Strain-Rate-Dependent Mechanical Behavior of a Non-Equimolar CoCrFeMnNi High Entropy Alloy with a Segmented Coarse Grain Structure: Supplementary Document

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Appendix A: Background and Computational Details of Gibbs Free Energy Calculations

0.1. Background

The Gibbs free energy for a given composition can be expressed as the following with respect to the equimolar reference case,

$$G = H^{\rm mix} + F^{\rm el} + F^{\rm vib} - TS_{\rm conf},\tag{1}$$

where H^{mix} , F^{el} , F^{vib} and S_{conf} are the enthalpy of mixing, the electronic Helmholtz energy, the vibrational Helmholtz energy and the configurational entropy with respect to the equimolar CoCrFeMnNi alloy, respectively.

The enthalpy of mixing, H^{mix} , can be approximated using the enthalpy of mixing of binary bulk metallic glasses, given by Youssef et al. [1],

$$H^{\text{mix}} = \sum_{i < j} 4c_i c_j H^{\text{mix}}_{ij},\tag{2}$$

where c_i is the molar fraction of the *i*-th element in the alloy and H_{ij}^{mix} for the relevant pairs are available within the Miedema's model in Ref. 2.

The electronic and vibrational Helmholtz free energies can be obtained using the approximate Kohn-Sham density-functional theory (KS-DFT) [3, 4] and its perturbative extension, namely the density-functional perturbation theory (DFPT) [5, 6]. The electronic component is given by [7–9],

$$F_{\rm el} = \left(\int dE \ N(E, V) fE - \int^{E_{\rm F}} dE \ N(E, V) E \right)$$

$$- T \left(-k_{\rm B} \int dE \ N(E, V) \left[fln(f) + (1 - f)ln(1 - f) \right] \right),$$
(3)

where $k_{\rm B}$ is the Boltzmann constant; N(E, V) is the electronic density of states (DOS); $f = f(E, E_{\rm F}, T)$ is the Fermi-Dirac distribution function around the Fermi level with the Fermi energy, $E_{\rm F}$. The vibrational component is given by [10, 11],

$$F_{\rm vib}(T) = k_{\rm B}T \int_0^\infty d\omega \,\ln\left[2 \,\sinh\left(\frac{\hbar\omega}{2k_{\rm B}T}\right)\right] g(\omega),\tag{4}$$

where $g(\omega)$ and $k_{\rm B}$ are the phonon DOS and the Boltzmann's constant, respectively. Furthermore, the spatial disorderliness of HEAs can be expediently achieved at a disordered mean-filed limit using the virtual-crystal approximation (VCA) [12, 13] by mixing the atomic pseudo-potentials [13, 14].

Finally, the configurational entropy due to the spatial disorderliness is given within the the Stirling approximation by Santodonato et al. [15],

$$S_{\rm conf}^M = -R \, \sum_i^N c_i ln(c_i), \qquad (5)$$

where R is the gas constant. To assess the thermal stability of the non-equimolar mixtures, we will compare the difference in the Gibbs free energies (ΔG) taking as reference the equimolar CoCrFeMnNi composition (G_{ref}),

$$\Delta G = G - G_{\text{ref}}.\tag{6}$$

0.2. Computational Details

The SG15 optimized norm-conserving Vanderbilt (ONCV) scalar-relativistic pseudo-potentials [16, 17] using the Perdew-Burke-Ernzerhof (PBE) exchangecorrelation functional [18–20] were used for elemental atomic pseudo-potentials. A generic face-centered-cubic was used for HEAs. Variable-cell geometry optimizations were performed using the Quantum ESPRESSO (QE) software [21, 22] with a common high kinetic energy cutoff of 150 Ry, and a choice of the smearing parameter for the Marzari-Vanderbilt cold smearing [23] equivalent to 300 K at a shifted $12 \times 12 \times 12$ Monkhorst-Pack-equivalent [24] uniform Brillouin zone with a 10^{-7} Ry total-energy, and 10^{-6} Ry·a₀⁻¹ total force convergence thresholds, and 10^{-10} self-consistency threshold. Thermal functions, elastic properties, and phonon dispersion were performed using "thermo_pw" package within the QE software. A uniform $4 \times 4 \times 4$ Monkhorst-Pack grid is used for phonon-dispersion simulations with a 10^{-12} self-consistency threshold. Supplementary Figures and Tables



Figure 1: Individual contributions to the relative Gibbs free energy (ΔG) of the Co-reduced $Co_{0.1}(CrFeMnNi)_{0.9}$ and Co-rich $Co_{0.3}(CrFeMnNi)_{0.7}$ alloys with respect to the equimolar CoCrFeMnNi alloy. For the Co-reduced $Co_{0.1}(CrFeMnNi)_{0.9}$ case, the negative vibrational Helmholtz free energy overcomes the more positive configurational entropy, which results in a thermally more stable product.



Figure 2: 1D-XRD spectrum showing single FCC phase present in the $Co_{11.3}Cr_{20.4}Fe_{22.6}Mn_{21.8}Ni_{23.9}$ (wt%) high entropy alloy. The stage background peaks are included for completeness.



Figure 3: EDS mapping taken within a single high angle coarse grain showing thick band like features allocated at the low angle sub grain boundaries (more obvious in the Mn and Fe maps).



 $\mathcal{E}_{\mathcal{XX}}$ -0.01 -0.02 -0.03 -0.04 -0.05 -0.06 -0.07 -0.08 -0.09 -0.10 -0.11 -0.12

Figure 4: (a) band contrast and (b) EBSD IPF map showing the deformation features at an intermediate strain rate ($\sim 120 \text{ s}^{-1}$). (c) The corresponding DIC axial strain contour showing an good alignment of surface deformation bands and the grain growth direction.

Table 1: Chemical composition of the SCG-HEA confirmed by using inductively coupled plasma mass spectrometry (ICP-MS), energy dispersive spectroscopy (EDS), and x-ray photoelectron spectroscopy (XPS) methods.

Element	ICP-MS method (wt%)	EDS method (wt%)	XPS method (wt%)
Fe	22.66	22.06	19.27
Mn	21.82	22.79	23.96
Ni	23.80	22.97	24.37
Cr	20.41	20.91	20.13
Co	11.31	11.27	12.27

Table 2: Summary of the mechanical properties of the SCG-HEA alloy.

Property	Values	
Density	$7.72 \pm 0.08 \text{ g/cm}^3$	
Yield strength	160 - 330 MPa	
Young's modulus	$96.2 \pm 4.1 \ \mathrm{GPa}$	
Poisson's ratio	0.350 ± 0.026	
Microhardness	$2.84\pm0.09~\mathrm{GPa}$	

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