\left[\frac{1}{6}N^{2} + 3N - \frac{4}{3}R_{1}^{2}\right] + \left[\frac{5}{3}nN + \frac{1}{3}N^{2} + N\right]R_{1} + \left[\frac{4}{3}nN + 2N\right]R_{2} + 3NR_{3} + 4NR_{4} + V\left[\frac{4}{3}NY_{1} + \frac{4}{3}NR_{1} + (2+\frac{1}{3}n)R_{2} + 4R_{3}\right] + V^{2}\left[\frac{1}{6}Y_{1} + R_{1}\right]\}$$

$$(5.39)$$

The parameters  $Y_1$  and  $\gamma$  remain to be determined.

## 5.3.5 Application of the boundary conditions - the kinematic approach

From (5.12), there are four boundary conditions on the mean magnetic field to be satisfied at  $z = z^*$  - namely,

$$\langle x \rangle = \langle Y \rangle = \langle dX/dz \rangle = \langle dY/dz \rangle = 0 \qquad (5.40)$$

In the normal approach to the solution of the problem, these conditions are satisfied by adjusting  $Y_1$ ,  $\gamma$ , and the two arbitrary constants available in the solution of the induction equation in  $z \le z \le 1$  after the conditions (5.14) have been satisfied.

There is, however, an alternative approach which may be used. Since the velocity field in the kinematic dynamo problem is arbitrary, apart from the requirements that it be allowable and that it satisfy the conditions (5.15), we may choose to fulfil the boundary conditions at z=z by adjusting the coefficients  $R_n$ . In this approach we may assign any desired value to  $Y_1$ . For example, we may plausibly require that

$$Y_1 = 0 \tag{5.41}$$

thus ensuring that the toroidal magnetic field will be small in the immediate vicinity of the boundary of the conducting medium.

It would also be possible in this approach to assign any desired value to the dimensionless decay constant  $\gamma$ . However, as we are interested in studying the temporal behaviour of the magnetic field in terms of the other parameters of the problem, we may choose instead to assign a particular value to one of the coefficients  $Y_n$  (n>1). In order to allow  $\gamma$  to be complex, we shall assume that

$$Y_5 = C$$
 constant (5.42)

## 5.3.6 The oscillating dipole field - "boundary layer control" of frequency

For the case of a dipole external field, n = 1. Substituting this value into equation (5.39), and combining (5.39), (5.41), and (5.42) we obtain

$$\begin{array}{lll}
\mathbf{x} &= -\frac{4}{3} \left\{ 1 + \frac{7}{16} x + \frac{1}{4} \beta x \right\} + \\
&\pm \left\{ \frac{16}{9} \left[ 1 + \frac{7}{16} x + \frac{1}{4} \beta x \right]^{2} + 80 \frac{C}{R_{1}} \right. \\
&- \frac{20}{3} \left[ 1 + \frac{1}{2} x + \frac{3}{20} \beta x + \frac{1}{40} \xi \beta x \right] \right\}^{V_{2}}
\end{array}$$

where

$$x = 2R_2/R_1 = R''(0)/R'(0) = -r_0 \alpha''(r_0)/\alpha'(r_0)$$
 (5.44)

$$\beta = 3R_3/R_2 = R'''(0)/R''(0) = -r_0 \alpha'''(r_0)/\alpha''(r_0)$$
 (5.45)

$$f = 4R_4/R_3 = R^{N}(0)/R^{M}(0) = -r_0 \alpha^{N}(r_0)/\alpha^{M}(r_0)$$
 (5.46)

If the coefficients  $\mathbf{R}_1$  ,  $\mathbf{R}_2$  , and  $\mathbf{R}_3$  are chosen in such a way that

$$1 + \frac{7}{16}x + \frac{1}{4}\beta x = 0$$
 (5.47)

then

$$x = \frac{-4}{\beta + \frac{7}{4}} \tag{5.48}$$

$$\beta x = -\left\{4 + \frac{7}{4}x\right\} \tag{5.49}$$

and

$$-8^{2} = \frac{8}{3} \left\{ \frac{\beta(1-\xi/4) - 5/8}{\beta + 7/4} \right\} - 80 \frac{C}{R_{1}}$$
 (5.49)

$$= \frac{8}{3} \left\{ (1 - \frac{7}{4}) + \frac{19}{32} (1 - \frac{7}{38}) \times \right\} - 80 \frac{C}{R_1}$$
 (5.49')

The imaginary part of  $\gamma$  provides a measure of the oscillation frequency of the external magnetic dipole field. If  $\dot{\gamma}$  is purely imaginary, this frequency can be interpreted as the frequency of polarity reversals. From the definition of  $\gamma$ , (5.21), we see that the number of polarity reversals per million years is

no. of reversals/m.y. 
$$\approx \frac{1}{47} (\eta/r_o^2) \sqrt{-\chi^2} \cdot \{3 \times 10^{18} \text{ sec/m.y.}\}$$
 (5.50)

if y is purely imaginary.

For the Earth,  $\eta \simeq 3 \text{ m}^2/\text{sec}$  and  $r_0 \simeq 3 \times 10^6 \text{ m}$ . Substituting these values into (5.50), we obtain

no. of reversals/m.y. 
$$\approx \frac{10}{11}\sqrt{-12}$$
 (5.51)

In Figure 23 the number of reversals per million years given by (5.51) is plotted as a function of x [i.e. of  $-r_0 a''(r_0)/a'(r_0)$ ] for the case in which

$$\xi = 0 = C \tag{5.52}$$

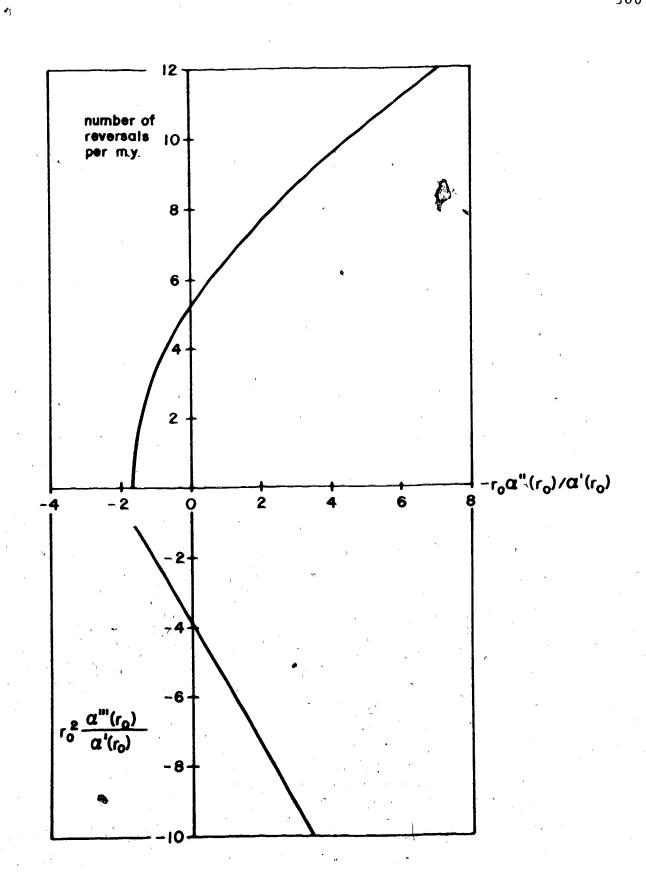
The value of  $\beta x$  [i.e.  $-r_0^2 \alpha^{\text{M}}(r_0)/\alpha'(r_0)$ ] given by (5.48') is also plotted as a function of x.

Figure 23. Parameters for the  $\alpha^2(r)$  dynamo in a spherical shell as functions of  $-r_0\alpha''(r_0)/\alpha'(r_0)$ .

Upper curve: No. of reversals per million years, given by equation (5.51), as a function of  $x = -r_0 \alpha''(r_0)/\alpha'(r_0)$ .

(In this plot,  $\eta$  and  $r_0$  have been assigned values appropriate to the Earth's fluid core.)

Lower curve:  $\beta = r_o^2 \alpha^m (r_o)/\alpha! (r_o)$  as a function of  $x = -r_o \alpha'' (r_o)/\alpha! (r_o)$ .



The curves plotted in Figure 23 correspond to a kinematic dynamo model in which the temporal behaviour of the external magnetic dipole field is controlled by turbulent motions near the boundary of the conducting fluid. A stationary state, corresponding to  $\gamma = 0$  in (5.49), is changed to an oscillatory one by small fluctuations in the dependence of  $\alpha$  on r near  $r = r_0$ . Of course, it must not be forgotten that a has been assumed time-independent in the solution of the induction equation described above. However, we may think in terms of a sporadic model in which the dependence of  $\alpha$  on r near  $r = r_0$  changes discontinuously at irregular intervals. It is interesting to note that values of the reversal frequency on the steepest part of the curve in Figure 23 correspond closely to the values observed for the geomagnetic field (see Figure 22).

#### 5.3.7 Consistency requirements

In order for the kinematic dynamo model described above to be consistent, the intensity of the turbulence in  $r \leqslant r \leqslant r_0$  must be sufficiently great to allow the boundary conditions at  $r = r^*$  to be satisfied by adjusting the values of the coefficients  $R_n$ . From (5.29)-(5.39) and (5.41)-(5.49), we see that when  $\gamma=0$  the values of X and Y at  $z=z^*$  are given by

$$X(\Xi^{a}) = 1 + \Xi^{a} + (\Xi^{a})^{2} + (\Xi^{a})^{3} + (\Xi^{a})^{4} + \{1 - \frac{1}{40}R_{i}^{2}\}(\Xi^{a})^{5} + \dots$$

$$(5.53)$$

$$Y(\Xi^{a}) = \frac{1}{2}R_{i}(\Xi^{a})^{2}\{1 + \frac{2}{19}\Xi^{a} + \frac{1}{57}(\Xi^{a})^{2} + \left[\frac{1}{3}\frac{R_{i}}{R_{i}} - \frac{1}{17i}\right](\Xi^{a})^{4} + \dots\}$$

$$(5.54)$$

If we assume that the boundary conditions on continuity of X and Y at  $z=z^*$  have been satisfied by adjusting the parameters of the solution to the induction equation in the region  $z^* \in z \in I$ , it follows from (5.53) and (5.54) that the conditions on continuity of X' and Y' at  $z=z^*$  can only be satisfied by adjusting  $R_1$  and  $R_5$  if

$$\frac{1}{8} R_i^2 (x'')^4 \sim \mathcal{O}(1) \tag{5.55}$$

and 
$$\frac{R_5}{R_1}(z^{\bullet})^4 \sim O(1) \tag{5.56}$$

Steenbeck, Krause, and Rädler (1966) have estimated the value of  $\alpha$  when a gradient of turbulent intensity is present in a system rotating with angular velocity  $\Omega$ .

$$\alpha \approx -\frac{u'\lambda_c^2 \tau_c}{\eta} \Omega \cdot \nabla u'$$
 (5.57)

We shall use this estimate as a rough guide, despite the objections raised by Lerche (1972e) to the turbulence spectrum tensor used by Steenbeck, Krause and Rädler. In (5.57) u' is the turbulent intensity,  $\lambda_{\rm C}$  the correlation length of the turbulence, and  $\tau_{\rm C}$  the correlation time.

For the case of the Earth we may write, very approximately,

$$-\Omega \cdot \nabla u \sim \frac{\Omega u'}{r_0 z^2} \qquad (5.58)$$

ignoring the departure from spherical symmetry introduced by the presence of a preferred axis. Also, from (5.26) and (5.22),

$$R(z^4) = \frac{\alpha(r^4)r_0}{\eta} \approx R_1 z^4 \qquad (5.59)$$

Combining (5.57)-(5.59) and applying the condition (5.55), we obtain

$$R_1 \cdot \left\{ z^{\alpha} \right\}^2 \sim \left\{ \frac{u' \lambda_c}{\eta} \right\}^2 \tau_c \Omega \sim \mathcal{O}(1) \tag{5.60}$$

or

$$u'\lambda_c\tau_c^{\nu_2} \sim 1/\Omega^{\nu_2} \tag{5.61}$$

For the Earth,  $\eta \simeq 3 \text{ m}^2/\text{sec}$  and  $\Omega \simeq 7 \times 10^{-5} \text{ rad/sec}$ sec. Substituting these values into (5.61), we have

$$U'\lambda_c \tau_c^{\nu_2} \sim 4 \times 10^2 \text{ m}^2/\text{sec}^{\nu_2}$$
 (5.62)

Taking  $u' \sim 10^{-4}$  m/sec as a reasonable estimate of the velocity near the surface of the core (Elsasser, 1950; Busse, 1971; Roberts and Soward, 1972), we find that the condition (5.62) reduces to

$$\lambda_c \tau_c^{\prime 2} \sim 4 \times 10^6 \text{ m} \cdot \text{sec}^{1/2}$$
 (5.63)

In order to determine whether or not (5.63) can be satisfied in the Earth's fluid core, we must estimate

the values of  $\lambda_{\rm C}$  and  $\tau_{\rm C}$  appropriate to turbulence near the core-mantle interface. We must also decide whether or not  $10^{-4}$  m/sec is a reasonable estimate for turbulent velocities in this region. In this connection, it may be noted that Steenbeck and Krause (1966) use the values

u' 
$$\sim 10^{-2} - 10^{-1}$$
 m/sec  
 $\lambda_{c} \sim 10^{2} - 10^{3}$  m  
 $\tau_{c} \sim 3$  hours  $\sim 10^{4}$  sec

for a general distribution of turbulence in the Earth's core. These values give

$$10^2 \text{ m}^2 \text{sec}^{-1/2} < \text{u'} \lambda_c \tau_c^{1/2} < 10^4 \text{ m}^2 \text{sec}^{-1/2}$$

4

a range which includes the value  $4 \times 10^2 \, \mathrm{m}^2 \mathrm{sec}^{-1/2}$  required by (5.62). On the other hand, if  $10^{-4} \, \mathrm{m/sec}$  is accepted as a reasonable value for u' near the coremantle interface, (5.63) implies that  $\tau_{\mathrm{C}}$  and  $\lambda_{\mathrm{C}}$  are related in the manner outlined in Table 16.

fluid core might well be associated with "bumps" on the Mide, 1967; core-mantle interface (Hide and Horai, 1968; Hide, 1969a; Hide and Malin, 1970, 1971a,b,c), estimated to have horizontal dimensions ~10 m and vertical dimensions ~10 m (Hide, 1969a; see Acheson and Hide, 1973). It may be seen from Table 16 that values of  $\lambda_c$  in the range  $10^3$ - $10^2$  m, corresponding to the estimated vertical dimensions of the

core-mantle "bumps", imply values of  $\tau_{\rm C}$  in the range 1-100 years. This is the range of time scales suggested by Braginskii (1964d, 1970a,b, 1971) and Currie (1968) for turbulent processes near the core-mantle boundary.

TABLE 16 Relationship between  $\tau_{C}$  and  $\lambda_{C}$  implied by (5.63)

τ <sub>C</sub>		λ <sub>C</sub>
	(seconds)	(metres)
1 hour	3 x 10 <sup>3</sup>	7 x 10 <sup>4</sup>
1 day	9 x 10 <sup>4</sup>	1 × 10 <sup>4</sup>
1 month	$3 \times 10^6$	2 x 10 <sup>3</sup>
l year	$3 \times 10^7$	$7 \times 10^{2}$
10 years	3 × 10 <sup>8</sup>	$2 \times 10^2$
100 years	3 x 10 <sup>9</sup>	7 × 100 1
1000 years	$3 \times 10^{10}$	2 x 10 <sup>1</sup>

## 5.3.8 Objections to the $\alpha^2(r)$ model for geomagnetic reversals

The kinematic  $\alpha^2(r)$  dynamo model in a spherical shell, described in the last few sections, is not intended as a serious explanation of how polarity reversals occur in the geodynamo. Several important objections to the model can be raised.

- a. The character of reversals in the model is considerably different from the irregular nature of geomagnetic reversals. The "geomagnetic reversal frequency" plotted in Figure 22 is really an average quantity. The durations of geomagnetic polarity intervals fluctuate widely about the mean. Furthermore, the transition time for a geomagnetic reversal is generally much shorter than the time between reversals (see section 5.1.2).
- b. The effects of rotation have been ignored. It is expected that in the Earth's core  $\alpha$  will depend on  $\theta$  as well as on r. As indicated in (5.57),  $\alpha$  will be proportional to  $\cos \theta$  if the gradient of turbulent intensity is radial and the axis of rotation is taken as the z-axis.
- c. It is perhaps unrealistic to assume that the external dipole field of the geodynamo is due principally to turbulent motions near the core-mantle interface.

d. No attempt has been made to include hydromagnetic effects in the model.

It must be emphasized that objection (d) applies to any kinematic model for geomagnetic reversals. If no stringent restrictions are placed on the form of the velocity field, reversals can be made to occur in many different ways - Levy's model provides one example, the present model another. Unless the hydromagnetic dynamo equations are considered, no firm conclusions can be drawn about the validity of any given model.

We may note, however, that the idea of boundary-layer control of the temporal behaviour of the geomagnetic field is worthy of closer investigation. This subject will be considered in greater detail in the remainder of this chapter.

#### 5.4 Integral properties of the kinematic dynamo equations

#### 5.4.1 Introduction

, One of the most useful approaches to the study of reversals and other temporal variations of the geomagnetic field has been the homorolar disk dynamo analogy proposed by Bullard (1955). In this model, the problems of boundary conditions and fluid motions are set aside on the assumption that the feature of the hydromagnetic dynamo most relevant to the temporal behaviour of the magnetic field is the nonlinearity of the interaction between the driving forces and the magnetic field.

Although a single disk dynamo of the type studied by Bullard (1855) does not exhibit reversals but see Malkus, 1972c), the magnetic field of a system of two or more coupled disk dynamos reverses and oscillates in an irregular manner remarkably similar to the observed behaviour of the geomagnetic dipole field (Rikitake, 1958; Lowes, 1960; Lebovits, 1960; Allan, 1962; Mathews and Gardner, 1963; Somerville, 1967; Suffolk, 1970; Cook and Roberts, 1970; Cook, 1972; Bullard and Gubbins, 1971, 1973; Malkus, 1972c). The principal advantage of studying a system of this type is its mathematical simplicity. The dynamo equations are replaced by a finite system of coupled ordinary differential equations, with time as the independent variable. It would clearly be very useful if the hydromagnetic

dynamo equations could be reduced to a system of this type.

Lorenz (1960, 1962) has proposed methods of reducing a system of coupled partial differential equations to a set of equations of the disk dynamo type, but his approach is not readily applicable to the hydromagnetic dynamo problem. It would appear to be more useful to examine the integral properties of the dynamo equations, particularly as the quantities of interest, such as the magnetic dipole moment of a current distribution, are themselves integral quantities. Some progress in this direction has been made by Runcorn (1955) and Backus (1958).

In the remainder of this chapter, we shall consider the integral properties of the kinematic dynamo equations. Consideration of hydromagnetic effects will be deferred until Chapter 6.

#### 5.4.2 Multipole representation of the external fields

The electric and magnetic fields in a non-conducting medium surrounding a conductor can be represented in terms of the electric and magnetic multipole moments of the charge and current distributions in the conducting medium. If the gauge

$$div A = 0 (5.64)$$

is used in the quasi-steady approximation, where  $\overset{\text{A}}{\sim}$  is the

vector potential defined in (1.58), these multipole expansions can be written in the form

$$\hat{E} = -\frac{1}{4\pi\epsilon} \sum_{m=1}^{\infty} \frac{(-1)^m}{m!} Q^{(m)} \cdot \nabla^m \left( \nabla \frac{1}{r} \right) +$$

$$-\frac{\mathcal{A}}{4\pi} \sum_{m=1}^{\infty} \frac{(-1)^m}{m!} \hat{T}^{(m)} \cdot \nabla^{m-1} \times \nabla \frac{1}{r}$$
(5.65)

$$\hat{\mathbf{B}} = -\frac{\mu}{4\pi} \sum_{m=1}^{\infty} \frac{(-1)^m}{m!} \mathbf{T}^{(m)} \cdot \nabla^m (\mathbf{v}_{\underline{r}})$$
 (5.66)

where

$$Q^{(m)} \equiv \int_{V} \Theta_{R}^{m} dn \qquad (5.67)$$

and

$$T^{(m)} \equiv \frac{m}{m+1} \int_{V} (rxj) r^{m-1} dv$$
 (5.68)

denotes dT<sup>(m)</sup>/dt. In (5.67) and (5.68), the integration is taken over the volume of the charge and current distribution. In (5.65)-(5.68) we have used the notation

$$\mathbf{F}^{(m)} \cdot \nabla^{m} = \mathbf{F}_{a_{1}a_{2} \dots a_{m}} \frac{\partial}{\partial x_{a_{1}}} \frac{\partial}{\partial x_{a_{2}}} \frac{\partial}{\partial x_{a_{m}}} \frac{\partial}{\partial x_{a_{m}}}$$
(5.69)

$$\mathbf{r}^{\mathbf{m}} = \mathbf{x}_{a_1} \mathbf{x}_{a_2} \dots \mathbf{x}_{a_m} \quad \mathbf{1}_{a_1} \mathbf{1}_{a_2} \dots \mathbf{1}_{a_m} \tag{5.70}$$

where the  $x_{a_i}$  are Cartesian components of the position vector r, the  $l_{a_i}$  are unit vectors, and the summation convention is implied in each case. (See Appendix 2 for the

derivation of these equations.) It should be noted that  $\theta$  and j in equations (5.67) and (5.68) are the charge and current densities defined in section 1.3.1.

# 5.4.3 Magnetic and electric multipole moments - representation in terms of the internal magnetic and velocity fields

From equations (1.4) and (1.6) we have

$$\theta = \epsilon \nabla \cdot E \tag{5.71}$$

so that, by (1.15)

$$\Theta = \epsilon \nabla \cdot \left\{ \frac{1}{\sigma} \mathbf{j} - \mathbf{u} \times \mathbf{B} \right\}$$
 (5.72)

Since 
$$\nabla \cdot \mathbf{j} = \mathbf{0}$$
 (5.73)

in the quasi-steady approximation, (5.72) reduces to

$$\Theta = -\epsilon \varphi_{\bullet} \{ u \times B \} \qquad (5.74)$$

and (5.67) becomes

$$Q^{(m)} = -\epsilon \int_{V} \nabla \cdot (\underline{u} \times \underline{B}) r^{m} dv \qquad (5.75)$$

Equation (5.75) can be further simplified by making use of the no-slip condition  $[n \times u] = 0$  on the boundary of v (see section 1.7.2) to obtain

$$Q^{(m)} = -\epsilon \int_{V} \left\{ \nabla \cdot \left[ (\mathbf{x} \times \mathbf{B}) \cdot \mathbf{y}^{m} \right] - (\mathbf{x} \times \mathbf{B}) \cdot \nabla (\mathbf{y}^{m}) \right\} dw$$

$$= -\epsilon \int_{V} (\mathbf{x} \times \mathbf{x}) \cdot \mathbf{B} \cdot \mathbf{y}^{m} dS + \epsilon \int_{V} (\mathbf{x} \times \mathbf{B}) \cdot \nabla (\mathbf{y}^{m}) dw$$

$$= \epsilon \int_{V} (\mathbf{x} \times \mathbf{B}) \cdot \nabla (\mathbf{y}^{m}) dw \qquad (5.76)$$

Equation (5.76) expresses the electric multipole moment tensor  $Q^{(m)}$  in terms of the fields  $\underline{u}$  and  $\underline{B}$  rather than their derivatives.

In Appendix 2 a similar representation is derived for the magnetic multipole tensor, expressing  $T^{(m)}$  in terms of B rather than in terms of j. When the conducting volume V is spherical, the expressions for the first few magnetic multipole moments become

[dipole moment]

$$T^{(i)} = \frac{3}{2\mu} \int_{V} \mathbf{B} dv \qquad (5.77)$$

[quadrupole moment]

$$T^{(2)} = \frac{2}{3\mu} \int_{V} \left\{ 4B\mathbf{r} + \mathbf{r}B - (\mathbf{r} \cdot B)\mathbf{I} \right\} d\omega \qquad (5.78)$$

[octupole moment]

$$T^{(3)} = \frac{3}{4\mu} \int \left\{ 5Brr + rBr + rrB \\ - (r.B)(Ir + 1.r1.) \right\} dw + \frac{4}{5}\mu r^2 \left\{ \frac{2}{3}T^{(1)}I - 1.T^{(1)}1. - I.T^{(2)} \right\}$$
(5.79)

In general, the expression for the  $2^{2n}$ -pole moment involves a summation over the  $2^{2i}$ -pole moments, and the expression for the  $2^{2n+1}$ -pole moment involves a summation over the  $2^{2i+1}$ -pole moments, where  $i=1,2,\ldots,n-1$  in each case. For example, the expression for the sedecimupole moment tensor (Winch, 1967a)  $T^{(4)}$  will contain terms involving the quadrupole moment tensor  $T^{(2)}$ , and the expression for the duotrigintupole moment tensor (Winch, 1967b)  $T^{(5)}$  will contain terms involving the dipole and octupole moment tensors  $T^{(1)}$  and  $T^{(3)}$ .

## 5.4.4 <u>Temporal behaviour of the external magnetic dipole</u> moment

The problem of the temporal variation of the external, magnetic field of a current distribution may now be studied with the aid of equations (5.76)-(5.79). Taking the time derivative of equation (5.77), and making use of the magnetic induction equation (1.16') and the boundary condition u = 0 on S (see section 1.7.2), we obtain

$$\dot{T}^{(r)} = \frac{3}{2\mu} \int_{V} \left\{ \frac{\partial \mathbb{B}}{\partial t} \right\} dv$$

$$= \frac{3}{2\mu} \int_{V} \left\{ \eta \nabla^{2} \mathbb{B} + \nabla \times (\mathbb{U} \times \mathbb{B}) \right\} dv$$

$$= \frac{3}{2\mu} \int_{V} \eta \nabla^{2} \mathbb{B} dv + \frac{3}{2\mu} \int_{S} \mathcal{D} \times (\mathbb{U} \times \mathbb{B}) dS$$

or

$$\dot{T}^{(i)} = \frac{3\eta}{2\mu} \int_{V} \nabla^{2} \vec{B} \, dv = -\frac{3\eta}{2} \int_{S} n \times j \, dS \qquad (5.80)$$

From (5.80) we see that the rate of change of the magnetic dipole moment depends only on the dissipation term  $\eta \nabla^2 B$  in the induction equation, and thus has no direct link with either the velocity field u or the external potential field  $\hat{B}$ . Differentiating again with respect to time, we obtain

$$\ddot{T}^{(i)} = \frac{3\eta}{2\mu} \int_{V} \nabla^{2} \left\{ \eta \nabla^{2} \ddot{B} + \nabla x (\dot{u} x \dot{B}) \right\} dv$$

$$= \frac{3\eta^{2}}{2\mu} \int_{V} \nabla^{4} \dot{B} + \frac{3\eta}{2\mu} \int_{S} \dot{n} x \nabla^{2} (\dot{u} x \dot{B}) dS \qquad (5.81)$$

The second time derivative of the magnetic dipole moment is thus directly linked to both the dissipative and the regenerative terms in the induction equation.

## 5.4.5 "Boundary-layer control" of the external dipole moment

Expanding the regenerative term in (5.81), we obtain

$$T_{i}^{(i)} = \frac{3\eta^{2}}{2\mu} \int_{V} \nabla^{4} B_{i} dar +$$

$$+ \frac{3\eta}{2\mu} \epsilon_{ijm} \epsilon_{mlk} \int_{S} \eta_{j} \left\{ B_{k} \nabla^{2} u_{l} + 2 \frac{\partial u_{l}}{\partial x_{r}} \frac{\partial B_{k}}{\partial x_{r}} \right\} dS$$
(5.82)

The three integrals on the right hand side of equation (5.82) can be estimated as follows:

$$I^{(1)} = \begin{vmatrix} \frac{3\eta^2}{2\mu} \int_{V} \nabla^4 \mathbf{B} \, d\mathbf{w} \end{vmatrix} \sim \frac{3\eta^2}{2\mu} \frac{4\pi}{3} r_0^3 \cdot \frac{\mathbf{B}_0}{L^4} \quad (5.83)$$

$$I^{(2)} = \begin{vmatrix} \frac{3\eta}{2\mu} \int_{S} n \mathbf{B} \nabla^2 \mathbf{u} \, d\mathbf{S} \end{vmatrix} \sim \frac{3\eta}{2\mu} \cdot 4\pi r_0^2 \cdot \mathbf{B}_0^{(3)} \cdot \frac{\mathbf{u}}{\delta^2} \quad (5.83')$$

$$I^{(3)} = \begin{vmatrix} \frac{3\eta}{2\mu} \int_{S} 2\eta \frac{\partial \mathbf{u}}{\partial \mathbf{x}_r} \frac{\partial \mathbf{B}}{\partial \mathbf{x}_r} \, d\mathbf{S} \end{vmatrix} \sim \frac{3\eta}{\mu} \cdot 4\pi r_0^2 \cdot \frac{\mathbf{B}_0^{(3)}}{\delta} \cdot \frac{\mathbf{u}}{\delta} \quad (5.83'')$$

where  $B_O$  is the average magnitude of the magnetic flux density in V,  $B_O^{(S)}$  the average magnitude of the flux density on S, and L a length scale defined in such a way as to make  $B_O/L^2$  the average value of  $|V^2B|$  in V.  $r_O$  is the radius of the spherical volume V,  $\delta$  the thickness of the boundary layer on S (assuming that one exists), and  $u_O$  the average change in velocity across the boundary layer.

Comparing terms in (5.83)-(5.83"), we have

$$I^{(s)}/I^{(s)} \sim \frac{\eta r_o}{3u_o} \frac{B_o}{B_o^{(s)}} \cdot \frac{\delta^2}{L^4}$$
 (5.84)

For the Earth, we may take

$$B_{o}/B_{o}^{(S)} \lesssim 10^{2}$$
 (5.85)  
 $r_{o} \sim 3 \times 10^{6} \text{ m}$  (5.86)  
 $\eta \sim 3 \text{ m}^{2}/\text{sec}$  (5.87)

Substituting these values into (5.84), we obtain

$$I^{(1)}/I^{(2)} \lesssim \{3 \times 10^8 \text{ m}^3/\text{see}\}^{8/2}/u_0L^4$$
 (5.88)

From equations (5.84') and (5.88) we see that if

$$\delta/L \ll 1$$
 (5.89)

and 
$$\delta_{\text{unl}}^2 \ll \{3 \times 10^{-9} \text{ sec/m}^3\}$$
 (5.90)

the dominant term in (5.81) will be the one involving ,  $\nabla^2 \underline{u} \ . \ \ \text{Under these conditions we may write, approximately,}$ 

$$T_i^{(s)} \approx \frac{3\eta}{2\mu} \, \epsilon_{ijm} \, \epsilon_{mgk} \, \int_S n_j \, B_k \, \nabla^2 u_k \, dS$$
 (5.91)

When equation (5.91) is valid, the temporal behaviour of the geomagnetic dipole moment is "controlled" by the velocity distribution in the boundary layer.

In deriving equation (5.91) we have ignored the possibility of turbulence near the core-mantle boundary. If turbulence is present an appropriate "mean field" equation is obtained from equation (5.81) by writing  $\overline{B}$  in place of B and  $\{\overline{u} \times \overline{B} + \overline{u' \times B'}\}$  in place of  $u \times B$  on the right hand side. Assuming for simplicity that  $\overline{u' \times B'} = \alpha \overline{B}$ , giving an  $\alpha$ -effect, we find that equation (5.91) must be replaced by

$$\widetilde{T}_{i}^{(1)} \approx \frac{3\eta}{2\mu} \int_{S} \left\{ (\underline{n} \cdot \overline{B}) \nabla^{2} \overline{u}_{i} - (\underline{n} \cdot \nabla^{2} \overline{u}) \overline{B}_{i} + \epsilon_{ijk} (\nabla^{2} \alpha) \eta_{j} \overline{B}_{k} \right\} dS$$
(5.92)

if we make the additional assumption that the term involving  $\nabla^2\alpha$  makes a contribution of the same order of magnitude as that involving  $\nabla^2\bar{u}$ .

#### 5.4.6 Simplification of notation

For simplicity in writing complicated expressions, we shall make use of the notation

$$\partial_{a_i} \equiv \partial_{\partial x_{a_i}}$$
 (5.93)

$$T^{(m)} \cdot \nabla^m \equiv T^{(m)} \quad \partial_{a_m} \quad \partial_{a_m} \quad (5.94)$$

We shall also make use of several theorems proved in Appendix 2. In particular,

$$\mathfrak{N} \cdot \nabla \left\{ \partial_{a_1} \cdots \partial_{a_m} \frac{1}{r} \right\} = -\frac{(m+1)}{r_0} \left\{ \partial_{a_1} \cdots \partial_{a_m} \frac{1}{r} \right\} \tag{5.96}$$

See section A.2.3 for further details.

#### 5.4.7 The "boundary-layer control" approximation

As it stands, equation (5.92) is not particularly useful, since it involves both  $\underline{T}^{(1)}$  and  $\underline{B}$ . However, since  $\underline{B}$  is continuous across the boundary  $S \cdot (see\ section\ 1.7.1)$ , we may replace  $\underline{B}$  in (5.92) with the multipole

expansion (5.66). Making this substitution and applying equation (5.96), we obtain

$$T_{i}^{(i)} \approx -\frac{3\eta}{8\pi} \sum_{m=1}^{\infty} \frac{(-1)^m}{m!} T_{a_1 \dots a_m}^{(m)} \cdot \int_{S} \left\{ -\frac{(m+1)}{r_o} (\nabla^2 \overline{u}_i) \partial_{a_1 \dots} \partial_{a_m} \frac{1}{r} - (\underline{n} \cdot \nabla^2 \overline{u}) \partial_{a_1 \dots} \partial_{a_m} \partial_i \frac{1}{r} + e_{ijk} (\nabla^2 \alpha) n_j \partial_{a_1 \dots} \partial_{a_m} \partial_k \frac{1}{r} \right\} dS$$

$$(5.97)$$

Writing out the first few terms of (5.97) in detail, we have

$$T_{i}^{(1)} \approx \frac{3\eta}{8\pi} \left\{ T_{\alpha_{1}}^{(1)} \int_{S} \left[ \frac{2}{r_{0}^{3}} (\nabla^{2} \overline{u}_{i}) n_{\alpha_{1}} + \frac{1}{r_{0}^{3}} (\eta \cdot \nabla^{2} \overline{u}) (\delta_{i\alpha_{1}} - 3n_{i}n_{\alpha_{1}}) \right. \right. \\ \left. - \frac{1}{r_{0}^{3}} \varepsilon_{ij\alpha_{1}} n_{j} (\nabla^{2} \alpha) \right] dS + \\ + \frac{1}{2} T_{\alpha_{1}\alpha_{2}}^{(2)} \int_{S} \left[ \frac{3}{r_{0}^{4}} (\nabla^{2} \overline{u}_{i}) (3n_{\alpha_{1}}n_{\alpha_{2}} - \delta_{\alpha_{1}\alpha_{2}}) + \right. \\ \left. + \frac{3}{r_{0}^{4}} (\eta \cdot \nabla^{2} \overline{u}) (n_{i} \delta_{\alpha_{1}\alpha_{2}} + n_{\alpha_{1}} \delta_{i\alpha_{2}} + n_{\alpha_{2}} \delta_{i\alpha_{1}} - 5n_{i}n_{\alpha_{1}}n_{\alpha_{2}}) \right. \\ \left. - \frac{3}{r_{0}^{4}} (\nabla^{2} \alpha) \varepsilon_{ijk} n_{j} (n_{k} \delta_{\alpha_{1}\alpha_{2}} - n_{\alpha_{1}} \delta_{k\alpha_{2}} + n_{\alpha_{2}} \delta_{k\alpha_{1}} - n_{\alpha_{1}} \delta_{k\alpha_{2}} + n_{\alpha_{2}} \delta_{k\alpha_{1}} \right] dS \\ \left. + \cdots \right\}$$

$$(5.98)$$

If  $|T^{(2)}/r_0| << |T^{(1)}|$ , equation (5.98) reduces.

 $T_{i}^{(1)} \approx \frac{3\eta}{8\pi r_{o}^{3}} T_{a_{i}}^{(1)} \int_{S} \left\{ 2n_{a_{i}} \nabla^{2} \overline{u}_{i} + \eta \cdot \nabla^{2} \overline{u} \left( \delta_{ia_{i}} - 3n_{i}n_{a_{i}} \right) \right\} (5.99)$   $- \epsilon_{ija_{i}} n_{i} \nabla^{2} \alpha d dS + ...$ 

to

A further reduction is obtained if the usual boundary layer approximation for fluid motions in a sphere is made. In this approximation, tangential derivatives of u are neglected in comparison with radial derivatives, and only the highest-order radial derivatives are retained, to first order. In addition, the component of velocity normal to the boundary is neglected in comparison with the tangential components. Thus,

$$\nabla^2 \overline{u} \approx \frac{3^2}{3r^2} u_0 + \frac{3^2}{3r^2} u_4 \qquad (5.100)$$

$$\nabla^2 \alpha \approx \frac{\partial^2}{\partial r^2} \alpha \tag{5.101}$$

and equation (5.99) becomes

$$\tilde{T}^{(i)} \approx \frac{3\eta}{8\pi r_o^3} \int_{S} \left\{ 2 \left( \frac{\partial^2 u_0}{\partial r^2} + \frac{\partial^2 u_0}{\partial r^2} \right) \left( \frac{\partial^2 u_0}{\partial$$

Equation (5.102) will be referred to as the boundary-layer control approximation. The validity of this approximation depends on a number of assumptions, which will be summarized here for convenience.

a) 
$$\delta/L \ll 1$$
 (5.89)

b) 
$$\delta^2/u_0L^4 \ll \{3 \times 10^{-9} \text{ sec/m}^2\}$$
 (5.90)

The notation used in (5.89) and (5.90) is defined above

in connection with (5.83). (5.90) is the form of the assumption  $I^{(1)} \ll I^{(2)}$  appropriate to the Earth's fluid core, where  $I^{(1)}$  and  $I^{(2)}$  are the integrals defined in (5.83) and (5.83'). It may be noted that (5.89) is more or less equivalent to the assumptions leading to the boundary-layer approximation, (5.100) and (5.101).

Within the framework of the kinematic dynamo problem, the boundary-layer control approximation, (5.102), gives a second-order ordinary differential equation for  $T^{(1)}$ , with time as the independent variable. When the hydromagnetic dynamo problem is considered, the coefficients of this equation depend on  $T^{(1)}$ , and the complexity of the equation is increased. This problem will be considered in section 6.3.

## 5.5 The boundary-layer control approximation and the geodynamo

### 5.5.1 <u>Time-scale restrictions on boundary-layer control</u> in the geodynamo

A rough estimate of the characteristic time scale of dipole moment variations governed by the boundary-layer control approximation may be obtained by scaling the terms in equation (5.102). When this is done, we find that the time scale  $\tau$  is given by

$$\tau \sim \sqrt{r_0 \delta^2/\eta u_0}$$
 (5.103)

For the case of the geodynamo,  $r_{_{\rm O}} \sim$  3 x 10  $^6$  m ,  $\eta \sim$  3 m $^2/{\rm sec}$  , and (5.103) becomes

$$\tau \sim 10^3 \cdot \sqrt{\frac{\delta^2}{u_o}} \left\{ \frac{m \cdot m^2}{(m^2/s)(m/s)} \right\}^{\frac{1}{2}}$$
 (5.103')

From (5.103') we see that in order to get dipole moment variations in the geodynamo with a time scale of  $10^K$  years, we must have

$$\delta^2/u_0 \sim 10^{2K+9} \text{ m. sec}$$
 (5.104)

Combining (5.104) with the assumption (5.90), we obtain a consistency condition for the boundary-layer control approximation in the geodynamo:

$$L > 3 \times 10^{4 + \frac{R}{2}} m$$
 (5.105)

In the geodynamo, L, defined as the length scale needed to make  $B_O/L^2$  the "average value" (defined in an integral sense - see section 5.4.5) of  $|\nabla^2 B|$  in the fluid core, is unlikely to be much larger than  $r_O$ , the core radius. Taking  $r_O \sim 3 \times 10^6$  m as an upper bound on L in (5.105), we see that the limitation on  $\kappa$  is

K < 4 (5.106)

The boundary-layer control approximation can therefore only be used to explain variations of the Earth's dipole moment which have a time scale shorter than 10<sup>4</sup> years.

## 5.5.2 Temporal variations of the Earth's magnetic dipole moment

As may be seen from Table 13, the geomagnetic dipole moment varies on several time scales in the range  $\tau < 10^4 {\rm y}$ . For example,

- a) the dipole axis precesses, or "wobbles", around the axis of rotation in an irregular fashion, with a time scale of about 10<sup>3</sup> years (see footnote [6], Table 13);
- b) energy is transferred from the dipole field to higher-order multipole fields with a time scale of about 2 x 10<sup>3</sup> years (see footnote [4], Table 13);
- c) the rate at which energy is transferred from the dipole field to higher-order multipole fields varies

on a time scale of about  $10^2$  years (see footnote [5], Table 13);

d) the direction and intensity of the dipole moment change on a time scale of 10<sup>3</sup>-10<sup>4</sup> years during a polarity reversal (see footnotes [8], [9], and [10], Table 13).

The "fundamental frequency" of dipole field strength  $\ell$  oscillations corresponds to a period  $\sim 10^4$  years. Since this period is so close to the maximum value of  $\tau$  allowed by (5.106), it seems unlikely that this variation can be explained in terms of the boundary-layer control approximation.

Of the variations listed above, only (a) and (d) can be discussed in terms of the boundary-layer control approximation, equation (5.102). In order to discuss variations (b) and (c), we would have to return to equation (5.97), and retain higher-order multipole terms. In this thesis, we shall restrict consideration to equation (5.102).

## 5.5.3 Detailed expansion of the approximate dipole moment equation

Equation (5.102) can be written in the form

$$\begin{bmatrix} \ddot{T}_{x}^{(i)} \\ \ddot{T}_{y}^{(i)} \\ \ddot{T}_{z}^{(i)} \end{bmatrix} = \frac{3\eta}{4\pi r_{o}^{3}} \begin{bmatrix} (i_{1}-i_{3}) & (i_{4}-i_{5}+i_{6}) & (i_{1}-i_{12}-i_{8}) \\ (i_{4}+i_{5}-i_{6}) & (i_{2}+i_{3}) & (i_{13}+i_{14}+i_{10}) \\ (-i_{7}+i_{8}) & (-i_{4}-i_{10}) & (i_{1}+i_{2}) \end{bmatrix} \cdot \begin{bmatrix} T_{x}^{(i)} \\ T_{y}^{(i)} \\ T_{z}^{(i)} \end{bmatrix}$$
(5.107)

where

$$i_1 = \int \frac{\partial^2 \bar{u}_{\theta}}{\partial r^2} \cos \theta \sin \theta \cos^2 \phi \ dS$$
 (5.108)

$$i_2 = \int_{\epsilon} \frac{\partial^2 \bar{u}_{\theta}}{\partial r^2} \cos \theta \sin \theta \sin^2 \phi dS \qquad (5.109)$$

$$\hat{l}_3 = \int_{\mathbb{R}} \frac{\partial^2 \overline{u} \phi}{\partial r^2} \sin \theta \sin \phi \cos \phi dS \qquad (5.110)$$

$$i_4 \equiv \int_S \frac{\partial^2 u_\theta}{\partial r^2} \cos \theta \sin \theta \cos \phi \sin \phi dS$$
 (5.111)

$$\hat{l}_{5} \equiv \int_{S} \frac{\partial^{2} \bar{u}_{\phi}}{\partial r^{2}} \sin \theta \sin^{2} \phi dS \qquad (5.112)$$

$$i_6 = \int \frac{1}{2} \frac{\partial^2 \alpha}{\partial r^2} \cos \theta \, dS \qquad (5.113)$$

$$i_7 \equiv \int_{c} \frac{\partial^2 \hat{u}_{\theta}}{\partial r^2} \sin^2 \theta \cos \phi \, dS \qquad (5.114)$$

$$l_8 = \int_{1}^{1} \frac{\partial^2 \alpha}{\partial r^2} \sin \theta \sin \phi dS \qquad (5.115)$$

$$i_q \equiv \int \frac{\partial^2 \vec{u}_0}{\partial r^2} \sin^2 \theta \sin \phi \, dS \qquad (5.116)$$

$$i_{\omega} = \int_{S} \frac{1}{2} \frac{\partial^{2} \alpha}{\partial r^{2}} \sin \theta \cos \phi \, dS \qquad (5.117)$$

$$i_{\rm H} \equiv \int_{\rm S} \frac{\partial^2 \vec{u}_{\rm e}}{\partial r^2} \cos^2 \theta \cos \phi \, dS \qquad (5.118)$$

$$i_{12} \equiv \int_{S} \frac{\partial^{2} u_{\phi}}{\partial r^{2}} \cos \theta \sin \phi dS \qquad (5.119)$$

$$\hat{l}_{13} \equiv \int_{S} \frac{\partial^{2} \bar{u}_{\theta}}{\partial r^{2}} \cos^{2}\theta \sin \phi dS \qquad (5.120)$$

$$\hat{i}_{H} \equiv \int_{S} \frac{\partial^{2} \overline{u}_{\phi}}{\partial r^{2}} \cos \theta \cos \phi dS \qquad (5.121)$$

Equation (5.107) may now be studied under various assumptions about the symmetry of the velocity field.

#### 5.5.4 "Dipole wobble"

If  $\overline{u}_{\theta} = 0$  and  $\overline{u}_{\phi}$  and  $\alpha$  are axially symmetric (i.e. independent of  $\phi$ ), equation (5.107) reduces to

$$T_{x_{c}}^{(i)} = -\left\{\frac{3\eta}{4\pi r_{d}^{3}}\right\}, (i_{5}-i_{6}) T_{y}^{(i)}$$
 (5.122)

$$T_y^{(0)} = \left\{ \frac{3\eta}{4\pi r_0^3} \right\} (i_5 - i_6) T_x^{(0)}$$
 (5.122')

Combining these two equations, and assuming that the time derivatives of  $u_{\phi}$  and  $\alpha$  are small enough to be neglected, we obtain

$$T_{x}^{(0)} = -\left[\frac{3\eta}{4\pi r_{o}^{3}}\right]^{2} (i_{5} - i_{6})^{2} T_{x}^{(0)}$$
 (5.123)

Solutions to equations (5.122) and (5.123) are of the form

$$T_{\mathbf{x}}^{(i)} = \mathbf{a}^{i} \mathbf{e}^{\mathbf{t} K t} \cos K t \tag{5.124}$$

$$T_y^{(i)} = \alpha e^{\frac{t}{Kt}} \sin Kt \qquad (5.125)$$

where

$$K = \sqrt{\frac{3\eta}{8\pi r_0^3}(i_5 - i_6)}$$
 (5.126)

These solutions indicate that the dipole moment vector precesses, or "wobbles", about the axis of symmetry, which may be taken as the axis of rotation in the case of the geodynamo. In (5.126)

$$i_5 = \pi r_0^2 \int_0^{\pi} \frac{\partial^2 \overline{u}}{\partial r^2} \sin^2 \theta \ d\theta \tag{5.127}$$

$$i_{\ell} \equiv \pi r_{0}^{2} \int_{0}^{\pi} \frac{\partial^{2} \alpha}{\partial r^{2}} \sin \theta \cos \theta d\theta \qquad (5.128)$$

Monzero contributions to (5.127) and (5.128) arise from velocity components which satisfy

$$\overline{u}_{\phi} \propto P_{2n}(\cos \theta)$$
 (5.129a)

$$\alpha \propto P_{2n+1}(\cos \theta) \tag{5.129b}$$

where the  $P_n$  are Legendre polynomials.

#### 5.5.5 Axial dipole moment variations

If  $\widetilde{u}_{\phi} = 0$  and  $\widetilde{u}_{\theta}$  and  $\alpha$  are axially symmetric (i.e. independent of  $\phi$ ), equation (5.107) reduces to

$$\hat{T}_{\mathbf{x}}^{(i)} = \left\{ \frac{3\eta}{4\pi r_{\mathbf{x}}^{3}} \right\} \left\{ i_{1} T_{\mathbf{x}}^{(i)} + i_{6} T_{\mathbf{y}}^{(i)} \right\}$$
 (5.130)

$$\tilde{T}_{y}^{(i)} = \left\{ \frac{3\eta}{4\pi r_{o}^{3}} \right\} \left\{ -i_{o}T_{x}^{(i)} + i_{i}T_{y}^{(i)} \right\}$$
 (5.130')

$$\tilde{T}_{z}^{(i)} = \left\{ \frac{3\eta}{2\pi r^{3}} \right\} \left\{ i_{i} T_{z}^{(i)} \right\}$$
 (5.130")

where

$$\hat{L}_{i} = \pi r_{o}^{2} \int_{S} \frac{\partial^{2} u_{0}}{\partial r^{2}} \cos \theta \sin^{2} \theta d\theta \qquad (5.131)$$

$$i_6 = \pi r_0^2 \int_S \frac{\partial^2 \alpha}{\partial r^2} \cos \theta \sin \theta \, d\theta \qquad (5.132)$$

Combining (5.130) and (5.130'), and neglecting time derivatives of  $\overline{u}_{\theta}^{}$  and  $\alpha$  , we obtain

$$\tilde{T}_{x}^{(i)} = \left\{ \frac{3\eta}{2\pi r_{s}^{3}} \right\} \hat{\iota}_{i} \tilde{T}_{x}^{(i)} + \left\{ \frac{3\eta}{4\pi r_{s}^{3}} \right\}^{2} (\hat{\iota}_{i}^{2} + \hat{\iota}_{6}^{2}) T_{x}^{(i)} = 0 \qquad (5.133)$$

Equations (5.130), (5.130"), and (5.133) may now be solved for  $T_X^{(1)}$ ,  $T_Y^{(1)}$ , and  $T_z^{(1)}$ .

$$T_{x}^{(i)} = \Re \left\{ a_{i} e^{\kappa_{i} t} + a_{z} e^{-\kappa_{i} t} \right\}$$
 (5.134)

$$T_y^{(i)} = \int_{m} \left\{ a_i e^{K_i t} + a_2 e^{-K_i t} \right\}$$
 (5.135)

$$T_z^{(i)} = b_i e^{K_2 t} + b_2 e^{-K_2 t}$$
 (5.136)

where the  $a_i$  are complex constants, the  $b_i$  are real

constants, and

$$K_{i} \equiv \sqrt{\frac{3\eta}{4\pi r_{o}^{3}}(i_{i}-ii_{o})}$$
 (5.137)

$$K_2 = \sqrt{\frac{3\eta}{2\pi r_0^3}} i_1 \tag{5.138}$$

The solution given in (5.136) for  $T_z^{(1)}$  requires  $i_1>0$ , so that  $K_2$  is real. If  $i_1<0$ , (5.136) must be replaced with

$$T_{z}^{(i)} = \Re \{be^{K_{z}t}\}$$
 (5.136')

where b is complex.

From equations (5.134)-(5.136') we see that an axisymmetric meridional flow near the boundary of the Earth's fluid core can produce large changes in the geomagnetic dipole moment on the time scale

$$\tau \sim \sqrt{r_{\circ} \delta^2/\eta u_{\circ}} \qquad (5.139)$$

As in section 5.5.4, the presence of an axisymmetric  $\alpha$ -effect can lead to "dipole wobble", but an  $\alpha$ -effect of this type has no effect on the axial dipole moment. As may be seen from (5.136'), the axial dipole moment  $T_Z^{(1)}$  can be made to "reverse", or even oscillate, if  $i_1$  is negative. In contrast to the oscillatory reversals discussed in section 5.3, reversals in the boundary-layer control model are governed by the properties of the mean

flow,  $\overline{\underline{u}}$  , rather than by the properties of the turbulence which gives rise to the  $\alpha$ -effect.

As pointed out in (5.129b),  $i_6$  is nonzero only if  $\alpha$  satisfies

α α P<sub>2n+1</sub> (cos θ)

(5-140a)

Similarly,  $i_1$  is nonzero only if

 $u_{\theta} \propto P_{2n} (\cos \theta)$ 

(5.140b)

where the Pn are Legendre polynomials,

## 5.5.6 <u>Limitations on the boundary-layer control</u> approximation in the geodynamo

The principal limitation on the boundary-layer control approximation in the geodynamo is the time-scale restriction discussed in section 5,5,1. However, other limitations must also be considered.

The dipole moment solutions obtained in sections 5.5.4 and 5.5.5 depend on the assumption that the velocity distribution is independent of time. If this is not the case, the behaviour of the dipole moment with time, within the framework of the boundary-layer control approximation, will be considerably more complicated. This aspect of the dipole moment variation is outside the scope of the kinematic dynamo problem. In order to determine the time

dependence of the velocity field, we must consider the hydromagnetic dynamo problem. (See Chapter 6.)

As noted in section 5.5.2, equation (5.102) does not permit discussion of the transfer of energy from the dipole field to higher-order multipoles. This problem can only be studied if the higher-order terms in (5.97) are retained, and expressions for the time derivatives of the higher-order multipole moments are obtained from equations (5.77)-(5.79). Unfortunately, simplifications of the type encountered in the derivation of equation (5.102) are not common. The quadrupole and octupole moment tensors  $T_{\infty}^{(2)}$  and  $T_{\infty}^{(3)}$  depend on the integral moments of the dissipative term in the induction equation, on the electric multipole moments, on the higher-order magnetic multipole moments, and so on. The integrals

### ∫(y×B) yrm dw

which must be evaluated if the higher-order moments are to be studied, do not have a useful representation in terms of the external potential fields. These integrals can only be treated sensibly within the context of the hydromagnetic dynamo problem.

The most serious disadvantage of the boundary-layer control approximation is the fact that dissipative effects are neglected. Although no attempt will be made here to

overcome this drawback, it may be possible to improve the approximation by including an estimate of the dissipative term in equation (5.82). Unfortunately, it is difficult to see how the time dependence of the term could be included in such an estimate.

Despite these limitations, we shall continue to use the boundary-layer control approximation in the next chapter. It is particularly encouraging that the dipole wobble appears to be well represented within the framework of the approximation. We shall consider this variation in more detail in section 6.3.4.

#### 5.6 Summary of Chapter 5

This chapter is concerned with temporal variations of astrophysical magnetic fields, with particular reference to the geomagnetic field. A summary of observational knowledge of the temporal behaviour of astrophysical fields is presented in section 5.1.

The  $\alpha^2(r)$  kinematic dynamo in a spherical shell is studied in detail in section 5.3. It is shown that regardless of the fluid motions in the deep interior of the sphere, it is possible to choose a turbulent velocity distribution near the outer boundary which makes the external magnetic dipole field vary with time in a periodic manner. The frequency of the dipole field oscillation is a sensitive function of the dependence of  $\alpha$  on r at the boundary. Application of this model to the Earth is discussed, and several serious shortcomings are pointed out.

The idea of boundary-layer control of the external magnetic field of a spherical volume of conducting fluid is discussed for more general distributions of velocity in section 5.4. A set of expressions is presented which relate the multipole moments of a spherical distribution of currents to the integral moments of the internal magnetic field in a novel manner. These expressions are used to derive a differential equation for the external magnetic dipole moment as a function of time.

In section 5.5 it is shown that boundary-layer control in the geodynamo is only possible for field variations with a time scale less than  $10^4$  years. It is also shown that dipole wobble and large variations of the axial dipole moment can be accounted for by certain distributions of velocity near the outer boundary of the Earth's fluid core.

# 6. MEAN FIELD ELECTRODYNAMICS AND THE HYDROMAGNETIC DYNAMO PROBLEM

### 6.1 The hydromagnetic dynamo problem

#### 6.1.1 The dynamo equations

As was pointed out in section 1.5, the hydromagnetic dynamo problem is concerned with the simultaneous solution of the electrodynamic and the hydrodynamic equations—usually in a rotating system. These equations are summarized in section 1.5.3. Rewriting them here for convenience, we have

where

$$P = P + \frac{B^2}{2\mu} - P(5 - \frac{2}{3}\nu)\nabla \cdot u + \frac{1}{2}PI\Omega \times rI^2$$
 (6.3").

The magnetic flux density B is subject to the condition

$$\nabla \cdot \mathbf{B} = \mathbf{O} \tag{6.4}$$

At the boundary of the conducting fluid, which, in the case of the geodynamo is the core-mantle interface,

$$\mathbf{u} = \mathbf{0} \tag{6.5}$$

$$\langle B \rangle = 0$$
 (6.6)

$$\langle \mathfrak{g} \times E \rangle = 0 \qquad \qquad (6.7)$$

In the conducting part of the solid mantle, the induction equation, (6.1), is replaced by the equation

$$\partial B/\partial t = \frac{1}{\mu \sigma_m} \nabla^2 B \qquad (6.8)$$

[where  $\sigma_{\rm m}$  is the mantle conductivity], subject to the condition (6.4) and the boundary conditions (6.6) and (6.7). In the external nonconducting region, equation (6.8) reduces further to

$$\nabla^2 \hat{\mathbf{g}} = \mathbf{O} \tag{6.9}$$

subject to (6.4) and the condition

$$|\mathbf{B}| \to \phi(r^{-3}) \text{ as } r \to \infty \tag{6.10}$$

where r is measured from within the conducting region.

#### 6.1.2 The neglect of inertial terms

In most studies of hydromagnetic planetary dynamos, the Navier-Stokes equation (6.3) is simplified by neglecting the first two terms on the left hand side (Hide, 1956, 1966a; Taylor, 1963; Braginskii, 1964d, 1967b, 1970a,b, 1971; Malkus, 1963, 1967a,b; P.H. Roberts, 1967b, 1971a; Hide and Stewartson, 1972; Moffatt, 1970b, 1972; Acheson and Hide, 1973). Comparing these terms to the Coriolis force term,  $2\Omega \times \dot{u}$ , we see that

$$\frac{10 \text{y/atl}}{12 \Omega \times \text{yl}} \sim \frac{1}{2 \Omega T} \tag{6'.11}$$

$$\frac{|\mathbf{y} \cdot \mathbf{y} \mathbf{y}|}{12\Omega \times \mathbf{y}!} \sim \frac{\mathbf{u}}{2\Omega L}$$
 (6.11')

where L and T are the length and time scales of the variation of  $\underline{u}$ .

For the case of the Earth, we may follow Hide (1956) and assume that

$$T \sim 10^2 \text{ years} \sim 3 \times 10^9 \text{ sec}$$
 (6.12)

$$L \sim 3 \times 10^6 \, \text{m}.$$
 (6.12)

$$u \sim 10^{-3} \, \text{m/sec.}$$
 (6:12")

$$\Omega \sim 7 \times 10^{-5} \text{ rad/sec.} \tag{6.12}$$

[N.B. (6.12") may be an overestimate for u - see, for example, Roberts and Soward, 1972.] Substituting these

values into (6.11) and (6.11'), we have

$$\frac{1}{2\Omega T} \sim \frac{4}{2\Omega L} \sim 2 \times 10^{-6} \tag{6.13}$$

indicating that neglect of the inertial terms  $\frac{\partial y}{\partial t}$  and  $\frac{\partial y}{\partial t}$  is a reasonable approximation in the geodynamo.

#### 6.1.3 The viscous boundary layer approximation

The ratio of the magnitudes of the viscous force term  $v(\nabla^2 \dot{u} + \nabla \nabla \cdot \dot{u})$  and the Coriolis force term  $2\Omega \times \dot{u}$  in (6.3) can be scaled as follows:

$$\frac{|\mathcal{P}(\nabla^2 \mathbf{u} + \nabla \mathbf{y} \cdot \mathbf{u})|}{|2\Omega \times \mathbf{u}|} \sim \frac{\mathcal{P}}{|2\Omega \mathbf{L}^2|} \equiv \mathcal{E}$$
 (6.14)

where  $\epsilon$  is an Ekman number. For the case of the Earth, taking  $\Omega \sim 7 \times 10^{-5} \ {\rm sec}^{-1}$  and  $L \sim r_{\rm O} \sim 3 \times 10^6 \ {\rm m}$ , we see that if  $\nu << 10^9 \ {\rm m}^2 {\rm sec}^{-1}$ , then  $\epsilon << 1$ . Under these conditions, the flow in the main body of the core can be assumed inviscid.

As pointed out by Hide~(1971b) and Gans~(1972a), the kinematic viscosity v in the Earth's fluid core is one of the most obscure parameters of the Earth. Estimates in the literature range from  $10^{-7}~\text{m}^2\text{sec}^{-1}$  to  $10^{+7}~\text{m}^2\text{sec}^{-1}$  (see Hide, 1971b; Gans, 1972b). However, in recent years arguments have been advanced which reduce the uncertainty in the

probable value of v.

Gans (1972a) has calculated the value of  $\nu$  at the boundary between the inner core and the outer core, assuming that this boundary is a melting transition, and using the Andrade hypothesis. His calculations indicate that in this region

$$2.8 \times 10^{-7} \, \text{m}^2 \text{sec}^{-1} < v < 1.5 \times 10^{-6} \, \text{m}^2 \text{sec}^{-1}$$

with a suggested typical value of  $6 \times 10^{-7} \text{ m}^2\text{sec}^{-1}$ . Gans points out that if the temperature gradient in the outer core is very shallow, as suggested by Higgins and Kennedy (1971), the range of  $\nu$  will be approximately the same throughout the outer core. If, on the other hand, a steeper temperature gradient is relevant, the value of  $\nu$  in the body of the outer core will be lower than that at the inner core-outer core boundary. Gans arguments are therefore summarized by the statement that

$$v \leq 6 \times 10^{-7} \,\mathrm{m}^2 \mathrm{sec}^{-1}$$
 (6.15)

in the outer core.

Hide (1971b) has considered the value of at the core-mantle boundary. He argues that if "bumps" on the core-mantle interface strongly influence the flow in the core, as suggested by Hide and Malin (1970, 1971a,b,c), their height must exceed the viscous boundary layer thickness by a certain factor. Using the estimate for the height

of these "bumps" provided by Hide and Horai (1968), he finds that the effective kinematic viscosity (eddy plus molecular) at the core-mantle interface must satisfy

$$v_{\rm eff} \le 10^2 \, \rm m^2 sec^{-1}$$
 (6.15')

It may be noted that seismic evidence indicates that compressional waves traverse the core without suffering appreciable attenuation (Rochester, 1970). This result has led to the estimate that  $v \sim 10^5 \text{ m}^2\text{sec}^{-1}$  in the outer core. Gans (1972b) has put forward the interesting speculation that a highly viscous region 5-10 km thick at the core-mantle interface, with  $v \sim 10^7 \text{ m}^2\text{sec}^{-1}$ , would allow the seismic result to be reproduced without upsetting the requirement that v be very small in the body of the core-

If we accept *Gans*' estimate (6.15) for the kinematic viscosity in the body of the Earth's fluid core, we see from (6.14) that

$$\mathcal{E} \lesssim 5 \times 10^{-16} \tag{6.16}$$

Viscous forces will thus be negligible in the main body of the core, and the flow can be considered inviscid. However, since neglect of the viscous terms implies a lowering of the order of the Navier-Stokes equation (6.3), we can only satisfy the boundary condition (6.5) by assuming the existence of a viscous boundary layer at the surface of the core.

In the viscous boundary layer approximation, we may write

$$\ddot{u} = u^{i} + u^{b} \tag{6.17}$$

$$\mathbf{B} = \mathbf{B}^{i} + \mathbf{B}^{b} \tag{6.18}$$

for the velocity and magnetic fields in the core. Here  $(\underline{u}^i, \underline{B}^i)$  are the fields in the main body of the core, satisfying the *inviscid* equations, and  $(\underline{u}^b, \underline{B}^b)$  are fields which adjust  $\underline{u}$  and  $\underline{B}$  to satisfy the boundary conditions at the core-mantle interface.

#### 6.1.4 The approximate dynamo equations

If density gradients and temporal variations of the angular velocity  $\Omega$  are neglected in (6.3), the equations for the fields  $(\underline{u}^{\hat{1}}, \underline{B}^{\hat{1}})$  become

$$\nabla \cdot \mathbf{u}^{i} = 0 \tag{6.20}$$

$$2\Omega \times u^{i} = -\frac{1}{P} \nabla P^{i} + \frac{1}{P^{\mu}} B^{i} \cdot \nabla B^{i} + \frac{1}{P} F \qquad (6.21)$$

$$= -\frac{1}{P} \nabla P_1 + \frac{1}{P\mu} (\nabla \times B^i) \times B^i + \frac{1}{P} F \qquad (6.21')$$

$$= \frac{1}{P} \left\{ F_{B}^{i} + F - \nabla P_{i} \right\}$$
 (6.21")

where  $F_B$  denotes the Lorentz force  $\frac{1}{\mu}(\nabla \times B) \times B$ , and

$$P_{i} \equiv P - \frac{1}{2} f |\Omega \times r|^{2}$$
 (6.22)

The boundary layer fields  $(\underline{u}^b, \underline{B}^b)$  must satisfy the equations

$$\partial \underline{B}^{b}/\partial t \approx \eta \partial^{2}\underline{B}^{b}/\partial n^{2} + B_{n}\partial \underline{u}^{b}/\partial n - u_{n}\partial \underline{B}^{b}/\partial n$$
 (6.23)

$$\nabla \cdot \mathbf{u}^{\mathbf{b}} = \mathbf{O} \tag{6.24}$$

$$2\Omega \times \mathcal{U}^{b} \approx \frac{1}{\beta \mu} \frac{\partial}{\partial n} \left\{ \frac{1}{n} \times \mathcal{B}^{b} \right\} \times \mathcal{B} + \mathcal{V} \frac{\partial^{2} \mathcal{U}^{b}}{\partial n^{2}}$$
 (6.25)

where we have made the usual boundary layer approximations,

$$\nabla^2 \underline{B}^b \approx \frac{\partial^2 \underline{B}^b}{\partial n^2} \qquad (6.26)$$

$$\nabla^2 u^b \approx \frac{\partial^2 u^b}{\partial n^2} \tag{6.26'}$$

$$\nabla x \{ u \times B - u' \times B' \} \approx B_n \partial u' / \partial n - u_n \partial B' / \partial n$$

$$(6.26")$$

In equations  $(6.23)-(6.26^h)$ , n is a coordinate normal to the boundary and directed into the fluid. The components  $B_n$  and  $u_n$  are given by

$$B_n = B \cdot 1_n \tag{6.27}$$

$$u_n = u \cdot 1_n \tag{6.27'}$$

We have also made the assumption that  $\underline{u}^i$  ,  $\underline{B}^i$  ,  $\underline{F}$  , and  $p_1$  do not vary significantly across the boundary layer.

In equations (6.21) and (6.25) we have neglected the inertial terms, as discussed in section 6.1.2. The

viscous force terms, discussed in \*eetion 6.1.3, have been neglected in equation (6.21). However, these terms are retained in equation (6.25), as is necessary in a boundary layer approximation. Equations (6.19)-(6.21") are frequently referred to as the equations of the magneto-geostrophic approximation (see section 1.9.1).

# 6.2 Solution of the approximate Navier-Stokes equation in a sphere

#### 6.2.1 Preliminary manipulation

Taking the vector cross product of  $\Omega$  with equation (6.21"), and introducing a cylindrical system of coordinates  $[\mathfrak{G},\phi,z]$  with the z-axis directed along the axis of rotation, we obtain

where

$$\begin{array}{ccc}
1 & = & \Omega/|\Omega| \\
 & = & \Omega/|\Omega|
\end{array}$$

Taking the divergence of (6.28), and applying the equation of mass conservation, (6.2), we have

$$\frac{\partial}{\partial z} \left\{ P u_z^i \right\} = -\frac{1}{2\Omega} \nabla \cdot \left\{ \left( F_B^i + F \right) \times 1_z \right\}$$
 (6.30)

The z-component of equation (6.21") is

$$\frac{\partial}{\partial z} P_1 = (F_B^i + F) \cdot \frac{1}{2}$$
 (6.31)

Integrating equations (6.30) and (6.31) with respect to z we obtain

$$P_i = (P_i)_b + \int_{z_b}^{z} (F_B^i + F) \cdot 1_z dz$$
 (6.33)

In equations (6.32) and (6.33), the quantities

$$(Pu_{\bar{x}}^i)_b = Pu_{\bar{x}}^i \{ \bar{\omega}, \phi, \bar{x}_b(\bar{\omega}, \phi) \}$$
 (6.34)

$$(p_i)_b = \prod_i p_i \{ \omega, \phi, \Xi_b(\omega, \phi) \}$$
 (6.34')

are boundary values of  $\rho u_z^i$  and  $\rho_l$ .  $(\rho u_z^i)_b$  must be determined by boundary layer analysis. In all these equations,  $z_b$  represents the value of z on the boundary for a particular pair of values  $(\omega,\phi)$ .

#### 6.2.2 Boundary layer analysis

The boundary-layer equations (6.23)-(6.25) will have a consistent solution if

$$|(B_{s}^{i})_{b}|/B_{s}^{(s)} = O(1)$$
 (6.35)

$$|B_{\bullet}^{b}|/B_{\circ}^{(s)} = O(\delta/L) = O(\epsilon')$$
 (6.35')

$$|B_n^b|/B_0^{(s)} = O(\delta^2/L^2) = O(\epsilon)$$
 (6.35"

and

$$|(u_t^i)_b|/u_o = O(1)$$
 (6.36)

$$|(u_n^i)_b|/u_o = O(\delta/L) = O(\epsilon^{1/2})$$
 (6.36')

$$|u_{+}^{b}|/u_{o} = O(1)$$
 (6.36")

$$|u_n^b|/u_o = O(\delta/L) = O(E^{1/2})$$
 (6.36")

where  $\delta$  is the thickness of the boundary layer and L is the length scale of variation of the "main flow" fields  $(\underline{u}^i, \underline{B}^i)$ . In these equations,  $B_0^{(S)}$  is the average magnitude of the magnetic flux density on the boundary surface, S, and  $\underline{u}$  is the average magnitude of the tangential component of  $\underline{u}^i$  on S. The parentheses () denote the boundary value of a "main flow" quantity such as  $\underline{u}^i$  or  $\underline{B}^i$ , while the subscripts "n" and "t" denote the normal and tangential components of vectors near the boundary. The tangential components of  $\underline{u}$  and  $\underline{B}$  are defined as follows:

$$u_t = u - u_n t_n \tag{6.37}$$

$$\mathcal{B}_{t} = \mathcal{B} - \mathcal{B}_{n} \mathbf{1}_{n} \tag{6.37'}$$

If (6.35)-(6.36) are valid, and the boundary of the conducting volume is spherical, we may take components of the equations (6.23)-(6.25) in spherical polar coordinates  $[r,\theta,\phi]$  to obtain (to zero order in  $\delta/L$ )

$$\left\{2P\Omega\cos\theta\right\}u_{\theta}^{b} = \frac{1}{\mu}(B_{n}^{i})_{b}\frac{\partial}{\partial n}B_{\phi}^{b} + \beta\nu\frac{\partial^{2}}{\partial n^{2}}u_{\phi}^{b} \qquad (6.38)$$

$$\{2P\Omega\cos\theta\}u_{\phi}^{b} = \frac{1}{\mu}(B_{n}^{i})_{b}\frac{\partial}{\partial n}B_{\theta}^{b} + P\nu\frac{\partial^{2}}{\partial n^{2}}u_{\theta}^{b}$$
 (6.39)

$$\frac{\partial^{2}}{\partial n^{2}} B_{\theta}^{b} = -\mu \sigma (B_{n}^{i})_{b} \frac{\partial}{\partial n} u_{\theta}^{b}$$
 (6.40)

$$\frac{\partial^2}{\partial n^2} B_{\phi}^b = -\mu \sigma (B_n^i)_b \frac{\partial}{\partial n} u_{\phi}^b \qquad (6.41)$$

Equations (6.40) and (6.41) may be integrated, subject to the condition

$$\{u^b, B^b\} \rightarrow 0$$
 as  $n \rightarrow \infty$  (6.42)

Carrying out the integration, we have

$$\frac{\partial}{\partial n} B_{\theta}^{b} = -\mu \sigma(B_{n}^{L})_{b} u_{\theta}^{b} \qquad (6.43).$$

$$\frac{\partial}{\partial n} B_{\phi}^{b} = -\mu \sigma(B_{n}^{i})_{b} u_{\phi}^{b} \qquad (6.44)$$

Substituting (6.43) and (6.44) into equations (6.38) and (6.39), and combining the equations, we obtain

$$\frac{\partial^{2}}{\partial n^{2}}(u_{\phi}^{b}+iu_{\theta}^{b}) = \frac{2\Omega}{\nu} \left\{ \frac{\sigma}{2P\Omega} (B_{n}^{i})_{b}^{2}-i\cos\theta \right\} (u_{\phi}^{b}+iu_{\theta}^{b}) \quad (6.45)$$

Equation (6.45) has the solution

$$(u_{\phi}^{b} + i u_{\phi}^{b}) = -i(u_{\phi}^{i} + i u_{\phi}^{i})_{b} e^{-v_{n}}$$
 (6.46)

satisfying the no-slip condition at the core-mantle interface, where

$$V = \sqrt{\frac{2\Omega}{v} \left\{ \frac{\sigma}{2\rho\Omega} (B_n^i)^2 - i\cos\theta \right\}} , \text{ Re } v > 0 \quad (6.47)$$

Writing

we obtain the expressions

$$u_{\theta}^{b} = -\left\{ \left( u_{\theta}^{i} \right)_{b} \cos \left( n \operatorname{fm} v \right) + \left( u_{\phi}^{i} \right)_{b} \sin \left( n \operatorname{fm} v \right) \right\} e^{-n \operatorname{Re} v}$$
(6.48)

$$u_{\phi}^{b} = -\{(u_{\phi}^{i})_{b}\cos(n \cdot 4m\tau) - (u_{\theta}^{i})_{b}\sin(n \cdot 4m\tau)\}e^{-nRe\tau}$$
 (6.48')

$$B_{\theta}^{b} = \frac{\mu \sigma}{\Re v} (B_{n}^{i})_{b} \left\{ (u_{\theta}^{i})_{b} \cos(n \operatorname{Sm} v) + (u_{\theta}^{i})_{b} \sin(n \operatorname{Sm} v) \right\} e^{-n \operatorname{Re} v}$$

$$+ (u_{\theta}^{i})_{b} \sin(n \operatorname{Sm} v) \right\} e^{-n \operatorname{Re} v}$$

$$B_{\phi}^{b} = \frac{\mu \sigma}{Rex} (B_{n}^{i})_{b} \left\{ (u_{\phi}^{i})_{b} \cos(n \mathcal{I}_{mx}) + -(u_{\phi}^{i})_{b} \sin(n \mathcal{I}_{mx}) \right\} e^{-n \mathcal{H}_{ex}}$$

$$(6.49)_{b} \sin(n \mathcal{I}_{mx}) e^{-n \mathcal{H}_{ex}}$$

for the tangential components of the boundary-layer fields  $(\underline{u}^b, \underline{B}^b)$ . The normal components of these fields are still to, be determined.

From the incompressibility condition (6,24),

Integrating this equation with respect to n, and making use of the condition (6.42), we obtain

$$u_n^b(o) = \int_0^\infty (\nabla \cdot u_t^b) dn$$
 (6.51)

From equation (6.51) and the condition that  $t_n$  must vanish on the boundary, it follows that

$$(u_n)_b = -\int_0^\infty (\nabla \cdot u_t^b) dn \Rightarrow -\nabla \cdot \int_0^\infty u_t^b dn$$
 (6.52)

Substituting (6.46) into equation (6.52), we have

$$(u_{n}^{i})_{b} = \nabla \cdot \left\{ \frac{1}{10} \operatorname{Re} \left[ (u_{\phi}^{i} + i u_{\theta}^{i})_{b} \int_{0}^{\infty} e^{-xn} dn \right] + \frac{1}{10} \operatorname{Im} \left[ (u_{\phi}^{i} + i u_{\theta}^{i})_{b} \int_{0}^{\infty} e^{-xn} dn \right] \right\}$$

$$= \nabla \cdot \left\{ \frac{1}{10} \frac{1}{|x|^{2}} \left[ (u_{\phi}^{i})_{b} \operatorname{Re} x + (u_{\theta}^{i})_{b} \operatorname{Im} x \right] \right\}$$

$$+ \frac{1}{10} \frac{1}{|x|^{2}} \left[ (u_{\theta}^{i})_{b} \operatorname{Re} x - (u_{\phi}^{i})_{b} \operatorname{Im} x \right] \right\}$$

$$= \frac{1}{10} \frac{1}{|x|^{2}} \left[ (u_{\theta}^{i})_{b} \operatorname{Re} x - (u_{\phi}^{i})_{b} \operatorname{Im} x \right]$$

Therefore, from equations (6.53) and (6.28) the boundary value of  $\rho u_z^i$  is given by

$$(Pu_{\bar{x}}^{i})_{b} = \frac{1}{2\Omega} \left\{ (\nabla P_{i})_{b} - (F_{B}^{i} + F)_{b} \right\} \cdot 1_{\phi} \tan \theta + (6.54)$$

$$+ P \nabla \cdot \left\{ 1_{\theta} \frac{1}{|\bar{x}|^{2}} \left[ (u_{\phi}^{i})_{b} \operatorname{Re} \bar{x} + (u_{\theta}^{i})_{b} \operatorname{Im} \bar{x} \right] + 1_{\phi} \frac{1}{|\bar{x}|^{2}} \left[ (u_{\theta}^{i})_{b} \operatorname{Re} \bar{x} - (u_{\phi}^{i})_{b} \operatorname{Im} \bar{x} \right] \right\}$$

# 6.2.3 The full solution of the approximate Navier-Stokes equation

We are now in a position to obtain a complete solution to the magnetogeostrophic equation (6.21"), correct to first order in the boundary layer parameters.

Substituting (6.32) and (6.54) into equation (6.28), we obtain

$$u^{i} = \frac{1}{2\rho\Omega} \left\{ f_{B}^{i} + f \right\} \tag{6.55}$$

where

$$f_{B}^{i} \equiv \left\{ F_{B}^{i}, -\nabla \int_{Z_{B}}^{Z} F_{B}^{i} \cdot 1_{Z} dz \right\} \times 1_{Z} +$$

$$+ 1_{Z} \left\{ \left( F_{B}^{i} \right)_{b} \cdot 1_{\phi} \tan \theta + 1_{Z} \cdot \left[ \nabla \times \int_{Z_{B}}^{Z} F_{B}^{i} dz \right] \right\} +$$

$$+ 1_{Z} 2\Omega \nabla \cdot \left\{ 1_{\theta} \frac{1}{|y|^{2}} \left[ \left( u_{\theta}^{i} \right)_{b} \operatorname{Re} y + \left( u_{\theta}^{i} \right)_{b} \operatorname{Im} y \right] \right\} +$$

$$+ 1_{\phi} \frac{1}{|y|^{2}} \left[ \left( u_{\theta}^{i} \right)_{b} \operatorname{Re} y - \left( u_{\theta}^{i} \right)_{b} \operatorname{Im} y \right] \right\}$$

$$\oint_{\mathbb{R}} \equiv \left\{ F - \nabla P_{i} - \nabla \int_{\mathbb{R}_{b}}^{\mathbb{R}} F \cdot 1_{\mathbb{R}} d\mathbb{Z} \right\} \times 1_{\mathbb{R}} +$$

$$-1_{\mathbb{R}} \left\{ (F)_{b} \cdot 1_{b} \tan \theta - \nabla (P_{i})_{b} \cdot 1_{b} \tan \theta +$$

$$+ 1_{\mathbb{R}_{b}} \left[ \nabla \times \int_{\mathbb{R}_{b}}^{\mathbb{R}_{b}} F d\mathbb{Z} \right] \right\}$$

It should be noted that equation (6.55) is a recursive definition of  $\mathbf{u}^{\mathbf{i}}$ , since  $\mathbf{u}^{\mathbf{i}}$  appears on both sides of the equation. However, the terms involving  $\mathbf{u}^{\mathbf{i}}$  on the right hand side are of order  $\lfloor \delta/L \rfloor$ . The boundary layer thickness,  $\delta$ , is given by

$$\delta \sim |\mathbf{r}|^{-1} \sim \sqrt{\frac{V}{2\Omega}} \left\{ \left( \frac{\sigma B_n^{1/2}}{2 \rho \Omega} \right)^2 + \cos^2 \theta \right\}^{-\frac{V}{4}}$$
 (6.58)

For the Earth's fluid core, we may take

$$\sigma \sim 3 \times 10^5 \text{ mho/m}$$
 (6.59)

(see, for example, Gardiner and Stacey, 1971),

$$\rho \sim 10^4 \text{ kg/m}^3 \tag{6.60}$$

(see, for example, Jacobs, 1971d), and

$$(\mathfrak{B}_{n}^{i})_{b} \sim 5 \text{ G} = 5 \times 10^{-4} \text{ T}$$
 (6.61)

(see Table 2). Substituting these values into (6.58), along with the value  $\Omega \sim 7 \times 10^{-5}~\text{sec}^{-1}$ , we obtain a range of values for the boundary layer thickness as  $\theta$  varies from 0 to  $\pi/2$ .

83 
$$\sqrt{V(m^2 \cdot sec^{-1})} \lesssim \delta(m.) \lesssim 370 \sqrt{V}$$
 (6.62)

It should be noted that the upper limit on  $\delta$ , obtained by setting  $\theta=\pi/2$  in equation (6.58), is only valid if  $(B_n^i)_b$  does not become small at this value of  $\theta$ . If, on the other hand, the external magnetic field is an axial dipole,  $(B_n^i)_b \propto \cos\theta$ , and  $\delta + \infty$  as  $\theta + \pi/2$ , in the first-order boundary layer approximation.

If the Gans (1972a) estimate of the kinematic viscosity in the Earth's fluid core is used (see equation 6.15), (6.62) becomes

If, on the other hand, the Hide (1971b) estimate of the effective kinematic viscosity near the core-mantle interface is used. (see, equation 6.15'), (6.62) gives

830 m. 
$$\lesssim \delta \lesssim 3700$$
 m. (6.62")

In both cases,  $\delta << L$ , when  $L \sim r_O \sim 3 \times 10^6$  m, as expected.

6.3 Temporal behaviour of the external magnetic dipole moment

### 6.3.1 The boundary-layer control approximation

We are now in a position to examine the houndary-layer control equation (5.102) within the framework of the hydromagnetic dynamo problem. To first order in  $[\delta/L]$ , equations (6.45)-(6.47) give

$$(\nabla^{2} \mathbf{u})_{b} \approx \left\{ \frac{1}{n} \frac{\partial^{2}}{\partial n^{2}} \mathbf{u}_{\theta}^{b} + \frac{1}{n} \frac{\partial^{2}}{\partial n^{2}} \mathbf{u}_{\theta}^{b} \right\}_{\mathbf{n} = 0}$$

$$\approx \frac{1}{n} \left\{ \frac{2\Omega}{\mathcal{V}} (\mathbf{u}_{\theta}^{i})_{b} \cos \theta - \frac{\sigma}{\rho \mathcal{V}} (\mathbf{B}_{n}^{i})_{b}^{2} (\mathbf{u}_{\theta}^{i})_{b} \right\}$$

$$= \frac{1}{n} \left\{ \frac{2\Omega}{\mathcal{V}} (\mathbf{u}_{\theta}^{i})_{b} \cos \theta + \frac{\sigma}{\rho \mathcal{V}} (\mathbf{B}_{n}^{i})_{b}^{2} (\mathbf{u}_{\theta}^{i})_{b} \right\}$$

Similarly, from (6.55) we have, to first order,

$$(u^{\lambda})_{b} \approx \frac{1}{2P\Omega} \left\{ \left[ F_{B}^{i} + F_{-} \nabla P_{i} \right] \times 1_{z} \right.$$

$$- 1_{z} \left[ F_{B}^{i} + F_{-} \nabla P_{i} \right] \cdot 1_{\phi} \tan \theta \right\}_{b}$$

$$\approx \frac{1}{2P\Omega} \left\{ \left[ \frac{3}{2} \times 1_{z} - 1_{z} \frac{3}{2} \cdot 1_{\phi} \tan \theta \right] \right\}$$

$$(6) 64)$$

where

$$\mathcal{J} = \left[ \left[ F_{B}^{i} + F - \nabla P_{i} \right]_{b} \right] \tag{6.65}$$

Combining equations (6.63) and (6.64), we obtain an expression for  $(\nabla^2 u)_b$  in terms of the boundary distributions of forces and magnetic fields

$$(\nabla^{2}\underline{u})_{b} \approx -\frac{2\Omega}{\nu} \cos\theta \int_{\Gamma} x(\underline{u}^{i})_{b} -\frac{\sigma}{\rho\nu} (B_{n}^{i})^{2} (\underline{u}^{i})_{b}$$

$$\approx -\frac{1}{\rho\nu} \cos\theta \left\{ \int_{\Gamma} x(\overline{J} \times 1_{\overline{z}}) - \int_{\Gamma} x 1_{\overline{z}} J_{\phi} \tan\theta \right\}$$

$$-\frac{\sigma}{2\rho^{2}\Omega\nu} (B_{n}^{i})_{b}^{2} \left\{ J_{x} \times 1_{\overline{z}} - I_{\overline{z}} J_{\phi} \tan\theta \right\}$$

$$\approx -\frac{1}{\rho\nu} \left\{ \int_{\theta} J_{\overline{w}} \cos\theta + \int_{\phi} J_{\phi} \right\}$$

$$= -\frac{\sigma}{2\rho^{2}\Omega\nu} (B_{n}^{i})_{b}^{2} \left\{ J_{\theta} \frac{J_{\phi}}{\cos\theta} - J_{\phi} J_{\overline{w}} \right\}$$

$$(6.66)$$

From the multipole expansion (5.66) of B on the boundary of the conducting volume, and condition (6.35),

$$(B_n^i)_b \approx (\hat{B}_n)_b \approx \frac{\mu}{2\pi r_o^3} \tilde{T}^{(i)} \cdot \frac{1}{r} + O\left\{\frac{\mu}{r_o^4} |\tilde{T}^{(i)}|\right\}$$

$$(6.67)$$

Substituting (6,66) and (6,67) into the boundary-layer control equation (5,102), with  $\alpha = 0$ , we obtain

$$\tilde{T}^{(i)} \approx \frac{3\eta}{4\pi r_o^3} \int_{S} (\nabla^2 u)_b \, \mathring{1}_r \cdot \tilde{T}^{(i)} \, dS$$

$$\approx -\frac{3\eta}{4\pi r_o^3 \rho_V} \, \tilde{T}^{(i)} \cdot \int_{S} \left\{ \mathring{1}_r \mathring{1}_o \, \Im_{\varpi} \cos \theta + \mathring{1}_r \mathring{1}_o \, \Im_{\varphi} \right\} dS +$$

$$-\frac{6\mu}{\rho^2 \Omega \, \nu \, (4\pi r_o^3)^3} \left\{ \tilde{T}^{(i)} \right\}^3 \cdot \int_{S} \mathring{1}_r^3 \left\{ \mathring{1}_o \, \frac{\Im_{\varphi}}{\cos \theta} - \mathring{1}_{\varphi} \, \Im_{\varpi} \right\} dS$$

## 6.3.2 The boundary force distribution in the geodynamo

In the geodynamo,

$$\vec{\mathcal{F}} = \left\{ \vec{P} \cdot \vec{Q} - \vec{\nabla} \cdot \vec{P} + \frac{1}{2} \vec{P} \cdot \vec{\nabla} (\Omega^2 \vec{\omega}^2) - \vec{P} \cdot \vec{\Omega} \times \vec{r} + \vec{F}_B + \vec{F}_{other} \right\}_b (6.69)$$

where g is the acceleration due to gravity. Assuming hydrostatic balance in (6.69), to first order, we obtain

$$\mathcal{F} = \left\{ F \Omega^2 \omega \mathcal{I}_{\omega} - P \dot{\Omega} \times r + F_B + F_{\text{other}} \right\}_b \qquad (6.70)$$

where f represents the fraction of the centrifugal force which does not contribute to the hydrostatic balance.

Taking components of (6.70) in cylindrical coordinates, we have

$$3_{\omega} = \left\{ \tilde{\xi} P \Omega^{2} \omega + (\tilde{\xi}_{8})_{\omega} + (\tilde{\xi}_{other})_{\omega} \right\}_{b}$$

$$(6.71)$$

$$3_{\phi} = \left\{ -P \Omega \omega + (\tilde{\xi}_{8})_{\phi} + (\tilde{\xi}_{other})_{\phi} \right\}_{b}$$

We may now estimate the various terms in (6.71) and (6.72). The Lorentz force at the core-mantle interface,  $(\mathbf{F}_{\mathrm{B}})_{\mathrm{b}}$ , is given by

$$\left\{ \left( \mathbf{F}_{\mathbf{B}} \right)_{\mathbf{\omega}} \right\}_{\mathbf{b}} = \left\{ \mathbf{j}_{\phi} \mathbf{B}_{\mathbf{z}} - \mathbf{j}_{\mathbf{z}} \mathbf{B}_{\phi} \right\}_{\mathbf{b}}$$

$$\left\{ \left( \mathbf{F}_{\mathbf{b}} \right)_{\phi} \right\}_{\mathbf{b}} = \left\{ \mathbf{j}_{\mathbf{z}} \mathbf{B}_{\mathbf{\omega}} - \mathbf{j}_{\mathbf{\omega}} \mathbf{B}_{\mathbf{z}} \right\}_{\mathbf{b}}$$

$$\left( 6.73^{\circ} \right)$$

Assuming that the external medium is a nonconductor, we have

$$(\mathbf{n} \cdot \mathbf{j})_{\mathbf{b}} = \mathbf{0} \tag{6.74}$$

or, for a spherical boundary,

$$(j_{\overline{\omega}})_{b} \sin \theta = \frac{1}{\mu} \left\{ \frac{1}{\omega} \frac{\partial}{\partial \phi} B_{\overline{z}} - \frac{\partial}{\partial \overline{z}} B_{\phi} \right\}_{b} \sin \theta$$

$$= -(j_{\overline{z}})_{b} \cos \theta = \frac{1}{\mu} \left\{ \frac{1}{\omega} \frac{\partial}{\partial \phi} B_{\omega} - \frac{1}{\omega} \frac{\partial}{\partial \omega} (\omega B_{\phi}) \right\}_{b} \cos \theta$$

$$(6.74')$$

Substituting (6.74') into (6.73'), we obtain

$${}^{\uparrow} \left\{ \left( \mathbb{E}_{\mathbf{B}} \right)_{\phi} \right\}_{b} = \frac{(j_{\mathbf{B}})_{b}}{\sin \theta} \left\{ \mathbb{E} \cdot \underline{n} \right\}_{b} \tag{6.75}$$

where, from (6.74'),

$$\langle (j_z)_b \sim \frac{1}{\mu} \left\{ \frac{1}{\omega} \frac{\partial}{\partial \omega} (\omega B_{\phi}) \right\}_b \qquad (6.76)$$

Furthermore,

$$(j_{\phi})_{b} = \frac{1}{\mu} \left\{ \frac{\partial}{\partial z} B_{w} - \frac{\partial}{\partial \omega} B_{z} \right\}_{b} \tag{6.77}$$

As may be seen from Table 2, the toroidal magnetic field at the core-mantle interface is expected to be much smaller than the poloidal field. Within the framework of the boundary-layer control approximation, we may take

$$(B_{\varpi})_{b} \sim (B_{\Xi})_{b} \sim B_{o}^{(3)} \sim 5 \times 10^{-4} \text{ T.}$$
 (6.78)

We may also take -

$$\left(\frac{\partial^2 B_{cs}}{\partial z}\right)_b \sim \left(\frac{\partial B_z}{\partial \omega}\right)_b \sim B_o^{(s)}/L \sim 2 \times 10^{-10} \text{ T/m}$$
 (6.79)

and

$$\left\{\frac{1}{\omega}\frac{\partial}{\partial\omega}(\omega B_{\phi})\right\}_{b} \sim \left\{\frac{\partial B_{\phi}}{\partial\omega}\right\}_{b} \leq \frac{B_{\phi}}{L} \sim 3 \times 10^{-9} \text{ T/m}.$$
 (6.79')

where  $B_0 \sim 10^{-2}$  T is the magnitude of the field deep in the core. (6.79') may well be an overestimate, as it seems unlikely that the toroidal field increases linearly from its value at the core-mantle interface to its value deep in the core. Substituting (6.78)-(6.79') into (6.73) and (6.75), we have

$$\{(F_B)_{\overline{w}}\}_b \sim \{B_o^{(5)}\}^2/\mu L \sim 7 \times 10^{-8} \text{ nt/m}^3$$

$$\{(F_B)_{\phi}\}_b \lesssim B_o B_o^{(5)}/\mu L \sim 1 \times 10^{-6} \text{ nt/m}^3$$

$$(6.81)$$

The remaining terms in (6.70) may be evaluated using the estimates

$$\rho \sim 10^4 \text{ kg/m}^3$$

$$L \sim 3 \times 10^6 \text{ m} \qquad (6.82)$$

$$\Omega \sim 7 \times 10^{-5} \text{ rad/sec}$$

and

O

$$\hat{\Omega} \sim 2 \times 10^{-21} \text{ rad/sec}^2$$
 (6.83)

(6.83) for  $\dot{\Omega}$  corresponds to the slow increase in the length of the day. Substituting these values into (6.71), and (6.72), we obtain

$$f\Omega^2 \approx -f\Omega^2 L \sim 150 \text{ mt/m}^3$$
 (6.84)

The forces denoted by  $F_{\text{other}}$  in equations (6.69)(6.72) can only be estimated in specific models. We shall include the precessional force term defined in (1.68) as an example. From (1.68'),

$$F_{P} \approx P\left\{(\Omega' \times \Omega) \times r - \frac{1}{2} \nabla \left[(2\Omega + \Omega') \times r\right] - \left[\Omega' \times r\right]\right\}$$
(6.86)

Assuming that the gradient term in (6.86), and a fraction  $[1-\frac{1}{\zeta}]$  of the term  $\rho[(\Omega'\times\Omega)\times\chi]$  are included in the hydrostatic balance in (6.69), we obtain

Follow 
$$\approx \frac{1}{5} P\{(\Omega' \times \Delta) \times r\}$$
 (6.87)

This term will have components in both the  $\frac{1}{20}$  and the  $\frac{1}{20}$  directions. The magnitude of these contributions can be estimated as

where  $[\Omega']$  sinx] is the magnitude of the equatorial component of  $\Omega'$ . Malkus (1971a) gives the values

$$\Omega'$$
  $\sqrt{23.5}$  rad/sec (6.89)

Using these values in (6.88), in conjunction with the values (6.82), we obtain

### 6.3.3 Radial forces

We may now consider the effects of the  $\mathfrak{a}$ -component of the boundary force distribution in the geodynamo on the temporal behaviour of the magnetic dipole moment. Ignoring the azimuthal component of  $\mathfrak{Z}$ , we have from (6.68) that

$$\frac{T^{(1)}}{2} \approx -\frac{3\eta}{4\pi r_0^3 \rho_V} T^{(1)} \cdot \int_{S} \frac{1}{r} r_0^4 J_{\infty} \cos \theta \, dS \qquad (6.91)$$

$$+ \frac{6\mu}{\rho^2 \Omega \nu (4\pi r_0^3)^3} \left\{ T^{(1)} \right\}^3 \cdot \int_{S} \frac{1}{r} \frac{1}{r} \int_{\Phi} J_{\infty} \, dS$$

From equations (6.71) and (6.88),

$$\exists \alpha \approx f(f\Omega_{2}\alpha)^{p} + \{(fB)\alpha\}^{p} + \frac{1}{2}\{f(\alpha)^{2}\alpha(\alpha)^{2$$

The last term on the right hand side of (6.92) will not contribute to the first integral in (6.91), since

$$\int_{S} \varpi \, 1 \varpi \, 1 r \, 1_{\theta} \cos \theta \, dS$$

$$= r_{\theta} \int_{S} (1_{x} \cos \phi + 1_{y} \sin \phi) \, 1_{r} \, 1_{\theta} \sin \theta \cos \theta \, dS$$

$$= 0$$

(6.93)

as may be seen from detailed evaluation of the integrals, bearing in mind that

$$\int_{S} f(\theta, \phi) dS \approx r_o^2 \int_{0}^{\pi} \sin \theta d\theta \int_{0}^{2\pi} f(\theta, \phi) d\phi , \qquad (6.94)$$

After the  $\phi$ -integration has been carried out in (6.93), the only terms remaining are proportional to

$$\left\{ \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} + \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \right\} \sin^2 \theta \cos^3 \theta$$

and  $\left\{ \frac{1}{2} \frac{1}{2} \frac{1}{2} - \frac{1}{2} \frac{1}{2} \frac{1}{2} \right\} \sin^4 \theta \cos \theta$ 

When the  $\theta$ -integration is carried out, both these terms vanish. Equation (6.92) may therefore be rewritten

$$\mathcal{J}_{\omega}^{\text{eff}} \approx \mathbb{I}(P\Omega^2 \omega)_b + \{(F_B)_{\omega}\}_b$$
 (6.95)

force term in (6.95) will be negligible provided that

$$\mathfrak{F} \gg 5 \times 10^{-10} \tag{6.96}$$

When (6.96) is valid, equation (6.91) becomes

$$\tilde{T}^{(i)} \approx -\frac{3\eta}{4\pi r_o^3 \rho_V} \tilde{T}^{(i)} \cdot \int_{S} \frac{1}{r_o^3} \tilde{\xi} P \Omega^2 \omega \cos \theta \, dS \qquad (6.97)$$

$$+ \frac{6\mu}{\rho^2 \Omega \nu (4\pi r_o^3)^3} \left\{ \tilde{T}^{(i)} \right\}^3 \cdot \left\{ \tilde{I}_r^3 \stackrel{1}{1}_{\Phi} \right\}_{\Phi} dS$$

or, expanding the first term,

$$\tilde{T}^{(i)} \approx -\frac{1}{5} \xi \frac{\eta \Omega^{2}}{v} \{ T_{x}^{(i)} \mathbf{1}_{x} + T_{y}^{(i)} \mathbf{1}_{y} - 2 T_{z}^{(i)} \mathbf{1}_{z} \} + \frac{6\mu}{\rho^{2} \Omega v (4\pi r_{o}^{3})^{3}} \{ \tilde{T}^{(i)} \}^{3} \cdot \int_{S} \mathbf{1}_{r}^{3} \mathbf{1}_{\phi} \mathcal{F}_{w} dS$$
(6.97')

Taking components of (6.97), we have

$$T_{x}^{(i)} \approx -\frac{1}{5} \xi \frac{\eta \Omega^{2}}{\nu} T_{x}^{(i)} \left\{ 1 + \frac{6\mu}{\eta^{2} \Omega (4\pi r_{o}^{3})^{2}} |\mathcal{T}^{(i)}|^{2} \right\}$$
 (6.98)

$$T_y^{(i)} \approx -\frac{1}{5} \xi \frac{\eta \Omega^2}{\nu} T_y^{(i)} \left\{ 1 + \frac{6\mu}{\eta \rho \Omega (4\pi r_o^3)^2} |T^{(i)}|^2 \right\}$$
 (6.98')

$$T_z^{(i)} \approx \frac{2}{5} \xi \frac{\eta \Omega^2}{V} T_z^{(i)}$$
 (6.98")

The nonlinear terms in (6.98) and (6.98') have been obtained by evaluating the second integral in (6.97) and (6.97). It can be shown that the precessional force term in (6.92) does not contribute to this integral, so that (6.95) is once again valid. As for the linear terms, the Lorentz force contribution has been ignored, subject to the assumption (6.96).

The characteristic time associated with variations governed by (6,98") is

$$\tau \sim \sqrt{\frac{5\nu}{2\xi\eta\Omega^2}} \tag{6.99}$$

For the geodynamo,

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$$\tau \sim \sqrt{5/3\xi} \times 10^5 \text{ sec}$$
 (6.99')

using the Hide (1971b) value (6.15') for the kinematic

viscosity at the core-mantle interface, the values (6.82), and the estimate

$$\eta \sim 3 \text{ m}^2 \text{sec}^{-1^{*}}$$
 (6.100)

for the magnetic diffusivity in the core.

It follows from equation (6.99') that radial forces can only account for dipole moment variations on a time scale of  $10^3$  years  $\sim 3 \times 10^{10}$  seconds if

$$\xi \sim 2 \times 10^{-11}$$
 (6.101)

However, this requirement is in direct contradiction to assumption (6.96). Thus there is no possibility of accounting for temporal variations of the geomagnetic dipole moment on scales  $\sim 10^3$  years in terms of radial forces alone unless the Lorentz force terms are included in equation (6.95).

the Lorentz force terms in equation (6.95) can only be evaluated if the spatial behaviour of the internal magnetic field near the boundary is known. Inclusion of these terms must therefore destroy the "closs ature of the boundary layer control approximation, and the time dependence of the external potential field to the behaviour of the internal magnetic field, as well as to the body force density at the core-mantle interface. It follows that if azimuthal forces at the core-mantle interface are neglected, temporal variations of the geomagnetic dipole moment on scales ~10<sup>3</sup> years cannot be accounted for in the "closed"

boundary-layer control approximation.

## 6.3.4 Azimuthal forces, dipole wobble, and reversals

We shall now consider the effects of the  $\phi$ -component of the boundary force distribution in the geodynamo on the temporal behavior of the magnetic dipole moment. Ignoring the  $\phi$ -component of 3 in equation (6.68), we have

$$\tilde{T}^{(i)} \approx -\frac{3\eta}{4\pi r_o^3 \rho \nu} \tilde{T}^{(i)} \cdot \int_{S} 1_r 1_{\phi} J_{\phi} dS + \frac{6\mu}{\rho^2 \Omega \nu (4\pi r_o^3)^3} \{\tilde{T}^{(i)}\}^3 \cdot \int_{S} 1_r^3 1_{\theta} \frac{J_{\phi}}{\cos \theta} dS$$
(6.102)

From equations (6.72) and (6.88),

$$\frac{1}{2} \approx -(\mathcal{L} \Omega \varpi)^{P} + \{(\mathcal{L}^{B})^{\Phi}\}^{P} + \frac{1}{2} \{\mathcal{L} \Omega \times (\mathcal{U}_{1} \times \mathcal{U}_{2}) \times \mathcal{L}_{2}\}^{P}$$

$$\approx -(\mathcal{L} \Omega \varpi)^{P} + \{(\mathcal{L}^{B})^{\Phi}\}^{P} - \frac{1}{2} \{\mathcal{L} \Omega \times (\mathcal{U}_{1} \times \mathcal{U}_{2}) \times \mathcal{L}_{2}\}^{P}$$

$$(6.103)$$

$$-\frac{1}{2} \{\mathcal{L} \Omega \times (\mathcal{L}^{B})^{\Phi}\}^{P} + \frac{1}{2} \{\mathcal{L} \Omega \times (\mathcal{U}_{1} \times \mathcal{U}_{2}) \times \mathcal{L}_{2}\}^{P}$$

In the "closed" boundary layer approximation, we must neglect the Lorentz force term,  $\{(F_B)_{\phi}\}_b$ , in equation (6.103). As may be seen from (6.81), (6.85), and (6.90), it is not clear that neglect of  $\{(F_B)_{\phi}\}_b$  is a good approximation. However, if the toroidal magnetic field satisfies

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the condition

$$\left|\left\{\frac{\partial \mathbf{B}^{\text{toroidal}}}{\partial \boldsymbol{\omega}}\right\}_{\mathbf{b}}\right| \ll \left|\left\{\frac{\mu P \Omega \boldsymbol{\omega}}{(\mathbf{B} \cdot \mathbf{n})}\right\}_{\mathbf{b}}\right| \sim 10^{-13} \text{ T/m} \qquad (6.104)$$

or if

$$\{(F_B)_{\phi}\}_{\phi} \propto P_{2m+1}(\cos\theta) \sin^{2n}\phi \cos^{2k}\phi$$
 (6.11.05)

so that  $\{(\mathbf{F}_{\mathrm{B}})_{\phi}\}_{\mathrm{b}}$  makes no contribution to the integrals in equation (6.102), then the azimuthal Lorentz force term may be neglected in (6.103), and the "closed" boundary layer approximation is valid.

Substituting (6.103) into (6.102) and assuming that at least one of the conditions (6.104)~(6.105) is valid in the geodynamo, we obtain

$$\begin{split} \ddot{T}_{\chi}^{(i)} &\approx -\frac{\eta \dot{\Omega}}{\nu} T_{y}^{(i)} + \frac{\eta \dot{\Omega} \dot{\Omega}_{x}^{i}}{25_{h}\nu} T_{z}^{(i)} + \\ &+ \frac{6\mu \dot{\Omega}}{5\rho \dot{\Omega} \sqrt{(4\pi r_{o}^{2})^{2}}} [T^{(i)}]^{2} T_{x}^{(i)} + \\ &+ \frac{3\mu}{105_{h}\rho_{\nu}(4\pi r_{o}^{2})^{2}} T_{z}^{(i)} \left\{ \dot{\Omega}_{y}^{i} (3T_{x}^{(i)^{2}} + T_{y}^{(i)^{2}} + 2T_{z}^{(i)^{2}}) + \\ &- 2\dot{\Omega}_{x}^{i} T_{x}^{(i)} T_{y}^{(i)} \right\} \end{split}$$

$$\ddot{T}_{y}^{(i)} \approx \frac{\eta \dot{\Omega}}{\nu} T_{x}^{(i)} + \frac{\eta \dot{\Omega} \dot{\Omega}_{y}^{i}}{25_{h}\nu} T_{z}^{(i)} + \\ &+ \frac{6\mu \dot{\Omega}}{5\rho \dot{\Omega} \nu (4\pi r_{o}^{3})^{2}} [T^{(i)}]^{2} T_{y}^{(i)} + \\ &- \frac{3\mu}{105_{h}\rho_{\nu}(4\pi r_{o}^{3})^{2}} T_{z}^{(i)} \left\{ \dot{\Omega}_{x}^{i} (T_{x}^{(i)^{2}} + 3T_{y}^{(i)^{2}} + 2T_{z}^{(i)^{2}}) + \right\} \end{split}$$

$$(6.106')$$

 $-2\Omega'_{y}T_{x}^{m}T_{y}^{m}$ 

$$\frac{T_{z_{0}}^{(i)}}{5P\Omega\nu(4\pi r_{o}^{3})^{2}} T_{z_{0}}^{(i)} \left\{ 2\left(T_{x_{0}}^{(i)2} + T_{y_{0}}^{(i)2}\right) + T_{z_{0}}^{(i)2} \right\} + \frac{6\mu}{55P\nu(4\pi r_{o}^{3})^{2}} |T_{0}|^{2} \left\{ \Omega_{x}^{\prime} T_{y_{0}}^{(i)} - \Omega_{y}^{\prime} T_{x_{0}}^{(i)} \right\} (6.106'')$$

on carrying out the integrations.

When the nonlinear terms are neglected in (6.106) and (6.106'), the equations can be written in the form

$$T_{eg}^{(i)} \approx i \frac{\eta \dot{\Omega}}{v} T_{eg}^{(i)} + \frac{\eta \Omega \Omega'}{2v \zeta_b} T_z^{(i)} e^{i \Omega' t} \sin \chi \qquad (6.107)$$

where

$$T_{eg}^{(i)} \equiv T_{x}^{(i)} + i T_{y}^{(i)}$$
 (6.108)

In equation (6.107) we have assumed that the equatorial component of the Earth's precession can be represented by

$$\Omega_{\mathbf{x}}' + i \Omega_{\mathbf{y}}' = (\Omega' \sin \mathbf{x}) e^{-i\Omega' t}$$
 (6.109)

where  $\Omega'$  and  $\chi$  are the quantities defined in (6.89) and (6.89').

The peneral solution of equation (6.108) is  $T_{eq}^{(i)} = A_i e^{(i-i)\sqrt{\frac{\eta_i\dot{\Omega}_i}{2\dot{\nu}}}} + A_2 e^{(i-i)\sqrt{\frac{\eta_i\dot{\Omega}_i}{2\dot{\nu}}}} + \frac{\eta_i\Omega_i^{\prime}(s_i)}{2\left(\Omega_i^{\prime 4} + \eta_i^2|\dot{\Omega}_i|^2/v^2\right)\sqrt{3}} T_{z}^{(i)} e^{-i\Omega_i^{\prime 4}}$ (6:110)

where A<sub>1</sub> and A<sub>2</sub> are complex constants. Thus a typical

solution will be of the form

$$T_{x}^{(i)} = \left\{ A_{i}^{\prime} \cos x't - A_{i}^{\prime} \sin x't \right\} e^{-x't} + \frac{\eta \Omega \Omega^{\prime} \sin x}{2\nu \zeta_{b} \left\{ \Omega^{\prime 4} + 4x'^{4} \right\}} T_{x}^{(i)} \left\{ \Omega^{\prime 2} \cos \Omega^{\prime} t + 2x'^{2} \sin \Omega^{\prime} t \right\}$$

$$T_{y}^{(i)} = \left\{ A_{i}' \sin x't + A_{2}' \cos x't \right\} e^{-x't} + \frac{\eta \Omega \Omega' \sin x}{2\nu \zeta_{b} \left\{ \Omega'^{4} + 4x'^{4} \right\}} T_{z}^{(i)} \left\{ \Omega'^{2} \sin \Omega't - 2x'^{2} \cos \Omega't \right\}$$

where  $A_1$  and  $A_2$  are real constants, and

$$\dot{\mathbf{Y}} \equiv \sqrt{\eta |\dot{\Omega}|/2\nu} \tag{6.112}$$

In deriving (6.111) and (6.111') from (6.110), we have retained only those terms which represent precession of the equatorial dipole moment with angular frequency  $\Omega^{\bullet}$ , and eastward drift with angular frequency  $\gamma^{\bullet}$ . (It should be noted that in (6.110) we have assumed that  $\dot{\Omega} < 0$ , as is the case in the geodynamo.) From equation (6.112), the period of eastward drift is given by

$$T_{e.d.} = 2\pi/\delta' = 2\pi\sqrt{22/\eta |\dot{\Omega}|}$$
 (6.113)

Substituting the estimates (6.83) and (6.100) into (6.113) we obtain the period

for the geodynamo.

Although the geomagnetic dipole axis has apparently drifted in a westward direction since 1700 A.D. (Rawai and Hiroska, 1967); prior to 1600 A.D. the drift was apparently eastward (Kawai and Hiroska, 1967; Marton, 1970). Several estimates have been made of the period of this eastward drift. For example, Kawai and Hiroska (1967) obtain the period Te.d. 1500 years, while Marton (1970) obtains Te.d. 1800 years. Fudovkin and Valuyeva (1967, 1982), using an eccentric dipole model with an elliptical drift trajectory, obtain the period T ~ 1200 years (it would be inapproximate to refer to this model as one of "eastward drift"). Substituting these estimates into (6.113'), we obtain estimates of the kinematic viscosity at the coremantle interface.

$$T = 1200 \text{ years} \rightarrow v \sim 1.0 \text{ m}^2/\text{sec}$$
 (6.114)  
 $T = 1500 \text{ years} \rightarrow v \sim 1.6 \text{ m}^2/\text{sec}$  (6.114')  
 $T = 1800 \text{ years} \rightarrow v \sim -2.3 \text{ m}^2/\text{sec}$  (6.114")

These values are consistent with the estimate of Hide (1971b) that the kinematic viscosity at the core-mantle interface is  $\leq 10^2$  m²/sec. From (6.62) we see that the estimates of  $\nu$  given in (6.114)-(6.114") imply that the boundary layer thickness at the core-mantle interface lies in the range 100 m  $\leq \delta \leq 600$  m, giving good agreement with Hide's estimate  $\delta < 1$  km.

In obtaining equations (6.111) and (6.111') from equation (6.110), we have ignored the terms which lead to westward drift with the angular frequency  $\gamma'$ . However, these terms may well be important for explaining the observed behaviour of the geomagnetic dipole. The data presented by Kawai and Hirooka (1967) appear to indicate that the amplitude of the equatorial dipole increases during periods of westward drift. It may be seen from equation (6.110) that westward drift with angular frequency  $\gamma'$  is associated with growing solutions, whereas eastward drift is associated with decaying solutions. A combination of the two types of solution might well account for the behaviour described by Kawai and Hirooka.

Westward drift also arises from the second group of terms in (6.111) and (6.111'). These terms are associated with the precession of the Earth's axis of rotation at the angular frequency  $\Omega'$ , corresponding to a period

$$T_{\rm pr} \sim 25,800 \text{ years}$$
 (6.115)

(Malkus, 1971a). In order to ensure that these terms do not dominate the terms described in the last paragraph, we must require that

$$\frac{\eta \Omega \Omega' \sin \chi}{2 \nu \zeta_b \sqrt{\Omega'^4 + 4 \kappa'^4}} \ll \frac{|T_{eq}^{(i)}|}{|T_{eq}^{(i)}|} \sim \tan\{11.5^{\circ}\} \sim 0.2$$
 (6.116)

or, making use of the values (6.82), (6.83), (6.89), (6.89), and (6.100), and the value of  $\nu$  given in (6.114),

$$\frac{1}{\zeta_b} \ll 3 \times 10^{-6}$$
 (6.116')

Thus nearly all the precessional borque on the core fluid at the core-mantle interface must be balanced. It is interesting to note that if the value of  $\zeta$  used by Malkus'(1971a) for the flow in the main body of the core  $(\zeta = 4)$  is used in place of  $\zeta_b$  in (6.116), the inequality can only be satisfied if  $v >> 7 \times 10^6 \text{ m}^2/\text{sec}$ .

The effect of the nonlinear terms in (6.106) and (6.106') can be assessed fairly simply if the dipole moment is predominantly axial. Under these circumstances, the magnitude of  $\mathbf{T}^{(1)}$  is approximately independent of  $\mathbf{T}^{(1)}_{\mathbf{X}}$  and  $\mathbf{T}^{(1)}_{\mathbf{Y}}$ . If (6.116') is valid, only the first nonlinear term in each equation need be considered. The effect of these terms will be to introduce a long-period modulation in the solution given in (6.110). The period of this modulation can be estimated as

$$T_{\text{mod}} \sim 4\sqrt{2} \pi \left\{ \eta |\dot{\Omega}|_{V} \right\}^{1/2} \left\{ \frac{10 f \Omega V_{M}}{3|\dot{\Omega}|B_{n}^{2}} \right\}$$

~ 8 × 1012 Sec. ~ 3 × 105 years

(6.117)

There will also be growth and/or decay on this time scale.

If the dipole moment is predominantly axial, equation (6.106"), which describes the behaviour of  $T_z^{(1)}$  may be rewritten approximately as

$$\hat{T}_{z}^{(i)} \approx P T_{z}^{(i)}^{3} \qquad (6.118)$$

where

$$P = \frac{4\mu |\dot{\Omega}|}{5f\Omega v (4\pi r_o^3)^2}$$
 (6.118')

Carrying out the first integration, we obtain

$$\left\{\dot{T}_{z}^{(i)}\right\}^{2} - \left\{\dot{T}_{z}^{(i)}\right\}_{o}^{2} = \frac{1}{2}P\left\{\left[T_{z}^{(i)}\right]^{4} - \left[T_{z}^{(i)}\right]_{o}^{4}\right\}$$
 (6.119)

indicating that the axial dipole moment varies on time scales of the order

$$\tau \sim \frac{1}{|T_z^{(i)}|} \sqrt{P/2} \sim \frac{1}{|T_z^{(i)}|} \sqrt{\frac{5\rho\Omega\nu(4\pi r_s^3)^2}{4\mu |\dot{\Omega}|}}$$
$$\sim \frac{1}{|B_n|} \sqrt{\frac{10\rho\Omega\mu\nu}{|\dot{\Omega}|}}$$

~ 1.3 x 10" seconds ~ 
$$4 \times 10^3$$
 years (6.120)

As may be seen from Table 13, the time scale given in (6.120) is similar to that characterizing the behaviour of the axial dipole moment during a reversal.

If, on the other hand, the axial dipole moment is small compared with the equatorial dipole moment, equation (6.106") is approximately linear in  $T_z^{(1)}$ . The solution to the equation will be of the form

$$T_{z}^{(i)} \approx a_{i}' e^{t/\tau_{i}} + a_{2}' e^{-t/\tau_{i}}$$
 (6.121)

where

$$\tau_{i} = \sqrt{\frac{5\rho\Omega\nu_{\mu}}{2B_{n}^{2}|\dot{\Omega}|}} \sim |B_{n}|^{-1} T \text{ year}$$
 (6.121')

where  $|B_n|$  represents the typical magnitude of the predominantly equatorial dipole field at the core-mantle interface. If  $|B_n|$  lies in the range

$$1 \times 10^{-4} \text{ T} \lesssim |B_n| \lesssim 5 \times 10^{-4} \text{ T}$$
 (6.122)

then

$$1 \times 10^4 \text{ y.} \gtrsim \tau_1 \gtrsim 2 \times 10^3 \text{ y.}$$
 (6.123)

and the time scale of variation of the axial dipole moment will be of the same order of magnitude as that estimated in (6.120).

Summarizing the results of this section, we may state that the azimuthal force term  $-\rho(\hat{\Omega}\times r)$  has a considerable influence on the temporal behaviour of the geomagnetic dipole moment. The linear terms in the equations for the equatorial components of the dipole moment account for the dipole wobble reported by Kawai and Hirooka (1967) if the kinematic viscosity at the core-mantle interface is of the order  $\nu \sim 1 \text{ m}^2/\text{sec}$ . When this value of  $\nu$  is assumed, the nonlinear terms in the equations for the equatorial geomagnetic dipole give rise to modulations on the time scale  $3 \times 10^5$  years – which is of roughly the same order as the observed interval between polarity reversals during the last 50 m.y. Finally, when the value of  $\nu$  implied by the dipole wobble is used, the

equation for the axial dipole moment indicates that the axial dipole can vary on time scales similar to those which characterize polarity transitions. It appears, therefore, that a detailed examination of simultaneous solutions to equations (6.106)-(6.106"), with the precessional force terms omitted, may well lead to a better understanding of dipole moment variations. However, before any great importance can be attached to variations predicted by these equations on time scales >> 10<sup>4</sup> years, it will be necessary to include estimates of dissipative terms, as was pointed out in section 5.5.1.

We shall not carry our investigation of the boundary layer control approximation any further in this thesis.

(6.125)

Effects of an inhomogeneous turbulent force distribution outside the boundary layer in the geodynamo

#### The fluctuating dynamo equations

In the mean field electrodynamic approach, the dynamo equations (6.1)-(6.4) become

$$= \frac{1}{2} \left[ \left[ \left( \vec{\Delta} \times \vec{B}_i \right) \times \vec{B}_i - \left( \vec{\Delta} \times \vec{B}_i \right) \times \vec{B}_i \right] + \left( \vec{\Delta} \times \vec{B}_i \right) \times \vec{B}_i + \left( \vec{\Delta} \times$$

$$\nabla \cdot \mathbf{u}' = -\{\nabla P/R\} \cdot \mathbf{u}' \tag{6.127}$$

$$\nabla \cdot \vec{B} = 0 \tag{6.129}$$

$$[\%c - \eta \nabla^2] \overline{U} + [\overline{U} \cdot \nabla \overline{U} + \overline{U'} \cdot \nabla \overline{U'}] + 2\Omega \times \overline{U} = (6.130)$$

In the hydromagnetic first order smoothing approximation, the fluctuating dynamo equations (6.124)-(6.127) become

$$\nabla \cdot \mathbf{B}' = \mathbf{O} \tag{6.134}$$

$$\nabla \cdot \mathbf{u}' = -\left\{ \nabla P/\rho \right\} \cdot \mathbf{u}' \tag{6.135}$$

It should be noted that in these equations the density is not assumed to have a fluctuating component.

### 6.4.2 The first-order solution of the fluctuating dynamo equations

Making use of the formalism developed in Chapter 4, and the Fourier-Stieltjes transforms (4.7a,b), we may rewrite equations (6.132)-(6.135) in the form

 $(i\omega + \eta k^2) \beta \{d \Upsilon^{(o)} + d \Upsilon^{(i)} + ...\} - 2i\eta k \nabla \beta \{d \Upsilon^{(o)} + d \Upsilon^{(i)} + ...\} +$   $- \eta \nabla^2 \beta \{d \Upsilon^{(o)} + d \Upsilon^{(i)} + ...\}$ 

$$\begin{split} & - \{ \vec{n} \cdot [q\vec{x}_{\omega} + q\vec{x}_{\omega} + \cdots] \} \cdot \Delta \vec{B} + \{ \vec{B} \cdot [q\vec{\lambda}_{\omega} + q\vec{\lambda}_{\omega} + \cdots] \} \cdot \Delta \vec{n} \\ & - i(\vec{k} \cdot \vec{n}) \vec{B} \cdot \{ q\vec{\lambda}_{\omega} + q\vec{\lambda}_{\omega} + \cdots \} - \vec{n} \cdot \Delta \vec{B} \cdot \{ q\vec{\lambda}_{\omega} + q\vec{\lambda}_{\omega} + \cdots \} + \\ & = i(\vec{k} \cdot \vec{B}) \vec{n} \cdot \{ q\vec{x}_{\omega} + q\vec{x}_{\omega} + \cdots \} + \vec{B} \cdot \Delta \vec{n} \cdot \{ q\vec{x}_{\omega} + q\vec{x}_{\omega} + \cdots \} + \end{split}$$

(6.136)

 $-!(\vec{k} \cdot \vec{\Omega}) \vec{h} \cdot \{ q \vec{x}_{(0)} + q \vec{x}_{(1)} + \dots \} - (\vec{n} \cdot \vec{A}) \vec{h} \cdot \{ q \vec{x}_{(0)} + q \vec{x}_{(1)} + \dots \} + (\vec{\lambda} \times \vec{B}) \times \vec{B} \cdot (q \vec{\lambda}_{(0)} + q \vec{\lambda}_{(1)} + \dots) \cdot \} + \\
+ \frac{1}{\mu^{N}} \left\{ \left[ i \vec{k} \times \vec{B} \cdot (q \vec{\lambda}_{(0)} + q \vec{\lambda}_{(1)} + \dots) + \vec{\lambda} \times \vec{B} \cdot (q \vec{\lambda}_{(0)} + q \vec{\lambda}_{(1)} + \dots) \right] \times \vec{B} + \\
- 5 i \lambda \vec{k} \cdot \vec{\Delta} \vec{h} \cdot \left\{ q \vec{x}_{(0)} + q \vec{x}_{(1)} + \dots \right\} + 5 \vec{D} \times \vec{h} \cdot \left\{ q \vec{x}_{(0)} + q \vec{x}_{(1)} + \dots \right\} + \\
- 5 i \lambda \vec{k} \cdot \vec{\lambda} \vec{h} \cdot \left\{ q \vec{x}_{(0)} + q \vec{x}_{(1)} + \dots \right\} + 5 \vec{D} \times \vec{h} \cdot \left\{ q \vec{x}_{(0)} + q \vec{x}_{(1)} + \dots \right\} +$ 

- { ~ [ q = 0 + q = 0 + 1 ] } . \$ \$

(6.137)

$$i \mathbf{k} \cdot \left\{ \mathbf{d} \mathbf{\chi}^{(0)} + \mathbf{d} \mathbf{\chi}^{(1)} + \dots \right\} = - \nabla \cdot \mathbf{k} \cdot \left\{ \mathbf{d} \mathbf{\chi}^{(0)} + \mathbf{d} \mathbf{\chi}^{(1)} + \dots \right\}$$
(6.139)

where

$$\mathbf{u}'(\mathbf{x},\mathbf{t}) = \iint_{\mathbf{z}} \mathbf{u} \cdot \{d\mathbf{z}^{\omega} + d\mathbf{z}^{\omega} + \dots\} e^{i\{\mathbf{z},\mathbf{x}+\omega\mathbf{t}\}} \qquad (6.140)$$

$$B'(x,t) = \iint_{\mathbb{R}^{\omega}} \underbrace{\left\{ d\gamma^{(\omega)} + d\gamma^{(t)} + \dots \right\}} e^{i\left\{ k \cdot x + \omega t \right\}}$$
(6.140')

$$F'(x,t) = \iint_{\mathbb{R}^{\omega}} \Im df(x,\omega) e^{i\frac{\pi}{2} + \omega t}$$
(6.140")

$$P'(x,t) = \iint_{\mathbb{R}\omega} Pdp(k,\omega) e^{i\{k,x+\omega t\}}$$
 (6.140")

In dealing with these equations, we shall assume that the mean flow  $\overline{u}$  is small enough in magnitude for the terms  $\overline{u} \cdot \nabla \cdot \underline{u}$  and  $\overline{u} \cdot \nabla \cdot \underline{B}$  so be treated as second-order quantities.

The first-order equations are

$$(i\omega + \eta k^2) \vec{R} \cdot d\vec{Y}^{(0)} = i(\vec{k} \cdot \vec{B}) \vec{U} \cdot d\vec{z}^{(0)} \qquad (6.141)$$

$$(i\omega + \gamma k^{2}) \ \underline{U} \cdot d\underline{z}^{(6)} + 2\underline{\Omega} \times \underline{U} \cdot d\underline{z}^{(6)} =$$

$$= \frac{1}{P} \left\{ \exists d\underline{f} - i\underline{k} P d\underline{p} \right\} + \frac{1}{P\mu} \left\{ i\underline{k} \times \underline{R} \cdot d\underline{\gamma}^{(6)} \right\} \times \overline{\underline{R}}$$

$$(6.142)$$

$$i \not k \cdot \not u \cdot d \not Z^{(0)} = O = i \not k \cdot \not k \cdot d \not Y^{(0)}$$
(6.143)

Solving for  $\beta \cdot dx^{(0)}$  and  $U \cdot dz^{(0)}$  under the assumption

$$R \cdot df(R, \omega) = 0 (6.144)$$

we obtain

$$\beta \cdot d\gamma^{(6)} = \frac{i(\mathbf{k} \cdot \vec{\mathbf{B}})}{\eta \mathbf{k}^2 + i\omega} \cdot \mathbf{y} \cdot dz^{(6)}$$
(6.145)

$$\underbrace{\nabla \cdot dZ^{(G)}}_{\infty} = \frac{3}{PD} \left\{ \sigma k^2 df - 2(\underline{k} \cdot \underline{\Omega}) \, \underline{k} \times df \right\}$$
 (6.146)

where

$$\sigma \equiv vk^2 + i\omega + \frac{(\mathbf{R}.\mathbf{B})^2}{P\mu\{\eta k^2 + i\omega\}}$$
(6.147)

$$D = \sigma^2 k^2 + 4(k \Omega)^2 \qquad (6.148)$$

In these equations we have adopted a notation closely similar to that used by Moffatt (1972).

# 6.4.3 Helicity and u'x B' for a locally isotropic force distribution

In a study of turbulent dynamo action, the principal quantities of interest are the turbulent intensity, the helicity, and the fluctuating e.m.f. These quantities are given by the expressions

$$\frac{\mathbf{u}' \cdot \mathbf{u}'}{\mathbf{z}'} = \iint_{\mathbb{R}^{\omega}} (\mathbf{v}^{\bullet} \cdot d\mathbf{z}^{(\omega)}) \cdot (\mathbf{v}^{\bullet} \cdot d\mathbf{z}^{(\omega)}) + \dots$$

$$= \iint_{\mathbb{R}^{\omega}} (\mathbf{v}^{\bullet} \cdot d\mathbf{z}^{(\omega)}) \cdot (\mathbf{v}^{\bullet} \cdot d\mathbf{z}^{(\omega)}) + \dots$$
(6.149)

$$+ \iiint \left\{ \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left[ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0)} \right] +$$

$$= \iiint \left\{ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0)} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\stackrel{\times}{\times}_{(0),\bullet} \left[ \prod_{\bullet} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right] \cdot \left\{ i \not k \times \vec{\Lambda} \cdot q \stackrel{\times}{\times}_{(0),\bullet} \right\} +$$

$$\frac{u' \times B'}{u' \times B'} = \Re \left[ \frac{(u'' \cdot dz'') \times (\beta \cdot dz'')}{(\alpha \cdot dz'') \times (\beta \cdot dz'')} + \frac{(\beta \cdot dz'')}{(\alpha \cdot dz'')} \right] \times \left[ \frac{1}{B} \cdot dz''' \right] + \left[ \frac{1}{B} \cdot dz''' \right] + \left[ \frac{1}{B} \cdot dz''' \right] \right]$$

The first-order terms in the integrands in equations (6.149)-(6.151) can be rewritten, making use of equations (6.145) and (6.146).

$$= \left| \frac{3}{PD} \right|^{2} \left\{ |\sigma|^{2} k^{4} \overline{d f^{*} \cdot d f} + 4(\underline{k} \cdot \underline{\Omega})^{2} \overline{(\underline{k} \times d f^{*}) \cdot (\underline{k} \times d f)} + -2k^{2} (\underline{k} \cdot \underline{\Omega}) \left[ \sigma^{*} \overline{d f^{*} \cdot (\underline{k} \times d f)} + \sigma \overline{d f^{*} \cdot (\underline{k} \times d f^{*})} \right] \right\}$$

We shall assume that the turbulent force distribution is locally isotropic, so that

$$\frac{\overline{df_i^*df_j}}{4\pi k^4} = \frac{\Psi(R,\omega)}{4\pi k^4} \left\{ k^2 \delta_{ij} - k_i k_j \right\} \qquad (6.155)$$

Under this assumption, df and df satisfy the equations:

$$df^{\bullet}. df = \frac{\psi}{2\pi k^2} \qquad (6.156a)$$

$$(k \times df^{\bullet}) \cdot (k \times df) = \frac{4}{2\pi}$$
(6.156b)

$$df^{\bullet} \cdot (k \times df) = 0 = (k \times df^{\bullet}) \cdot df \qquad (6.156c)$$

$$\frac{df^{\bullet} \times (\cancel{k} \times df)}{df^{\bullet} \times (\cancel{k} \times df)} = \frac{\cancel{k} \times df^{\bullet}}{2nk^{2}} = -(\cancel{k} \times df^{\bullet}) \times df \qquad (6.156d)$$

$$\frac{df^{\bullet} \times df}{df^{\bullet} \times df} = 0 = (k \times df^{\bullet}) \times (k \times df) \qquad (6.156e)$$

Substituting (6.156a-e) into equations (6.152)-(6.154), we obtain

$$(\underbrace{\underline{\mathbf{y}^{\bullet}}.\,d\underline{\mathbf{z}^{(\omega)}}^{\bullet})\cdot(\underline{\mathbf{y}}.d\underline{\mathbf{z}^{(\omega)}})}_{=[PD]} = \left|\frac{3}{PD}\right|^{2} + 4(\underline{\mathbf{k}}\cdot\underline{\Omega})^{2}$$
(6.157)

$$\left\{ \underbrace{\mathbf{U}^{\bullet}.\,\mathbf{d}\,\mathbf{Z}^{(\omega)}}^{\dagger} \right\} \cdot \left\{ i\,\mathbf{k}\,\mathbf{x}\,\underbrace{\mathbf{U}\,.\,\mathbf{d}\,\mathbf{Z}^{(\omega)}}_{\bullet} \right\} = \left| \frac{\mathbf{J}}{PD} \right|^{2} \frac{\mathbf{J}}{2\pi} \,\mathbf{J}\,\mathbf{k}^{2}(\mathbf{k}\,.\Omega) \,\mathbf{J}\,\mathbf{m}\,\mathbf{\sigma} \qquad (6.158)$$

As may be seen from equations (6.147) and (6.148),  $|\sigma|^2$  and  $|D|^2$  are even functions of  $\omega$ , while Im  $\sigma$  is an odd function of  $\psi\omega$ . Thus, when the expressions (6.157)-(6.159) are integrated over the range  $-\infty$  to  $+\infty$  in  $\omega$ , (6.157) will be the only term to give a nonzero result, if  $\psi(k,\omega)$  is an even function of  $\omega$ . Both the helicity, given by (6.150), and the fluctuating e.m.f., given by (6.151), are therefore zero to first order when  $\psi(k,\omega)$  is even in  $\omega$ .

Moffatt (1972) has considered equations (6.157)
(6.159) in some detail, and has obtained nonzero helicity and fluctuating e.m.f. by assuming that

$$\psi(k,\omega) = 0$$
 when  $\omega(k\cdot\Omega) < 0$  . (6.160)

He has then examined the asymptotic behaviour of the kinetic and magnetic energy of the system in the limit of large times. In this thesis, however, we shall retain the assumption that F' is locally isotropic - i.e.

$$\psi(k,\omega) = \psi(k,-\omega) \qquad (6.161)$$

and examine the effects of inhomogeneity and of nonzero mean flow.

## 6.4.4 The second-order fluctuating equations and their solutions

From equations (6.136)-(6.139), and the assumption that terms involving  $\overline{\underline{u}}$  contribute only to second order, the second-order fluctuating dynamo equations are

$$(i\omega + \eta k^2) \hat{\mathbf{g}} \cdot d\hat{\mathbf{y}}^{(i)} = 2i\eta \, \mathbf{k} \cdot \nabla \hat{\mathbf{g}} \cdot d\hat{\mathbf{y}}^{(o)} + i(\mathbf{k} \cdot \mathbf{\bar{g}}) \, \mathbf{y} \cdot d\hat{\mathbf{z}}^{(o)} + (6.162)$$

$$+ \, \mathbf{\bar{g}} \cdot \nabla \mathbf{y} \cdot d\hat{\mathbf{z}}^{(o)} - i(\mathbf{k} \cdot \mathbf{\bar{u}}) \mathbf{g} \cdot d\hat{\mathbf{y}}^{(o)} - (\mathbf{y} \cdot d\hat{\mathbf{z}}^{(o)}) \cdot \nabla \mathbf{\bar{g}}$$

$$(i\omega + \gamma k^{2}) \underline{\mathcal{U}} \cdot d\underline{\mathcal{Z}}^{(0)} + 2\underline{\Omega} \times \underline{\mathcal{U}} \cdot d\underline{\mathcal{Z}}^{(0)} =$$

$$= 2i\gamma \underline{k} \cdot \underline{\gamma} \underline{\mathcal{U}} \cdot d\underline{\mathcal{Z}}^{(0)} - \frac{1}{P} \underline{\gamma} P dp - i(\underline{k} \cdot \underline{u}) \underline{\mathcal{U}} \cdot d\underline{\mathcal{Z}}_{0} +$$

$$+ \frac{1}{P^{\mu}} \left[ [i\underline{k} \times \underline{R} \cdot d\underline{\gamma}^{(0)} + \underline{\nabla} \times \underline{R} \cdot d\underline{\gamma}^{(0)}] \times \underline{R} + (\underline{\nabla} \times \underline{R}) \times \underline{R} \cdot d\underline{\gamma}^{(0)} \right]$$

$$(6.163)$$

$$(6.164)$$

$$i \overset{\circ}{R} \cdot \overset{\circ}{U} \cdot d \overset{\circ}{Z}^{(0)} = - \overset{\circ}{V} \cdot \overset{\circ}{U} \cdot d \overset{\circ}{Z}^{(0)} - \left\{ \overset{\circ}{V} \overset{\rho}{P} \right\} \cdot \overset{\circ}{U} \cdot d \overset{\circ}{Z}^{(0)} \qquad (6.165)$$

Solving these equations for  $\beta \cdot dy^{(1)}$  and  $y \cdot dz^{(1)}$ , we obtain

$$\frac{1}{\mathbf{B}} \cdot \mathbf{Q} \mathbf{Y}^{(0)} = \frac{1}{i\omega + \eta R^2} \left\{ i(\mathbf{R} \cdot \mathbf{B}) \mathbf{Y} \cdot \mathbf{d} \mathbf{Z}^{(0)} + 2i\eta \mathbf{K} \cdot \mathbf{Y} \mathbf{B} \cdot \mathbf{d} \mathbf{Y}^{(0)} + (6.166) \right.$$

where

$$-\frac{h}{l} \overset{\text{Lin}}{\mu} \times \left\{ \left( \tilde{\Delta} \times \tilde{\beta} \cdot q \tilde{\lambda}_{(0)} \right) \times \tilde{B} + (\tilde{\Delta} \times \tilde{B}) \times \tilde{B} \cdot q \tilde{\lambda}_{(0)} \right\}$$

$$-\frac{h}{l} \frac{i(\tilde{\mu} \cdot \tilde{h}) \tilde{\mu}}{i(\tilde{\mu} \cdot \tilde{h}) \tilde{\mu}} \times \left\{ 3i J (\tilde{\mu} \cdot \tilde{\Delta}) \tilde{B} \cdot q \tilde{\lambda}_{(0)} + \tilde{B} \cdot \tilde{\lambda} \tilde{h} \cdot \tilde{h} \cdot$$

The occurrence of nonzero second-order contributions to the helicity and the fluctuating e.m.f. is guaranteed by the nature of the second-order terms in (6.150) and (6.151). From equations (6.145) and (6.146),

$$\left[ \mathbf{U}^* \mathbf{d} \mathbf{Z}^{(\omega)} \right] = \left[ \text{even in } \omega \right] + i \left[ \text{odd in } \omega \right] \qquad (6.169)$$

$$\left[\beta \cdot d\gamma^{(\omega)}\right] = \left[\text{odd in }\omega\right] + i\left[\text{even in }\omega\right] \qquad (6.169')$$

Similarly, from equation, (6.168),

so that

If we assume that the fluctuating pressure and force distributions are uncorrelated - i.e. if

- then it follows from (6.169)-(6.170') that

etc.

From (6.172), (6.150), and (6.151) we see that only evenorder contributions (i.e. second-order, fourth-order, etc.)
to the helicity and the fluctuating e.m.f. can be nonzero.

# 6.4.5 Second-order contributions to ux B in the geodynamo

It is clear from equations (6.166)-(6.168) that there are a large number of terms which contribute to  $\overline{u'x'}\overline{B'}$  in the second-order approximation. We shall scale these terms in order to determine which of them are important in the geodynamo.

With the scaling

$$[k] \sim \frac{1}{R}$$
,  $[w] \sim \frac{1}{T}$ ,  $[\nabla] \sim \frac{1}{L}$  (6.473)

and the definitions

$$V_{A} = \overline{B}/\sqrt{P\mu}$$
 (6.174)

$$R_{A} \equiv V_{A} \ell / \eta \qquad (6.175)$$

$$R_{\rm m} \equiv \overline{u} L/\eta$$
 (6.176)

equation (6.147) reduces to

$$[\sigma] \sim \frac{\eta}{\ell^2} \left\{ \left[ \frac{R_A}{(1+q^2)} + \frac{\nu}{\eta} \right] + iq \left[ \frac{R_A}{(1+q^2)} + 1 \right] \right\}$$
 (6,4178)

Similarly, equation (6.168) scales as

$$\begin{bmatrix} d\mu_{\bullet} \end{bmatrix} \sim i \frac{u'\eta}{\ell^{2}L} \left\{ \left[ \frac{R_{A}^{2}R_{m}}{(i+iq)^{2}} \right] + \left[ R_{m} \right] + \left[ \frac{\Omega \ell^{2}/\eta}{\eta} \right] + \left[ \frac{R_{A}^{2}}{(i+iq)^{2}} \right] + \left[ \frac{R_{A}^{2}}{(i+iq)^{2}} \right] + \left[ \frac{R_{A}^{2}}{\eta} \right] + \left[ \frac{1}{P} R \times \nabla P dp \right]$$

$$(6.179)$$

$$(6.179)$$

where

$$\mathbf{O} = -\frac{1}{\rho_{\mu}} \frac{\mathbf{R} \cdot \mathbf{B}}{(i\omega + \eta \mathbf{R}^2)} \overset{\mathbf{R}}{\approx} (\mathbf{R} \cdot \mathbf{u}) \overset{\mathbf{B}}{\approx} d \overset{\mathbf{C}}{\sim} \mathbf{O}$$
(6.180a)

$$3 = 2i\Omega \left\{ \nabla \cdot \mathbf{v} \cdot d\mathbf{z}^{(0)} + (\nabla P/P) \cdot \mathbf{v} \cdot d\mathbf{z}^{(0)} \right\}$$
 (6.180c)

$$\Phi = -\frac{1}{1} \left\{ \frac{i(\vec{k} \cdot \vec{\beta})}{i\omega + ik_{3}} \, \vec{k} \, \times \left[ \vec{\beta} \cdot \vec{\lambda} \vec{h} \cdot q \vec{z}_{(0)} - (\vec{h} \cdot q \vec{z}_{(0)}) \cdot \vec{\lambda} \vec{\beta} \right] \right\} \tag{6.180d}$$

In the fluid core of the Earth, we may take

$$\eta \sim 3 \text{ m}^2/\text{sec}$$
 (6.181a)  
 $v \sim 6 \times 10^{-7} \text{ m}^2/\text{sec}$  (6.181b)  
 $L \sim 3 \times 10^6 \text{ m}$  (6.181c)  
 $\bar{u} \sim 1 \times 10^{-4} \text{ m/sec}$  (6.181d)  
 $\Omega \sim 7 \times 10^{-5} \text{ rad/sec}$  (6.181e)  
 $R_{\text{m}}^{\prime} \sim 10^2$  (6.181f)  
 $V_{\text{A}} \sim 10^{-1} \text{ m/sec}$  (6.181g)

making use of the estimates (6.15), (6.82), and (6.100), taking the value of  $\overline{u}$  suggested by Roberts and Soward

(1972), and taking the estimate for the Alfvén speed,  $V_{\bf A}$ , given by Acheson and Hide (1973). From (6.175), (6.181a), and (6.181g) we see that

$$R_{A}$$
 (6.182)

Also, from (6.181a,b) we see that

$$\frac{\nu}{\eta} \ll 1 \tag{6.183}$$

in the main body of the core if the Gans (1972a) estimate of  $\nu$  is valid.

In considering equation (6.179), we may distinguish three possible sets of conditions.

(A) 
$$\frac{l < 30\sqrt{14q^2}}{000}$$
 m. and  $q < 70$   
OR  $\frac{l < 2km}{000}$  and  $q > 70$  (6.184)

Under these conditions, the various terms in equation (6.179) stand in the relationship:

The leading term in (6.179) is thus (2), and

is the appropriate approximation for dH

(6.185')

(6.186!)

(B) 
$$l > 30\sqrt{1+q^2}$$
 m. and  $q < 70$  (6.185)

Under these conditions,

so that

$$dH_{o}^{(B)} \approx -\frac{1}{P\mu} \frac{(\underline{R} \cdot \underline{B})}{(i\omega + \eta k^{2})} \, \underline{k} \times (\underline{k} \cdot \underline{u}) \underline{\beta} \cdot d\underline{\gamma}^{(o)} +$$

$$+ \frac{1}{P} \, \underline{k} \times \underline{\nabla} P \, d\underline{P}$$

$$(6.185")$$

(c) 
$$l > 2000 \text{ m. and } q > 70$$
 (6.186)

Under these conditions

$$[3] > [4]$$

so that

$$d\mathcal{H}_{\infty}^{(c)} \approx 2i\Omega \{ \nabla \cdot \mathbf{u} \cdot d\mathbf{z}_{\infty} + (\nabla b/b) \cdot \mathbf{u} \cdot d\mathbf{z}_{\infty} \}$$

$$+ \frac{1}{p} \mathbf{k} \times \nabla \mathbf{p} d\mathbf{p}$$

$$(6.186'')$$

In all three cases, (A), (B), and (C), term has been ignored. This approximation is certainly valid in the

geodynamo, since [6] < [2] even when the estimate obtained in section 6.3.4 for the effective kinematic viscosity near the core-mantle interface is used.

We may also note that in equation (6.166)

Since  $R_{m} >> 1$  in the geodynamo, we may ignore the term on the left hand side. Equation (6.166) thus reduces to

$$\frac{1}{2} \cdot d\underline{Y}^{(i)} \approx \frac{i(\underline{k},\underline{\tilde{B}})}{(i\omega + \eta k^2)^{\frac{1}{2}}} \cdot d\underline{Z}^{(i)} + \frac{(\underline{k},\underline{\tilde{U}})\underline{k},\underline{\tilde{B}})}{(i\omega + \eta k^2)^2} \underbrace{\underline{U}} \cdot d\underline{Z}^{(o)} + \frac{1}{(i\omega + \eta k^2)} \underbrace{\{(\underline{\tilde{B}},\underline{V})\underline{U}} \cdot d\underline{Z}^{(o)} - (\underline{U}} \cdot d\underline{Z}^{(o)}) \cdot \underline{V}\underline{\tilde{B}} }$$

$$+ \frac{1}{(i\omega + \eta k^2)} \underbrace{\{(\underline{\tilde{B}},\underline{V})\underline{U}} \cdot d\underline{Z}^{(o)} - (\underline{U}} \cdot d\underline{Z}^{(o)}) \cdot \underline{V}\underline{\tilde{B}} }_{i} \right}$$
(6.187)

Scaling the terms in (6.187), we obtain

$$[\underline{\beta},\underline{dY^{(i)}}] \sim \frac{\overline{\beta}\underline{\ell}}{\eta(1+iq)} \Big\{ [\underline{\nu},\underline{dZ^{(i)}}] + \Big[ \frac{R_m}{(1+iq)} + \frac{\ell}{L} \Big] [\underline{\nu},\underline{dZ^{(i)}}] \Big\}$$
(6.187')

Examination of (6.187') leads to the conclusion that the terms in braces on the right hand side of (6.187) can be neglected, provided that

$$q < Rm(L/p)$$
 (6.188)

Equation (6.187) may then be rewritten

$$\frac{1}{(k \cdot \overline{k} \times \overline{k})} = \frac{1}{(k \cdot \overline{k})} = \frac{1}{(k \cdot \overline{k} \times \overline{k})$$

We may now evaluate the second-order terms in the integral expression for  $\overline{\underline{u}' \times \underline{B}'}$  in the geodynamo for each of the three cases (A), (B), and (C). From equations (6.155) and (6.146),

$$\frac{\left\{ \mathbf{y}^{\bullet} \cdot \mathbf{d}\mathbf{z}^{(0)} \right\} \times \left\{ \mathbf{y} \cdot \mathbf{d}\mathbf{z}^{(0)} \right\}}{\left\{ \mathbf{p} \right\}^{2} + \left( \mathbf{k} \cdot \mathbf{p} \right) \right\} \operatorname{mor} \mathbf{k}} \qquad (6.190)$$

$$\frac{\{U^{\bullet} - dZ^{\hat{\omega}}\} - \{U \cdot dZ^{\hat{\omega}}\}}{\{PD\}} = \left|\frac{3}{PD}\right|^{2} \frac{\psi}{2\pi} \{|\sigma|^{2}k^{2} + 4(k\Omega)^{2}\}$$
(6.191)

The second-order terms in the integrand of equation (6.151) are therefore given by

$$\operatorname{Re}\left\{\left[\underline{U}^{\bullet}\cdot d\,\overline{z}^{(i)*}\right] \times \left[\underline{\beta}\cdot d\,\underline{\gamma}^{(o)}\right] + \left[\underline{U}^{\bullet}\cdot d\,\overline{z}^{(o)*}\right] \times \left[\underline{\beta}\cdot d\,\underline{\gamma}^{(i)}\right]\right\} = \\
= \operatorname{Re}\left\{\frac{i(\underline{k},\underline{\beta})}{(i\omega+\eta\,\underline{k}^{2})}\left[\left(\underline{U}^{\bullet}\cdot d\,\underline{z}^{(i)},\underline{\gamma}\right) \times \left(\underline{U}\cdot d\,\underline{z}^{(o)}\right) + \left(\underline{U}^{\bullet}\cdot d\,\underline{z}^{(o)*}\right) \times \left(\underline{U}\cdot d\,\underline{z}^{(o)}\right)\right\} + \\
+ \frac{(\underline{k}\cdot\underline{u}\,\underline{\chi}\,\underline{k}\cdot\underline{\beta})}{(i\omega+\eta\,\underline{k}^{2})^{2}}\left[\underline{\underline{U}^{\bullet}\cdot d\,\underline{z}^{(o)*}}\right] \times \left[\underline{\underline{U}\cdot d\,\underline{z}^{(o)}}\right]\right\} + \\
+ \frac{2\eta\,\underline{k}^{2}(\underline{k}\cdot\underline{\beta})}{(\eta^{2}\,\underline{k}^{4}+\omega^{2})}\operatorname{Im}\left\{\left[\underline{\underline{U}^{\bullet}\cdot d\,\underline{z}^{(o)*}}\right] \times \left[\underline{\underline{U}\cdot d\,\underline{z}^{(o)}}\right]\right\} + \\
+ \frac{4\eta\,\underline{k}^{2}\omega\,(\underline{k}\cdot\underline{\mu}\,\underline{\chi}\,\underline{k}\cdot\underline{\beta})}{(\eta^{2}\,\underline{k}^{4}+\omega^{2})^{2}}\left[\underline{\underline{J}}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{k}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}^{2}\,\underline{\mu}\,(\underline{\mu}\cdot\underline{\Omega})^{*}\,\underline{J}$$

In deriving (6.192), we have made use of equations (6.145), (6.189), and (6.190).

When case (A) is considered, so that dH is given by equation (6.184"),

$$\begin{split} & \int_{\mathbb{R}} \left\{ (\underline{y}^{\bullet} \cdot d\underline{z}^{(0)\bullet})^{(A)} \times (\underline{y} \cdot d\underline{z}^{(0)}) \right\} = \\ & = \int_{\mathbb{R}} \left\{ \frac{1}{D^{\bullet}} \left[ 2(\underline{R} \cdot \Omega) d\underline{H}^{(A)\bullet}_{\bullet} + \sigma^{\bullet} (\underline{R} \times d\underline{H}^{(A)\bullet}_{\bullet}) \right] \times \left[ \underline{y} \cdot d\underline{z}^{(0)} \right] + \\ & - \frac{\sigma^{*2}}{D^{\bullet}} \left[ \underline{y} \cdot \underline{y}^{\bullet} \cdot d\underline{z}^{(0)\bullet} + (\underline{y}P_{P}) \cdot \underline{y}^{\bullet} \cdot d\underline{z}^{(0)\bullet} \right] \underline{R} \times \left[ \underline{y} \cdot d\underline{z}^{(0)} \right] + \\ & = \int_{\mathbb{R}} \frac{1}{D^{\bullet}} \left\{ -2i(\underline{R} \cdot \Omega) X\underline{R} \cdot \underline{u} \right) (\underline{R} \times \underline{y}^{\bullet} \cdot d\underline{z}^{(0)\bullet}) \times (\underline{y} \cdot d\underline{z}^{(0)}) + \\ & -i\sigma^{*} (\underline{R} \cdot \underline{u}) \left[ \underline{R} \times (\underline{R} \times \underline{y}^{\bullet} \cdot d\underline{z}^{(0)\bullet}) \times (\underline{y} \cdot d\underline{z}^{(0)}) + \\ & -i\sigma^{*} (\underline{R} \cdot \underline{u}) \left[ \underline{R} \times (\underline{R} \times \underline{y}^{\bullet} \cdot d\underline{z}^{(0)\bullet}) \right] \times (\underline{y} \cdot d\underline{z}^{(0)}) + \\ & -i(\sigma^{*})^{2} \left( \underline{y} \cdot \underline{y}^{\bullet} \cdot d\underline{z}^{(0)P} + \frac{1}{P} \underline{y} P \cdot \underline{y}^{\bullet} \cdot d\underline{z}^{(0)\bullet}) \underline{R} \times (\underline{y} \cdot d\underline{z}^{(0)}) \right\} \\ & = \int_{\mathbb{R}} \frac{1}{P} \left\{ 2i(\underline{R} \cdot \underline{\Omega}) X\underline{R} \cdot \underline{u} \right) \underline{R} \left[ \underline{H}^{2} \right] \frac{1}{P} \frac{1}{P} \underline{R} + \\ & -i(\sigma^{*})^{2} \left( \underline{y} \cdot \underline{y}^{\bullet} \cdot d\underline{z}^{(0)\bullet} + \frac{1}{P} \underline{y} P \cdot \underline{y}^{\bullet} \cdot d\underline{z}^{(0)\bullet}) \underline{R} \times (\underline{y} \cdot d\underline{z}^{(0)}) \right\} \\ & = \left[ \frac{3}{P} \underline{J}^{2} \left\{ 2 \, \underline{R} \underline{P} D (\underline{R} \cdot \underline{\Omega}) X\underline{R} \cdot \underline{u} \right\} \frac{1}{2\pi} \left[ \underline{H} \underline{H}^{2} \underline{R}^{2} + \frac{1}{R} \underline{R} \cdot \underline{\Omega} \right] \underline{R} + \\ & + 2 \, \underline{R} \underline{P} D (\underline{R} \cdot \underline{\Omega}) X\underline{R} \cdot \underline{u} \right\} \frac{1}{2\pi} \left[ \underline{H} \underline{H}^{2} \underline{R}^{2} + \frac{1}{R} \underline{R} \cdot \underline{\Omega} \right] \underline{R} + \\ & + 2 \, \underline{R} \underline{P} D (\underline{R} \cdot \underline{\Omega}) X\underline{R} \cdot \underline{u} \right\} \frac{1}{2\pi} \left[ \underline{H} \underline{H}^{2} \underline{H}^{2} \underline{H}^{2} + \frac{1}{R} \underline{R} \cdot \underline{\Omega} \right] \underline{R} + \\ & + 2 \, \underline{R} \underline{P} D (\underline{R} \cdot \underline{\Omega}) X\underline{R} \cdot \underline{u} \right\} \frac{1}{2\pi} \left[ \underline{H} \underline{H}^{2} \underline{H}^{2} \underline{H}^{2} + \underline{H}^{2} \underline{\Omega} \right] \underline{R} + \\ & + 2 \, \underline{R} \underline{P} D (\underline{R} \cdot \underline{\Omega}) X\underline{R} \cdot \underline{u} \right\} \frac{1}{2\pi} \left[ \underline{H} \underline{H}^{2} \underline{H}^{2} + \underline{H}^{2} \underline{H}^{2} \underline{H}^{2} \right] \underline{R} + \\ & + 2 \, \underline{H} \underline{H}^{2} \underline{H$$

From (6.193), (6.178), and (6.184), the terms on the right hand, side of equation (6.194) scale as

$$\frac{u^{2}\sigma\overline{u}}{\ell^{3}D}\left\{\frac{\ell^{2}\Omega}{\eta^{2}}+\frac{1}{2}+\frac{1}{R_{m}}(v_{n}^{2}+iq)\right\}$$

It is therefore reasonable to neglect the last group of terms in (6.194) reasonable to neglect the last group of terms in (6.194) reasonable to neglect the last group of terms in (6.194) reasonable to neglect the last group of terms in (6.194) reasonable to neglect the last group of terms in (6.194) reasonable to neglect the last group of terms in (6.194) reasonable to neglect the last group of terms in (6.194) reasonable to neglect the last group of terms in (6.194) reasonable to neglect the last group of terms in (6.194) reasonable to neglect the last group of terms in (6.194) reasonable the description of the d

(6.195) will be valid under the first set of conditions characterizing case (A) (see equation 6.184).

Substituting equation (6.194) into (6.192), we see that in case (A)

if 
$$l < 30\sqrt{1+q^2} \, \text{m.}$$
,  $q < 70$ 

$$Re \left\{ \left( \underbrace{U^* \cdot dZ^{(0)*}} \right) \times \left( \underbrace{\beta} \cdot dY^{(0)} \right) + \left( \underbrace{U^* \cdot dZ^{(0)*}} \right) \times \left( \underbrace{\beta} \cdot dY^{(0)} \right) \right\} \times \left( \underbrace{\beta} \cdot dY^{(0)} \right) \times \left( \underbrace{\beta} \cdot dY^{(0)} \right)$$

$$\approx \left| \frac{\exists}{PD} \right|^{2} \frac{\psi}{2\pi} \left( \underbrace{\mathbb{R} \cdot \Omega}_{X} \underbrace{\mathbb{K} \cdot \overline{\mathbb{R}}}_{X} \underbrace{\mathbb{K} \cdot \overline{\mathbb{R}}}_{X} \right) \frac{4\eta k^{2} \omega}{(\eta^{2} k^{4} + \omega^{2})^{2}} \int_{\mathbb{R}^{2}} \int_{\mathbb{R}^{2}} \left( \underbrace{\mathbb{R} \cdot \overline{\mathbb{R}}}_{X} \right) \frac{4\eta k^{2} \omega}{(\eta^{2} k^{4} + \omega^{2})^{2}} \int_{\mathbb{R}^{2}} \int_{\mathbb{R}^{2}} \left( \underbrace{\nabla \cdot \underbrace{\mathbb{Q}}_{X} \cdot d\underbrace{\mathbb{Q}}_{X} \cdot d\underbrace{\mathbb{Q}}$$

Similarly, when case (B) is considered, so that  $dH_{\infty}$  is given by equation (6.185"),

$$\begin{split}
& \operatorname{Jm}\left\{ \left( \underbrace{\overset{\circ}{\mathbb{V}}^{\bullet} \cdot d \, \Xi^{(0) + } \right)^{(B)} \, \times \left( \underbrace{\overset{\circ}{\mathbb{V}} \cdot d \, \Xi^{(0)}} \right) \right\} = \\
& = \operatorname{Jm}\left\{ \frac{2i}{P_{\mu} \, D^{\bullet}} \, \frac{\left( \underbrace{\overset{\circ}{\mathbb{K}} \cdot \underline{\mathcal{U}} \, \times \overset{\circ}{\mathbb{K}} \, \times \overset{\circ}{\mathbb{K}} \, \times \overset{\circ}{\mathbb{K}}} \right)^{2}}{\left( \eta \, \mathsf{K}^{2} - i \omega \right)^{2}} \, \left[ \underbrace{\overset{\circ}{\mathbb{K}} \, \times \, \overset{\circ}{\mathbb{U}}^{\bullet} \cdot d \, \Xi^{(0) + } \right) \, \times \left( \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0)}} \right) + \\
& + \frac{i \, \sigma^{\bullet}}{P_{\mu} \, D^{\bullet}} \, \frac{\left( \underbrace{\overset{\circ}{\mathbb{K}} \cdot \overset{\circ}{\mathbb{U}} \, \times \, \overset{\circ}{\mathbb{K}} \, \times \overset{\circ}{\mathbb{K}}} \right)^{2}}{\left( \eta \, \mathsf{K}^{2} - i \omega \right)^{2}} \, \left[ \underbrace{\overset{\circ}{\mathbb{K}} \, \times \, \overset{\circ}{\mathbb{U}}^{\bullet} \cdot d \, \Xi^{(0) + } \right) \, \right] \, \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0)}} \right] + \\
& - \frac{i \, \sigma^{\bullet 2}}{D^{\bullet}} \left( \underbrace{\overset{\circ}{\mathbb{V}} \cdot \overset{\circ}{\mathbb{U}}^{\bullet} \cdot d \, \Xi^{(0) + } + \overset{\circ}{P} \, \nabla P \cdot \overset{\circ}{\mathbb{U}}^{\bullet} \cdot d \, \Xi^{(0) + } \right) \, \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0)}} \right] + \\
& - \frac{i \, \sigma^{\bullet 2}}{D^{\bullet}} \left( \underbrace{\overset{\circ}{\mathbb{V}} \cdot \overset{\circ}{\mathbb{U}}^{\bullet} \cdot d \, \Xi^{(0) + } + \overset{\circ}{P} \, \nabla P \cdot \overset{\circ}{\mathbb{U}}^{\bullet} \cdot d \, \Xi^{(0) + } \right) \, \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0)}} \right] + \\
& - \frac{i \, \sigma^{\bullet 2}}{D^{\bullet}} \left( \underbrace{\overset{\circ}{\mathbb{V}} \cdot \overset{\circ}{\mathbb{U}}^{\bullet} \cdot d \, \Xi^{(0) + } + \overset{\circ}{P} \, \nabla P \cdot \overset{\circ}{\mathbb{U}}^{\bullet} \cdot d \, \Xi^{(0) + } \right) \, \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0)}} \right] + \\
& - \frac{i \, \sigma^{\bullet 2}}{D^{\bullet}} \left( \underbrace{\overset{\circ}{\mathbb{U}} \cdot \overset{\circ}{\mathbb{U}}^{\bullet} \cdot d \, \Xi^{(0) + } + \overset{\circ}{P} \, \nabla P \cdot \overset{\circ}{\mathbb{U}}^{\bullet} \cdot d \, \Xi^{(0) + } \right) \, \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0)}} \right] + \\
& - \frac{i \, \sigma^{\bullet 2}}{D^{\bullet}} \left( \underbrace{\overset{\circ}{\mathbb{U}} \cdot \overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } + \overset{\circ}{\mathbb{U}} \, \overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right) \, \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \, \Xi^{(0) + } \right] \times \left[ \underbrace{\overset{\circ}{\mathbb{U}} \cdot d \,$$

Scaling the terms on the right hand side of (6.198), we obtain

$$\frac{u^{2}\eta \eta \bar{u}}{\ell^{3}D^{2}}\left\{\frac{2\Omega \ell^{2}}{\eta(1+q_{1})}+\frac{R_{A}^{2}}{(1+q^{2})}+\frac{(1+q_{1})R_{A}^{2}}{(1+q^{2})R_{m}}\right\}$$

The second term is dominant under the conditions specified in (6.185). Substituting (6.198) into (6.192), we obtain

if 
$$l > 30\sqrt{1+q^2} \, m.$$
,  $q < 70$ 
 $\Re \left\{ ( \underbrace{U^*. \, d \, z^{(n)*} ) \times ( \underbrace{\beta}. \, d \, \gamma^{(n)} )}_{\times} + ( \underbrace{U^*. \, d \, z^{(n)*} ) \times ( \underbrace{\beta}. \, d \, \gamma^{(n)} )}_{\times} \right\} \approx \frac{1}{|PD|^2} ( \underbrace{k.D}_{\times} \chi_{\underline{k}.\underline{B}} \chi_{\underline{k}.\underline{B}} ) \frac{4\eta \, k^2}{(\eta^2 k^4 + \omega^2)^2} \frac{\psi}{2\pi} \, \operatorname{Jm}_{\sigma} \, \underline{k} \, .$ 
 $(6.199)$ 
 $\cdot \left\{ \omega - \frac{2}{|D|^2} \omega \eta \, k^4 \frac{( \underline{k}.\underline{B} )^2}{P \mu (\eta^2 k^4 + \omega^2)} ( \operatorname{Re}_{\sigma} \, \operatorname{Re}_{D} + \operatorname{Jm}_{\sigma} \, \operatorname{Jm}_{D} ) + ( \underline{k}^2 ( \eta^2 k^4 - \omega^2) \frac{( \underline{k}.\underline{B} )^2}{P \mu (\eta^2 k^4 + \omega^2)} ( \operatorname{Re}_{\sigma} \, \operatorname{Jm}_{D} - \operatorname{Jm}_{\sigma} \, \operatorname{Re}_{D} ) \right\}$ 

Finally, when case (C) is considered, so that  $dH_{\infty}$  is given by equation (6.186"),

$$\int_{\mathsf{m}} \left\{ \left( \underbrace{\mathbb{Q}^{\mathbf{e}} \cdot \mathsf{d} \mathbf{z}^{(\mathbf{c}) \cdot \mathbf{e}}}_{\mathsf{p}} \right)^{(\mathbf{c})} \times \left( \underbrace{\mathbb{Q}} \cdot \mathsf{d} \mathbf{z}^{(\mathbf{c})} \right) \right\} = (6.200)$$

$$= \int_{\mathsf{m}} \left\{ -\frac{2(\underline{\mathsf{k}} \cdot \underline{\mathsf{Q}})}{D^{\mathbf{e}}} 2i \left( \underbrace{\nabla} \cdot \underline{\mathbb{Q}}^{\mathbf{e}} \cdot \mathsf{d} \mathbf{z}^{(\mathbf{c}) \cdot \mathbf{e}} + \frac{1}{p} \underbrace{\nabla} P \cdot \underline{\mathbb{Q}}^{\mathbf{e}} \cdot \mathsf{d} \mathbf{z}^{(\mathbf{c}) \cdot \mathbf{e}} \right) \underbrace{\Omega}_{\mathsf{p}} \times \left( \underbrace{\mathbb{Q}} \cdot \mathsf{d} \mathbf{z}^{(\mathbf{c})} \right) + \dots \right. \\
\left. - 2i \underbrace{\frac{\sigma^{\mathbf{e}}}{D^{\mathbf{e}}} (\underline{\mathsf{k}} \times \underline{\Omega}) \times \left( \underbrace{\mathbb{Q}} \cdot \mathsf{d} \mathbf{z}^{(\mathbf{c})} \right) \times \left( \underbrace{\mathbb{Q}} \cdot \mathsf{d} \mathbf{z}^{(\mathbf{c}) \cdot \mathbf{e}} + \frac{1}{p} \underbrace{\nabla} P \cdot \underline{\mathbb{Q}}^{\mathbf{e}} \cdot \mathsf{d} \mathbf{z}^{(\mathbf{c}) \cdot \mathbf{e}} \right) + \dots \right. \\
\left. - i \underbrace{\left( \sigma^{\mathbf{e}} \right)^{2} \left( \underbrace{\nabla} \cdot \underline{\mathbb{Q}}^{\mathbf{e}} \cdot \mathsf{d} \mathbf{z}^{(\mathbf{c}) \cdot \mathbf{e}} + \frac{1}{p} \underbrace{\nabla} P \cdot \underline{\mathbb{Q}}^{\mathbf{e}} \cdot \mathsf{d} \mathbf{z}^{(\mathbf{c}) \cdot \mathbf{e}} \right) \underbrace{\mathbb{k}}_{\mathsf{p}} \times \left( \underbrace{\mathbb{Q}} \cdot \mathsf{d} \mathbf{z}^{(\mathbf{c})} \right) \right\} \right.$$

Scaling the terms on the right hand side of (6.200), we obtain

$$\frac{u'^{2}\Omega^{2}}{\ell L IDI} \left\{ 1 + \frac{|\sigma|}{\Omega} + \frac{|\sigma|^{2}}{\Omega^{2}} \right\}$$

$$\sim \frac{u'^{2}\Omega^{2}}{\ell L IDI} \left\{ 1 + \frac{qR_{A}^{2}}{\ell^{2}\Omega q} + \frac{\eta^{2}R_{A}^{4}}{\ell^{4}\Omega^{2}q^{2}} \right\} \quad \text{if} \quad V_{A} > \frac{\ell}{\tau}$$

$$\sim \frac{u'^{2}\Omega^{2}}{\ell L IDI} \left\{ 1 + (\tau\Omega)^{-1} + (\tau\Omega)^{-2} \right\} \quad \text{if} \quad V_{A} < \frac{\ell}{\tau}$$

Under the conditions specified in (6.186), (6.182), and (6.181), the first term on the right hand side of (6.200) is dominant when  $V_{\rm A} > l/\tau$ . When  $V_{\rm A} < l/\tau$ , on the other hand, the first term on the right hand side of (6.200) will dominate only if  $\tau > 1$  day. Substituting (6.200) into (6.192), and assuming that the first term in (6.200) is dominant, we obtain

if 
$$l > 2km$$
,  $q > 70$  (and  $\tau > 1 day$ , if  $V_A < L/\tau$ )

$$Re \left\{ (U^*.dZ^{(1)*}) \times (\beta \cdot dY^{(0)}) + (U^*.dZ^{(0)}) \times (\beta \cdot dY^{(1)}) \right\} \approx$$

$$\approx \frac{4\eta k^2}{(\eta^2 k^4 + \omega^2)} (k \cdot \Omega) (k \cdot \overline{B}) \cdot (6.201)$$

$$\cdot \left\{ 2 Re \left[ \frac{1}{D^*} (\nabla \cdot U^*.dZ^{(0)*} + \frac{1}{P} \nabla P \cdot U^*.dZ^{(0)*}) \Omega \times (V \cdot dZ^{(0)}) \right] +$$

$$\cdot + \left| \frac{3}{PD} \right|^2 \frac{\psi}{2\pi} (k \cdot \overline{U}) \frac{\omega}{\eta^2 k^4 + \omega^2} Sm\sigma R \right\}$$

In equations (6.196), (6.197), (6.199), and (6.201), we have, from (6.147) and (6.148),

$$\int_{\mathbb{R}^{n}} \sigma = \omega \left\{ 1 - \frac{(\underline{R}.\overline{B})^{2}}{\rho_{\mu} (\eta^{2} k^{4} + \omega^{2})} \right\}$$
(6.202)

$$\operatorname{Re}\sigma = \eta k^{2} \left\{ \frac{v}{\eta} + \frac{(k \cdot \overline{B})^{2}}{\rho \mu (\eta^{2} k^{4} + \omega^{2})} \right\}$$
 (6.202')

$$\int_{m} D = 2k^{2} \int_{m\sigma} Re\sigma \qquad (6.203)$$

$$ReD = k^2 \{ (Re\sigma)^2 - (Jm\sigma)^2 \} + 4(k.\Omega)^2$$
 (6.203')

We may now write explicit expressions for the fluctuating e.m.f.  $u \times B'$  in the various cases considered above. Substituting equations (6.196), (6.197), (6.199) and (6.201) into equation (6.151), we obtain

(A1) 
$$\underline{I} < 30\sqrt{1+q^2} \text{ m}$$
,  $q < 70$ 

$$\underline{u}' \times \underline{B}' \approx \iint_{\mathbb{R}^{2}} d\underline{k} d\omega \left| \frac{3}{PD} \right|^2 \frac{\psi}{2\pi} \frac{4\eta k^2}{(\eta^2 k^4 + \omega^2)} (\underline{k} \cdot \underline{\Omega} \times \underline{k} \cdot \underline{u} \times \underline{k} \cdot \underline{B}) \underline{k} \cdot \left[ \frac{k^2}{|D|^2} \operatorname{Im} D \operatorname{Im} \operatorname{Re} \sigma - \frac{1}{|D|^2} \operatorname{Re} D \left[ |\sigma|^2 k^2 + (\operatorname{Im} \sigma)^2 k^2 + 4(\underline{k} \cdot \underline{\Omega})^2 \right] + \frac{2\omega \operatorname{Im} \sigma}{(\eta^2 k^4 + \omega^2)}$$

$$\left. + \frac{2\omega \operatorname{Im} \sigma}{(\eta^2 k^4 + \omega^2)} \right\}$$
(6.204)

(A2) 1 < 2km , q > 100

$$\frac{u' \times B'}{\mu} \approx \iint_{\mathbb{R}^{\omega}} dk \, d\omega \, \left| \frac{3}{\rho D} \right|^{2} \frac{4qk^{2}\omega}{2\pi} \, (k \cdot \Omega) \, k \cdot \overline{\mu} \times \overline{\mu} \times$$

(B) 1 > 30 /1+q2 m , q < 70

$$\begin{split} \overline{\underline{u}' \times \underline{B}'} &\approx \iint_{\underline{B}\omega} d\underline{k} \ d\omega \ \Big| \frac{\exists}{\rho D} \Big|^2 \frac{\downarrow}{2\pi} \frac{4\eta \, k^2}{(\eta^2 k^4 + \omega^2)^2} (\underline{k} \cdot \underline{\Omega} \, \underline{\chi} \, \underline{k} \cdot \underline{\overline{u}} \, \underline{\chi} \, \underline{k} \cdot \underline{\overline{B}}) \, \underline{4} m \sigma \, \underline{k} \cdot \\ \cdot \Big[ \omega - \frac{k^2 (\underline{k} \cdot \underline{\overline{B}})^2}{\beta \mu (\eta^2 k^4 + \omega^2)} \Big[ 2\eta \omega k^2 (\text{Re} \sigma \, \text{Re} \, D + \text{Im} \sigma \, \text{Im} \, D) + \\ + (\eta^2 k^4 - \omega^2 \underline{\chi} \, \text{Re} \sigma \, \text{Im} \, D - \text{Im} \sigma \, \text{Re} \, D) \Big] \Big\} \end{split}$$

(6.206)

(c) 
$$L > 2 \text{ km.}$$
,  $q > 70$  (and  $\tau > 1 \text{ day}$ , if  $V_A < L/\tau$ )

$$\overline{\underline{u}' \times \underline{B}'} \approx \iint_{\underline{B}\omega} d\underline{k} \, d\omega \, \frac{4\eta k^2}{(\eta^2 k^4 + \omega^2)} \, (\underline{k} \cdot \underline{\Omega}) (\underline{k} \cdot \underline{\overline{B}}) \, .$$

$$\cdot \left\{ 2 \operatorname{Re} \left[ \frac{1}{D^{*}} (\nabla \cdot \underline{y}^{*} \cdot d\underline{z}^{\omega)^{*}} + \frac{1}{p} \nabla P \cdot \underline{y}^{*} \cdot d\underline{z}^{\omega)^{*}} \right] \Omega \times (\underline{y} \cdot d\underline{z}^{\omega}) \right] + \\
+ \left| \frac{3}{PD} \right|^{2} \frac{\psi}{2\pi} (\underline{k} \cdot \underline{u}) \frac{\omega}{(\eta^{2}k^{4} + \omega^{2})} \operatorname{Im} \sigma \underline{k} \right\} \qquad (6.207)$$

### 6.4.6 The effects of locally isotropic turbulence in the geodynamo

The expressions (6.204)-(6.207), along with equations (6.202)-(6.203'), allow us to comment on the possible effects of a turbulent force distribution in the Earth's fluid core. The first question which must be answered is: what value of q is appropriate to the evaluation of the expressions for  $\overline{u' \times B'}$ ? In his study of the first-order terms, Moffatt (1972) has suggested that the largest contributions to the integration over  $\omega$  will come from the "natural" frequencies of the undamped system - i.e. from the frequencies at which

$$\frac{1 \text{im}}{v_1 n \to 0} |D|^2 = |D_0|^2 = 0 \qquad (6.208)$$

From equations (6.202) and (6.203) it may be seen that these "natural" frequencies are given by the roots of

$$D_o = 4(\underline{R} \cdot \underline{\Omega})^2 - R^2 \left\{ \omega - \frac{(\underline{R} \cdot \overline{\underline{B}})^2}{\rho_\mu \omega} \right\}^2 = 0 \qquad (6.209)$$

Solving equation (6.209), we obtain the expression

$$\omega_n = \pm \frac{(\Omega \cdot k)}{k} \pm \sqrt{\frac{(\Omega \cdot k)^2}{k^2} + \frac{(k \cdot \overline{B})^2}{\beta \mu}}$$
 (6.210)

for the "natural" frequencies  $\omega_n$ 

To a very crude approximation, it follows from equation (6.210) that

$$|\omega_n| \sim \sqrt{\Omega^2 + V_A^2/\varrho^2}$$
 (6.211)

The value of q implied by the "natural" frequencies is therefore

$$q_n \equiv \ell^2 |\omega_n|/\eta \sim \sqrt{(\Omega \ell^2/\eta)^2 + R_A^2}$$
 (6.212)

Checking equation (6.212) against the requirements specified in each of (6.204)-(6.207), we see that the "natural" frequencies  $\omega_n$  are likely to be consistent with cases (A1) and (C), but not with cases (A2) or (B). Assuming that the crude approximation (6.211) is valid in some sense as an "average" over the range of integration in k, we may restrict consideration to equations (6.204) and (6.207) when the "natural" frequencies are dominant.

It must, however, be pointed out that the "natural" frequencies will not necessarily give the largest contributions to the integration over  $\omega$  in equations (6.204)— (6.207). If the spectrum function  $\psi(k,\omega)$  of the force distribution vanishes in the neighbourhood of the "natural" frequencies, or if the spectrum function is sharply peaked at a "driving" frequency  $\omega_O$ , contributions from the "natural" frequencies may well be negligible. We may distinguish two possible sets of conditions:

- a.  $\psi(k,\omega)$  is a "broad band" spectrum function, with at least one of the "natural" frequencies  $\omega_n$  included in the band in which  $\psi$  is nonzero.
- b.  $\psi(k,\omega)$  is sharply peaked at one or more "driving" frequencies.

When (a) is valid, contributions from the "natural" frequencies will dominate the integrals in (6.204) and (6.207), and the approximate method of integration suggested by Moffatt (1972) will be applicable. Because of the condition (6.212), it will not be necessary to consider equations (6.205) and (6.206). It should be noted that in the remaining two equations it will be necessary to include contributions from all four "natural" frequencies. Moffatt (1972) obtains contributions from only two of these frequencies because of his assumption that  $\psi(k,\omega)$  satisfies the condition (6.160).

On the other hand, when (b) is valid contributions from the "driving" frequencies will dominate the integrals in (6.204)-(6.207), and it will be appropriate to replace  $\psi(k,\omega)$  with a sum of terms of the form  $\psi(k)\delta(\omega-\omega_0)$ . As there are no restrictions on q in this case, it will be necessary to consider all four sets of conditions (6.204)-(6.207).

Because of the labour involved, we shall not carry the evaluation of  $\overline{u}' \times \overline{B}'$  any further in this thesis. However, the principal features of the various contributions are already apparent from the equations in their present form. We shall first point out several general properties, shared by all four equations, (6.204)-(6.207).

- In each case; integration with respect to  $\omega$  over the range  $-\infty$  to  $+\infty$  can give a nonzero result, since all the terms in the integrands are even functions of  $\omega$ .
- [2] In each case, the integral vanishes if  $\eta = 0$ . Thus dissipation is essential to the production of nonzero u'x B' (see section 1.4.2). This property is shared by the expressions obtained by Moffatt (1972).
- [3] In each case, the expression for  $\overline{\underline{u}'x}$   $\overline{\underline{B}'}$  gives an  $\alpha$ -effect at low values of the mean field,  $\overline{\underline{B}}$ .

It should be noted that the integrands in equations (6.204)-(6.207) are nearly all rotation-dependent. The only exception is the second term in equation (6.205). When the necessary "averaging" in this term is carried out, we obtain

$$(\nabla \cdot \mathbf{U}^{\bullet} \cdot d\mathbf{z}^{(o)})^{\bullet} + \frac{1}{P} \mathbf{V}^{P} \cdot \mathbf{U}^{\bullet} \cdot d\mathbf{z}^{(o)}) \mathbf{R} \times (\mathbf{U} \cdot d\mathbf{z}^{(o)}) = (6.123)$$

$$= \frac{\Psi}{4\pi R^{2}} \left\{ \frac{3\sigma}{P^{2}D} \mathbf{R}^{+} \left[ \mathbf{R} \times \mathbf{V} \left( \frac{3\sigma}{D} \right)^{\bullet} \right] + \frac{43}{P^{2}D} \mathbf{R}^{2} (\mathbf{R} \cdot \mathbf{\Omega})^{2} \left[ \mathbf{R} \times \mathbf{V} \left( \frac{3}{D} \right)^{\bullet} \right] + \frac{23}{P^{2}D} \mathbf{R}^{2} (\mathbf{R} \cdot \mathbf{\Omega})^{2} \left[ \mathbf{R} \times \mathbf{V} \left( \frac{3}{D} \right)^{\bullet} \right] + \frac{23}{P^{2}D} \mathbf{R}^{2} (\mathbf{R} \cdot \mathbf{\Omega}) \left[ 2i \operatorname{Sm} \sigma \mathbf{V} \left( \frac{3}{D} \right)^{\bullet} - \left( \frac{3}{D} \right)^{\bullet} \mathbf{V} \sigma^{\bullet} \right] \cdot (\mathbf{R} \mathbf{R} - \mathbf{R}^{2} \mathbf{I}) \right\}$$

making use of equations (6.146), (6.155), and (6.156). Thus, from equation (6.205), the contribution to  $\overline{u}' \times \overline{B}'$  which does not vanish with  $\Omega$  is

$$\left\{ \underbrace{\mathbf{u}' \times \mathbf{B}'}_{\mathbf{\Omega}=0} \right\}_{\mathbf{\Omega}=0} =$$

$$= \iint_{\mathbf{B}} d\mathbf{k} d\omega \frac{2\eta \mathbf{k}^4}{(\eta^2 \mathbf{k}^4 + \omega^2)} \frac{\Psi}{2\pi} \left( \mathbf{k} \cdot \overline{\mathbf{B}} \right) \Re \left\{ \frac{3|\sigma|^2 \sigma^4}{\rho^2 |\mathbf{D}|^2} \frac{\mathbf{k} \times \nabla \left( \frac{3\sigma}{\mathbf{D}} \right)^4}{\mathbf{k}^2 |\mathbf{D}|^2} \right\}$$

$$= \underbrace{\left\{ \frac{3|\sigma|^2 \sigma^4}{\rho^2 |\mathbf{D}|^2} \frac{\mathbf{k} \times \nabla \left( \frac{3\sigma}{\mathbf{D}} \right)^4}{\mathbf{k}^2 |\mathbf{D}|^2} \right\}}_{\mathbf{A}}$$

subject to the conditions  $\ell < 2 \text{ km}$ , q > 100. This term may be regarded as an example of the introduction of a fluctuating e.m.f. (and of helicity) through large-scale variation of the turbulent force intensity (see the discussion in section 4.3.7).

The various terms in the integrands in equations (6.204)-(6.207) nearly all depend on the presence of a mean flow  $\widehat{\mathbf{u}}$ . The only exceptions are the second term in equation (6.205), discussed in the last paragraph, and the first term in equation (6.207). It may be shown (see Table 17 below) that the second term in (6.205) is dominant when  $\widehat{\mathbf{B}}$  is large, while the first term in (6.205) is not. Since  $\widehat{\mathbf{B}}$  may be considered large in the geodynamo, the importance of mean flow in turbulent dynamo action in the Earth appears to depend critically on the values of  $\ell$  and  $\tau$  appropriate to turbulence in the core.

The integrands in (6.204)-(6.207) show a variety of dependences on  $\overline{B}$ . These dependences are summarized in Table 17, overleaf. It can be seen from the table that most of the terms lead to a simple  $\alpha$ -effect at low values of  $\overline{B}$ . However, the second and third terms in equation (6.206) have

a  $\overline{B}^3$  dependence at low values of  $\overline{B}$ . At high values of  $\overline{B}$  all terms are small, but the second term in equation (6.205), discussed in the last two paragraphs, falls off more slowly with increasing  $\overline{B}$  than do the other terms.

Dependence of integrands on  $\overline{B}$  in expressions for  $\overline{\underline{u}^T x \ \underline{B}^T}$ 

	·		· · · · · · · · · · · · · · · · · · ·
Equation	Term	Dependence on $\overline{\mathtt{B}}$	
		Low B	$High \overline{B}$
(6.204)	ı	$\overline{\mathbf{B}}$	
c .	.2	B	→ <del>B</del> -7
	3	B	<u>B</u> −5
(6.205)	1 ;	B	
	2	$\overline{\mathbf{B}}$	<u>B</u> −3
(6.206)	1	B	<u>B</u> −5
	2	$\overline{B}^3$	<u>B</u> −5
· .	3	$\overline{\mathtt{B}}^3$ .	B̄ -5
(6.207)	1	$\overline{\mathtt{B}}$	<u></u>
*	2	$\overline{\mathbf{B}}$	<del>B</del> −5

(It should be noted\_that in the last few paragraphs, and in Table 17,  $\vec{B} \equiv |\vec{p}|$  .)

We may now summarize the effects to be expected from a locally isotropic turbulent force distribution in the Earth's fluid core. The dominant effect of turbulent forces outside the boundary layer is determined in large part by the characteristic length scale & of the turbulence, and by the ratio of the diffusion time on this length scale to the effective time scale of the turbulence. This time ratio is denoted by q.

If both  $\ell$  and q are relatively "small" (see equation 6.204), an  $\alpha$ -effect appears at low values of  $\overline{B}$  (the magnitude of the mean flux density). This effect depends for its existence on the presence of both rotation and a mean flow. At large values of  $\overline{B}$ ,  $\overline{q}$ 'x  $\overline{B}$ ' goes to zero as  $\overline{B}$   $r^5$ 

If both  $\ell$  and q are relatively "large" (see equation 6.207), a rotation-dependent  $\alpha$ -effect again appears at low values of  $\overline{B}$ . Only part of this effect depends on the presence of a mean flow; the remainder depends on the presence of gradients of the turbulent force intensity. At large values of  $\overline{B}$ ,  $\overline{u}$  x  $\overline{B}$  again goes to zero. However, the part of the effect which is mean flow-dependent disappears more gradually than the remainder, going to zero as  $\overline{B}$  -5. rather than as  $\overline{B}$  -7.

If is "Small" while q is "large" (see equation 6.205), an  $\alpha$ -effect again appears at low values of  $\overline{B}$ ,

One part of this effect depends for its existence on the presence of both rotation and a mean flow. A second part depends on the presence of both rotation and large-scale variations of the turbulent force intensity. The remainder of the effect depends only on the presence of large-scale variations of the turbulent force intensity. At large values of  $\overline{B}$ , all three parts of the effect disappear. However, the second and third parts fall off more slowly with increasing  $\overline{B}$  than does the first ( $\overline{B}^{-3}$  compared with  $\overline{B}^{-5}$ ). In general,  $\overline{u}'x \overline{B}'$  is unlikely to have the behaviour described in this paragraph if the spectrum of the turbulent force distribution has a fairly uniform amplitude over a broad band of frequencies w.

If  $\ell$  is relatively "large" and q is relatively "small" (see equation 6.206), an  $\alpha$ -effect appears only at very small values of  $\overline{B}$ . At somewhat larger values of  $\overline{B}$ ,  $\overline{u'} \times \overline{B'}$  varies as  $\overline{B}^3$ . Both the  $\alpha$ -effect and the  $\overline{B}^3$  effect depend for their existence on the presence of rotation and mean flow. All terms contributing to  $\overline{u'} \times \overline{B'}$  go to zero as  $\overline{B}^{-5}$  at large values of  $\overline{B}$ . In general,  $\overline{u'} \times \overline{B'}$  is unlikely to have the behaviour described in this paragraph if the spectrum of the turbulent force distribution is "broad-band" in  $\omega$ .

#### 6.5 Summary of Chapter 6

This chapter is concerned with the hydromagnetic dynamo problem as it applies to the Earth's fluid core. The magnetogeostrophic approximation is considered, and a general expression for the fluid velocity in the core is obtained, giving the velocity as a function of the distribution of body forces, the magnetic field, and the boundary conditions.

The equation obtained in Chapter 5 for boundary-layer control of the external magnetic field is investigated in terms of the distribution of body forces at the coremantle interface. It is shown that radial forces at the coremantle interface cannot account for the observed temporal variations of the geomagnetic dipole moment. Azimuthal forces, on the other hand, can account for these variations. The azimuthal force term  $-\rho(\Omega \times r)$  is shown to explain the dipole wobble reported by Kawai and Hirooka (1967) if the kinematic viscosity at the core-mantle interface is of the order  $\nu \sim 1-2$  m/sec. This term also leads to non-periodic variations in the axial dipole moment on time scales similar to those which characterize geomagnetic polarity transitions.

The effects of a turbulent distribution of body forces in the Earth's core are also considered. Turbulent forces outside the boundary layer produce a variety of effects. If the turbulent force distribution is locally

part by the characteristic length scale of the turbulence and the ratio of the diffusion time on this length scale to the effective time scale of the turbulence. In most cases a rotation-dependent  $\alpha$ -effect is dominant when the mean magnetic flux density,  $\overline{B}$ , is small. This effect may also depend on the presence of a mean flow, or the presence of large-scale variation of the turbulent force intensity. At large values of  $\overline{B}$ , the fluctuating e.m.f.  $\overline{U} \times \overline{B}$  goes to zero. The various types of behaviour which may occur are summarized at the end of section 6.4.6.

## 7. FINAL SUMMARY

The principal aims of this thesis have been to summarize present-day knowledge of astrophysical magnetic fields, and to discuss the possibility of their maintenance by dynamo action, with particular reference to the effects of turbulent distributions of force and of velocity.

Chapter 1 is devoted to an overall review of the dynamo problem, from both the observational and the theoretical points of view. Schuster's hypothesis concerning the magnetic fields of massive rotating bodies is also discussed. It is pointed out that this hypothesis has no experimental justification, and that it leads to incorrect predictions in certain cases. Extreme caution must therefore be employed when the hypothesis is used to predict the surface magnetic fields of bodies for which no observational data are available.

In Chapter 2 a review of mean field electrodynamics is presented, and the mean field dispersion relation for "wave" mean fields is cast in a novel determinantal form. a new terminology is proposed for several types of homogeneous, stationary turbulence with particular invariance properties. It is hoped that this terminology will reduce the confusion which has sprung up in recent years in connection with the terms isotropic and mirror-symmetric.

turbulence (i.e. stationary, homogeneous turbulence who e average properties are invariant under space-time inversion) on magnetic fields which vary on scales larger than the turbulence correlation length and time. It is proved that the claim of Lerche and Low (1971) that isotropic turbulence in an incompressible fluid can support dynamo action is unfounded. Indeed, no PT-invariant turbulence can support dynamo action in an incompressible fluid, in the first order smoothing approximation.

The decay of "wave" mean fields in the presence of PT-invariant turbulence is also studied in Chapter 3. is found that a number of conditions must be satisfied by the turbulence and the mean field if spatially periodic mean fields are to exist\ The case of isotropic Gaussian turbulence is considered in detail, and several restrictions on the parameters of the turbulence and the mean field are derived. These restrictions can be interpreted as restrictions on the usefulness of the Rädler expansion, (Rädler, 1968; Krause and Rädler, 1971) as a representation of the fluctuating e.m.f.  $u \times B'$ . It is also shown that the Rädler expansion is not useful when the mean field oscillates with time. Several restrictions on the existence of spatially periodic, oscillatory, decaying mean fields are derived, and the behaviour of fields satisfying these restrictions is studied numerically. It is suggested that

the numerical techniques used here may well provide the most convenient method for investigating dynamo action generated by non-PT-invariant turbulence. The possibility of a dynamo with sporadic helicity is also discussed.

inhomogeneous turbulence and its treatment within the framework of mean field electrodynamics. A successive approximation technique is developed, and is applied to the kinematic dynamo problem in this chapter. Later, in Chapter 6, the technique is used in an investigation of the hydromagnetic dynamo problem. The possibility of introducing helicity through large-scale variations of the turbulent velocity distribution is also discussed in Chapter 4. In Chapter 6, an example is provided in which helicity is produced by means of large-scale variations in the turbulent body force distribution.

astrophysical magnetic fields is studied, and the suggestion is made that variations of this sort may well be subject to boundary-layer control in the geodynamo, This possibility first arises in connection with the "a²(r)" dynamo in a spherical shell, which is studied in detail. A more general study is then carried out, making use of a novel representation of the magnetic multipole moments of a spherical current distribution in terms of the integral moments of the internal magnetic flux density. It is shown

that for the geodynamo, boundary-layer control is only likely for field variations on time scales less than 10<sup>4</sup> years. Dipole wobble and large-scale variations of the axial magnetic dipole moment are shown to arise from certain distributions of velocity near the outer boundary of the Earth's fluid core.

In Chapter 6 the idea of boundary-layer control of the external magnetic field of a spherical current distribution is studied in connection with the hydromagnetic dynamo problem. It is shown that radial forces at the core-mantle interface in the geodynamo cannot account for the observed temporal variations of the geomagnetic dipole moment. However, it is shown that the slow, systematic decrease of the Earth's speed of rotation can explain the observed wobble of the geomagnetic dipole axis if the viscosity at the core-mantle interface is of the order  $v \sim 1-2$  m<sup>2</sup>/sec. Non-periodic variations in the axial dipole moment on time scales similar to those which characterize geomagnetic polarity transitions can also arise from the slow decrease of the Earth's speed of rotation.

The effects of a turbulent distribution of body forces in the Earth's fluid core are also considered in Chapter 6. Turbulent forces deep in the core can produce a variety of effects. The dominant effects are determined, in large part, by the characteristic length scale of the

turbulence and the ratio of the diffusion time on this length scale to the effective time scale of the turbulence. In most cases, a rotation-dependent  $\alpha$ -effect is dominant at low values of the mean magnetic flux density, the effect being controlled either by the mean flow in the core or by gradients of the turbulent force intensity. However, under certain conditions other effects can be dominant. The relevance of these conditions to the Earth's core is discussed. At large values of the mean magnetic flux density, the fluctuating e.m.f.  $\overline{u}$   $\times$   $\overline{E}$  goes to zero. A detailed description of the types of behaviour which may occur is given at the end of section 6.4.6.

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35

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## APPENDÎX 1

### UNITS AND CONVERSION-FACTORS

### A.1.1 SI units

In this thesis, SI units are used as a gereral rule. For convenience, a summary of units commonly encountered is given in Tables 18 and 19. These tables include conversion factors relating SI units to unrationalized c.g.s. electromagnetic units. More complete summaries are to be found in many standard texts. (See, for example, Stratton, 1941, pp. 601-603; Allen, 1963, pp. 21-29; Land, 1972, pp. 3-4.)

It should be noted that in Tables 1-6, magnetic flux densities are quoted in gauss to facilitate comparison with values given in the literature on astrophysical magnetic fields. As may be seen from Table 19, the conversion factor which must be used to convert these flux densities to SI units is

1' gauss (G) = 
$$10^{-4}$$
 weber/m<sup>2</sup> (Wb/m<sup>2</sup>) (A1.1)  
=  $10^{-4}$  tesla (T) (A1.1)

## A.1.2 Magnetic dipole moments

In the literature on astrophysical magnetic fields, magnetic dipole moments are frequently given in gauss-cm<sup>3</sup> (see, for example, Warwick, 1971; Sharp, Russell and

in contrast to the dimensions  $L^2T^{-1}Q$  quoted for magnetic moment in Table 19. The discrepancy lies in the definition of "magnetic dipole moment". In e.g.s. electromagnetic units, the "dipole moment" measured in gauss em has exactly the same magnitude as the "dipole moment" measured in oersted-cm (or erg/gauss), provided that  $\mu = 1$ . Since this condition is satisfied in rest astrophysical situations, we may treat astrophysical dipole moments given in gauss-cm on the same footing as those given in erg/gauss (oersted-cm). The conversion factor to be used is

 $1 \text{ erg/gauss} = 10^{-3} \text{ amperc-m}^2 (\text{Ay·m}^2)$  (A1.2) as indicated in Table 19.

It should be noted that several detailed discussions of the problem of units in electromagnetic theory have appeared in the last few years. A particularly useful account is given by F. Primdahl, in Analysis of units in electromagnetism, Publications of the Earth Physics Branch, Department of Energy, Mines and Resources, Ottawa, Canada, vol. 42, no. 1, 1971.]

TABLE 18 - MECHANICAL UNITS

Quantity	Symbol	Dimensions	sı, mis	Conversion	sion to cgs unit	
Length		1	metre (m)	= 10 <sup>2</sup>	centimetre (cm)	
Mass		Σį	kilogram (kg)	= 103	gram (g)	
Time		Ė	second (sec, s)		second	
Speed	, p	LT-1	m/sec	= 102	cm/sec	
Density	o.	ML-3	kg/m³	= 10-3	g/cm <sup>3</sup>	
Force	l well f	MLT-2	newton (nt)	105	dyne	-
Pressure '	,Ω, (	ML-17-2	nt/m <sup>2</sup>	= 10	dyne/cm <sup>2</sup>	
Force density	4	ML-2T-2	nt/m <sup>3</sup>	- 10-1	dyne/cm <sup>3</sup>	
Energy		ML 2 T-2	joule	= 107	erd	
Angular frequency	υ, ω	$T^{-1}$	radian/sec	11	radian/sec	
Angulak momentum	, J	$ML^2\dot{r}^{-1}$	joule sec	7 - 10	erg•sec .	
Moment of inertia	Ţ	ML <sup>2</sup>	kg·m²	= 107	g.cm <sup>2</sup>	
Bulk Viscosity	آلام	$ML^{-1}T^{-1}$	nt·sec/m <sup>2</sup> "	п 10	poise	
Kinematic viscosity	2	L2T-1	m <sup>2</sup> /sec	= 104	2, to 2, to 3, to	

cds e.m.u (0e) oersted maxwell (Mx) Conversion erg/gauss erg/gauss (<u>U</u> gauss (G)  $cm^2/sec$ unrationalized e.m.u. e.m.u, e.m.u. e.m.u, е. ш. е e.m.c, gauss 4# x 10-3 10-11 10-5 101 10-7 10-1 106 108 103 104 104 103 104 ELECTROMAGNETIC UNITS Ή Ħ 11 Ħ 11 Ħ Ħ H coulomb/m<sup>3</sup> ampere (A) tesla (T) SI unit weber (Wb) conjomp henry/m m<sup>2</sup>/sec volt/m A·turn/m joule/Te A/m<sup>2</sup> A.m<sup>2</sup>  $wb/m^2$ m/oqm Symbol Dimensions M-12-3TQ2  $ML^2T^{-1}Q^{-1}$  $L^{-2}T^{-1}Q$ MLT-20-1 L-TT-I MT-10-1 MLQ-2 12T-1  $L^{2}T^{-1}Q$ , 14 O TTO TABLE 19.  $_{\mathbf{T}}$  (1) ۶ 二 ø р M Electric field strength Magnetic field strength Magnetic dipole moment Magnetic flux density Magnetic diffusivity Quantity Current density Charge density Permeability. Magnetic flux Conductivity Current Charge

### APPENDIX'2

### MULTIPOLE MOMENTS OF CURRENTS IN A SPHERE

## A.2.1 The multipole expansion of the external magnetic field

Consider the magnetic flux density  $\underline{B}$  due to a current distribution  $\underline{j}$  in a volume V whose exterior,  $\hat{V}$ , is insulating. The magnetic vector potential at the point  $\underline{r}$  is (Stratton, 1941, p, 234).

$$A(r) = \frac{\mu}{4\pi} \int_{\sqrt{|r-\bar{r}|}} d\bar{r}$$
(A2.1)

For points in  $\hat{V}$ , the quantity  $|x-\xi|^{-1}$  in the integrand of (A2.1) may usefully be expanded in a Taylor series to give

$$A(r) = \frac{\mu}{4\pi} \sum_{m=0}^{\infty} \frac{(-1)^m}{m!} \left\{ \frac{\partial^m}{\partial x_{a_1} \partial x_{a_2} \dots \partial x_{a_m}} \frac{1}{r} \right\}$$

$$= \int_{\mathbb{T}} \xi_{a_1} \xi_{a_2} \dots \xi_{a_m} j(\xi) d\xi$$
(A2.2)

$$=\frac{\mu}{4\pi}\sum_{m=0}^{\infty}\frac{(-1)^m}{m!}\left\{\left(\mathbf{r}\cdot\mathbf{v}\right)^m\frac{1}{r}\right\}\mathbf{j}(\mathbf{r})\,d\mathbf{r}$$
(A2.3)

The integrand in equation (A2.3) may be expanded as follows

$$\{(\underline{x}.\underline{y})^{m} \stackrel{!}{\vdash}\}_{\underline{j}} = \frac{1}{(m+1)} \left\{ \sum_{i=0}^{m} \underline{x}^{i} \underline{j} \underline{x}^{m-i} \cdot \underline{y}^{m} \stackrel{!}{\vdash} + \sum_{i=1}^{m} (\underline{j} \underline{x}^{m} - \underline{x}^{i} \underline{j} \underline{x}^{m-i}) \cdot \underline{y}^{m} \stackrel{!}{\vdash} \right\}$$

$$+ \sum_{i=1}^{m} (\underline{j} \underline{x}^{m} - \underline{x}^{i} \underline{j} \underline{x}^{m-i}) \cdot \underline{y}^{m} \stackrel{!}{\vdash}$$

$$+ \sum_{i=1}^{m} (\underline{j} \underline{x}^{m} - \underline{x}^{i} \underline{j} \underline{x}^{m-i}) \cdot \underline{y}^{m} \stackrel{!}{\vdash}$$

where we have used the notation

From (A2.4) we see that

$$= \frac{1}{(m+1)} \left\{ (\tilde{\mathbf{j}} \cdot \tilde{\mathbf{y}}') \tilde{\mathbf{j}}^{m+1} \cdot \tilde{\mathbf{y}}^{m} + \sum_{i=1}^{m} \left[ \tilde{\mathbf{j}} (\tilde{\mathbf{j}} \cdot \tilde{\mathbf{y}})^{m} - \tilde{\mathbf{j}} (\tilde{\mathbf{j}} \cdot \tilde{\mathbf{y}})^{m-1} \right] \frac{1}{r} \right\}$$

$$= \frac{1}{(m+1)} \left\{ \left[ \tilde{\mathbf{y}}' \cdot (\tilde{\mathbf{j}} \tilde{\mathbf{j}}^{m+1}) - (\tilde{\mathbf{y}}' \cdot \tilde{\mathbf{j}}) \tilde{\mathbf{j}}^{m+1} \right] \cdot \tilde{\mathbf{y}}^{m} \frac{1}{r} + \right.$$

$$+ m (\tilde{\mathbf{j}} \tilde{\mathbf{j}} - \tilde{\mathbf{j}} \tilde{\mathbf{j}}) (\tilde{\mathbf{j}} - \tilde{\mathbf{y}})^{m-1} \cdot \tilde{\mathbf{y}} \frac{1}{r} \right\}$$

$$= \frac{1}{(m+1)} \left\{ \left[ \tilde{\mathbf{y}}' \cdot (\tilde{\mathbf{j}} \tilde{\mathbf{j}}^{m+1}) - (\tilde{\mathbf{y}}' \cdot \tilde{\mathbf{j}}) \tilde{\mathbf{j}}^{m+1} \right] \cdot \tilde{\mathbf{y}}^{m} \frac{1}{r} \right\} + (A2.6)$$

$$+ \frac{m}{(m+1)} \left\{ (\tilde{\mathbf{j}} \cdot \tilde{\mathbf{y}})^{m-1} (\tilde{\mathbf{j}} \times \tilde{\mathbf{j}}) \times \tilde{\mathbf{y}} \frac{1}{r} \right\}$$

where

$$\nabla' \equiv \frac{1}{2}i \frac{\partial}{\partial t_i} \qquad (A2.7)$$

$$\nabla \equiv \frac{1}{2}i \frac{\partial}{\partial t_i} \equiv \frac{1}{2}i \frac{\partial}{\partial x_i} \qquad (A2.7')$$

Substituting (A2.6) into (A2.3), and applying Gauss' theorem, we obtain

$$A(\mathbf{r}) = \frac{\mu}{4\pi} \sum_{m=0}^{\infty} \frac{(-i)^m}{m!} \left\{ \frac{1}{(m+i)} \left[ \int_{\mathbf{S}} \mathbf{r} \cdot \mathbf{j} \, \mathbf{r}^{m+i} \, d\mathbf{s} \right] + \left[ (\mathbf{r} \cdot \mathbf{r}) \, \mathbf{r}^{m+i} \, d\mathbf{r} \right] \cdot \mathbf{r}^{m+i} \right\} + \frac{\mu}{(m+1)} \left[ \int_{\mathbf{S}} \mathbf{r} \cdot \mathbf{j} \, \mathbf{r}^{m+i} \, d\mathbf{r} \right] \cdot \mathbf{r}^{m+i} \, d\mathbf{r} \right\}$$

where S is the surface bounding the volume V. On S the boundary condition (1.59) applies - i.e.

$$\mathbf{n} \cdot \mathbf{j} = \mathbf{O}$$
 on  $\mathbf{S}$  (A2.9)

Also, in the quasi-steady approximation equation (1.15) . implies that

$$\nabla' \cdot \mathbf{j} = \mathbf{O} \tag{A2.10}$$

in V. Equation (A2.8) thus reduces to

$$A(r) = \frac{\mu}{4\pi} \sum_{m=1}^{\infty} \frac{(-1)^m}{m!} T^{(m)} \sqrt[n]{r} \times \sqrt[n]{r}$$
(A2.11)

where

$$T^{(m)} = \frac{m}{(m+1)} \int_{V} (\tilde{\chi} \times \tilde{\chi}) \tilde{\chi}^{m-1} d\tilde{\chi}$$
 (A2.12)

and we have used the notation

$$T^{(m)}, \nabla^{m-1} \times \nabla \frac{1}{r} \triangleq$$
(A2.13)

$$= \frac{1}{2} \left\{ \epsilon_{i,a,k} T_{a_{i},...,a_{m}}^{(m)} \frac{\partial^{m}}{\partial x_{k} \partial x_{a_{k},a_{k},a_{k}}} \frac{1}{\eta} \right\}$$

The magnetic flux density  $\overset{\circ}{\mathbf{B}}$  in  $\overset{\circ}{\mathbf{V}}$ , the exterior of volume V, is given by the curl of equation (A2.11).

$$\mathbf{B}(\mathbf{r}) = -\frac{\mu}{4\pi} \sum_{m=1}^{\infty} \frac{(-1)^m}{m!} \left\{ \mathbf{T}^{(m)} \cdot \mathbf{v}^m \right\} \mathbf{v}^{\frac{1}{\mu}}$$
(A2.14)

'Since B is continuous across S, by equations (1.56) and (1.57), equation (A2.14) is also valid on S.

# A.2.2 The magnetic multipole moments of a spherical current distribution

From equation (1.15) we have that

$$\mathbf{j} = \frac{1}{\mu} \mathbf{\Sigma}' \times \mathbf{B} \qquad (A2.15)$$

in V . Therefore

$$- \tilde{\Delta}_{i} \cdot (\tilde{k} \tilde{B} \tilde{k}_{m-1}) + (m+1) \tilde{B} \tilde{k}_{m-1}$$

$$= \frac{1}{\mu} \left\{ \tilde{\Delta}_{i} (\tilde{B} \cdot \tilde{k}_{m}) - (\tilde{B} \cdot \tilde{k}) \tilde{\Delta}_{i} \tilde{k}_{m-1} + (B^{2} \cdot 16) \right\}$$

$$= \frac{1}{\mu} \left\{ \tilde{\Delta}_{i} (\tilde{B} \cdot \tilde{k}_{m}) - (\tilde{B} \cdot \tilde{k}) \tilde{\Delta}_{i} \tilde{k}_{m-1} + (B^{2} \cdot 16) \right\}$$

$$= \frac{1}{\mu} \left\{ \tilde{\lambda}_{i} (\tilde{B} \cdot \tilde{k}_{m}) - (\tilde{B} \cdot \tilde{k}) \tilde{\lambda}_{m-1} + (B^{2} \cdot 16) \right\}$$

where we have made use of the identity

Substituting (A2.16) into (A2.12), we obtain

$$\frac{\mu(m+1)}{m} T^{(m)} = \int_{0}^{\infty} \{ \vec{y} \cdot (\vec{B} \cdot \vec{z}^{m}) - \vec{y} \cdot (\vec{z} \cdot \vec{B} \cdot \vec{z}^{m-1}) + (m+1) \vec{B} \cdot \vec{z}^{m-1} - (\vec{B} \cdot \vec{z}) \vec{y} \cdot \vec{z}^{m-1} \} d\vec{z}$$

$$= \int_{0}^{\infty} \{ \vec{y} \cdot \vec{B} \cdot \vec{z}^{m} - \vec{y} \cdot \vec{z} \cdot \vec{B} \cdot \vec{z}^{m-1} \} d\vec{z}$$

$$+ \int_{0}^{\infty} \{ (m+1) \vec{B} \cdot \vec{z}^{m-1} - (\vec{B} \cdot \vec{z}) \vec{y} \cdot \vec{z}^{m-1} \} d\vec{z}$$

$$+ \int_{0}^{\infty} \{ (m+1) \vec{B} \cdot \vec{z}^{m-1} - (\vec{B} \cdot \vec{z}) \vec{y} \cdot \vec{z}^{m-1} \} d\vec{z}$$

$$+ \int_{0}^{\infty} \{ (m+1) \vec{B} \cdot \vec{z}^{m-1} - (\vec{B} \cdot \vec{z}) \vec{y} \cdot \vec{z}^{m-1} \} d\vec{z}$$

When V is a spherical volume,

$$\mathfrak{n} \equiv \left\{ \mathfrak{I}/|\mathfrak{x}| \right\}_{s} , \qquad (A2.19)$$

and

$$\frac{n}{n} \frac{B}{n} \cdot \frac{m}{n} = n \cdot \frac{B}{n} \frac{m}{n} \quad \text{on} \quad S$$
(A2.20)

Also,

$$\underbrace{\mathbf{n} \cdot \mathbf{x}}_{n} \underbrace{\mathbf{g}}_{n} \underbrace{\mathbf{x}}_{m-1}^{m-1} = \mathbf{r}_{n}^{m} \underbrace{\mathbf{g}}_{n} \underbrace{\mathbf{n}}_{m-1}^{m-1} \quad \text{on} \quad \mathbf{S} \tag{A2.21}$$

where we have defined

$$r_0 \equiv |\xi|$$
 on  $S$  (A2.22)

Substituting (A2.20) and (A2.21) into equation (A2.18), weobtain

$$\frac{\mu(m+1)}{m} T^{(m)} =$$

$$= -c_{m} \int_{s} \vec{B} \, \vec{u}_{m-1} \, ds +$$

$$= -c_{m} \int_{s} \vec{B} \, \vec{u}_{m-1} \, ds + \int_{s} \vec{\Delta} \cdot (\vec{B} \, \vec{k}_{m-1}) \, d\vec{a} +$$

$$+ \int_{s} \{(m+1) \, \vec{B} \, \vec{k}_{m-1} - (\vec{B} \cdot \vec{k}) \, \vec{\Delta} \cdot \vec{k}_{m-1} \} \, d\vec{k}$$

$$= -c_{m} \int_{s} \vec{B} \, \vec{u}_{m-1} \, ds + \int_{s} \vec{\Delta} \cdot (\vec{B} \, \vec{k}_{m-1}) \, d\vec{a} +$$

$$+ \int_{s} \{(m+1) \, \vec{B} \, \vec{k}_{m-1} - (\vec{B} \cdot \vec{k}) \, \vec{\Delta} \cdot \vec{k}_{m-1} \} \, d\vec{k}$$

$$= -c_{m} \int_{s} \vec{B} \, \vec{u}_{m-1} \, ds + \int_{s} \vec{\Delta} \cdot (\vec{B} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k} \, \vec{k}_{m-1}) \, d\vec{a} + \int_{s} \vec{\Delta} \cdot (\vec{k}_{m-1}) \, d\vec{a} + \int$$

$$= -r_{o}^{m} \int_{S} B n_{o}^{m-1} dS +$$
(A2.23)

since

$$\nabla' \cdot \mathbf{B} = \mathbf{O}_{q} \tag{A2.24}$$

by equation (1.3).

### A.2.3 Surface terms, and theorems on spherical harmonics

Since the expansion (A2.14) is valid on S, we may substitute it into the surface integrals in equation (A2.23). Carrying out this substitution, and making use of the notation (5.93)-(5.95), we obtain

$$\int_{S} \overset{\mathbf{B}}{\approx} \overset{\mathbf{n}^{m-1}}{\alpha} dS =$$

$$= -\frac{\mu}{4\pi} \sum_{k=1}^{\infty} \frac{(-1)^{k}}{k!} T_{a_{1} \dots a_{k}}^{(k)} \int_{S} \partial_{a_{1} \dots} \partial_{a_{k}} \overset{\mathbf{v}}{\sim} \frac{1}{r} \overset{\mathbf{n}^{m-1}}{n} dS$$
(A2.25)

In order to evaluate the integrals on the right hand side of (A2.25), we must consider the properties of spherical harmonics.

Since the differential operators  $\partial_{a_i} \equiv \partial/\partial x_{a_i}$  and  $\nabla$  are commutative,

$$\nabla^2 \partial_{a_1} \dots \partial_{a_R} \frac{1}{r} = \partial_{a_1} \dots \partial_{a_R} \nabla^2 \frac{1}{r} = 0 \qquad (A2.26)$$

Thus  $\partial_{a_1} \cdots \partial_{a_n \frac{1}{r}}$  is a spherical harmonic. In general, for any polynomial homogeneous function  $f_n(x,y,z)$  of degree n,  $f_n(\partial_x,\partial_y,\partial_z)\frac{1}{r}$  is a spherical harmonic of

The expression vanishes is zero (Hobson, 1931, p. 127).

The expression vanishes is and only if  $f_{\Pi}(x,y,z)$  is a multiple of  $\{x^2 + y^2 + z^2\}_{\overline{x}}$ . It follows that  $\partial_{a_1} \dots \partial_{a_k} \frac{1}{r}$  is a spherical harmonic of degree - (k+1). From the properties of spherical harmonics, we have that

$$\frac{n \cdot \nabla}{n} \partial_{a_{1}} \dots \partial_{a_{R}} \frac{1}{r} = \frac{\partial}{\partial r} \partial_{a_{1}} \dots \partial_{a_{R}} \frac{r}{r}$$

$$= -\frac{(R+1)}{r_{0}} \partial_{a_{1}} \dots \partial_{a_{R}} \frac{1}{r} \qquad (A2.27)$$

on S, as pointed out in equation (5.96).

It may also be shown (Hobson, 1981, pp. 147-148) that the components  $\{n_i\}$  of the unit vector normal to S satisfy

$$n_{b_1} \dots n_{b_q} = \frac{1}{r_q^q} x^{p_1} y^{p_2} z^{p_3}$$
, where  $(p_1 + p_2 + p_3) = q$ 

$$= \sum_{i \neq 0} Y_{q-2i} (r_i; \theta_i; \phi)$$
(A2.28)

where [q/2] denotes the largest integer less than or equal to q/2, and  $Y_n(r;\theta,\phi)$  is a solid spherical harmonic of degree n. It follows that the integrals appearing on the right hand side of equation (A2.25) are of the form

$$\int_{S} \partial_{a_{1}} \cdots \partial_{a_{k}} \frac{1}{r} n_{k_{1}} \cdots n_{k_{m}} dS = \frac{1}{r_{k}^{m}} \sum_{i=0}^{\lfloor m/2 \rfloor} \int_{S} Y_{k_{i}} Y_{q-2i} dS$$
(A2.29)

where  $Y_k$  and  $Y_{q-2i}$  are spherical harmonics of degrees n and q-2i respectively.

In general (Hobson, 1931, p. 144), if  $Y_m$  and  $Y_n$  are spherical harmonics of degrees m and n respectively,

$$\int_{S} Y_{m}' Y_{n} dS = 0 , m \neq n$$
 (A2.30).

Combining (A2.29) and (A2.30), and substituting the resulting expression into equation (A2.25), we find that

$$\int_{S} B \, n^{m-1} \, dS =$$

$$= -\frac{\mu}{4\pi} \sum_{k=1}^{\lfloor (m-1)/2 \rfloor} \frac{(-1)^{m+1}}{(m-2k)!} \, T_{a_1 \dots a_{m-2k}}^{(m-2k)}$$

$$= \int_{S} \partial_{a_1} \dots \partial_{a_{m-2k}} \partial_{b_1} \frac{1}{r} \, n_{b_2} \dots n_{b_m} \frac{1}{r} b_{a_m} \frac{1}{r} b_{a_m}$$
(A2.31)

In order to obtain explicit expressions for the integrals on the right hand side of (A2.31) we must apply the theorems

$$\int_{S} n_{b_{1}} \sin n_{b_{2}} dS = 4\pi r_{0}^{2} \frac{2^{3/2} (9/2)!}{(94!)!} \sum_{\substack{pairs \\ (b_{1} \dots b_{q})}} \delta_{y_{1} y_{2} \dots y_{q}} \delta_{y_{q-1} y_{q}},$$

$$(9/ever) \qquad (A2, 32)$$

$$\int_{S}^{1} n_{b_{1}} n_{b_{2}} dS = 0 \qquad (q, odd) \qquad (A2.32!)$$

$$\partial_{a_{i}}...\partial_{a_{m}}\frac{1}{r} = \frac{(-i)^{m}}{r^{m+1}}\sum_{i=0}^{\lfloor m/2\rfloor}(-i)^{i}\frac{(2m-2i)!}{2^{m-i}(m-i)!}$$
 (A2.33)

$$\sum_{\substack{(a_1 \dots a_m) \\ (\epsilon_{2i} \mid \eta_{m-2i})}} \eta_1 \eta_2 \dots \eta_{m-2i} \sum_{\substack{\text{pairs} \\ (\epsilon_1 \dots \epsilon_{2i})}} \gamma_1 \tau_2 \dots \delta_{\tau_{2i-1} \tau_{2i}}$$

where

∑ (a,...am) (e<sub>21</sub>1η<sub>m-21</sub>) denotes a summation over all distinct partitions of the set  $(a_1, a_2, \dots, a_m)$  into one subset of 2i elements and another of m-2i elements,

and

\(\sum\_{\text{pairs}}\)
\((c\_1 \ldots c\_{2l})\)

denotes a summation over all distinct groupings of the elements of the set  $(c_1, c_2, \dots, c_{2i})$  into pairs  $(\gamma_1 \gamma_2; \gamma_3 \gamma_4; \dots; \gamma_{2i-1} \gamma_{2i})$ .

Equations (A2.32) and (A2.32') can be verified from the formula given on p. 156 of Hobson (1931). Equation (A2.33) can be verified by induction.

Substituting (A2,32)-(A2,33) into equation (A2,31), we obtain the expression

$$r_{0}^{n} \int_{S} \frac{8}{n} n^{n-1} dS = \frac{(n-1)/2}{2} \frac{2^{n} r_{0}^{2k}}{(n-2k)!} T_{a_{1} \dots a_{n-2k}}^{(n-2k)} \frac{1}{2^{n} b_{1} \dots b_{n}}$$

$$= \frac{2\mu}{k} \sum_{k=1}^{n} \frac{2^{n} r_{0}^{2k}}{(n-2k)!} T_{a_{1} \dots a_{n-2k}}^{(n-2k)} \frac{1}{2^{n} b_{1} \dots b_{n}} \frac{1}{2^{n} b_{1} \dots b_{n}}$$

$$= \frac{n+1}{2} - k \frac{1}{2^{n} - k} \frac{(2n-4k-2i+2)! (n-k-i)!}{(2n-2k-2i+1)! (n-2k-i+1)!}$$

(A2.34)

$$\sum_{\substack{(a_1 \dots a_{n-2k}, b_i) \\ (\epsilon_{2i} \mid \eta_{n-2k+1-2i})}} \sum_{\substack{pairs \\ (\eta_1 \dots \eta_{n-2k+1-2i}, b_2 \dots b_n)}} \delta_{\xi_1 \xi_2 \dots \xi_{2n-2k-2i-1}} \delta_{\xi_{2n-2k-2i-1}} \delta_{\xi_{2n-2k$$

## A.2.4 Expressions for the magnetic multipole moments

Equation (A2.34) may now be substituted into equation (A2.23) to give the following expression for the magnetic multipole moments of a current distribution in a sphere.

This expression is written out in full for m = 1,2,3in equations (5.77)-(5.79).

It may be seen from equation (A2.35) that the expression for the  $2^m$ -pole moment tensor  $T_{a_1a_2...a_m}^{(m)}$  involves terms of two different types. The first type of term, represented by the volume integrals in (A2.35), relates  $T^{(m)}$  to the (m-1)-order integral moments of the

magnetic flux density B in the spherical volume V. The second type of term, represented by the summation terms in (A2.35), relates T<sup>(m)</sup> to the magnetic multipole tensors of order {[m-2], [m-4], [2 or 1]}. Thus T<sup>(m)</sup> has explicit relationships only with the lower-order magnetic multipole moments of the same parity (i.e. me even or odd). Relationships with multipole moments of the opposite parity will arise from the integral terms in equation (A2.35).

### A.2.5 Electric multipole moments

The multipole expansion of the electric field is obtained in much the same way as that for the magnetic field. In general, the electric field E satisfies

$$\mathbf{E} = -\mathbf{\nabla} \Phi - 2\Delta/\mathbf{at} \qquad (A2.36)$$

In the exterior region  $\hat{V}$ , the vector potential  $\underline{A}$  is given by the expansion (A2.11), while the scalar potential  $\underline{\Phi}$  is given by

$$\frac{1}{4\pi\epsilon} \int_{V} \frac{\theta(\xi)}{|\chi - \xi|} d\xi$$

$$= \frac{1}{4\pi\epsilon} \sum_{m=0}^{\infty} \frac{(-1)^{m}}{m!} \int_{V} \theta(\xi) \left\{ \xi \cdot \nabla \right\}^{m} \frac{1}{r} d\xi$$

$$= \frac{1}{4\pi\epsilon} \sum_{m=0}^{\infty} \frac{(-1)^{m}}{m!} \left\{ \int_{V} \theta \xi^{m} d\xi \right\} \cdot \nabla^{m} \frac{1}{r} \qquad (A2.37)$$

The electric multipole moment tensors,  $\varrho^{(m)}$  , may therefore be defined as

$$\mathbf{Q}^{(m)} \equiv \int_{\mathbf{V}} \mathbf{\theta}(\mathbf{x}) \mathbf{x}^{m} d\mathbf{x}$$
 (A2.38)

Substituting (A2.11), (A2.37), and (A2.38) into equation (A2.36), we obtain the expansion

$$E = -\frac{1}{4\pi\epsilon} \sum_{m=1}^{\infty} \frac{(-1)^m}{m!} Q^{(m)} \cdot \nabla^m \nabla^{\frac{1}{r}} +$$

$$-\frac{A}{4\pi\epsilon} \sum_{m=1}^{\infty} \frac{(-1)^m}{m!} \dot{T}^{(m)} \cdot \nabla^{m-1} \times \nabla^{\frac{1}{r}}$$
(A2.39)

There is no contribution from the zero-order electric multipole moment tensor  $Q^{(0)}$  in (A2.39) since, as shown in equation (5.75);

$$Q^{(0)} = -\epsilon \int_{V} \nabla \cdot \{ u \times B \} d\xi$$

$$= -\epsilon \int_{S} n \cdot \{ u \times B \} dS \qquad (A2.40)$$

in the quasi-steady approximation. When the no-slip condition (1.62) applies on S, equation (A2.40) reduces to

$$\mathbf{Q}^{(o)} = \mathbf{O} \tag{A2.40'}$$

Equation (A2.39) is the expansion used for E in  $\hat{V}$  in section 5.4.2.

### APPENDIX 3

# EVALUATION OF INTEGRALS ASSOCIATED WITH INITIAL CONDITION I IN CHAPTER 3

## A.3.1 Integrals of section 3.7.4

Many of the integrals associated with the mean field dispersion relation studied in Chapter 3 must be evaluated numerically. In this appendix we shall deal with the integrals associated with initial condition I.

In section 3.7.4 the dispersion relation for Gaussian isotropic turbulence and non-oscillatory mean fields is considered. An approximate form of the relation is obtained by assuming equality on the right hand side of condition (3.105) - i.e. assuming that

$$\int_{\eta K^2} \Omega = (R_m)^2 J_2$$
 (A3.1)

where  $J_2$  is defined in (3.107). The present author and Dr. K.D. Aldridge have developed a program which evaluates the integral in (A3.1), thus giving R' as an approximate function of Im  $\Omega/\eta K^2$ , q,  $\lambda_C K$ , and  $T/\eta \tau_C$ .

The required inputs to the program are:

$$Q \equiv q \qquad (A3.2)$$

YNOT 
$$\equiv \text{Im } \Omega/\eta K^2$$
 (A3.3)

$$ALP \equiv \lambda_C/L = \lambda_C K/2\pi \qquad (A3.4)$$

$$XUL \equiv T/q\tau_C \tag{A3.5}$$

NX 3 half the number of integration steps (A3.6)

The integration is carried out using a Simpson's Rule technique. The program outputs are:

ALP 
$$\equiv \lambda_{\rm c}/L$$

Al  $\equiv J_2(q,\lambda_{\rm c}K;T)$ , defined in (3.107) (A3.7)

A2  $\equiv [R_{\rm m}^*/q]^2$ , defined by (A3.1) (A3.8)

A3  $\equiv R_{\rm m}^*/q$  (A3.9)

The integral in (3.107) is denoted by VOLR.

```
2 WRITE(6.750)
         750 FORMAT( NEED Q. YNOT !)
             READ(5.250.END=40)
         250 FORMAT(2F10.7)
           7 WRITE(6,930)
             READ(5.940.END=2)
          .3 WRITE(6,850)
         850 FORMAT ( 'NEED XUL, NX')
             READ(5,350,END=7)
         350 FORMAT(1F10.7.13)
        . 930 FORMAT ('NEED ALP')
13
                                                       (A3.10)
         940 FORMAT(F10.7)
20
              VOLRESIMRE (ALP, Q, YNOT, XUL, NX)
20.25
              A1= VOLR/3.
20.5
              A2=(YNOT-1.)/(A1+Q+Q)
20.51
              A3=SQRT(A2)
          21 WRITE(6,920) ALP+A1+A2,A3
23
              WRITE(6.970)
         970 FORMAT(//)
         920 FORMAT (F7.4,3E18.8)
26
             GO TO 3
27
          40 STOP
```

```
30
               FUNCTION ENV(ALP.Q.YNOT.X)
31
               PI=3.141592653
32
               GX=4.*PI*PI*ALP*ALP*X
33
               T=1./(1.+2.*X)
34
               EX = -X + X + Q + Q/2 + GX + (YNOT - T)
35
               IF(EX.GT.170) GO TO 40
36
               GO TO., 60
                                                          (A3.10')
37
            40 ENV=0
38
               GO TO 100
39
            60 ENV=EXP(EX) *T * * 2.5
40
               GD TO 300
41
           100 WRITE (6.200) EX
42
          200 FORMAT (*EXPONENT=*.F10.2)
43
          300 RETURN
               END
45
               FUNCTION SIMREXALP, Q. YNOT . XUL'N)
               EXTERNAL ENV
46
47
               PI=3.141592663
48
               H=XUL/(2.*N)
49
               SUME V=0
50
               SUMOD=0
51
               DO 49 J=1.N
52
               HOD=H*(2.*J-1)
                                                          (A3.10")
53
               HEV=H*(2.*J-2.)
54
               SUMEV=SUMEV+ENV(ALP+Q+YNOT+HEV)"
55
               SUMOD=SUMOD+ENV(ALP,Q,YNOT,HOD)
56
           49 CONTINUE
57
              FST=ENV(ALP.Q.YNOT.0)
58
              FFN=ENV(ALP.Q.YNOT.XUL)
59
              SUM=4. *SUMOD+2. *SUME V-FST+FFN
60
              SIMRE=H+SUM/3.
61
              RETURN
62
              END
```

Ŷ

#### A.3.2 Integrals of section 3.8.5

Section 3.8.5 deals with conditions on the turbulence for stable decay to be established before significant energy is lost from the mean field. It is shown that the stabilization time  $T_1$  must be less than  $T^*$ , where  $T^*$  is defined by (3.132). Combining (3.132) and (3.133), we see that  $T^*$  may also be determined from the equation

$$DELT (T/\tau_c) = \begin{cases} 4m \frac{\Omega}{\eta K^2} \int_0^{T/\eta \tau_c} e^{-\frac{1}{2}q^2x^2 + q\tau_c \eta K^2 \left[4m \frac{\Omega}{\eta K^2} - \frac{1}{1+2x}\right]x} \frac{dx}{(1+2x)^{5/2}} \\ - \frac{1}{(\lambda_c K)^2} \right\} (\lambda_c K)^2 \end{cases}$$

$$= 0 \qquad (A3.11)$$

The program given below finds approximate zeroes of DELT.

The required inputs are:

$$Q \equiv q$$
 
$$ALP \equiv \lambda_{C}/L$$
 
$$YNOT \equiv trial\ value\ of\ Im\ \Omega/\eta K^{2}$$
 
$$(A3.12)$$
 
$$XUL \equiv T/q\tau_{C}$$
 
$$NX \equiv half\ number\ of\ integration\ steps$$

TOL = upper limit on DELT for acceptable solution of (A3.11)

Outputs from the program are

$$Q = q$$

$$ALP = \lambda_{G}/L$$

```
YNOT value of Im \Omega/\eta K^2 for which (A3.11) is approximately satisfied

The value of T/\tau_C for which (A3.11) is approximately satisfied

(A3.13)

Ale value of R_m/q defined by The and (3.134)
```

DELT E final value of DELT

It should be noted that (A3.11) is in fact a generalization of (3.132), since the upper limit of integration in (3.132) has been allowed to go to  $\infty$ .

```
PI=3.141592653
            2 WRITE (6.750)
          750 FORMAT( NEED d.ALP. YNOT . XUL. NX. TOL.)
 3
              READ(5.250-END=40) Q.ALP.YNOT.XUL.NX.TOL
 5
          250 FORMAT(4F10,7.13.F10.7)
              TPA=2.*PI*ALP
           25 YPHYNOT+TOL+(YNOTHIA)
 6.25
 6.5
              YM=YNOT-TOL*(YNOT-1.)
              VOLTES IMRE (ALP. Q. YP. XUL. NX)
 6.6
 6.7
              VOLMASIMRE(ALP.Q.YM.XUL.NX)
              VOLR=SIMRE(ALP+Q+YNOT+XUL+NX)
              DELIT=TPA+TPA+YNOT+VOLR-1.
              IF (ABS(DELT).LT.TOL) GO TO 311
              DOEL=TPA+TPA+(VOLR-YNOT+(VOLP-VOL
 8.35
             1 (YNOT-1.)))
 8.5
              IF(DDEL.EQ.O) GO TO 2
 8.6
              YNOT=YNOT-DELT/DDEL
 8.7
              IF(YNOT.LT.1.) GO TO 40
 8.8
              GO TO 25
         311 T1=Q/(TPA+FPA+YNOT)
16
17
              A1=TPA*SQRT(3.*YNOT*(YNOT-1.))/Q
18
            WRITE(6,920) Q.ALP.YNOT.T1.A1.DELT
19
         920 FORMAT (2F7.4.F7.5.3E18.8.//)
20
             GO TO 2
21
          40 STOP
22
            / END
23
```

```
FUNCTION ENV(ALP.Q.YNOT.X)
24
25
              PI=3.141592653
26
              GX=4.*PI*PI*ALP*ALP*X
              T=1./(1.+2.*X)
27
              EX=-X*X*Q*Q/2*+GX*(YNOT-T)
28
              IF(EX.GT.170) GO TO 40
29
30
              GO TO 60
           40 ENV=0
31
32
              GO TU 100
           60 ENV=EXP(EX) +T ++ 2.5
33
              GO TO 300
34
          100 WRITE (6,200) EX
35
          200 FORMAT( *EXPONENT= *. F10.2)
36
          300 RETURN
37
              END
38
                                                        (A3.14')
              FUNCTION SIMRE (ALP, Q, YNOT, XUL, N)
39
40
              EXTERNAL ENV
41
              PI=3.141592653
              H=XUL/(2.*N)
42
              SUME V=0
43
44
              SUMOD=0
              DO 49 J=1.N
45
              HOD=H*(2.*J-1)
46
              HEV=H+(2.+J-2.)
47
48
              SUMEV=SUMEV+ENV(ALP+Q+YNOT+HEV)
              SUMOD= SUMOD+ENV(ALP.Q.YNOT.HOD)
49
           49 CONTINUE
50
              FST=ENV(ALP,Q,YNOT,0)
51
52
              FFN=ENV(ALP,Q,YNOT,XUL)
              SUM=4. *SUMOD+2. *SUMEV-FST+FFN
53
54
              SIMRE=H+SUM/3. ,
              RETURN
55
56
```

## A.3.3 Integrals of section 3.9.2

When the dispersion relation for Gaussian isotropic turbulence and oscillatory mean fields is considered, the integrals to be evaluated are those defined in section 3.9.2. The techniques of the last two sections can be used in the case when the approximate dispersion relation (3.143) is to be solved. The subroutines given below evaluate the integrals in (3.144a) and (3.144b) by a Simpson's Rule technique similar to that used in (A3.10"). The required inputs are:

ALP 
$$\equiv \lambda_{\rm C}/L$$

BEP  $\equiv \tau_{\rm C}\eta K^2/2\pi$ 

ZNOT  $\equiv {\rm Re} \Omega/\eta K^2$ 

(A3.15)

 $N \equiv half$  number of integration points and the outputs are:

SIMRE 
$$\equiv 3J_{2R}$$
, defined in (3.144a) (A3.16) SIMIM  $\equiv 3J_{2I}$ , defined in (3.144b)

The subroutine ENV is ancluded for completeness.

No outline is given here of the methods used in searching for solutions to (3.143a) and (3.143b). See section 3.9.4 and Appendix 4.

```
44
               COSE V=COS(2.*P1*BEP*ZNOT*HEV)
 45
               SUME V=SUME V+ENV (ALP.BEP.ZNOT.YNOT, HEV.K)*COSEV
46
               COSOD=COS(2.*PI*BEP*ZNOT*HOD)
47
               SUMOD=SUMOD+ENV(ALP.BEP.ZNOT.YNOT.HOQ.K)*COSOD
48
           49 CONTINUE
49
               FST=ENV(ALP.BEP.ZNOT.YNOT.O.K)
50
               COSLST=COS(2.*PI*BEP#ZNOT*XUL)
51
              ,FFN=ENV(ALP,BEP,ZNOT,YNOT,XUL,K)*COSLST
52
               SUM=4. *SUMOD+2*SUMEV-FST+FFN
53
               SIMRE=H*SUM/3.
54
              RETURN
55
              END
                                                          (A3.17)
56
              FUNCTION SIMIM(ALP. BEP. ZNOT. YNOT. XUL. N)
57
              EXTERNAL ENV
58
              PI=3-141592653
59
              H=XUL/(2.*N)
60
              SUME V=0
61
              SUMOD=0
62
              DO 49 J=1.N
63
              HOD = H * (2 * J - 1)
64
              HEV=H+(2.+J-2.)
65
              SINEV=SIN(2.*PI*BEP*ZNOT*HEV)
66
              SUMEVESUME V+ENV (ALP.BEP.ZNOT.YNOT.HEV) + SINEV
67
              SINOD=SIN(2.*PI*BEP*ZNOT*HOD)
              SUMOD=SUMOD+ENV(ALP.BEP.ZNOT, YNOT.HOD) *SINOD.
68
69
           49 CONTONUE
70
              FST=0.
71
              SINLST=SIN(2.*PI*BEP*ZNOT*XUL)
72
              FFN=ENV(ALP.BEP.ZNOT.YNOT.XUL) +SINLST
73
              SUM=4. *SUMOD+2*SUMEY-FST+FFN
74
              SIMIM=H+SUM/3.
75
              RETURN
76
```

FUNCTION SIMPE (ALP, BEP, ZNOT, YNOT, XUL, N.K)

EXTERNAL ENV

H=XUL/(2.4N)

DO 49 J=1.N

HOD=H\*(2.\*J~1)

MEV=H\*(2.\*J-2.)

SUME V=0

SUMOD=0

PI=3:141592653

35

36

37

38

39

40

41

42

43

```
19
              FUNCTION ENV(ALP, BEP, ZNOT, YNOT, X, N)
20
              BEPX=BEP+X
21
              PI=3.141592653
22
              PALPSQ=PI*ALP*ALP
23
              T=PALPSQ/(PALPSQ+BEPX)
24
              EX=-X*X/2.+2.*P[*BEPX*(YNOT-T)
25
              IF(EX.GT.170) GO TO 40
26
              GO TO 60
27
          40 ENV=0
28
              GO TO 100
28.25
           60 IF(N.EQ.0) ENV=EXP(FX)+#***2.5
29
              IF(N.GT.0) ENV=EXP(EX)AT++2.5+X++N
30
              GO TO 300
31
          100 WRITE(6,200) EX
32
         200 FURMAT ( *EXPONENT = * . F 10.2)
33
         300 RETURN
34
              END
```

(A3.17")

#### APPENDIX 4

# EVALUATION OF INTEGRALS ASSOCIATED WITH INITIAL CONDITION 11 IN CHAPTER 3

# A.4.1 The integrals of section 3.10.1

In this appendix we shall consider the numerical solution of equations (3.165a) and (3.165b). The program described here was developed by the present author and Dr. K, D. Aldridge to obtain the results plotted in Figures 16-21.

The integrals in equations (3.165a,b), corresponding to the case of Gaussian turbulence in an incompressible fluid, are not in the most convenient form for numerical evaluation. We shall first obtain an explicit expression for 0. Combining equations (3.42) and (3.43), and carrying out the integration, we have

$$\Theta = 25^{4} \int_{0}^{\pi} \frac{\sin^{3}\theta \ d\theta}{(1+5^{2} - p + 25\cos\theta) + i\nu}$$

$$= 5^{3} \int_{0}^{\pi} \frac{(1-x^{2}) \ dx}{x+x}$$

$$= 25^{3} \left\{ x + (x^{2}-1) - \frac{1}{2} \ln \frac{x-1}{x+1} \right\}$$

where

$$x = \cos \theta$$
 (A4.2)

(A4.1)

$$X = \frac{1}{25} \{ 1 + \xi^2 - P + i P \}$$
 (A4.3)

Defining

$$F \equiv 1 + \xi^2 - P \tag{A4.4}$$

so that

$$X = \frac{1}{25} \{ F + i \nu \}$$
 (A4.5)

we may take real and imaginary parts of (A4.1) to obtain

$$Re \Theta = F \xi^{2} + \frac{1}{8} \xi (F^{2} - v^{2} - 4 \xi^{2}) ln \left\{ \frac{(F - 2\xi)^{2} + v^{2}}{(F + 2\xi)^{2} + v^{2}} \right\} + \frac{1}{2} F \xi \hat{v} tan^{-1} \left\{ \frac{4 \xi v}{F^{2} - 4 \xi^{2} + v^{2}} \right\}$$
(A4, 6a)

$$\int m \Theta = \nu \xi^{2} + \frac{1}{4} F \nu \ln \left\{ \frac{(F-2\xi)^{2} + \nu^{2}}{(F+2\xi)^{2} + \nu^{2}} \right\} + \frac{1}{4} \xi (F^{2} - \nu^{2} - 4\xi^{2}) \tan^{-1} \left\{ \frac{4\xi \nu}{F^{2} - 4\xi^{2} + \nu^{2}} \right\}$$

Further simplification of the integrals in (3.165a,b) can be obtained by making use of the fact that Re  $\theta$  is even in  $\nu$ , while Im  $\theta$  is odd in  $\nu$ . Thus if

$$I^{(3,165)} = \int_{-\infty}^{\infty} d\nu \int_{-\infty}^{\infty} d\xi \, e^{-\frac{1}{2} \left\{ (\lambda_c \kappa \xi)^2 + (\eta \kappa^2 \tau_c)^2 (\nu + \Re \frac{\Omega}{\eta \kappa^2})^2 \right\}}$$

$$\Theta(\xi, \nu; \oint_{-\infty}^{\infty} \frac{\Omega}{\eta \kappa^2}) \qquad (A4.7)$$

we may write

$$Re I^{(3.165)} = 2 \int_{0}^{\infty} dv \int_{0}^{\infty} d\xi Re \Theta \cosh \{\sqrt{2} \tau_{c} \Re \Omega \cdot v\} - \frac{1}{2} \{(\lambda_{c} \kappa \xi)^{2} + (\eta \kappa^{2} \tau_{c})^{2} (\theta^{2} + [\Re \frac{\Omega}{\eta \kappa^{2}}]^{2})\}$$

 $\int_{0}^{\infty} I^{(3.45)} = 2 \int_{0}^{\infty} d\vec{r} \int_$ 

$$Re I^{(3.165)}$$

$$= \int_{0}^{\infty} dv \left[ \frac{1}{4} \left[ (\lambda_{c} K_{c}^{2})^{2} + (\nu - Re \frac{\Omega_{c}}{\eta k_{c}})^{2} \right] + e^{-\frac{1}{2} \left[ (\lambda_{c} K_{c}^{2})^{2} + (\nu - Re \frac{\Omega_{c}}{\eta k_{c}})^{2} \right]} \right]$$

$$\int_{0}^{\infty} \int_{0}^{(3.465)} dY \int_{0}^{\infty} dY \int_{0}^{\infty} dY \int_{0}^{\infty} dY \int_{0}^{\infty} \left[ (\lambda_{cK} Y)^{2} + (\nu_{c} Re \frac{\Omega}{\eta K^{2}})^{2} \right] + e^{-\frac{1}{2} \left[ (\lambda_{cK} Y)^{2} + (\nu_{c} Re \frac{\Omega}{\eta K^{2}})^{2} \right]} dY \int_{0}^{\infty} dY \int_{0}^{\infty}$$

Equations (A4.9a,b) show the form of the integrals in (3.165a,b) used in the program.

## A.4.2 The nature of the program

or

A brief outline of the numerical search procedure used is given in section 3.10.2. The integrations in (A4.9a,b) are carried out using an n-point Gaussian technique. The first input required by the program is a listing of the Gaussian points and weights to be used. A convenient form for the storage of this data is shown in section A.4.4.

The next set of inputs required is listed on line 370 of the program (see section A.4.3). For example,

EPY1  $\equiv$  fraction of the peak value of the integrand in (A4.9a,b) below which contributions from the region near  $\xi = 0$  can be ignored

Similar definitions apply to EPY4 , EPG1 , and EPG2

These quantities refer to the regions  $\xi \to \infty$  ,  $\nu \to 0$  , and  $\nu \to \infty$  , respectively. In most cases it was assumed that

$$EPY1 = EPY4 = EPG1 = EPG2 = 0.0001$$
 (A4.10)

The last input requested in line 370 - the "number of steps, K" - is a measure of the "fineness" of the search for the point at which the value of the integrand drops to a fraction EPY(i) or EPG(i) of its peak value. In general, it was assumed that

$$K = 80 \qquad (A4 \sqrt{10'})$$

The remaining inputs are as follows:

ZNOT  $\equiv \text{Re } \Omega/\eta K^2$ 

YNOT  $\equiv \text{Im } \Omega/\eta K^2$ 

STALF = initial value of  $\lambda_C/L$ 

ALFSTP  $\equiv$  increment in  $\lambda_C/L$ 

TALF  $\equiv$  number of steps in  $\lambda_{c}/L$  (A4.11)

STBET  $\equiv$  initial value of  $\tau_{c}^{2}\eta\kappa^{2}/2\pi$ 

BETSTP = increment in  $\tau_C^{\eta K^2/2\pi}$ 

IBET = number of steps in  $\tau_{c} \eta K^{2}/2\pi$ 

For convenience in calculation,  $\lambda_{\rm C}/L$  and  $\tau_{\rm C}\eta K^2/2\pi$  values are multiplied by a factor  $\sqrt{2}\cdot\pi$  in lines 480-520. The program then works with the quantities

ALFA = AL = 
$$\lambda_c K / \sqrt{2}$$
 (A4.12)

BETA = BE 
$$\equiv \tau_C \eta K^2 / \sqrt{2}$$
 (A4.12')

The program carries out the necessary integrations in lines 530-2080, with the integrand of (3.165a) being split up into three parts, as described in section 3.10.2. The values of the integrals are then combined in lines 2090-2150 to give

RATIO 
$$\Xi$$
 D, as defined in (3.166) (A4.13)

RNLDS 
$$\equiv R_{\rm m}^{\bullet}$$
 (A4.14)

In lines 2160-2610, the program searches for zero crossings in D. If a zero crossing is found, a linear interpolation is performed to locate the zero approximately. The interpolation is carried out between the value of D at (ALFA, BETA) and the value at (ALFA+ALFSTP, BETA), for a given pair of values (ZNOT,YNOT): Finally, the position of the interpolated zero in D is used to give an approximate interpolation between the values of ALFA and RNLDS on either side of the zero crossing (see lines 2460-2540 and 2320-2340).

The output of the program is a tabular display of the form shown overleaf. If a zero crossing has been found in D, the values of D on either side of the zero are displayed as  $D_1$  and  $D_2$ .  $\alpha_{interp}$  and  $\alpha_{interp}$  are then the approximate interpolated values of ALFA and RNLDS at the zero in D. If no zero crossing is found,

the values of D and RNLDS at the last pair of ALFA values considered are displayed as  $[D_1, D_2]$  and  $[(R_m')_1, (R_m')_2]$ , while  $[\alpha_{interp'}, (R_m')_{interp}]$  are set equal to zero.

## Form of output

BETA

(Rm) interp (Rm) 2

D VALUES  $\begin{array}{c} D \\ 1 \\ D_2 \end{array}$ 

The program then asks if iteration is required (line 2870). If an integer N is read in at this point, a successive iteration of the interpolation will be carried out. The values of D and RNLDS corresponding to ALFA =  $\alpha_{interp}$  are calculated, and the new value of D (say  $D_{new}$ ) is used to determine whether the zero in D lies between  $D_{1}$  and  $D_{new}$  or between  $D_{new}$  and  $D_{2}$ .

A new interpolation is then carried out between the appropriate pair of values. The interpolation is iterated N times, and a new set of output values is generated.

If further interpolation is not required, a blank read in at line 2880 will send the program back to ask for a new set of ALFA and BETA values.

It should be noted that the values of ALFA and BETA presented in the output have been re-converted to the input form, so that

ALFA = 
$$\lambda_{C}/L$$
 (A4.16)  
BETA =  $\tau_{C}\eta K^{2}/2\pi$ 

The factor  $2\pi$  is included in the definition of BETA so that

BETA·ZNOT = 
$$[\tau_C \eta K^2/2\pi] \cdot [\text{Re } \Omega/\eta K^2]$$
  
=  $\tau_C \cdot \text{Re } \Omega/2\pi$   
=  $\tau_C/T$  (A4.17)

# A.4.3 The program

The program described in the last section and in section 3.10.2 is listed on the next few pages.

```
GAUSSIAN.
                                                                                                           REAL *8 F (40,40) + G(40,40) | GZ1(40) + GY1(40) + WTGZ1(40) + WTGY1(40)
                                                                                                                                                                           YM2Y, YP2Y, YMYP, ARITÀN, ARLOG, FACTR, FACTI
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         GAUSSIAN
                                                                                                                                                                                                                                                                                                         BLANK;
                                                                                                                                                                                                                                                                                                                                                                                                         BLANK
                                                                                                                           RATID(10); RNLDS(10); ALFA(12); BETA(20); YL(15)
                                                                                                                                                           DOUBLE PRECISION YNOT, ALF AS 0, BETASO, ZNOT, XLSO, XHSO
                                                                                                                                                                                                                                                                                                                                                                                                         ENTER
                                                                                                                                                                                                                                                                                                          FORMAT ( . TO READ POINTS FOR REAL INTEGRATION ENTER
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         POINTS', 13.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         GAUSSIAN Y POINTS ', 13, '
                                                                                                                                            DOUBLE PRECISION ARINUM, ARIDEN, 82A, SCALE, STRET
                                                                                                                                                                                                                                                          EOF!)
                                                                                                                                                                                                                                                                                                                                                                                                         FOR IMAG INTEGRATION
REAL +8 GZR(40), GYR(40), WTGZR(40), WTGYR(40)
                                                                                                                                                                                                                                                         FORMAT( "TO CONTINUE ENTER BLANK, OTHERWISE
                                                                                                                                                                                            REAL#4 AI(20,3); RI(20,3), D(20,2), T(20)
                                                                                                                                                                                                                                                                                                                                                                                                                                                         CALL ROATA GY 1, 62 1, WT GY 1, WT GZ 1, NI, MI)
                                                                                                                                                                                                                                                                                                                                                                           CALL RDATA (GYR+GZR+WTGYR+WTGZR+NR+MR)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         GAUSSIAN Y
                                                                                                                                                                                                                           INTEGRATION DATA
                                                                                                                                                                                                                                                                                                                           . IMAGINARY ONLY ENTER EOF!)
                                                                                               DIMENSION AP (20) BETAP (20)
                                                                                                                                                                                                                                                                                                                                                                                                           705 FORMAT(*TO READ POINTS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                             SE ON
                                                                                                                                                                                                                                                                             READ(5.7.00.END=40) 4
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           Z
                                                                                                                                                                                                                                                                                                                                                                                                                                          READ(5, 700, END=5) 1
                                                                                                                                                                                                                                                                                                                                                                                                                           . OTHERWISE EOF!)
                DIMENSION AMI (2013)
                                                                                                                                                                                                                                                                                                                                             RE AD (5,700, END=7)
                                                                                                                                                                              PRECISION
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             FORMAT(//* IMAG
                                                                                                                                                                                                                              SECTION TO READ
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            FORMAT(// REAL
                                                                                                                                                                                                               XYZ=4.442882938
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            Z POLNTS'//)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             POINTS! //
                                 SIMDBL
                                                                                                                                                                                                                                                                                                                                                                                                                                                                            WRITE(6,400)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           WRITE(6,807)
                                                                                                                                                                                                                                                                                                                                                                                             WRI TE (6+705)
                                                                                                                                                                                                                                                                                              WRITE(6,703)
                                                                                                                                                                                                                                             WRITE (6,936)
                                                  LOGICAL LV2
                                                                   7
                                                                                                                                                                                                                                                                                                                                                              FORMAT(12)
                                 EXTERNAL
                                                                                   INTEGER
                                                                   LOGICAL
                                                                                                                                                                               DOUBLE
                                                                                                                                   REAL #8
                                                                                                                                                                                                                                                                                                                                                              100
                                                                                                                                                                                                                                                                                                                703
                                                                                                                                                                                                                                                                 936
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               350
                                                                                                                                                                                                                                                                                                                                                                                                                                             280
                                                                                                                                                                                                                                                                                                                                                                                                                                                             290
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              320
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              330
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               340
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              360
                                                                                                                                                                                                                                                                                                                                                                                               250
                                                                                                                                                                                                                                                                                                                                                                                                              260
                                                                                                                                                                                                                                                                                                                                                                                                                              270
                                                                                                                                                                                                                                                                                                                                                                                                                                                                               300
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              310
                                                                                                                                                                                                                                                                                                061
                                                                                                                                                                                                                                                                                                                                210
                                                                                                                                                                                                                                                                                                                                                220
                                                                                                                                                                                                                                                                                                                                                                230
                                                                                                                                                                                                                                                                                                                                                                                240
                                                                                                                                                                                 20
                                                                                                                                                                                                                04
                                                                                                                                                                                                                               20
                                                                                                                                                                                                                                                                170
                                                                                                                                                                                                                                                                                081
                                                                                                                                                                                                                                                                                                                 200
                                                                                                                                                  8
                                                                                                                                                                                                30
                                                                                                                   80
                                                                                                                                   8
                                                                                                                                                                  0
                                                                                                                                                                                                                                                  9
                                                                                    9
                                                                                                   20
                                                                    50
                                   30
                                                    0
```

```
STEPS!)
420 FORMAT(//'NEED JOLERANCES EPY1, EPY4, EPG1, EPG2 AND NO OF
                                                                                                                               READ(5.502. END=5) STALF, ALFSTP, LALF, STBET, BETSTP, 18ET
                                                                                                       FORMAT (// WEED STALF, INCR, #, STBET, INCR, #!)
            READ(5.421,END=1) EPY1,EPY4,EPG1,EPG2,K
                                                   FORMAT(///*NEED RE, IM OMEGA STAR/KSQ*)
                                                                                                                                                                                                                                                                             FORMAT(+4NTEGRATION LIMITS2 TYPE 1
                                                                                                                                                                                                                                                                                                                                  TYPE 1 IF YES!)
                                                                                                                                               BY PI*ROOT
                                                                   ZNOT, YNOT
                                                                             SLOPE = (YNOT-1.0)/ZNOT
                                                                                                                                                                                                                                                                                                                                                Ħ
                                                                                                                                                                                                                                                                                                                                                                     FDRMAT(2(2F20.7,12))
                                                                                                                                             SECTION TO MULTIPLY
                                                                 READ(5,500, END=3)
                                                                                                                                                                                                                                                                                                                                                                                                             IF (MP.GE.1) IALF=1
                         FORMAT (4F 10 . 5 . 13)
                                                                                                                                                                       ALF STP=ALFSTP #XYZ
                                                                                                                                                                                                 BETSTP=BETSTP#XYZ
                                                                                                                                                                                                                                                                                                                                            READ(5,744,END=2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                Y2=DSORT(YNOT-1.)
                                                                                                                                                                                                                                                                                                                               FORMAT ( * VOLUMES ?
                                                                                                                                                          STALF = STALF * XYZ
                                                                                           FORMAT(2F20.15)
                                                                                                                                                                                    STBET=STBET*XYZ
                                                                                                                                                                                                                                                                                         READ(5,744) PL
                                                                                                                                                                                                                                                                                                                                                                                   00 36 I=1, IBET
                                                                                                                   WRITE (6,401)
                                                                                                                                                                                                                                                                                                                                                                                                                                      ALFA(1)=STALF
                                                                                                                                                                                                                                                                                                                                                                                                                                                  BETA(1)=$TBET
                                      WRITE(6,399)
                                                                                                                                                                                                                                                                WRITE (6,743)
                                                                                                                                                                                                                                                                                                                   IRITE(6,843)
                                                                                                                                                                                                                                                                                                                                                         WRITE(6,901)
                                                                                                                                                                                                                                                                                                       FORMAT(11)
                                                                                                                                                                                                                                                                                                                                                                                                T(1)=1.
                                                                                                                                                                                                                                                                                                                                                                                                                           NZE RO=K
                                                                                                                                                                                                                           M = 0
                                                                                                                                                                                                                                        O II O I
                                                                                                                                                                                                              PL=0
                                                                                                                                                                                                                                                     17=0
                                                   399
                                                                                           500
                                                                                                       401
                                                                                                                                                                                                                                                                              743
                                                                                                                                                                                                                                                                                                                                                                        502
                                                                                                                                                                                                                                                                                                                                                                                    22
                                                                                                                                                                                                                                                                                                         744
                                                                                                                                                                                                                                                                                                                                 843
            380
                         390
                                     400
                                                  410
                                                               420
                                                                                                                                                                                                                       540
                                                                            430
                                                                                         440
                                                                                                      $50
                                                                                                                   460
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                                                                                                                                                         490
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                                                                                                                                                                                                                                                                                                                                                                                   999
                                                                                                                                                                                                                                                                            580
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                                                                                                                                                                                                                                                                                                                                                                                              670
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                                                                                                                                                                                                                                                                                                                                                                                                                        069
                                                                                                                                                                                                                                                                                                                                                                                                                                                  710
                                                                                                                                                                                                                                                                                                                                                                                                                                     700
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730		
740		BETA(N+1)=BETA(N)+BETSTP
750		ij.
760	•	
770	•	IF (MP.GE.1) ALFA(L)=AI(N,2)
OD.	,	IF (ALFA(L), E0.0.) GO TO 37
O		ALFA(L+1)=ALFA(L)+ALFSTP .
0		ALFASO=ALFA(L) *ALFA(L)
-		
N	,	BE=BETA(N)
m		
•	r	LV1=.TRUE.
850		LV2=+FALSE+
S		ز
~	, )	SECTION TO FIX LIMITS ON REGION BEYOND FIRST + PEAK IN 3.165(A)
00		(AL*Y3.GT.2.*ZNOT#BE) LV2=,TRUE.
C)		IF ( ((2. #BE#ZNOT) ##2#(AL#Y3) ##2) .GT.100) LV) = .FALSE.
O		IF (.NOT.LVI.AND.LV2) GO TO 4
-		IF(BE*ZNOT.LT.2.0) GO TO 53
N		YINC=.2/AL
m		¥S=¥3
◂		CALL EXTEND(AL, BE, ZNOT, YNOT, EXT, ZNOT, 0, YS, YINC, 9, K)
ഹ		IF(EXT.EQ.O) YS=X3
vo.		TOL =E PY4 * EXI
_		YINC=2. #YINC
മ		Y4=Y5,
On-		CALL CORY (AL, BESZNOT SYNOT, K, TOL, Y INC, Y4, ZNOT, 9, K)
0		11
_		G2=ZNOT+2./BE
N		Ð
1030	Ų	
4	5.	3 CALL R3(ALFA(L), BETA(N), ZNOT, YNOT, G1, G2, Y3, Y4, EPG1, EPG2, EPY4, K)
S		CALL
1060		VOL 3R=08L1N1(#TGYR,#TGZR,F,NR,MR) + (Y4-Y3) + (G2-G11/4
1070	u	IF ( . NOT . L.VI . AND NOT . L.V2) GO TO 1001

```
CALL CORY (AL. BE, ZNOT, YNOT, NZERO, TOL, YINC, Y1, GS, 18, K)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     CALL CORG(AL, BE, ZNOT, YNOT, NZERO, TOL, GINC, G2, Y0, 13, K)
                                                                                                                                                                                                                                                                                        CALL CORGIAL, BE, ZNOT, YNOT, NZERO, TOL, GINC, 62, YO, 15, K)
                                                                                                                                                                                                     CORY (AL, BE, ZNOT, YNOT, NZERO, TOL, YINC, YI, GS, 16, K)
                                                                                                                    EXTFND{AL, BE, ZNOT, YNOT, CFRIN, GS.O, YO, YSTP, O, K)
                                                                                                                                                                                                                                                                                                                                                                                            CALL CORY (AL. BE, ZNOT, YNOT, K, TOL, YINC, YI, ZNOT, 18, K)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                  CALL EXTFNO (AL, BE, ZNOT, YNOT, BIG, GS, GESC, YQ, 0, 18, K)
SECTION TO FIX LIMITS ON NEGATIVE-VALUE REGION IN
                                                                                                                                                                        CFRIN=-CFR(ALFA(L), BETA(N), 2NOT, YNOT, 0, YN)
                                                                                                                                                                                                                                                                                                                                                                                TOL=EPY: +CFR (AL, BE, ZNOT, YNOT, ZNOT, YN)
                                                                                                                                                       IF ((ZNOT#BETA(N)), GT.0.707) GO TO 65
                                  F ( • NQT • L V I • AND • AL * Y 3 • GT • 7 • ) Y3=7 • / AL
                                                                                                                                                                                                                                                                                                                                GG TO
                                                                                                                                                                                                                                                                                                                                IF(BE#ZNOT.LT.2.)
                   YN=050RT (YNOT)-1.
                                                                     rg=0SQRT (YNOT-1.)
                                                                                                                                                                                                                                                                                                                                                                                                                                                    GESC=ZNOT#1.1X
                                                                                                                                                                                          OL = EPY 1 *CFRIN
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          IF(LV1) GO TO
                                                                                       YSTP= (Y3-Y0)/X
                                                                                                                                                                                                                                                                                                                                                 G1=ZNOT-2./BE
                                                                                                                                                                                                                                                                                                                                                                 62=ZNOT+2./BE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        TOL = E PY 1 * 81 G
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            GINC= . 2/BE
                                                                                                                                                                                                                                              9
                                                                                                                                                                                                                                                                              GINC= . 2/BE
                                                        メノストリンスにん
                                                                                                                                                                                                                                                                                                                                                                                                                                     GD TO 56
                                                                                                                                                                                                                                                                                                                GO TO 64
                                                                                                                                                                                                                                             (F(LV1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            62=65
                                                                                                                                                                                                                                                               62=65
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       Y1=0
                                                                                                                                                                                                                                                                                                                                                                                                                     V 1=0
                                                                                                                                                                                                             CALL
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           V 1=0
                                                                                                                         CALL
                                                                                                                                                                                                                              Y1=0
                                                                                                                                          V1=0
                                                                                                                                                                                                                                                                                                                                                                                                                                                      57
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             400
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                                       1100
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       080
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CALL SETUPR(ALFA(L), BETA(N), ZNOT, YNOT, GYR, 62R, NR, MR, Y2, Y3, 61, 62, F)
                                  CALL SETUPR (ALFA(L), BETA(N), ZNOT, YNOT, GYR, GZR, NR, MR, YI, YZ, GI
                                                                                                                                                                                                                                                                       IF(1.414.GT.AL*(DSORT(YNOT)+1.).AND.GS.GT.0.3) GO TO 158
                                                                                        INTEGRATION OF REGION AROUND FIRST + PEAK IN 3.165(A)
                                                     VOL 1 R=08L I NT (MT GYR, WT, GZR, F, NR, MR) # (Y2+Y)) # (G2-G1)/4
                                                                                                                           VOL 2R=DBLINT(#TGYR,#JGZR,F,NR,MR)#(Y3-Y2)#(G2-G1)/A
                                                                                                                                                                                                                                                                                                                                                                                                                     CALL EXTFND(AL, BE, ZNOT, YNGT, EXT, GS, 0, YS, YESC, 21, KO)
                 INTEGRATION OF NEGATIVE-VALUE REGION IN 3.165(A)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           CORY (AL, BE, ZNOT, YNOT, K, TOL, YESC, Y4, 65, 21, K)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               CALL (CORY (AL, BE, ZNOT, TNOT, K, TOL, YESC, Y1, GS, 23, K)
                                                                                                                                                                                                          62=',E20.8)
                                                                                                                                                                                                                            3,165(8)
                                                                                                                                                                                FORMAT( / LIMITS FOR REAL INTEGRATION , / )
                                                                      IF (.NOT.LVI.AND.AL#Y3.GT.7.) Y3=7./AL
                                                                                                                                                               IF(PL.EQ.1) WRITE(6,365) YI.Y4.61.62
                                                                                                                                                                                                                            F 0.10
                                                                                                                                                                                                       G1=', E20.8,
                                                                                                                                                                                                                   SECTION TO FIND REGION BOUNDS
                                                                                                                                            IF ( . NOT . EVI . AND . L V2) YOL 3R=0
                                                                                                                                                                                                                                      IF(BE*ZNOT.LT.2) GO TO 153
      61=0
                                                                                                                                                                                                                                                                                                          KD= ( DSORT ( YNOT ) +1 . ) / . 2 + 1 0
64 IF ( .NDT .L VI . AND .L V2)
                                                                                                                                                                                                   Y4= ', E20 .8 ;
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 GS= ZNOT+1/BETA(N)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   GESC=68#3./(2.*K)
                                                                                                                                                                                                                                                                                                                             IF (KG.LT.K) KO=K
                                                                                                                                                                                                                                                                                                                                                                                                                                                                         OL = EPY 4 * EXT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              TOL=EPY1*EXT
                                                                                                                                                                                                                                                                                                                                                               YESC= . Z/AL
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            YESC-YSZK
                                                                                                                                                                                                                                                                                                                                              GO TO 157
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                GO TO 156
                                                                                                                                                                                                                                                                                                                                                                                                    YS= .0001
                                                                                                                                                                                                                                                                                          YESC= .2'
                                                                                                                                                                                                                                                       LONZ =SD
                                                                                                                                                                                                                                                                                                                                                                                                                                       Y4=YS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           CALL
                                                                                                                                                                                                                                                                                                                                                                                    XUUX
                                                                                                                                                                                                                                                                                                                                                                                                                                                          V 1=0
                                                                                                                                                                                  365
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              740
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                750
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SETUPI (ALFA(L), BETA(N), ZNOT, YNOT, GY I, GZ I, NI, MI, YI, Y4, GI, GZ, G)
                                                                                                                                             TEMP=SFMIN(AL, BE, ZNOT, YNOT, TX, TX, GESC, YESC, GS, YS, YP, XQ)
                                                                                                                                                                                                                                                                                                                                                CALL CORG(AL, BE, ZNOT, YNOT, NZERO, TOL, GESC, G2, YS, 26, K)
                                                                                                                                                                                                                                                                         CALL CORY (AL, BE, ZNOT, YNOT, NZERO, TOL, YESC, Y1, GS, 20, K)
                                                                                                                                                                                                                                                                                                                                                                                                                      CORGIAE BE, ZNOT, YNOT, NZERO, TOL, GESC, GI, YS, 24, K)
                                                                                                                                                                                                                    CORY (AL .BE, ZNOT, YNOT, NZERO, TOL, YESC, Y4, 65,22, K)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    VOL [ = DBL! NT ( WTGY Is MT GZ I + G + N I + M I ) # ( Y4 - Y1 ) # ( G2 - G1 ) / 4
      S
F(1.414.6T.AL*(DSORT(YNOT)+1.). AND. 65.6T.0.3)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     62=1,E20.8)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                FURNATIVILIMITS FOR IMAGINARY INTEGRATION:, /
                                                                                                                                                                                                                                                                                                                                                                                                                                                                             F.(PL.EO.1) WRITE(6,366) Y1,Y4,G1,G2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    G1=", E20.8,"
                                                                                                                                                                                                                                                                                                                                                                                                                                         SECTION TO INTEGRATE 3.165(8)
                                  KO= (DSQRI(YNDT)+1.)/.2+10
                                                                                                                                                                                                  TOL = EPY 4 * TEMP
                                                                                                                                                                                                                                                        OF FEPY 1 + TEMP
                                                                                                                                                                                                                                                                                                              TOL=EPG2+TEMP
                                                                                                                                                                                                                                                                                                                                                                                                      COL-EPG1 * TEMP
                                                    IF (KQ .LT .K)
                                                                                                                              TX=GESC/10.
                                                                                                                                                                                                                                      YESC=YS/K
                                                                                                                                                                                                                                                                                           GESC= . 2 / BE
                                                                                         YESC= . 2 / AL
                                                                                                                                                                                                                                                                                                                                                                  GE SC=GS/K
                 YESC= . 2
                                                                       60 TO 28
                                                                                                                                                                                                                                                                                                                                 62=GS
                                                                                                                                                                 Y4=YS
                                                                                                                                                                                                                     CALL
                                                                                                                                                                                                                                                                                                                                                                                                                       CALL
                                                                                                                                                                                                                                                                                                                                                                                                                                                             CALL
                                                                                                                                                                                                                                                                                                                                                                                     61=0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               366
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                                                                                                                            28
                                                                                                                                                                                                                                                                                                                                                                                                                                                           156
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                                 810
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# IF (ML.EQ.1.AND FIT.EQ.MP) WRITE(6,800) VOLIR, VOL2R FVOL3R, VOL) 800 FORMAT (/'VOLIR=', E20'8, ' VOL2R=', E20.8, ' VOL2R=', E20.8, '
                                 RNL DS (L) = ALFA(L) #DS GRT (RN#6. #3.14159265/BETA(N))
  RATIO(L)=(VOL1R+VOL2R+VOL3R)/(VOL1+SLOPE)+1
                                                                                                                                                                                                                                                                                                                                                                                              AI(N.2) HAI(N.3) - (AI(N.3) - AI(N.1)) *FR
                                                                                                                                                                                                                                                                                                                                                                                                              RI (N.2)=RI (N.3) - (RI (N,3) - RI (N,1)) *FR
                                                                                                                          SECTION TO CARRY OUT INTERPOLATION
                   RN=-ZNOT/((ALFA(L) ##5) #VOL1 #2.)
                                                                                                                                                                                                                             68,68,67
                                                                                                                                                                                                          FEIN-GT . FALF) GO TO 59
                                                                                                                                             IF (MP.GE.1) GO TO 159
                                                                                                                                                                                                                                                                                                                                                                                                                                                                            AI (N. I) = ALFA( IALF-I
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         0 (N. 1) = KATIO( 1ALF-1
                                                                                VOL 1= . . E20 . 8/)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           AI (N.3) JALFA( IALF)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        0(N.2)=RATIO( IALF
                                                                                                                                                                                                                        IF (RATIO(M) *TEMP)
                                                                                                                                                                                                                                                                                                                                                                  TER=TEMP/RATIO(M)
                                                                                                                                                                                                                                                                       AI(N.1) = ALFA(M-1)
                                                                                                                                                                                                                                                                                                     RI (N, I FERNLOS (M-)
                                                                                                                                                                                                                                                                                                                     RI (N. 3) = RNLDS (N)
                                                                                                                                                                                                                                                                                       AI (N.3) = ALFA(N)
                                                                                                                                                                                                                                                                                                                                                   0(N,2)=RATIO(M)
                                                                                                                                                                                                                                                                                                                                                                                 FR=1./(1.-TER)
                                                                                                                                                                                                                                        TEMP=RATIO(M)
                                                                                                                                                                            TEMP=RATIO(1)
                                                                                                                                                                                                                                                                                                                                   D(N.1)=TEMP
                                                                                                                                                                                                                                                                                                                                                                                                                                                             AI (N.2) #0.
                                                                                               CONTINUE
                                                                                                                                                                                                                                                        50 TO 66
                                                                                                                                                                                                                                                                                                                                                                                                                               60 TD 38
                                                                                                                                                                                             ZHX+1
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AND

SECTION TO EVALUATE

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N=1, 18ET
                                                                                                                                                                                                                                                                                                                                                                                                            (AP(N) - NH1 - 18ET)
                                                                                                                                                                                                                                                                                                                         (BETAP(N)
                                                                                                                                                                                                                                                                                                                                                                                                           IF ( IT .EQ.MP) WRITE (6,903)
                                                                                                                                                                                                                                                                                                                                                                                                                      IF(IJ.EQ.MP) WRITE(6,909)
                                                                                                                                                                                                                                                                                                                       IF (II. EQ. MP) WRITE (6, 902)
                                                                                                                                                                                                                                                                                                                                               WRITE 6, 908)
                                                                                                                                                                                                                                                                                                                                   F.ORMAT(14X,8E123.5377)
            RI(N) I) = BNLDS(I) ALF-1)
                                                                                                                                                                                                                                                                                  FORMAT ( /4 0%, ' BETAR //
                                                                        10 38
                                                                                                                                                                                                                                                                                                           BETAP (1) = BETA(1)/XXZ
                         RI (N, 3) = RNLDS ( JALF
                                                                                                                                                                                                                                                                                                                                                                                                AP(1)=A1(1,3)-7XYZ
                                                                                                                                                                                                                                                                                                                                                                                                                                    FORMAT(//*RNLDS*)
                                                                                                                                                                                                                                                                                                                                                           FORMAT (//*ALFA:)
                                                                                                                                                                                     AI (N, 1)=AI(N,2)
                                                                          0
                                                                                                            A1 (N.3) = A1 (N.2)
                                                                                                                                                                                                 RI (N.1) =RI (N.2)
                                                                                                                         RI (N, 3) = RI (N, 2)
                                                                                                                                                                                                                                                                  OUTPUT SECTION
                                                                                                                                                                                                                                                                                               DO 29 1=1,18ET
                                                                                                                                                                                                                         FR= 1 ./(1.-TER)
                                                                                                                                                                                                                                                                                                                                                                              DO 32 1=1. (DE)
                                                                                                                                                 FR= 1./(1.-TER)
                                                                                                                                     TER=0(N,1)/DD
                                                                                                                                                                                                                                                                                                                                                                        DO 343 J=1, W
                                                                                                                                                                                                             TER-00/0(N.2)
                                                                                     IF ( DO # D(N, 1))
                                                                                                                                                                                                                                                                                                                                              FF ( IT . EO . MP )
                                                                        (F(DD.EQ.0)
                                                            DD=RATIO(1)
RI(N,2)=0.
                                                                                                 D(N.2)=DD
                                                                                                                                                                         D(N.1)=DD
                                                                                                                                                             60 70 26
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                                                                                                                                                                                                                  IF(IT.EQ.MP) WRITE(6,903) (D(N,J),
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                                 IF(IT.EQ.MP) -WRITE(5.904)
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FACTI=YSQ#G+Y#G#F#DLGG{ARLOG}/A*+Y#{YMYP+G#G}#DATAN2{ARINUM,
                                                                                                                                                                                                                                                                                                                                                                                                                                         (81,14)
                                                                                                                                                                                                                                                                                  EXARGI=-(ALFASO*YSO*BETASO*(G-ZNOT)*(G-ZNOT))
                                                                                                                                                                                                                                                                                                                                                                                                                                      Y=1, E20,8,1
                                                                                                                                                                                                                                                                                                                EXARGE=- (ALFASOFYSOFBETASOF (G+ZNOT) + (G+ZNOT))
                                                                                                                                                                                                                                                                                                                                           SFI=FACTI*(DEXP(EXARGI)-DEXP(EXARG2))/2.
                                                                                                                                                                                                                                                                                                  IF(EXARGI.LT.-170) EXARGI=-170
                                                                                                                                                                                                                                                                                                                              IF(EXARG2 -LT - 170) EXARG2 - 170
                                                                                                                                                                                                                                                                                                                                                                                                                                      16= ", E20.8,"
                                                                                                                                                                                                                                                                                                                                                                                                     SUBROUTINE ALARMIGS YSEX, N
                                                                                                                                                                                           IF(DENLOG.E0.0) GO TO 34
                                                                                                                                                               IF (UPLOG. E.0.0) GO TO 34
                                                                                                                                                                              DENLOG= (YP2Y*YP2Y+G*G)
                                                                                                                                                 UPLOG= (YM2Y*YM2Y+G*G)
REAL * 8 EXARGI . EXARGE
                                                                                                                                                                                                                                                                                                                                                                                       OVERFLOW SUBROUTINE
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                                                                                                                                                                                                                                                                                                                                                                                                                     WRITE(6.34) G.Y.
              ALF ASO=ALFA#ALFA
                             BETASO=BETA*BETA
                                                                                                                                  ARI DENEYMYP+G+G
                                                                                                     YMYP=YM2Y#YP2Y
                                                                                                                    ARTNUMEA. #Y#G
                                                           トロペイーののよ 十二十二
                                                                                      YP2Y=F+2.*Y
                                                                        YM2Y=F-2.4Y
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                                              Y*Y=08Y
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SUBROUTINE EXTENDIAL, BE, ZNOT, YNOT, EXT, GS, GESC, YS, YESC, NUMB, K)
                                                                                                                                                                          DIFF=ABS (CFR (AL, BE, ZNOT, YNOT, G,Y))-TEMP
                                                                                                                                                                                                                                                                                                                           OIFF=-(SFI(AL,BE,ZNOT,YNOT,G,Y)+TEMP)
                                                                                                         TEMP#ABS (CFR (AL. BE, ZNOT, YNOT, 65, YS))
                                                                                                                                                                                                                                            FEMP=-SFI (AL, BESZNOT, YNOT, GS, YS)
                                                                                                                                                                                                                                                        FORMAT ("IMAGINARY PART =", E20,8)
                                                                                                                                                                                        IF ((SEOPE * DIFF) .LT. 0) 60 TO 200
                                                                                                                                                                                                                                                                                                                                       F((SLOPE*DIFF).LI.9) GO TO 200
EXTREMUM-FINDING SUBROUTINE
                                                                                           IF(NUMB.6T.19) GO TO 100
                                                                                                                                                                                                                 IF(DIFF.GT.0) SLOPE=DIFF
                                                                                                                                                                                                                                                                                                                                                                  IF(DIFF.GT.O) SLOPE=01FF
                                                                                                                                                              IF (N. GT .X.) GO TO 300
                                                                                                                                                                                                                                                                                                              IF (N. GT.K.) GO TO 300
                          EXTERNAL CFR, SFI
                                                                                                                                                                                                                                                                                                                                                    TEMP=TEMP+DIFF
                                                                                                                                                                                                     TEMP=TEMP+01FF
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                                                                                                                      Y=Y+YESC
                                                                                                                                    G=G+GESC
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                                                                                                                                                                                                                                                                                                  G=6+GESC
                                      SLOPE=0
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(AL, BE, ZN, YN, Y, DY, G, OG)  BE, ZN, YN, GPOG, YPOY)  BE, ZN, YN, GMOG, YMOY)  ECND)/(2.*SORT(DG*DG+DY*DY))  ECND)/(2.*SORT(DG*DG+DY*DY))  EX, EIX LIMITS ON REGION BEYOND F  (ALFA, BETA, ZNOT, YNOT, YNOT, GI, GZ, Y3, SFI  EA, BETA, ZNOT, YNOT, O, YN)  PA, BETA, ZNOT, YNOT, NZERO, TOL, Y IN  1G  A, BETA, ZNOT, YNOT, NZERO, TOL, Y IN  1G  A, BETA, ZNOT, YNOT, NZERO, TOL, GIN  1G  A, BETA, ZNOT, YNOT, NZERO, TOL, GIN  1G	4170	U	INTERPOLATION SUBROUTINE FOR USE WITH (B) INTEGRAND
### ### ### ### #### #### ############	_		TION SSFI(AL.BE.ZM.YN.Y.DY.S.OS)
### ### ### ### ### ### ### ### ### ##	_		ANAL
### ### ### ### ### ### ### ### ### ##	"	o	= Y + D Y
### CPDG=G+DG ### GPDG=G+DG ### CPDG=G+DG ### CPDG=G+DG ### CPDG=G+DG ### CPDG=G-DG ### CDDG=G-DG ### CDG	'4		\O+\alpha+\O\A
### 6MDG=G-DG ### 6MDG=G-DG ### 6MDG=G-DG ### 6MDG=SFI(AL, BE, ZN, YN, GPDG, YPDY) ### 6MDG=SFI(AL, BE, ZN, YN, YN, YN, GPDG, YPD) ### 6MDG=SFI(AL, BE, ZN, YN, YN, YN, YN, YN, YN, YN, YN, YN, Y	"		90+9=90d9
FIRST=SFI(AL, BE, ZN, YN, GPOG, YPOY)  SECND=SF (IAL, BE, ZN, YN, GWOG, YWOY)  SSF I= (FIRST-SECND)/(2.*SGRT(DG*DG*DY*DY))  RETURN  END  SUBROUTINE TO FIX LIMITS ON REGION BEYOND FIRST + PEAK  SUBROUTINE R3 (ALFA, BETA, ZNOT, YNOT, G1, G2, Y3, Y4, EPG1, EPG2  310  EXTERNAL CFR, SFI  NZERO=K  G1=0  YINC=.22 ALFA  G110  F(12.*ALFA*(SORT(YNOT)+1)).G7.1.0) G0 T0 60  YA=YM  YA=YM  CALL CORY (ALFA, BETA, ZNOT, YNOT, O, YM)  701 FORMAT(IREAL PARI=*), E20.8)  G2=0  TOL=EPG2*CFRBIG  CALL CORY (ALFA, BETA, ZNOT, YNOT, NZERO, TOL, YINC, Y4, GS, 2, K)  G2=0  TOL=EPG2*CFRBIG  CALL CORG (ALFA, BETA, ZNOT, YNOT, NZERO, TOL, YINC, Y4, GS, 2, K)  G2=0  TOL=EPG2*CFRBIG  CALL CORG (ALFA, BETA, ZNOT, YNOT, NZERO, TOL, YINC, Y4, GS, 2, K)  G2=0  TOL=EPG2*CFRBIG  CALL CORG (ALFA, BETA, ZNOT, YNOT, O, Y3)  TOL=EPG2*CFRBIG  CALL CORG (ALFA, BETA, ZNOT, YNOT, O, Y3)  TOL=EPG2*CFRBIG  CALL CORG (ALFA, BETA, ZNOT, YNOT, O, Y3)  TOL=EPG2*CFRBIG  CALL CORG (ALFA, BETA, ZNOT, YNOT, O, Y3)  TOL=EPG2*CFRBIG  CALL CORG (ALFA, BETA, ZNOT, YNOT, O, Y3)  TOL=EPG2*CFRBIG  CALL CORG (ALFA, BETA, ZNOT, YNOT, O, Y3)  TOL=EPG2*CFRBIG  CALL CORG (ALFA, BETA, ZNOT, YNOT, O, Y3)	W		0WD C=C=DC
SECND=SF ((AL. BE.ZN., YN. GMOG, YMDY)  SSF1=(FIRST-SECND)/(2.*SORT(OG*DG+DY*DY))  RETURN  END  SUBROUTINE TO FIX LIMITS ON REGION BEYONG FIRST + PEAK  SUBROUTINE R3(ALFA, BETA, ZNOT, YNOT, G1. G2, Y3, Y4, EPG1. EPG2  3300  SUBROUTINE R3(ALFA, BETA, ZNOT, YNOT, G1. G2, Y3, Y4, EPG1. EPG2  3340  YINC=.2/ALFA  GI = 0  YM=1/ALFA  YM=1/ALFA  YM=1/ALFA  YM=1/ALFA  YM=1/ALFA  YM=1/ALFA  GS = 0  TOL=EPY*CFRBIG  CALL CORY(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, Y INC, Y4, GS, 2, X)  GS = 0  TOL=EPG2*CFRBIG  CALL CORG(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, Y INC, Y4, GS, 2, X)  GS = 0  TOL=EPG2*CFRBIG  CALL CORG(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, Y INC, Y4, GS, 2, X)  GS = 0  Y4=Y0  GS = 0  Y4=Y0  CALL CORG(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, Y INC, Y4, GS, 2, X)  GS = 0  Y4=Y0  CALL CORG(ALFA, BETA, ZNOT, YNOT, NOX, X)  GS = 0  Y4=Y0  CALL CORG(ALFA, BETA, ZNOT, YNOT, O, Y3)  CFRBIG=CFR(ALFA, BETA, ZNOT, YNOT, O, Y3)  CFRBIG=CFR(ALFA, BETA, ZNOT, YNOT, O, Y3)	(A		F=SFI(AL
SECONDINE TO FIX LIMITS ON REGION BEYOND FIRST + PEAK  SUBROUTINE TO FIX LIMITS ON REGION BEYOND FIRST + PEAK  SUBROUTINE TO FIX LIMITS ON REGION BEYOND FIRST + PEAK  SUBROUTINE TO FIX LIMITS ON REGION BEYOND FIRST + PEAK  SUBROUTINE R3(ALFA, BETA, ZNOT, YNOT, SI, S2, Y3, Y4, EPGI, EPGZ  SI320  NZERO=K  GINC=.2/BETA  IF (12.*ALFA* SORT (YNOT) +11) .GT.1.0) GO TO 60  YM=1/ALFA  SOR (SINC=.2/BETA  IF (12.*ALFA* SORT (YNOT) +11) .GT.1.0) GO TO 60  YM=1/ALFA  TO FORMAT(''REAL PART=', E20.8)  GS=0  TOL=EPY**CFRBIG  CALL CORY (ALFA, BETA, ZNOT, YNOT, NZERO, TOL, Y INC, Y4, GS, 2, K)  G2=0  TOL=EPY**CFRBIG  CALL CORG (ALFA, BETA, ZNOT, YNOT, NZERO, TOL, Y INC, Y4, GS, 2, K)  G2=0  TOL=EPGZ**CFRBIG  CALL CORG (ALFA, BETA, ZNOT, YNOT, NZERO, TOL, SINC, GZ, YM, A, K)  G0 TO 101  CFRBIG=CFR(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, SINC, GZ, YM, A, K)  SOO Y***PY**  CFRBIG=CFR(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, SINC, GZ, YM, A, K)  CFRBIG=CFR(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, SINC, GZ, YM, A, K)  CFRBIG=CFR(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, SINC, GZ, YM, A, K)	14	•	=SF I(AL
RETURN  RETURN  RETURN  REBOUTINE TO FIX LIMITS ON REGION BEYOND FIRST + PEAK  SUBROUTINE TO FIX LIMITS ON REGION BEYOND FIRST + PEAK  SUBROUTINE TO FIX LIMITS ON REGION BEYOND FIRST + PEAK  SUBROUTINE TO FIX LIMITS ON REGION BEYOND FIRST + PEAK  SUBROUTINE TO FIX LIMITS ON REGION BEYOND FIRST + PEAK  SUBROUTINE TO FIX LIMITS ON REGION BEYOND FIRST + PEAK  SUBROUTINE TO FIX LIMITS ON REGION BEYOND FIRST + PEAK  SUBROUTINE TO FIX LIMITS ON REGION BEYOND FIRST + PEAK  SUBROUTINE TO FIX LIMITS ON TO TO TO TO  SUBROUTINE TO TO TO TO TO TO TO TO  SUBROUTINE TO TO TO TO TO  SUBROUTINE TO TO TO TO TO  SUBROUTINE TO TO  SUBROUTINE TO TO TO  SUBROUTINE TO TO TO  SUBROUTINE TO  SUBROUTINE TO	C		SSF [# (F [ RST + SECNO ) / (2) # SORT = DOMED + DV # DV
END SUBROUTINE TO FIX LIMITS ON REGION BEYOND FIRST + PEAK SUBROUTINE R3(ALFA, BETA, ZNOT, YNOT, GI, GZ, Y3, Y4, EPG1, EPG2 SUBROUTINE R3(ALFA, BETA, ZNOT, YNOT, GI, GZ, Y3, Y4, EPG1, EPG2 SUBROUTINE R3(ALFA, BETA, ZNOT, YNOT, GI, GZ, Y3, Y4, EPG1, EPG2 SUBROUTINE R3(ALFA, BETA, ZNOT, YNOT, GI, GZ, Y3, Y4, EPG1, EPG2 SUBROUTINE R3(ALFA, BETA, ZNOT, YNOT, GI, GI, GO, GO, YA=YM SERO=K SUBROUTINE R3(ALFA, BETA, ZNOT, YNOT, GI, GI, GO, GO, GO, GO, GO, GO, GO, GO, GO, GO	10		RE TURN
SUBROUTINE TO FIX LIMITS ON REGION BEYONG FIRST + PEAK SUBROUTINE R3(ALFA, BETA, ZNOT, YNOT, GI.G2, Y3, Y4, EPG1, EPG2 1310  EXTERNAL CFR, SF I  1320  NZERO=K GI=0  YING=, Z/ALFA GINC=, Z/BETA GINC GINC, GINC, GINC, YA, GS, Z, X)  400  CFRBIG=CFR(ALFA, BETA, ZNOT, YNOT, O, YM) GS=0  TOL=EPY**CFRBIG CALL CORY(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, YINC, Y4, GS, Z, X)  400  GS=0  TOL=EPY**CFRBIG CALL CORY(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, YINC, Y4, GS, Z, X)  400  GS=0  TOL=EPY**CFRBIG CALL CORY(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, YINC, Y4, GS, Z, X)  400  GS=0  TOL=EPY**CFRBIG CALL CORG(ALFA, BETA, ZNOT, YNOT, NO, Y3)  GS=0  Y4=Y3  CALL CORG(ALFA, BETA, ZNOT, YNOT, O, Y3)  CFRBIG=CFR(ALFA, BETA, ZNOT, YNOT, O, Y3)	(7)		
SUBROUTINE R3(ALFA, BETA, ZNOT, YNOT, G1, G2, Y3, Y4, EPG1, EPG1  EXTERNAL CFR, SF I  NZERO=K  G1=0  Y INC=-2/BETA  G1NC=-2/BETA  G1NC=-2/BETA  G1NC=-2/BETA  G1NC=-2/BETA  G1NC=-2/BETA  G1NC=-2/BETA  G1NC=-2/BETA  G1NC=-2/BETA  G1+0  Y==YM  Y==YM  Y==YM  CFR B1G=CFR(ALFA, BETA, ZNOT, YNOT, O, YM)  TOL =EPY4*CFR B1G  CALL CORY(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, Y INC, Y4, GS, 2, K)  G2=0  TOL=EPY4*CFR B1G  CALL CORY(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, Y INC, Y4, GS, 2, K)  G2=0  TOL=EPG2*CFR B1G  CALL CORY(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, Y INC, Y4, GS, 2, K)  G2=0  TOL=EPG2*CFR B1G  CALL CORY(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, Y INC, Y4, GS, 2, K)  G0 TO 101  CFR B1G=CFR(ALFA, BETA, ZNOT, YNOT, O, Y3)  CFR B1G=CFR (ALFA, BETA, ZNOT, YNOT, O, Y3)	<b>₩</b>	U	DUTINE TO FIX LIMITS ON REGION BEYOND FIRST A DEAL STATE OF
### ### ##############################	P)		DUTINE R3 (ALFA, BETA, ZNOT, VNOT, 61 62 V3 VA FOCA FOCA
1320 1330 1340 1350 1360 1370 1370 1370 1370 1370 147(2	r)		NAL CF
1330 1340 1350 151NC= 1350 151NC= 1350 151(2 17(2) 1370 1410 1400 1410	r)		XII
1340 1350 1350 1350 1370 1370 1380 1390	17)		0=19
4350 410 400 400 400 400 400 400 600 60	m		YINC=.2/ALFA
15 ( ( 2 ) 350   15 ( ( 2 ) 370   17 ( ( 2 ) 390   17 ( ( 2 ) 390   17 ( ( 2 ) 390   17 ( ( 2 ) 390   17 ( ( 2 ) 390   17 ( ( 2 ) 390   17 ( ( 2 ) 390   17 ( ( 2 ) 390   17 ( ( 2 ) 390   17 ( ( 2 ) 390   17 ( ( 2 ) 390   17 ( ( 2 ) 390   17 ( ( 3 ) 390   17 ( (	ריו		GINC=.2/BETA
370 IF ((2 390 YM=1/ 390 CFRB1 400 CFRB1 410 701 FORMA 420 GS=0 440 CALL 450 G2=0 460 TOL=E 470 CALL 480 GO TO 490 GO TO 500 Y4=Y3 510 CFRB1	רייו		NOT # BETA) . GT . 0 . 707) GO TO
390 YW=1/ 400 CFRB1 410 701 FORMA 420 GS=0 440 CALL 450 G2=0 460 TOL=E 470 CALL 60 GS=0 500 Y4=Y3 510 CFRB1	m		(2.*ALFA*(SORT(YNOT)*1)), GT.1.0) GO TO
390	m		I/ALFA
400 CFRBI 410 701 FORMA 420 GS=0 70L=E 440 G2=0 70L=E 470 G2=0 470 G2=0 470 G2=0 490 G0 T0 490 G5=0 500 Y4=Y3	m		
410 701 FORMA 420 6S=0 440 CALL 450 62=0 460 TOL=E 470 CALL 480 60 GS=0 500 Y4=Y3 510 CFRBI	4		m
420 6S=0 440 CALL 450 G2=0 460 TOL=E 470 CALL 480 60 TO 500 Y4=Y3 510 CFRBI	4	701	3
430 TOL=E 440 CALL 450 G2=0 460 TOL=E 470 CALL 480 G0 TO 490 60 GS=0 500 Y4=Y3 510 CFRBI	4		· o
440 CALL 450 G2=0 460 TOL=E 470 CALL 480 G0 TO 490 60 GS=0 500 Y4=Y3 510 CFRBI	4		9
450 G2=0 460 TOL=E 470 CALL 480 G0 TO 490 60 GS=0 500 Y4=Y3 510 CFRBI	4		ALL
460 TOL=EPG2*CFRBIG 470 CALL CORG(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, GINC, G2, YM, 480 G0 TO 101 490 60 GS=0 74=73 510 CFRBIG=CFR(ALFA, BETA, ZNOT, YNOT, 0, Y3)	4		2=0
470 CALL CORG (ALFA, BETA, ZNOT, YNOT, NZERO, TOL, GINC, G2, YM, 60 G5=0	4		9
480 GO TO 101 490 60 GS=0 500 Y4=Y3 510 CFRBIG=CFR(ALFA,BETA,ZNOT,YNOT,0,Y3)	4		ALL CORG (ALFA, BETA, ZNOT, YNOT, NZERO, TOL GING, 62, XN.
490 60 GS=0 500 Y4=Y3 510 CFRBIG=CFR (ALFA, BETA, ZNOT, YNOT, 0, Y3)	4		101 OT C
500 Y4=Y3 510 CFRBIG=CFR(ALFA,BETA, ZNOT, YNOT, 0.Y3)	9		0=8
510 CFRBI	20		£ ¥ 3
	51		FRBI

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FOUND IN 13.7 WHEN X LIMIT, REACHED YES.
                                                                                                                                                                                                                                                                                                                                                                                                              CALL CORY (ALFA, BETA, ZNOT, YNOT, NZERO, TOL, Y INC, Y4, GS, 10, K)
                                                                                                                                                                                                                                                                                                           CALL CORG(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, GINC, 62, YS, 14, K)
              CALL CORY (ALFA, BETA, ZNOT, YNOT, NZERO, TOL, YINC, Y4, GS, 6, K)
                                                                  CALL CORGIALFA, BETA, ZNOT, YNOT, NZERO, TOL, GINC, G2, Y3, 8, K)
                                                                                                                                                                                                                       CALL EXTEND (ALFA, BETA, ZNOT, YNOT, EXT, 65, GESC, YS, 0, 12, XX)
                                                                                                                                  CALL EXTFND(ALFA, BETA, ZNOT, YNOT, EXT, GS, 0, YS, YINC, 10, K)
                                                                                                                                                                                                                                        IF(EXTARGUS) CALL TRUBL(YS, GS, 12, .TRUE.)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   SUBROUTINE TRUBLITY, G, NUMB, L)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    FORMAT ( * COORDINATE NOT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   #RITE(6,300) NUMB, Y, G
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       WRITE(6,400) NUMB, Ya G
                                                                                                                                                  IF (EXT.E0.0.) YS=Y3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                WARNING SUBROUTINE
TOL = EPY 4 * CFRBIG
                                                 TOL =EPG2*CFRB1G
                                                                                                                                                                                      GESCHZNOT#1.VX
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   IF(L) GO TO 7
                                                                                                                                                                                                                                                                                          GINC= 2/BETA
                                                                                                                                                                                                                                                                                                                                           YINC= . 2/ALFA
                                                                                                                                                                                                                                                                                                                                                                            YINCHO #YING
                                                                                                                                                                                                                                                                         TOL = EPG2*EXT
                                                                                                                                                                                                                                                                                                                                                           TOL = EPY4 * EXT
                                                                                   GO TO 101
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   LOGICAL L
                                                                                                     6.5=ZNOT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       GO TO 8
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      E20.8.
                                                                                                                                                                       XXII N #X
                                                                                                                                                                                                                                                                                                                                                                                                                               RETURN
                                                                                                                    YS=Y3
                                                                                                                                                                                                                                                                                                                                                                                               Y4= YS
                                                                                                                                                                                                                                                          62=65
                                                                                                                                                                                                       0=89
                                 62=0
                                                                                                                                                                                                                                                                                                                                                                                                                                                  FNO
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∞ o∧	1620.8.1
0064	FICEN
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N	SUBROUTINE TO SET UP INTEGRATION IN 3.165(A)
m	SUBROUTINE SETUPR (ALFA, BETA, ZNOT, YNOT, YY, GG. M, NN, A, B, C, D, F)
4	XTERNAL CF
in	REAL #8 F(40,40), YY (40), GG(40)
Q	N. 13 1 13 1 2 1 00
~	00 13 J=1.NX
80	Y=YK(I) + (B-A) /2+ (B+A) /2
σ	H=66(J)*(D-C)/2+(D+C)/2
0	3 F(I, J)=CFR(ALFA, BETA, ZNOT, YNOT, H, Y)
-	w
(V	
3	SUBROUTINE TO SET UP INTEGRATION IN 3.165(B)
d ·	SUBROUTINE SETUPL (ALFA, BETA, ZNOT, YNOT, YY, 66, M, NN, A, B, C, D, F)
S	EXTERNAL SFI
S	REAL#8 F(40,40), YY3403, GG(40)
~	X*1=1 61 00
(CO)	DO 13 JH1, NN
0	Y=YY(1)*(B-A)/2+3.B+A)/2
0	H=66(J) *(D-C) /2+(D+C) /2
-	3 F(1, J)=SF1(ALFA, BETA, ZNOT, YNOT, H, Y)
Ň	
m	ENO
٠	SUBROUTINE TO FIND PEAK IN INTEGRAND OF 3,165(B)
S	FUNCTION SFMIN(AL, BE, ZN, YN, DY, DG, GESC, YESC, GS, YS, YST, K)
Š	XTERNAL SFITSSFI
~	1 6=0
00	0=1
0	S60=-1.
0	3 Y=YST
~	G=6+6ESC
Ω.	SYO=SSFI(AL, BE, ZN3YN3Y, DY, 650.)
3	11

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FORMAT ( "NEED EVEN NUMBER OF Y GAUSSIAN POINTS!)
                                                                                                                                                                                                                                                                                                                               SUBROUTINE ROATA (GY, GZ, WTGY, WTGZ, NN, M)
                                                                                                                                                                                                                                                                                                                                             REAL #8 GY(40), GZ(40) 3MTGY(40), WTGZ(40)
                                                                                                                                                                                                                                                                                                                    SUBROUTINE TO READ INTEGRATION DATA
             SY=SSFI(AL, BE, ZN, YN, Y, DY, G, O.)
                                                   SG= SSF I (AL, BE, ZN, YN, Y, 0; 6, 06)
                                                                                                                                                                                                                                                                                                                                                                                                                       6Y(1)3NT6Y(1)
                                                                                                                                                                                                                                                                                SFRINE-SFI(AL, BE, ZN, YN, G, Y)
                          IF(SY#SYD.GI.0) 60 JO 26
                                                                                                                                                                                                     CALL TRUBL(Y, G, 2033TRUE.)
                                                                          IF(SG*SGO.GT.0) GO TO
                                                                                                                                                                                                                  READ(5.402.END=301) X
                                      Y=Y-SY#YESC/(SY-SYG)
                                                                                      6#6-S6*6ESC/(S6-S60)
                                                                                                                IF (M.GT.K.) GO TO 46
                                                                                                                                                                             IF (N. 6T.K) GO TO 46
                                                                                                                                                                                                                                                                                                                                                                                                          DO 20 1=1.NN,2
                                                                                                                                                                                                                                                                                                                                                                                                                                                2.5 KN . T = C
                                                                                                                                                                                                                                                                                                                                                         WRITE (6,200)
                                                                                                                                                                                                                                                                                                                                                                                  READ(5,201)
                                                                                                                                                                                                                                                                                                                                                                                                                       READ(5,202)
                                                                                                                                                                                                                                                                                                                                                                                             FORMAT(12)
                                                                                                                                                                                                                               FORMAT(13)
                                                                                                  50 TO 300
Y=Y+YESC
                                                                                                                                                                                         GO TO 14
                                                                                                                                         GC TO 13
                                                                                                                                                                                                                                                                                                                                                                                                                                  CONTINUE
                                                                                                                             SC0=SC
                                                                                                                                                                                                                                                                                           RETURN
                                                                                                                                                                                                                                            60 10
                                                                                                                                                     SYO=SY
                                                                「十三川王
                                                                                                                                                                                                                                                                                                                                                                                                                                                00 16
                                                                                                                                                                 「ナスリス
                                                                                                                                                                                                                                                                     9489
                                                                                                                                                                                                                                                        YS=Y
                                                                                                                                                                                                                                                                                                         END
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SUBROUTINE CORY (ALFA, BETA, ZNOT, YNOT, NZERO, TOL, YINC, YI, G, NUMB, K)
                                                                                                                                                                   O LRECT LON
                             Z GAUSSIAN POINTS+)
                                                                                                                                                                                                                                             SI=ABS (CFR(ALFA, BETA, ZNOT, YNOT, 6, Y1))-TOL
                                                                                                                                                                                                                                                                      SI=ABS(SFI(ALFA, BEIA, ZNCT ; YNOT, G, Y)))-TOL
                                                                                                                                                                                                                                                                                                                            SZ=ABS(CFR(ALFA,BEIA,ZNOT,YNOT,G,Y2))-TOL
                                                                                                                                                                                                                                                                                                                                                       S2=ABS(SFI(ALFA,BETA,ZNOT,YNOT,G,Y2))-10L
                                                                                                                                                             SUBROUTINE TO FIND INTEGRATION LIMIT IN
                                                                  6211 33 162(1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                    18 CALL TRUBLIYI, G. NUMB, .F ALSE.)
                              Ö
                          FORMATI * NEED EVEN NUMBER
                                                                                                                                                                                                                                1F(NUMB.GT.19) GO TO 23
                                                                                                                                                                                                                                                                                                                IF (NUMB.GI.19) 60 JO 61
                                                                                                                                                                                                                                                                                    1F(S1.EQ.0) GO TO 100
                                                                                                                                                                                                                                                                                                                                                                                                                        IF(KC.E0.K) GO TO 1.8
                                                                                                                                                                                                                                                                                                                                                                      33,99,34
                                                                                                                     # 182 ( )+1)=WTGZ ( )
                                                                                                                                                                                       EXTERNAL CFR, SF1
FORMAT (2F30.15)
                                                                                                          62(3+1)=-62(3)
                                                                                              J=1, M, 2
                                                     DO 30 1=1,M,2
              WRITE(6,300)
                                       READ(5,201)
                                                                READ(5, 202)
                                                                                                                                                                                                                                                                                                    Y2=Y1+Y1NC
                                                                                                                                                                                                                                                                                                                                                                     IF (S1 * S2)
                                                                              CONTINUE
                                                                                                                                                                                                                                                          G0 T0 43
                                                                                                                                                                                                                                                                                                                                           GO TO 44
                                                                                                                                                                                                                                                                                                                                                                                                                                      60 10 27
                                                                                                                                                                                                                                                                                                                                                                                                          KC=KC+1
                                                                                                                                   RETURN
                                                                                             00 10
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                                                                                                                                                                                                                                                                                                                                                                                               Y1=Y2
                                                                                                                                                                                                                    XC II O
                                                                                                                                                   END
202
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WTGY(J+1)=WTGY(J)

91

5610

5620

GY (J+1)=-6Y(J)

```
SUBROUTINE CORG(ALFA, BETA, ZNOT, YNOT, NZERO, TOL, GING, GI, Y, NUMB, K)
                                                                                                                                                                                                                                                                                                      DIRECTION
                                                            SNOT=ABS(CFR(ALFA, BETA, ZNOT, YNOT, G, YZERO))-TOL
                                                                                SNOT=ABS (SFI (ALFA, BETA, ZNOT, YNOT, G, YZERO))-TOL
                                                                                                                                                                                                                                                                                                SUBROUTINE TO FIND INTEGRATION LIMIT IN . V
                                                                                                                                                                                                                                                                                                                                                                                             = ABS(SFI(ALFA, BETA, ZNOT, YNOT, 61, Y)) - TOL
                                                                                                                                                                                                                                                                                                                                                                         1=ABS(CFR(ALFA,BETA,ZNOT,YNOT,G1;Y))-TOL
                                                                                                   60 TO 47
                                                  GO TO 71
                                                                                                                                                                                                                                                                                                                                                             F(NUMB.61.19) 60 70 21
                                                                                                                                                                                                                                                                                                                                                                                                                                          9
                                                                                                                                                                                                                                                                                                                                                                                                               F(S1.60.0) 60 TO 300
                                                                                                                                                                                                                                                                                                                                                                                                                                      IF (NUMB.64.19) GO TO
                                                                                                                                   IF(SNOT#52) 50,49351
                                                                                               IF (.(NZERO-N) . GT .0)
                       EPS=YINC/(1-51/52)
                                                                                                                                                                                                                                                                                                                         EXTERNAL CFR, SFI
                                               F ( NUMB . GT . 19)
                                                                                                                                                                                                YINC=YINC-EDS
                                    YZERO=Y2-EPS
                                                                                                                                                                                                                                                                                                                                                                                                                           62=61+61NC
GO TO 100
                                                                                                                        GO TO 100
                                                                                                                                                             GO TEN 100
                                                                        60 TO×45
                                                                                                            YI=YZERO
                                                                                                                                                 YI=YZERO
                                                                                                                                                                                    Y2=YZERO
                                                                                                                                                                                                            GO TO 33
                                                                                                                                                                                                                                    Y INCHEPS
                                                                                                                                                                                                                                                GO TO 33
                                                                                                                                                                                                                                                                                                                                                                                     0 10 43
                                                                                                                                                                       S2=SNOT
                                                                                                                                                                                                                        S1= SN01
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            一十2.112
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SNOT = ABS (CFR(ALFA, BETA, ZNOT, YNOT, GZERO, Y)) - TOL
                                                                                                                                                                                                 GO TO 45
SNOT=#BS(SFI(ALFA.BEIA.ZNOT.YNOT.GZERO,Y))-TOL
S2=ABS (CFR (ALFA.BETA, 2NCT, YNOT, G2,Y))-TOL
                        S2=ABS(SFI(ALFA, BETA, ZNOT, YNOT, G2, Y))-TOL
                                                                                                           TRUBL(Y, G) , NUMB, .FALSE.)
                                                                                                                                                                                                                         IF ( (NZERO-N), GT .0) - 60 TO 47
                                                                                     IF (KC. EQ.K) GO TO 18
                                                                                                                                                                                                                                                                50,49,5
                                                                                                                                                  EPS=GINC/(1-S1/S2)
                                                                                                                                                                          IF ( NUMB . GT . 19)
                                                                                                                                                                                                                                                                                                                           STACE SINCE EPS
                                                                                                                                                             GZER0=G2-EPS
                                                                                                                                                                                                                                                              1F ( SNOT #52)
                                                                                                                         GO TO 100
                                                                                                                                                                                                                                                                                       GO TO 100
                                                                                                                                                                                                                                                 GO TO 100
                                   44. IF (SI #52)
                                                                                                                                                                                                                                     G1 = GZERO
                                                                                                GO TO 27
                                                                                                                                                                                                                                                                           61=6ZER0
                                                                                                                                                                                                                                                                                                               G2=GZERO
                                                                                                                                                                                                                                                                                                                                       GO TO 33
                                                                                                                                                                                                                                                                                                                                                               GINCHEDS
                                                                                                                                                                                                                                                                                                                                                                            GO TO 33
                                                                        KC=KC+1
                                                                                                                                                                                                                                                                                                   51, S2=SNOT
                                                                                                                                                                                                                                                                                                                                                    S1=SNOT
                                                                                                                                                                                                                                                                                                                                                                                                   RETURN
                                                            61=62
                                                 51=25
                                                                                                                                                                                                                                                                                                                                                                                         61 = 62
                                                                                                                                      一 十 2 川 2
                                                                                                             CALL
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# A.4.4 Gaussian paints and weights

The Gaussian integration points and weights required by the program listed in the last section can be stored in a particularly convenient fdrm, as shown below. If the data is kept in a file "PTSWTS", the instruction

CONTINUE WITH PTSWTS (800,804) RETURN (A4.18) will provide the program with the information required for an n-point integration with n=8. Similarly, if PTSWTS (1600,1608) is used in place of PTSWTS (800,804), the program will be given the information required for an integration with n=16. The points and weights listed are taken from bramowitz and Stegun (1964).

400	A •		
401	0.339981043584856.0.652145154862546.		
402	0.861136311594053.0.347854845137454.		
800	8.	· 1	
801	0.183434642495650.0.362683783378362.	1	
802	0.525532409916329.0.313706645877887.	* '	
803	0.796666477413627.0.222381034453374.	1	
80A	0.960289856497536.0.101228536290376.		
1200	12.	<b>X</b>	
1201	0.125233408511469,0.249147045813403,		
1202	0.367831498998180,0.233492536538355.		
1203	0.587317954286617.0.203167426723066.		
1204	0.769902674194305.0.160078328543346.	1	
1205	0.904117256370475.0.106939325995318.	. ,	
1206	0.981560634246719.0.047175336386512.	· · · ·	1 .
		/	

1600	.16.
1601	0.095012509837637440185.0.189450610455068496285,
1602	0.281603550779258913230.0.162603415044923588867,
1603	0.458016777657227386342.0.169156519395002538189,
1604	0.617876244402643748447.0.149595988816576732081,
1605	0.755404408355003033895.0.124628971255533872052.
1606	0.865631202387831743880,0.095158511682492784810,
1607	0.944575023073232576078,0.062253523938647892863,
1608	0.989400934991649932596.0.027152459411754094852.
2000	20,
2001	0.076526521133497333755.0.152753387130725850698.
2002	0.227785851141645078080.0.149172986472603746788.
2003	0.373706088715419560673.0.142096109318382051329.
2004	0.510867001950827098004.0.131688638449176626898.
2005	0.636053680726516025453.0.118194531961518417312.
2006	0.746331906460150792614.0.101930119817240435037.
2007	0.839116971822218823395.0.083276741576704748725.
2008	0.912234428251325905868,0.062672048334109063570,
2009	0.963971927277913791268.0.040601429800386941331.
2010	0.993128599185094924786.0.017614007139152118312.
2400	24,
2401	0.064056892862605626085.0.127938195346752156974.
2402	0.191118867473616309159,0.125837456346828296121.
2403	0.315042679696163374387,0.121670472927803391204,
2404	0.433793507626045138487,0.115505668053725601353.
2405	0.545421471388839535658,0.107444270115965634783,
2406	0.648093651936975569252.0.097618652104113888270.
2407	0.740124191578554364244.0.086190161531953275917.
2408 2409	0.820001985973902921954.0.073346481411080305734.
2410	0.886415527004401034213.0.059298584915436780746.
2411	0,938274552002732758524,0.044277438817419806169,
2412	0.974728555971309498198.0.028531388628933663181.
3200	0.995187219997021360180.0.012341229799987199547.
3201	0.048307665687738316236.0.096540088514727800567.
3202	0-144471961582796493485.0.095638720079274859419.
3203	0.239287362252137074545.0.0938443.990808
3204	0.331868602282127649780.0.091173878695195884713.
3205	0.421351276130635345364,0.08765209300440381
3206	0.506899908932229390024.0.08331192422694675
3207	0.587715757240762329041.0.078193895787070306472.
3208	0.663044266930215200975.0.07234579410884850622
3209	0.732182118740289680387.0.065822222776361846838.
3210	0.794483795967942406963,0.058684093478535547145.
3211	0.849367613732569970134.0.050998059262376176196.
3212	0.896321155766052123965.0.042835898022226680657.
3213	0.934906075937739689171.0.034273862913021433103.
3214	0.9647622555875 06430774.0.025392065309262059456.
3215	0.985611511545268335400.0.016274394730905670605.
3216	0,997263861849481563545.0.007018610009470096600.
E.	