















where  $U_j$  is the solution by parallel-in-time method. The system equations can be solved by Newton-Raphson method according to

$$U_j^k = \widehat{U}_j^k + \frac{\partial \widehat{U}_j^k}{\partial U} \Delta U_{j-1}^k, \quad (32)$$

where  $\Delta U_{j-1}^k = U_{j-1}^k - U_{j-1}^{k-1}$ .  $U_{j-1}^k$  is the system output at  $k$ th iteration.

Because both the coarse and the precise operator use the same model and system parameters,  $\widehat{U}_j^k$  and  $U_j^k$  are approximately the same with the acceptable error. Based on the backward differentiation formula, the partial differential item in equation (32) can be approximately obtained by

$$\frac{\partial F}{\partial U} = \frac{\widehat{U}_j^k - \widehat{U}_j^{k-1}}{U_{j-1}^k - U_{j-1}^{k-1}}. \quad (33)$$

Thus, when substituting the assumption into system equations (31), the solution by parallel-in-time algorithm can be obtained by

$$U_j^k = \widehat{U}_j^k + U_j^k - U_j^{k-1}. \quad (34)$$

Notice that the parallel-in-time method is differentiated by the iteration number index  $k$  not the time-step  $j$ . As shown in Fig. 4, the solution process starts from  $t = 0$  time step, when  $k = 1$ . The coarse operator provides the initial value of  $\widehat{U}_j^k$  for precise operator iteratively.  $N_{po}$  precise operators are running in parallel from the perspective of time with time-step of  $\Delta t$ .

### B. Parallel-in-Time Simulation of EV Power System

The parallel-in-time algorithm is implemented in device-level simulation due to the computation burden is mainly caused by the solution process for MMC. Fig. 5 shows the parallel-in-time design in GPU kernels. The powertrain model generates the IM speed, and the SOC model calculates the required power in the CPU. Then these data and global variables are sent to GPU through PCIe bus.

The first value  $U_0^0$  of MMC and IM at  $k = 0$  is assumed known at the beginning. The coarse operator is initialized with the system states  $U_0$  with the time-step with  $\Delta T = 100$  ns.

Meanwhile, there are multiple precise operators to solve the system ODE at the time-step of  $\Delta t$  in a parallel manner. Each precise operator is programmed as a grid which is also known as a kernel, which simulates the output voltage and current of MMC, the output power, and the inner variables of IGBT and diode pairs using the initial values from the coarse operator.

For each kernel, there are eight threads of parallelism, which is the same as the number of arms in the MMC. As shown in Fig. 6, each thread is designed to solve the dynamics of individual arms including phase-shift control and the NBM model of IGBT and diode pair.

Finally, the device-level parallel-in-time simulation results are available based on equation (34) using the solution vectors of coarse operators and precise operators. The deviation between

TABLE II  
PARAMETERS OF TESLA X 75D [34]

Parameters	Value	Parameters	Value
Engine power	193 kW	$m_{ev}$	2352 kg
Engine torque	329 Nm	$C_{r,ev}$	0.02
Battery capacity	75 kWh	$C_{ae,ev}$	0.24
Range EPA	381 km	$\eta_{gr}$	8.2752

$U^k$  and  $U^{k-1}$  is calculated by

$$errU^k = \sum_{j=k}^{Num_1} \frac{\|U_j^k - U_j^{k-1}\|}{\|U_j^k\|}. \quad (35)$$

In this work,  $errU^k$  is expected to less than 1%.

The parallel-in-time implementation in device-level simulation for power systems generally requires 4 GB of memory and 100 GB/s bandwidth between CPU and GPU. For a specific MMC (e.g., five-level), at least 100 GPU cores are used for the proposed parallel-in-time method.

## V. SIMULATION RESULTS AND DISCUSSION

The device-level simulation was carried out on both CPU and GPU on the 2.2 GHz Intel Xeon E5-2698 v4 CPU and 192 GB RAM. The GPU configuration is the Nvidia Tesla V100 with 5120 CUDA cores, 16 GB of memory whose bandwidth is 900 GB/s [33]. In addition, the system-level simulation results are validated by the datasheet of the Tesla Model X 75D whose parameters as listed in Tab. II.

### A. Device-Level Switching Transients

The switching transients of IGBT/diode pair from five-level MMC with the DC bus voltage of 400 V are provided in Fig. 7. The gate voltage is  $\pm 15$  V and the gate resistance is 10  $\Omega$ . With the dead-time of 5  $\mu$ s and switching frequency of 4 kHz, the turn-on current of IGBT overshoots lightly at around 0.382 ms. During the turn-off period,  $V_{CE}$  increased from 0 V to 600 V, which is the same as  $V_{CE}$  from the datasheet. Fig. 7(c) shows the diode reverse recovery process.

Figs. 7(d) and 7(e) show the upper and lower switch currents of one submodule. When the IGBT turns on, the switch current is changed according to the submodule currents, while when the IGBT turn-off the switch current increased in the reverse direction which accounts for the diode reverse recovery. In the Fig. 7(f), the junction temperature of the IGBT suddenly surges when the MMC starts to operate, and the curve decreases gradually along with the steady-state of MMC. Simulation is also conducted in the commercial EMT tool to validate the NBM of IGBT and diode pair and the designed MMC GPU kernel.

Fig. 8 shows the MMC output voltage with the source frequency of 60 Hz, the submodule capacitor of 6 m $\Omega$ , and the arm inductance of 1 mH. Fig. 8(a) demonstrates the capacitor voltage in the first submodule of the upper arm. Since the DC voltage is 400 V, the capacitor voltage reference for individual submodules in the five-level MMC is expected to be 100 V. Fig. 8(a) shows the voltage overshoot during the MMC start-up, with the maximum value of 132.1 V, and eventually remains at



TABLE III  
EXECUTION TIME AND SPEED-UP OF EV SIMULATION FOR 10 s DURATION

Time-step (ns)	Execution Time ( $\times 10^2$ s)				Parallel-in-time Speed-up		Max. Memory (MB)	
	CPU	GPU	Parallel-in-time (10 kernels)	Parallel-in-time (30 kernels)	10 kernels	30 kernels	CPU	GPU
10	84.31	78.35	19.06	12.72	4.11	6.16	1081	1256
40	31.57	24.56	8.62	6.88	2.85	3.57	786	846
80	22.67	18.87	7.63	6.55	2.47	2.88	571	691

100 V at steady-state. The phenomenon in the zoomed-in figure is also caused by the diode reverse recovery. The single-phase voltage and three-phase voltage of MMC are shown in Figs. 8(b) and 8(c). The accuracy of these results is validated by SaberRD.

### B. System-Level Simulation for EVs

As is well known, different types of EVs have been recently designed with a wide capacity of driving range. As shown in Fig. 7, the speed profiles of Environmental Protection Agency (EPA) urban dynamometer driving schedule and the New York City Cycle (NYCC) [13] are chosen for the system-level testing.

Figs. 9(a) and 9(b) show  $v_{eh}$  from EPA and NYCC, respectively, using which the load power and angular velocity can be calculated using the powertrain model. Figs. 9(g) and 9(h) demonstrate the SOC variation along with the EPA and NYCC cycles.

Fig. 10 provides the five-level MMC connected with the IM responses to the vehicle speed variation from 60 s to 70 s under the condition of the EPA driving cycle. The angular velocity increased to 51.2 rd/s, then gradually decreased started at about 64 s. During this period, the current of MMC phase A decreased at around 63 s when the rate of the angular velocity changing decreased. During 65 s to 70 s,  $\omega_m$  keeps increasing, while the rate varies with time after 68 s.

Table III summarizes the execution times, the parallel-in-time speed-up, and maximum used memory for device-level simulation of EV in different time steps. The test is conducted on the five-level MMC at the switching frequency of 4 kHz during 10 s. The results show that the GPU processor takes less time than CPU simulation since the submodules of MMC are processed in a parallel manner in several threads. The proposed parallel-in-time simulation can significantly reduce the execution time using 10 kernels and 30 kernels. Table III shows that the proposed parallel-in-time interpolation strategy significantly accelerates the device-level and system-level MMC-based EV simulation.

Furthermore, the parallel-in-time performs better when the precise time-step becomes smaller, because more nonlinear solution procedures can be processed in a parallel manner. In other word, the larger the difference between the operator's time interval, the more significantly the proposed method performs. However, the time step of coarse operator cannot be too large, which will cause the convergence problem of device-level simulation. Moreover, with the increasing kernel number of precise operators, the proposed method requires less execution time.

## VI. CONCLUSION

In this paper, a parallel-in-time device-level simulation method is proposed for the MMC-based power system of EVs. The NBM can reveal thermal information and EMT behavior during the MMC operation, which is essential for the design of energy management strategy and EVs testing. Particularly, an interpolation strategy is designed based on the parallel-in-time algorithm to reduce the simulation execution time with the two operators working at different time-step. The proposed interpolation strategy can significantly speed up the device-level simulation by processing the nonlinear solution procedures in precise operators in a parallel manner, using the coarse operators' initial values. The simulation results show that system-level EMT simulation involving NBM of IGBT and diode pair is feasible when the parallel-in-time algorithm is utilized. The simulation execution time shows that the proposed parallel-in-time simulation method can speed up the device-level simulation of EVs. Future research will extend the approach to achieve a comprehensive multi-domain simulation of EVs.

## APPENDIX

The Siemens BSM300GA160D IGBT behavioral model parameters  $i_{sD1} = 0.01$ ,  $L_{D1} = 10^{-11}$  H,  $r_{D1} = 12.8 \mu\Omega$ ,  $V_{bD1} = 0.1495$ ,  $K_{rr} = 9874.1$ ,  $V_{ch} = 6.3$  V,  $a_1 = 0.022$ ,  $b_1 = 0.004$ ,  $a_2 = 92.5129$ ,  $b_2 = 4.0188$ ,  $a_3 = -0.1943$ ,  $b_3 = -0.4827$ ,  $x = 0.974$ ,  $y = 1.429$ ,  $z = 0.369$ ,  $r_{tail} = 1 \mu\Omega$ ,  $C_{tail} = 10$  F.

## REFERENCES

- [1] A. Hintz, U. R. Prasanna, and K. Rajashekara, "Novel modular multiple-input bidirectional DCDC power converter (MIPC) for HEV/FCV application," *IEEE Trans. Ind. Electron.*, vol. 62, no. 5, pp. 3163–3172, May 2015.
- [2] M. Quraan, P. Tricoli, S. D'Arco, and L. Piegari, "Efficiency assessment of modular multilevel converters for battery electric vehicles," *IEEE Trans. Power Electron.*, vol. 32, no. 3, pp. 2041–2051, Mar. 2017.
- [3] M. Narimani, B. Wu, and N. R. Zargari, "A novel five-level voltage source inverter with sinusoidal pulse width modulator for medium-voltage applications," *IEEE Trans. Power Electron.*, vol. 31, no. 3, pp. 1959–1967, Mar. 2016.
- [4] W. Yang, Q. Song, S. Xu, H. Rao, and W. Liu, "An MMC topology based on unidirectional current H-bridge submodule with active circulating current injection," *IEEE Trans. Power Electron.*, vol. 33, no. 5, pp. 3870–3883, May 2018.
- [5] C. Gan, Q. Sun, J. Wu, W. Kong, C. Shi, and Y. Hu, "MMC-based SRM drives with decentralized battery energy storage system for hybrid electric vehicles," *IEEE Trans. Power Electron.*, vol. 34, no. 3, pp. 2608–2621, Mar. 2019.
- [6] D. Ronanki and S. S. Williamson, "Modular multilevel converters for transportation electrification: Challenges and opportunities," *IEEE Trans. Transport. Electric.*, vol. 4, no. 2, pp. 399–407, Jun. 2018.

- [7] A. Salem and M. Narimani, "A review on multiphase drives for automotive traction applications," *IEEE Trans. Transport. Electrification*, vol. 5, no. 4, pp. 1329–1348, Dec. 2019.
- [8] D. Gao, C. Mi, and A. Emadi, "Modeling and simulation of electric and hybrid vehicles," *Proc. IEEE*, vol. 95, no. 4, pp. 729–745, Apr. 2007.
- [9] Y. Zhang, S. Lu, Y. Yang, and Q. Guo, "Internet-distributed vehicle-in-the-loop simulation for HEVs," *IEEE Trans. Veh. Technol.*, vol. 67, no. 5, pp. 3729–3739, May 2018.
- [10] C. M. Martinez, X. Hu, D. Cao, E. Velenis, B. Gao, and M. Wellers, "Energy management in plug-in hybrid electric vehicles: Recent progress and a connected vehicles perspective," *IEEE Trans. Veh. Technol.*, vol. 66, no. 6, pp. 4534–4549, Jun. 2017.
- [11] Y. Lee, A. Khaligh, and A. Emadi, "Advanced integrated bidirectional AC/DC and DC/DC converter for plug-in hybrid electric vehicles," *IEEE Trans. Veh. Technol.*, vol. 58, no. 8, pp. 3970–3980, Oct. 2009.
- [12] L. Li, B. Yan, C. Yang, Y. Zhang, Z. Chen, and G. Jiang, "Application-oriented stochastic energy management for plug-in hybrid electric bus with AMT," *IEEE Trans. Veh. Technol.*, vol. 65, no. 6, pp. 4459–4470, Jun. 2016.
- [13] T. Mesbahi, F. Khenfri, N. Rizoug, P. Bartholomeus, and P. L. Moigne, "Combined optimal sizing and control of li-ion battery/supercapacitor embedded power supply using hybrid particle swarm/eldermead algorithm," *IEEE Trans. Sustain. Energy*, vol. 8, no. 2, pp. 59–73, Jan. 2017.
- [14] R. Xiong, Y. Zhang, J. Wang, H. He, S. Peng, and M. Pecht, "Lithium-ion battery health prognosis based on a real battery management system used in electric vehicles," *IEEE Trans. Veh. Technol.*, vol. 68, no. 5, pp. 4110–4121, May 2019.
- [15] J. Yang, B. Xia, Y. Shang, W. Huang, and C. C. Mi, "Adaptive state-of-charge estimation based on a split battery model for electric vehicle applications," *IEEE Trans. Veh. Technol.*, vol. 66, no. 12, pp. 10889–10898, Jul. 2017.
- [16] B. J. Baliga, "Analytical modeling of IGBTs: Challenges and solutions," *IEEE Trans. Electron Devices*, vol. 60, no. 2, pp. 535–543, Feb. 2013.
- [17] A. S. Bahman, K. Ma, P. Ghimire, F. Iannuzzo, and F. Blaabjerg, "A 3-D-lumped thermal network model for long-term load profiles analysis in high-power IGBT modules," *IEEE J. Emerg. Sel. Topics Power Electron.*, vol. 4, no. 3, pp. 1050–1063, Sep. 2016.
- [18] N. Lin and V. Dinavahi, "Exact nonlinear micromodeling for fine-grained parallel EMT simulation of MTDC grid interaction with wind farm," *IEEE Trans. Ind. Electron.*, vol. 66, no. 8, pp. 6427–6436, Aug. 2019.
- [19] R. Zhu, N. Lin, V. Dinavahi, and G. Liang, "An accurate and fast method for conducted EMI modeling and simulation of MMC-based HVDC converter station," *IEEE Trans. Power Electron.*, vol. 35, no. 3, pp. 4689–4702, May 2020.
- [20] S. Esmaeili and S. Kouhsari, "A distributed simulation based approach for detailed and decentralized power system transient stability analysis," *Electr. Power Syst. Res.*, vol. 77, no. 5–6, pp. 673–684, Apr. 2007.
- [21] M. Tomim, J. Marti, and L. Wang, "Parallel solution of large power system networks using the Multi-Area Thévenin Equivalents (MATE) algorithm," *Int. J. Electr. Power Energy Syst.*, vol. 31, no. 9, pp. 497–503, Sep. 2009.
- [22] G. Gurralla, A. Dimitrovski, S. Pannala, S. Simunovic, and M. Starke, "Parallel in time for fast power system dynamic simulations," *IEEE Trans. Power Syst.*, vol. 31, no. 3, pp. 1820–1830, May 2016.
- [23] Y. Song and B. Wang, "Analysis and experimental verification of a fault-tolerant hev powertrain," *IEEE Trans. Power Electron.*, vol. 28, no. 12, pp. 5854–5864, Feb. 2013.
- [24] P. Igetic, "Exponential ade solution based compact model of planar injection enhanced IGBT dedicated to robust power converter design," *IEEE Trans. Power Electron.*, vol. 30, no. 4, pp. 1914–1924, Apr. 2015.
- [25] N. Lin and V. Dinavahi, "Variable time-stepping modular multilevel converter model for fast and parallel transient simulation of multiterminal DC grid," *IEEE Trans. Ind. Electron.*, vol. 66, no. 9, pp. 6661–6670, Sep. 2019.
- [26] M. Khayami, A. Nasiri, and O. Okoye, "Development of an equivalent circuit for batteries based on a distributed impedance network," *IEEE Trans. Veh. Technol.*, vol. 69, no. 6, pp. 6119–6128, Apr. 2020.
- [27] J. Xu, C. C. Mi, B. Cao, J. Deng, Z. Chen, and S. Li, "The state of charge estimation of lithium-ion batteries based on a proportional-integral observer," *IEEE Trans. Veh. Technol.*, vol. 63, no. 4, pp. 1614–1621, May 2014.
- [28] P. Krause, O. Wasynczuk, S. Sudhoff, and S. Pekarek, *Analysis of Electric Machinery and Drive Systems*. Hoboken, NJ, USA: Wiley.
- [29] S. Inc., *Saber Model Architect Tool User Guide*, USA, Sep. 2009.
- [30] N. Lin, P. Liu, and V. Dinavahi, "Component-level thermo-electromagnetic nonlinear transient finite element modeling of solid-state transformer for DC grid studies," *IEEE Trans. Ind. Electron.*, vol. 68, no. 2, pp. 938–948, Feb. 2021.
- [31] R. E. Araujo, R. Castro, C. Pinto, P. Melo, and D. Freitas, "Combined sizing and energy management in EVs with batteries and supercapacitors," *IEEE Trans. Veh. Technol.*, vol. 63, no. 7, pp. 3062–3076, Sep. 2014.
- [32] T. Cheng, T. Duan, and V. Dinavahi, "Parallel-in-time object-oriented electromagnetic transient simulation of power systems," *IEEE Open Access J. Power Energy*, vol. 7, pp. 296–306, Jul. 2010.
- [33] NVIDIA Tesla V100 GPU Architecture, Aug. 2017. [Online]. Available: <https://images.nvidia.com/content/volta-architecture/pdf/volta-architecture-whitepaper.pdf>
- [34] Tesla Model X 75D, Jan. 2018. [Online]. Available: <https://www.guideautoweb.com/en/makes/tesla/model-x/2018/specifications/75/d/>



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