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**Test Methods for Evaluating
Mechanical Properties
of Waferboard:
A Preliminary Study**

by
M. MacIntosh
and
J. Longworth

May, 1982

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Test Methods for Evaluating
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A Preliminary Study

by

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May, 1982

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ABSTRACT

Results of a preliminary study of test methods for evaluating mechanical properties of 11.1 mm (7/16") waferboard are presented. Waferboard properties are compared with properties obtained from identical tests on 9.5 mm (3/8") unsanded western white spruce plywood.

Detailed computer programs used to analyze the data and the computer output of all test results and statistical quantities are presented.

The tests included small scale flexure tests, compression tests, bond tests, large scale post flexure tests and concentrated load tests. In addition, specific gravity and moisture content values were obtained.

The properties determined include modulus of rupture, modulus of elasticity, ultimate compressive stress, stiffness (EI), and ultimate bond stress.

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1. INTRODUCTION

1.1 General

In the spring of 1981 the Forest Products Working Group of the Alberta Research Council expressed interest in evaluating structural testing procedures for determining the mechanical properties of waferboard. As a result, this project was initiated as a preliminary study.

1.2 Scope

The primary purpose of the test program was to assess test methods for determining various mechanical properties of waferboard. To provide a basis of comparison identical tests were performed on plywood. The waferboard tested was 11.1 mm (7/16 inch) thick and was manufactured by Weldwood of Canada, Ltd. in Slave Lake. The plywood tested was 9.5 mm (3/8") unsanded sheeting grade plywood made from western white spruce, and manufactured by Zeidler Forest Industries Ltd. of Edmonton.

The choice of thickness was based on Table 9.23.15.A of the 1980 National Building Code of Canada which states that 9.5 mm plywood and 11.1 mm waferboard can be used interchangeably as roof sheathing for joists at 400 mm on centre without edge support, or for joists at 600 mm on centre with edge support.

The following tests were performed:

1. Small scale flexural tests (CSA Standard CAN3-

0188.0-M78, Section 6.6)

2. Small scale compression tests (Longworth, J., "Moisture-Strength Relations for Sheathing Grade Douglas Fir Plywood", Department of Civil Engineering, The University of Alberta, 1974)
3. Bond tests (CSA Standard CAN3-0188.0-M78, Section 6.7)
4. Post flexural tests (ASTM D 3043-72, Section 7)
5. Concentrated load tests on panels (ASTM E661)

In addition specific gravity and moisture content values were obtained. The number of individual tests was limited by the time available. Therefore values obtained for the various mechanical properties are not necessarily definitive values.

2. TEST PROGRAM

The following is an outline of the test procedures and equipment employed in various tests to determine mechanical properties of waferboard and plywood. Some of the test procedures used in this pilot program could be modified to increase the efficiency in testing large numbers of specimens.

2.1 Small Scale Tests

Specimens for the small scale tests were taken from ten 1200 mm x 2400 mm (4' x 8') sheets of 11.1 mm (7/16") waferboard and ten 1200 mm x 2400 mm sheets of 9.5 mm (3/8") unsanded spruce plywood. Each sheet was divided laterally into three parts, and equal numbers of samples for various tests were cut from each part.

The 880 kN capacity Baldwin universal testing machine located in the Civil Engineering building was used in all the small scale load tests.

2.1.1 Small Scale Flexural Tests

The procedure described in Section 6.6 of CSA Standard CAN3-0188.0-M78 was used for the small scale flexural tests.

2.1.1.1 Selection of Specimens

Four flexure specimens were cut from each of the three parts, for a total of twelve specimens per panel. Of the four per part, two were cut parallel and two were cut

perpendicular to the longitudinal axis of the panel. Of these, one half were tested with the trademark on the tension side and one half were tested with the trademark on the compression side.

2.1.1.2 Preparation of Specimens

- (i) The specimens were cut to a width of 75 mm and a length of 300 mm.
- (ii) The specimens were labelled.
- (iii) The thickness was measured at three points across the midspan of the specimen. Three width measurements were also taken, one at either end and one at the centre of the specimen. The average values for the width and thickness were used in calculations of modulus of rupture (M.O.R.) and modulus of elasticity (M.O.E.). All measurements were taken with calipers having an accuracy of ± 0.01 mm.

2.1.1.3 Equipment

The supports and centre loading block used in the test conformed to Figure 1 of Section 6.6 in CAN3-0188.0-M78. Load was applied by the Baldwin universal testing machine and load versus deflection curves were directly plotted by means of an x-y plotter.

2.1.1.4 Test Procedure

- (i) The span of the support frame was set to $24t$ where t is the nominal specimen thickness in mm.

- (ii) The specimen was placed on the support frame such that load was applied at mid-span. See Figure 1 on page 19.
- (iii) The linear variable differential transducer (LVDT), which activated the x axis movement (displacement) of the x-y plotter, was placed under the specimen at mid-span as shown in Plate 1 on page 22. The y axis movement (load) was activated by the Baldwin machine.
- (iv) The Baldwin machine was set to the low load range. Load was applied at a rate of 0.48 t mm/min.
- (v) The specimen was loaded to failure and the value of the ultimate load was read from the machine scale and recorded.

2.1.1.5 Results

The results of the small scale flexure tests are recorded in Tables 1.1, 1.2 and 1.3 on pages 34 and 35. See Appendix C for the method of calculation.

2.1.2 Compression Tests

For the small scale compression tests, the procedure followed was that described in the following report:
Longworth, J.: "Moisture-Strength Relations for Sheathing Grade Douglas Fir Plywood." Department of Civil Engineering, The University of Alberta, 1974.

2.1.2.1 Selection of Specimens

Two compression specimens were cut from each of the three parts of each panel, for a total of six compression specimens per panel. Of the two samples per part, one was cut parallel and one was cut perpendicular to the longitudinal axis of the panel.

2.1.2.2 Preparation of Specimens

- (i) The specimens were cut to a width of 190.5 mm (7.5") and a length of 381 mm (15").
- (ii) The specimens were labelled.
- (iii) a) Prior to testing the waferboard specimens, six thickness measurements were taken, one at each corner, and two at midspan of the specimen. Calipers with an accuracy of ± 0.01 mm were used for these measurements. The average of these values was used in calculations.
Two length and width measurements were taken, to an accuracy of ± 0.5 mm using a steel scale. The averages were used in calculations.
- (b) Prior to testing the plywood specimens, all of the measurements taken for waferboard were taken, and in addition, measurements of parallel ply thickness were taken. For specimens cut parallel

to the longitudinal axis of the panel, the thickness of the two outer plies was measured at each of the four corners. The average was used in calculations. For specimens cut perpendicular to the longitudinal axis of the panel, the thickness of the inside ply was measured at each of the four corners and the average value was used in calculations. All thickness measurements were taken to ± 0.01 mm with calipers.

2.1.2.3 Equipment

The frame described in the above mentioned report was used for supporting the specimens. The load was applied by the Baldwin machine and load versus deflection curves were plotted directly on an x-y plotter.

2.1.2.4 Test Procedure

- (i) The loading frame was positioned under the loading head.
- (ii) The specimen was placed in the loading frame and the edge supports and third-point rollers were tightened. Care was taken to avoid overtightening as this would affect the failure location. See Figure 2 on page 19.

- (iii) The loading head of the frame was checked to ensure that it did not bind on the edge supports of the frame.
- (iv) The LVDT, attached to the x-y plotter, was positioned such that it measured the vertical movement of the loading head as shown in Plate 2 on page 22.
- (v) The Baldwin machine was set to the medium load range. Load was applied at a constant strain rate of 1.14 mm/min. (0.045 in./min.).
- (vi) The specimen was loaded to failure and the value of the ultimate load was read from the machine scale and recorded.

2.1.2.5 Results

Tables 2.1, 2.2 and 2.3 on pages 36 and 37 list the results of the small scale compression tests. See Appendix C for method of calculation.

2.1.3 Bond Tests

Small scale bond tests were conducted in accordance with Section 6.7 of CSA Standard CAN3-0188.0-M78. Although this is not the standard procedure for testing plywood in bond, the plywood specimens were tested in the same manner as the waferboard specimens to provide a basis for comparison of results.

2.1.3.1 Selection of Specimens

Two bond specimens were cut from each of the three parts of each panel, resulting in a total of six specimens per panel.

2.1.3.2 Preparation of Specimens

- (i) The specimens were cut to 50 mm x 50 mm (± 0.2 mm).
- (ii) The specimens were labelled.
- (iii) The length of each of the four sides was measured to ± 0.01 mm using calipers.
- (iv) The specimens were glued to the aluminum loading blocks with Sikadur Gel, a two component epoxy-resin. Although a three day curing period is recommended, the ten hour strength proved to be sufficient.

2.1.3.3 Equipment

Loading blocks and rod attachments as illustrated in Figure 2 of Section 6.7 of CSA Standard CAN3-0188.0-M78 were used. Specimens were tested in the Baldwin machine. See Figure 3 on page 20.

2.1.3.4 Test Procedure

- (i) The assembly, consisting of the specimens, loading blocks, and attachment rods, was placed in the testing machine as shown in Plate 3 on page 23.
- (ii) The Baldwin machine was set to the low load range. Load was applied at a rate of 0.08 t mm/min.

- (iii) The specimen was loaded to failure and the value of the ultimate load was read from the machine scale and recorded. A qualitative description of the failure was also recorded.

2.1.3.5 Results

The results of the bond tests are given in Tables 3.1, 3.2 and 3.3 on pages 38 and 39. See Appendix C for method of calculation.

2.1.4 Specific Gravity and Moisture Content Tests

The specific gravity and moisture content tests conformed with Section 6.5 of CSA Standard CAN3-0188.0-M78.

2.1.4.1 Selection of Samples

Specific gravity and moisture content samples were cut from every fourth failed flexure test specimen, thus three samples were taken from each panel.

2.1.4.2 Preparation of Samples and Test Procedure

- (i) The samples were cut to approximately 75 mm x 75 mm.
- (ii) The length of each of the four sides, and two thickness measurements were taken using calipers with an accuracy of ± 0.01 mm.
- (iii) The samples were weighed.
- (iv) The samples were placed in an oven at 105°C for 24 hours.
- (v) The samples were weighed again.

2.1.4.3 Results

The results of the specific gravity and moisture content tests are tabulated in Tables 4.1, 4.2 and 4.3 on pages 39 and 40. See Appendix C for method of calculation.

2.2 Large Scale Tests

2.2.1 Post Flexure Tests

The large scale post flexure tests were performed in the laboratory of the Council of Forest Industries in Vancouver in accordance with test method C of Section 7 of ASTM D 3043-72.

2.2.1.1 Selection of Specimens

Twenty panels each of waferboard and plywood were tested. Each panel was cut in two, resulting in forty waferboard specimens and forty plywood specimens. For each panel, one half was tested parallel, and the other half was tested perpendicular to the longitudinal axis of the panel. Also, half of the specimens were tested with the trademark on the tension side and half were tested with the trademark on the compression side.

2.2.1.2 Preparation of Specimens

- (i) The full size panels were cut into square halves and trimmed to metric dimensions (1200 mm x 1200 mm).
- (ii) The longitudinal direction was marked on each half, with one half labelled to be

tested parallel, and the other half labelled to be tested perpendicular to this mark.

- (iii) For the plywood specimens, the thickness of each ply was measured, and for the waferboard specimens, the overall thickness was measured. Because the laboratory saw cut produced a sharper edge than the factory saw cut, the thickness measurements were taken along an edge that had been sawn in the laboratory and at the intersection of the central axis about which bending was applied.

2.2.1.3 Equipment

The testing equipment conformed to ASTM D 3043-72, and was designed for the specific purpose of testing large scale plywood specimens in pure flexure. See Figure 4 on page 20. A LVDT was placed at the centre of each sample and load versus deflection curves were plotted directly by an x-y plotter.

2.2.1.4 Test Procedure

- (i) The specimen was placed between the loading bars of the test machine as shown in Plate 4 on page 24.
- (ii) The frame holding the LVDT in place was attached at the centre of the specimen and the LVDT was secured in the frame as shown

in Plate 5 on page 24. The LVDT measured deflection over a span of 406 mm (16").

- (iii) The load was applied.
- (iv) To avoid damage, the LVDT and frame were removed from the specimen before failure.
- (v) The specimen was loaded to failure and the ultimate load and time required to fail the specimen were recorded.

2.2.1.5 Results

Results of these tests are recorded in Tables 5.1, 5.2 and 5.3 on pages 41 and 42. See Appendix C for method of calculation.

2.2.2 Specific Gravity and Moisture Content Tests

The moisture content tests conformed to Section 8.1 of ASTM D3043. The specific gravity tests conformed to Section 8.2.2 of ASTM D2395.

2.2.2.1 Selection of Samples

After flexural testing, a specific gravity and moisture content sample was taken from each of the failed specimens.

2.2.2.2 Preparation of Samples and Test Procedure

- (i) The samples were cut to 100 mm x 100 mm.
- (ii) The samples were weighed.
- (iii) The samples were oven dried at $103^{\circ}\text{C} \pm 2^{\circ}\text{C}$ until weight was constant within $\pm 2\%$.
- (iv) The samples were weighed again and the moisture content calculated.

- (v) The samples were immersed in paraffin to seal the pores in accordance with Section 8.2.5 of ASTM D2395.
- (vi) The weight of a container of water was measured.
- (vii) The sample was submerged in the water by holding it down with a sharp, slender rod.
- (viii) The container with the water and sample was weighed again, and the additional weight was recorded as the weight of water displaced. This was used to determine the volume of the specimen on the basis of which the specific gravity was calculated.

2.2.2.3 Results

The results of these tests are recorded in Tables 6.1, 6.2 and 6.3 on pages 44 and 45. See Appendix C for method of calculation.

2.2.3 Concentrated Load Tests

The concentrated load tests were performed in accordance with ASTM E661. The purpose of these tests was to simulate conditions of actual use.

2.2.3.1 Selection of Specimens

For the concentrated load tests, ten sheets of waferboard and six sheets of plywood were tested. Eight tests were performed per panel. Of these, four were performed along a free edge and are classified as

unsupported, and four were performed along an edge supported by an aluminum H-clip and are classified as partially supported. Half of the tests were located in one of the centre spans and are referred to as interior tests, and half of the tests were located in one of the edge spans and are referred to as exterior tests. See Figure 5 on page 24.

2.2.3.2 Preparation of Specimens

- (i) Each full-size panel was weighed.
- (ii) The panels were cut in half longitudinally.
- (iii) The specimens were labelled.
- (iv) The thickness of each specimen was measured at the midpoint of one of the longitudinal edges.

2.2.3.3 Equipment

A steel loading frame made up of hollow structural steel (H.S.S.) sections, channels, and angles was used to support five 38 mm x 184 mm (2" x 8") joists spaced at 600 mm (24") on centre as shown in Plate 6 on page 25. Wood wedges were wedged between the joists and the vertical legs of the angles to prevent lateral movement of the joists. The H-clips used were 9.5 mm (3/8") in depth for the plywood panels and 11.1 mm (7/16") in depth for the waferboard specimens. The manufacturer of the H-clips is Plateau Manufacturing of Calgary.

A hand operated pump was used to apply the load through an 90 kN jack, to which was attached a 76.2 mm (3") diameter loading disk. A 18 kN capacity load cell was used to

measure the load, and a dial gage was used to measure the deflection. The deflection dial gage was mounted on a tripod seated over the framing members adjacent to the load as shown in Plate 8 on page 26. Thus deflection of the load point was measured relative to the joist. Both load and deflection readings were recorded manually.

2.2.3.4 Test Procedure

- (i) The two halves of one panel were placed on the joists with the longitudinal direction of the panel perpendicular to the joists.
- (ii) One half of the panel was nailed to the joists using 57 mm (2 1/4"), double headed nails. The nail spacing used on the two outer joists was 152.4 mm (6"). On the three inner joists, 304.8 mm (12") spacing was used. The end distance was equal to one-half the nail spacing.
- (iii) H-clips were placed between the two halves at midspans.
- (iv) The second half panel was positioned with a 2 mm gap relative to the first half and then nailed to the joists as shown in Plate 7 on page 25.
- (v) The load points were marked on the panels.
- (vi) The cross beam was lined up with the test locations and clamped in place.

- (vii) The jack was positioned directly over a test location and a small preload was applied to hold the jack in place.
- (viii) The support tripod was positioned along the adjacent joist and the deflection gage was set in place.
- (ix) Initial load and deflection readings were taken.
- (x) Load was then applied and deflection readings were taken at 222.4 N (50 lb.) increments from 222.4 N to 889.6 N (200 lb.).
- (xi) The load was removed and the deflection gage was removed to avoid damage.
- (xii) The load was reapplied to failure as shown in Plate 9 on page 26 and the ultimate load was recorded. The mode of failure and failure load for the H-clips was also recorded.
- (xiii) After the load had been applied to all test locations for the panel, the panel was removed and replaced with a new test panel. This panel was placed 13 mm (1/2") further along the joists than the previous one to assure nails would clear the previous nail holes. When the full length of the joists was used up, the joists were

turned over and further tests were
conducted.

2.2.3.5 Results

The results of the concentrated load tests are recorded in Tables 7.1, 7.2 and 7.3 on pages 46 and 47. See Appendix C for method of calculation.

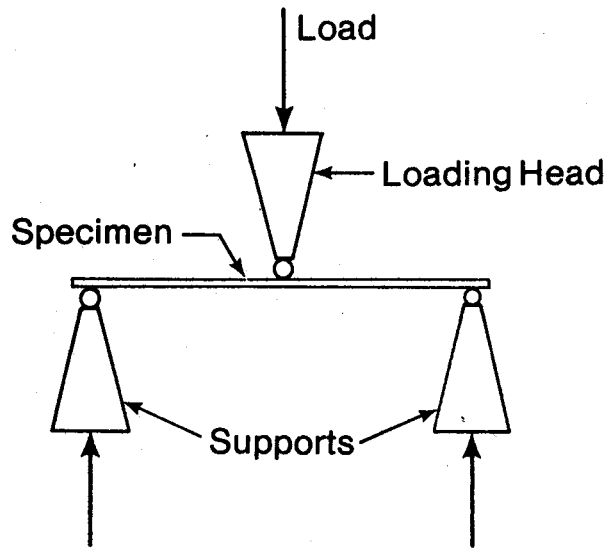


Figure 1. Schematic Diagram of Small Scale Flexure Test Apparatus

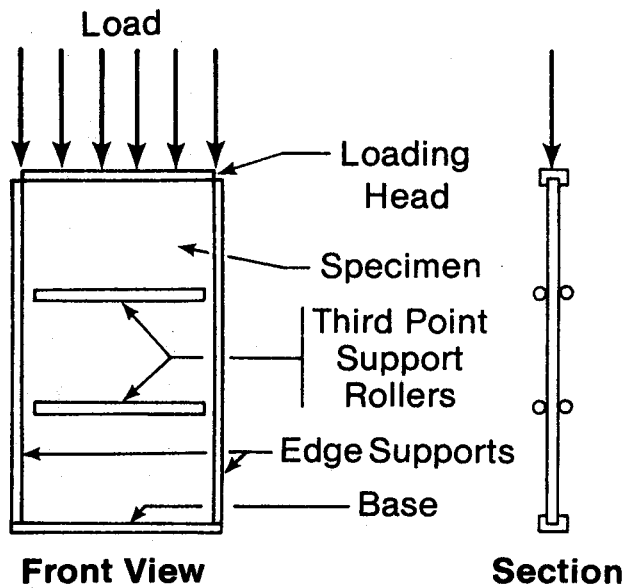


Figure 2. Schematic Diagram of Small Scale Compression Test Apparatus

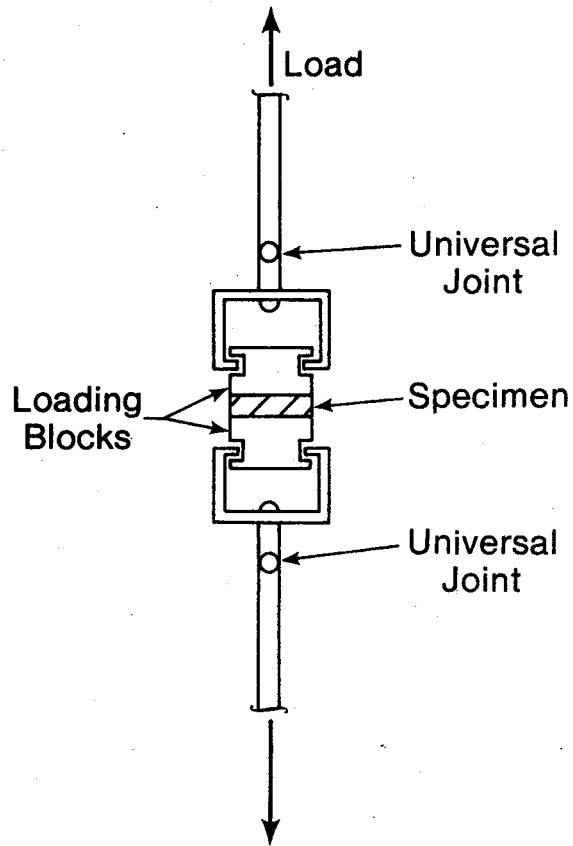


Figure 3. Schematic Diagram of Bond Test Apparatus

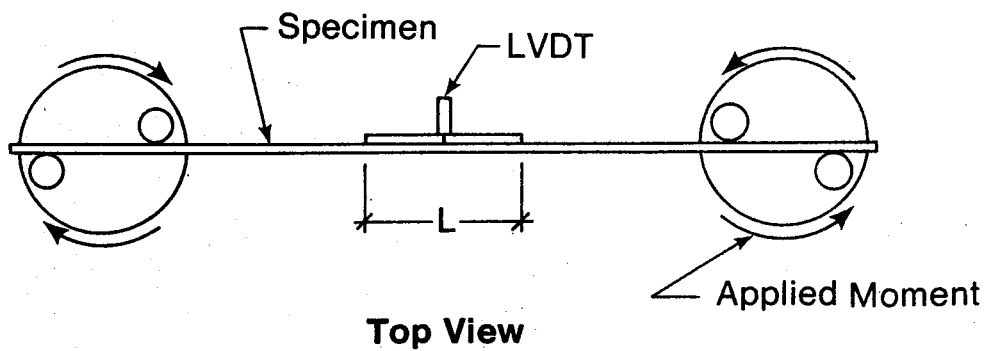


Figure 4. Schematic Diagram of Large Scale Post Flexure Test Apparatus

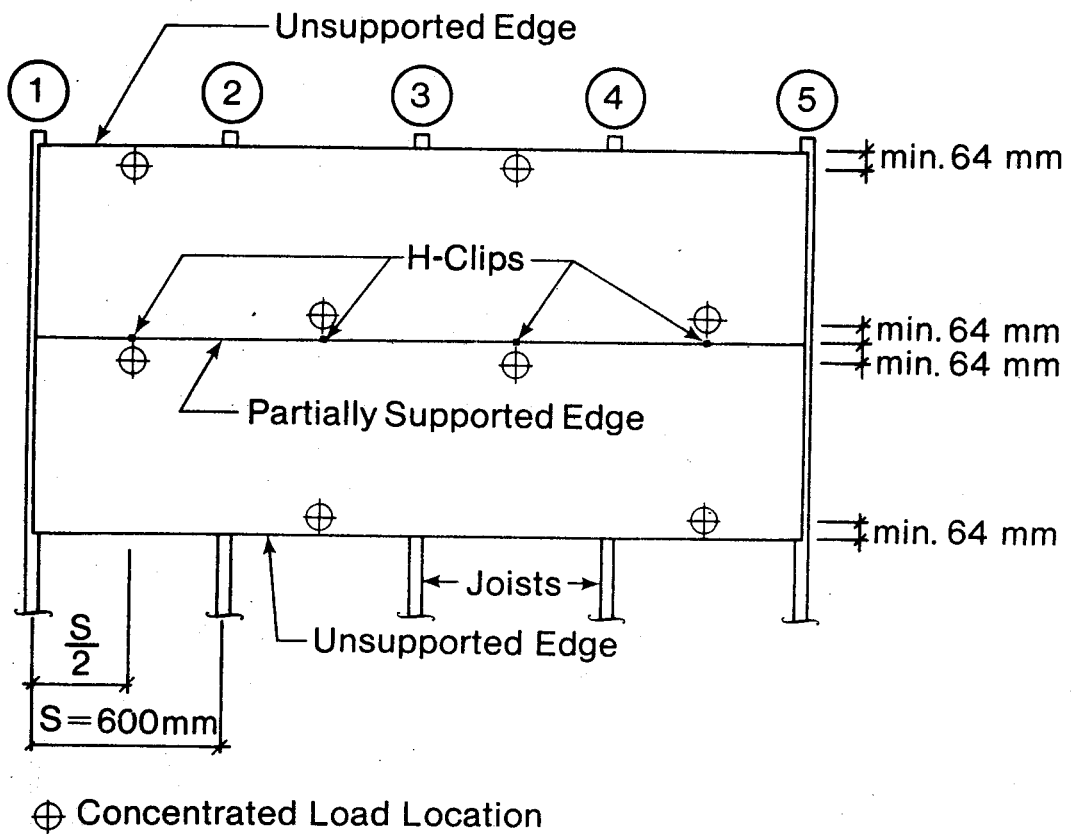


Figure 5. Location of Concentrated Load Tests

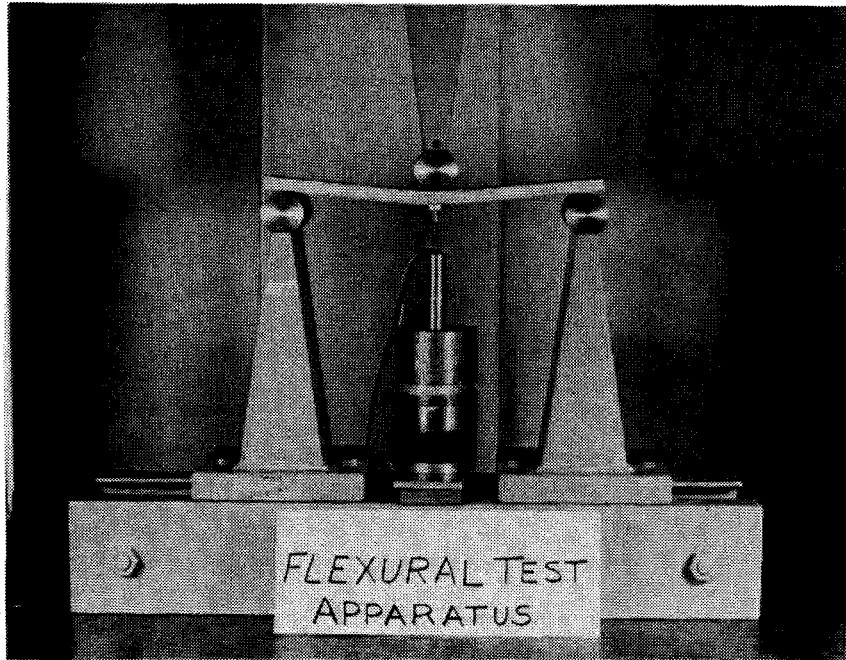


Plate 1. Flexural Test apparatus

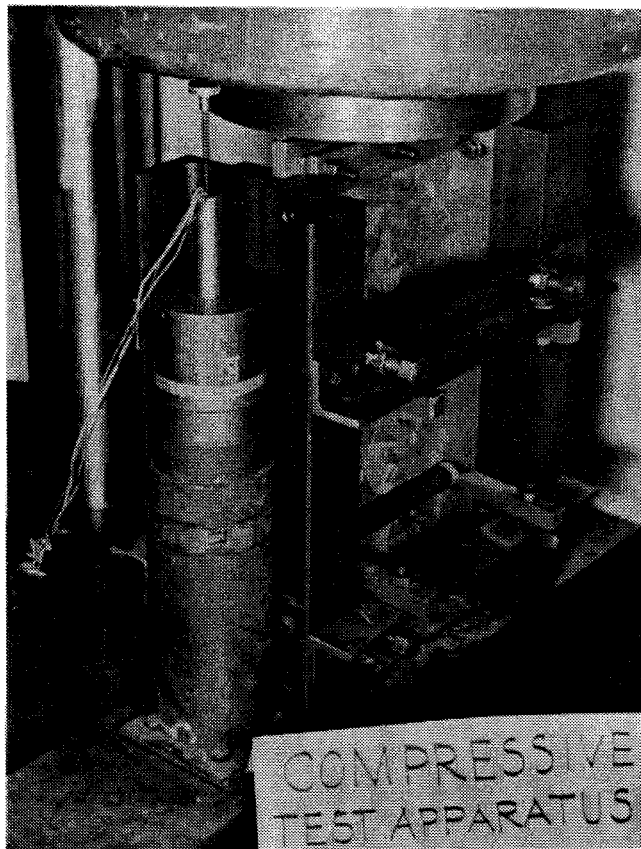


Plate 2. Compressive Test Apparatus

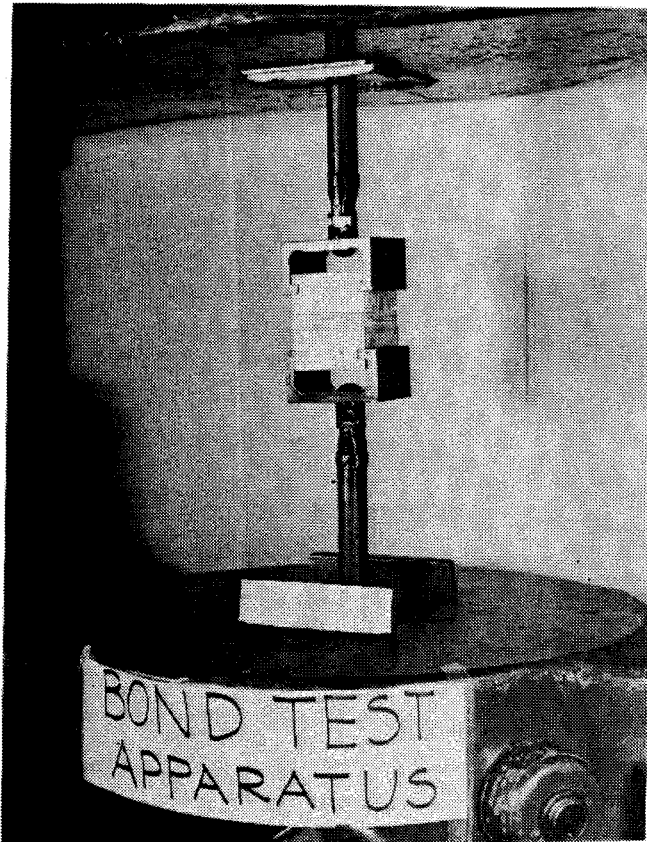


Plate 3. Bond Test Apparatus

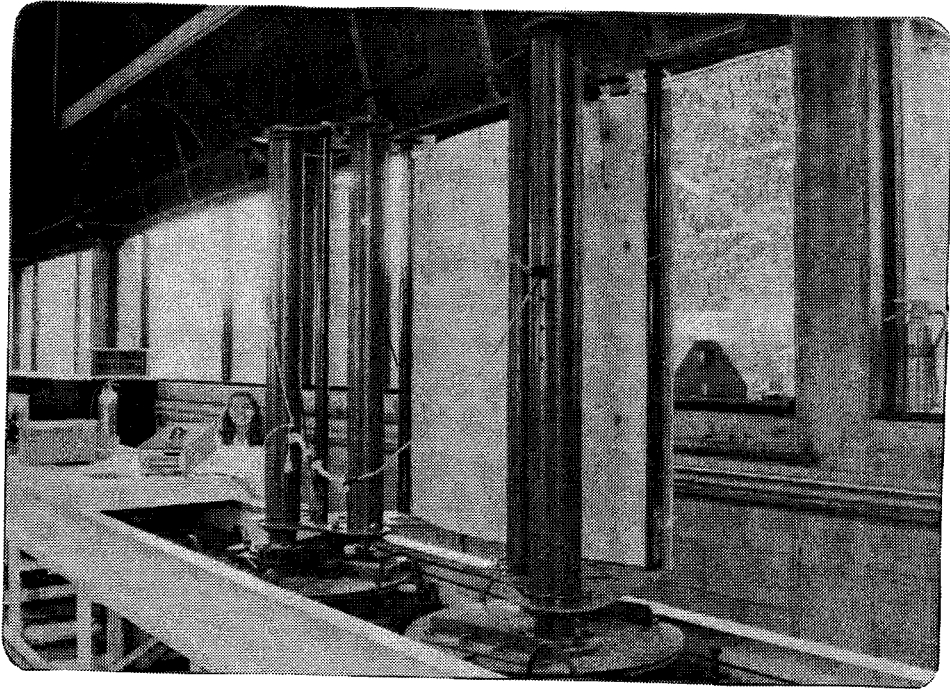


Plate 4. Large Scale Flexural Test

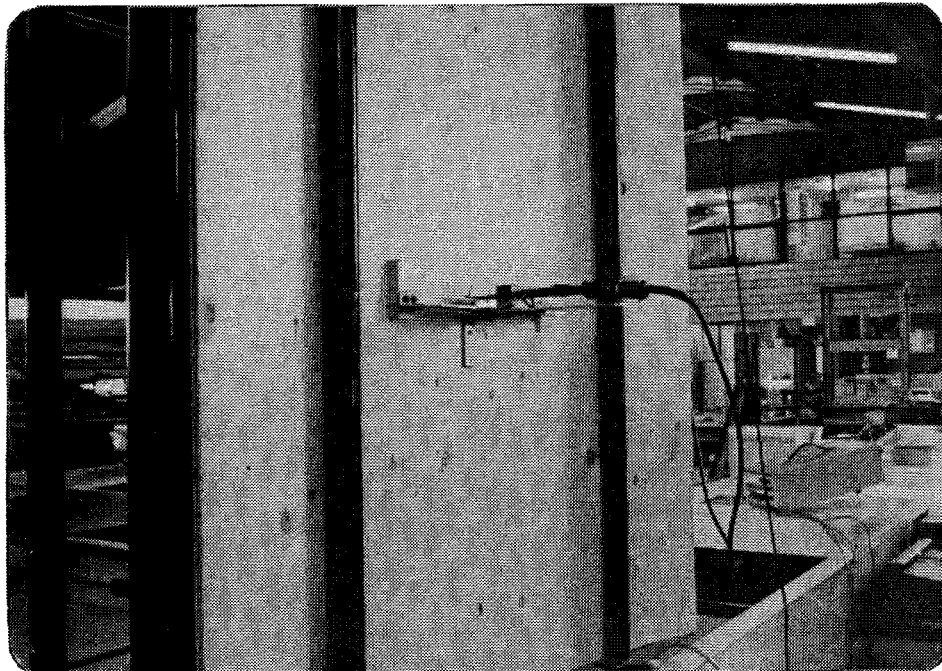


Plate 5. LVDT used in the Large Scale Flexure Tests

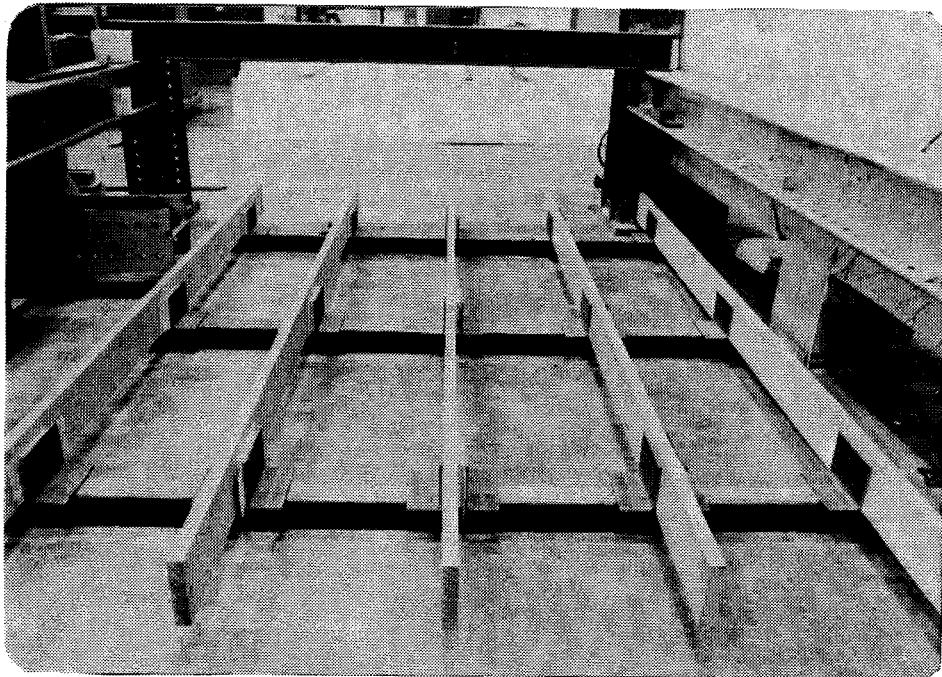


Plate 6. Steel Frame and Wood Joists used for the Concentrated Load Tests

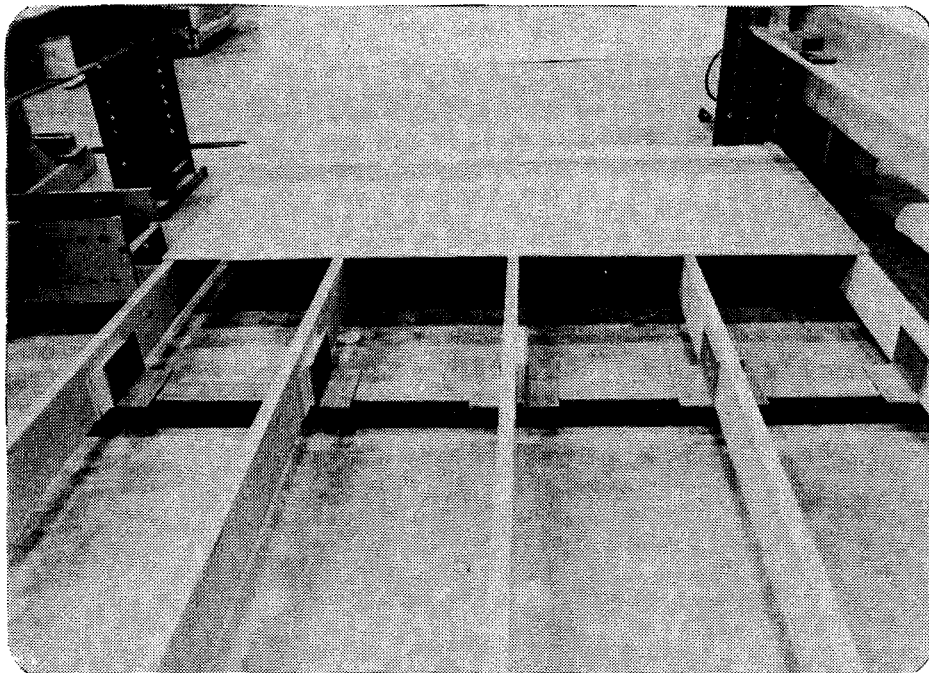


Plate 7. Concentrated Load Test Panel nailed in place on the joists.

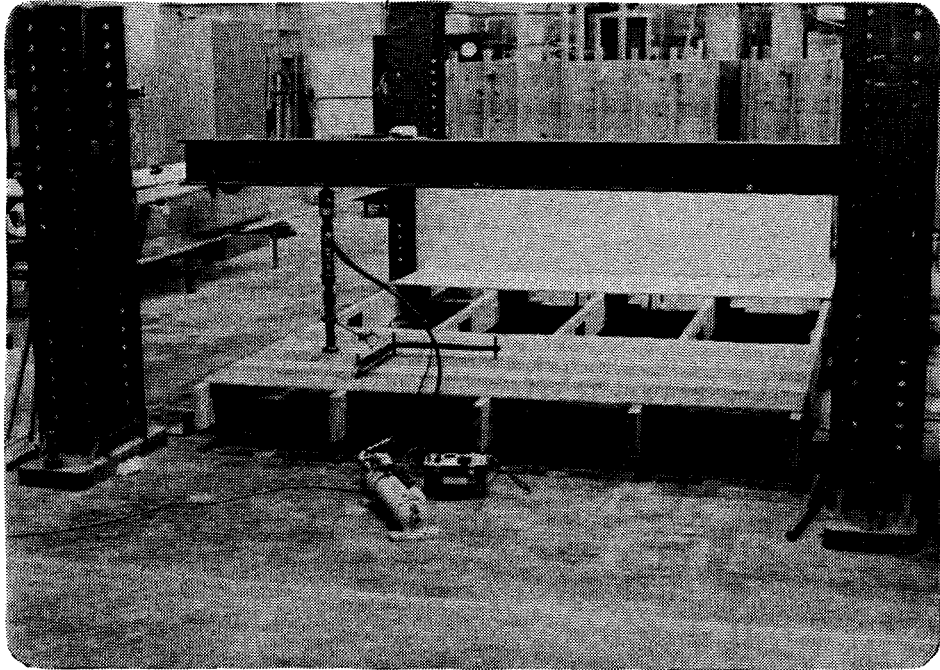


Plate 8. Concentrated Load Test Apparatus

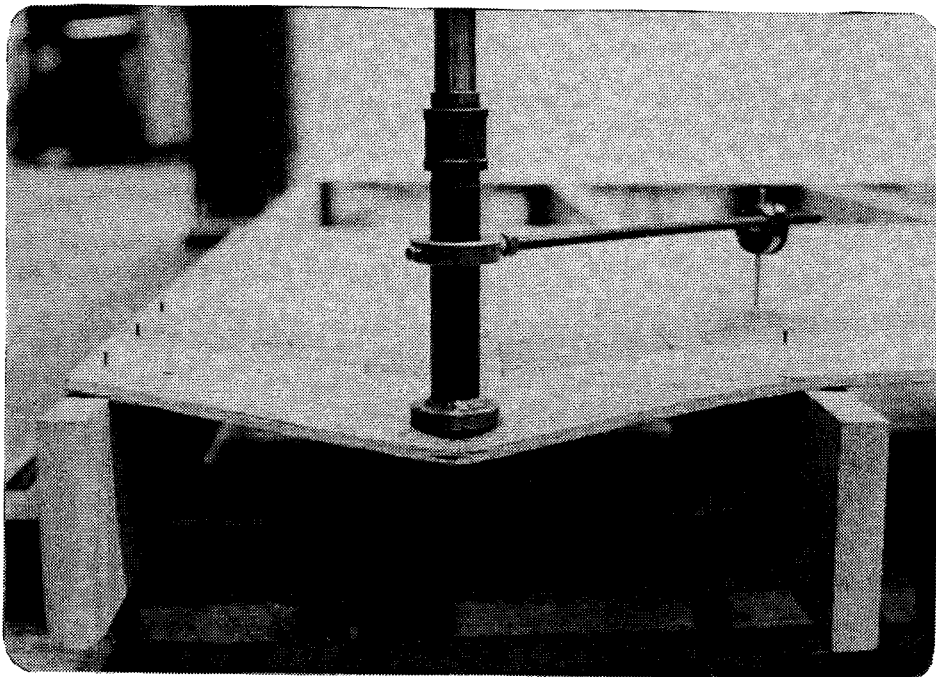


Plate 9. Concentrated Load Test Failure for Waferboard

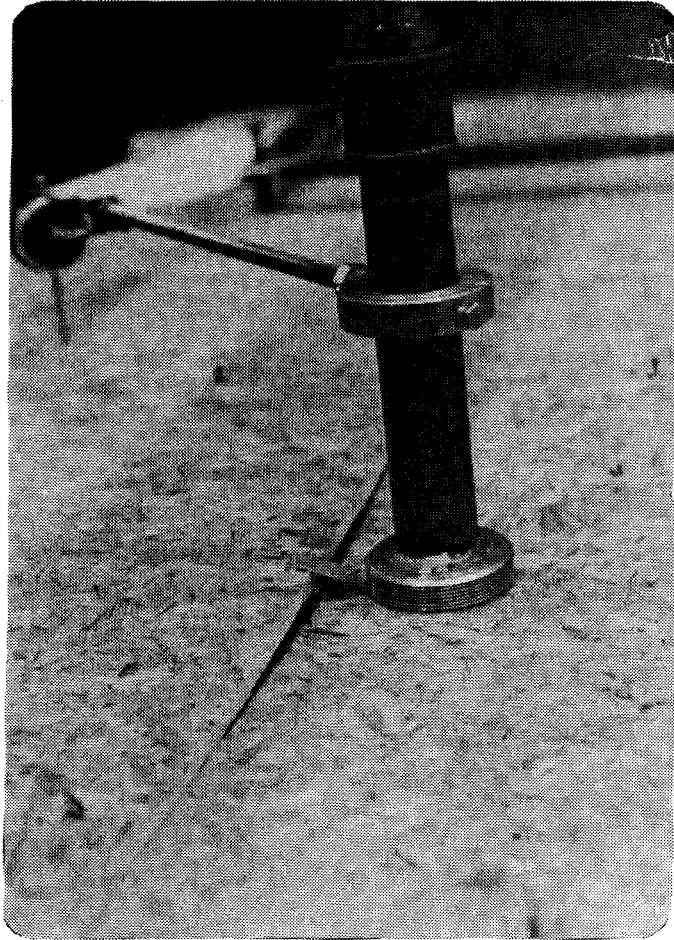


Plate 10. Concentrated Load Test. H-clip Shear Failure

3. DISCUSSION OF RESULTS

This section includes tables summarizing the results of all tests and tables comparing results of plywood and waferboard tests.

3.1 Small Scale Tests

3.1.1 Small Scale Flexural Tests

The Baldwin testing machine was not sensitive enough to measure very small loads. As a result, no tests were performed on plywood specimens cut perpendicular to the longitudinal panel axis.

For plywood, there was little difference in test results between specimens tested with the trademark side in tension and those tested with the trademark side in compression.

For waferboard, there was no significant difference in properties between specimens tested parallel and those tested perpendicular to the longitudinal axis of the panel, or between specimens tested with the trademark on the compression side and those tested with the trademark on the tension side.

3.1.2 Compression Tests

For the plywood, the values for ultimate compressive stress and modulus of elasticity, based on gross area, were

significantly greater for the specimens cut parallel to the longitudinal axis of the panel than for those cut perpendicular to the longitudinal axis of the panel. The results for the waferboard specimens indicate no significant change in properties with direction. As a result, for specimens tested parallel, the stress and modulus of elasticity were greater for plywood, and for specimens tested perpendicular, the stress and modulus of elasticity were greater for waferboard.

3.1.3 Bond Tests

In all bond tests the percentage wood failure was estimated. Failures ranged from 100% wood failure to 100% glue failure. For the plywood specimens it was estimated that, on average there was approximately 40% wood failure. For the waferboard specimens, it was estimated that, on average there was approximately 30% wood failure.

3.2 Large Scale Tests

3.2.1 Large Scale Flexural Tests

The stiffness, modulus of elasticity, ultimate moment, and modulus of rupture for plywood specimens tested parallel to the longitudinal panel axis were significantly higher than for plywood specimens tested perpendicular to the longitudinal panel axis. For the waferboard, there was no significant change in properties with direction. As a

result, the values for specimens tested parallel to the longitudinal panel axis were higher for plywood, and the values for specimens tested perpendicular to the longitudinal panel axis were higher for waferboard. For both plywood and waferboard, there was no significant change in properties between panels tested with the trademark side in tension and panels tested with the trademark side in compression.

3.2.2 Concentrated Load Tests

The ultimate load and the deflection at an 890 N (200 lb.) load were greater for plywood than for waferboard for all test locations.

For plywood, the ultimate load was greater and the deflection was less for interior load locations and at locations partially supported with H-clips than for exterior or unsupported load locations.

For waferboard, the same was true for interior load locations compared to exterior load locations. For partially supported load locations, the ultimate load and deflection were both less than for unsupported load locations.

The 11.1 mm (7/16") aluminum H-clips fitted very tightly on the waferboard specimens and 80% of them failed in shear as shown in Plate 10 on page 27. The 9.5 mm (3/8") aluminum H-clips fitted loosely on the plywood specimens and all of them failed by sliding out as the panel deflected at

the point of the load application. For the waferboard, the slight impact load due to the shear failure of the H-clips may have resulted in the decrease in ultimate load for partially supported as compared with unsupported load locations.

The waferboard results showed no significant increase in ultimate load for interior or continuous span test locations as compared with exterior or non-continuous span test locations. This may be due to the localized nature of the failure in waferboard which does not allow effective distribution of stresses to adjacent spans. At failure, the wood flakes appeared to slide over one another at the location of the load as shown in Plate 9 on page 26.

Key to Tables

The following is an explanation of the terms and symbols used in the tables.

- number of specimens or samples tested

Parallel (//) - refers to specimens cut parallel to the longitudinal axis of the panel

Perpendicular (⊥) - refers to specimens cut perpendicular to the longitudinal axis of the panel

Up (U) - refers to specimens tested with the trademark on the tension side

Down (D) - refers to specimens tested with the trademark on the compression side

Supported - load location with H-clips

Unsupported - load location without H-clips

Interior - load location with a continuous span on both sides

Exterior - load location with a continuous span on one side only

Metric Unit Conversion Factors

1 mm = 0.0393701 inch

1 m = 3.28084 ft.

1 N = 0.224809 lbf

1 kN = 224.809 lbf

1 N·m = 0.737562 lbf·ft.

1 N·m² = 2.41982 lbf·ft.²

1 kPa = 0.145038 psi

1 MPa = 145.038 psi

1 GPa = 145038 psi

Small Scale Flexural Test Results

Table 1.1 9.5 mm (3/8") Plywood

Moisture Content = 7.0% (see Table 4.1)

Property Type of Test	#	MOE (GPa)		MOR (MPa)	
		Average	5% Exclusion Limit	Average	5% Exclusion Limit
All Parallel	60	7.56	5.79	58.4	36.8
Parallel & Up	30	7.50	5.56	59.2	37.5
Parallel & Down	30	7.62	6.00	57.7	35.8

Table 1.2 11.1 mm (7/16") Waferboard

Moisture Content = 4.9% (See Table 4.2)

Property Type of Test	#	MOE (GPa)		MOR (MPa)	
		Average	5% Exclusion Limit	Average	5% Exclusion Limit
All Parallel	55	3.61	2.48	19.3	12.3
Parallel & Up	27	3.68	2.45	18.9	11.4
Parallel & Down	28	3.53	2.50	19.7	28.9

Note: All values are calculated on the basis of gross cross-sectional area.

Small Scale Flexural Test Ratios

Table 1.3 Ratio Comparison of Results

9.5 mm (3/8") Plywood versus 11.1 mm (7/16") Waferboard

Property	MOE Ratio		MOR Ratio	
	Average	5% Exclusion Limit	Average	5% Exclusion Limit
<u>Plywood</u> <u>Waferboard</u>	2.10	2.35	3.09	3.01
<u>// Plywood</u> <u>// Waferboard</u>	2.09	2.33	3.02	2.99
<u>1 Plywood</u> <u>1 Waferboard</u>	< 1	< 1	< 1	< 1
PLYWOOD				
<u>// U Plywood</u> <u>// D Plywood</u>	0.98	0.93	1.03	1.05
WAFERBOARD				
<u>// Waferboard</u> <u>1 Waferboard</u>	1.01	1.01	1.05	1.00
<u>// U Waferboard</u> <u>// D Waferboard</u>	1.04	0.98	0.96	0.87
<u>1 U Waferboard</u> <u>1 D Waferboard</u>	1.04	1.07	1.02	0.92

Note: All values are calculated on the basis of gross cross-sectional area.

Small Scale Compression Test Results

Table 2.1 9.5 mm (3/8") Plywood
Moisture Content = 7.0% (see Table 4.1)

Property	#	Ultimate Load (kN)	Ultimate Compressive Stress (MPa)	MOE (GPa)			
Type of Test		5% Average	5% Exclusion Limit	5% Average			
				5% Exclusion Limit			
All Parallel	30	42.0	35.2	23.4	19.8	4.31	3.78
All Perpendicular	30	20.8	16.7	11.6	9.38	1.85	1.38

Table 2.2 11.1 mm (7/16") Waferboard
Moisture Content = 4.9% (See Table 4.2)

Property	#	Ultimate Load (kN)	Ultimate Compressive Stress (MPa)	MOE (GPa)			
Type of Test		5% Average	5% Exclusion Limit	5% Average			
				5% Exclusion Limit			
All Parallel	30	27.9	23.1	12.9	10.7	2.57	2.13
All Perpendicular	29	28.1	22.8	13.1	10.6	2.50	2.17

Note: All values are calculated on the basis of gross cross-sectional area.

Small Scale Compression Test Ratios

Table 2.3 Ratio Comparison of Results

9.5 mm (3/8") Plywood versus 11.1 mm (7/16") Waferboard

Property	Ultimate Load Ratio		Ultimate Compressive Stress Ratio		MOE Ratio	
	Average	5% Exclusion Limit	Average	5% Exclusion Limit	Average	5% Exclusion Limit
<u>// Plywood</u> <u>// Waferboard</u>	1.51	1.53	1.82	1.84	1.67	1.78
<u>⊥ Plywood</u> <u>⊥ Waferboard</u>	0.74	0.73	0.89	0.89	0.74	0.64
PLYWOOD						
<u>// Plywood</u> <u>⊥ Plywood</u>	2.02	2.11	2.01	2.11	2.33	2.74
WAFERBOARD						
<u>// Waferboard</u> <u>⊥ Waferboard</u>	0.99	1.01	0.98	0.98	1.03	1.02

Note: All values are calculated on the basis of gross cross-sectional area.

Bond Test Results

Table 3.1 9.5 mm (3/8") Plywood
Moisture Content = 7.0% (See Table 4.1)

Property Type of Test	#	Ultimate Load (N)		Stress (kPa)	
		Average	5% Exclusion Limit	Average	5% Exclusion Limit
Overall Results	57	2220	625	881	248
Panel #1	6	3140	2040	1250	812
Panel #2	5	2570	1180	1020	470
Panel #3	6	1550	10	617	2.8
Panel #4	5	2010	1170	797	464
Panel #5	6	2080	616	823	244
Panel #6	6	2310	1240	916	492
Panel #7	5	1930	877	766	348
Panel #8	6	1830	907	725	359
Panel #9	6	2800	1670	1110	664
Panel #10	6	1970	658	780	263

Table 3.2 11.1 mm (7/16") Waferboard
Moisture Content = 4.9% (See Table 4.2)

Property Type of Test	#	Ultimate Load (N)		Stress (kPa)	
		Average	5% Exclusion Limit	Average	5% Exclusion Limit
Overall Results	58	1250	813	496	290
Panel #1	6	1140	889	452	352
Panel #2	5	1450	1120	571	437
Panel #3	6	1240	524	493	208
Panel #4	6	1160	870	461	345
Panel #5	6	1220	953	482	378
Panel #6	6	1360	1250	539	495
Panel #7	6	1220	964	481	382
Panel #8	6	1260	1060	497	418
Panel #9	5	1260	1040	499	403
Panel #10	6	1260	826	499	327

Bond Test Ratios

Table 3.3 Ratio Comparison of Results

9.5 mm (3/8") Plywood versus 11.1 mm (7/16") Waferboard

Property	Stress Ratio	
	Average	5% Exclusion Limit
<u>Plywood</u> <u>Waferboard</u>	1.78	0.86

Specific Gravity and Moisture Content (Edmonton)

Table 4.3 Ratio Comparison of Results

9.5 mm (3/8") Plywood versus 11.1 mm (7/16") Waferboard

Property	Specific Gravity Ratio		Moisture Content Ratio	
	Average	5% Exclusion Limit	Average	5% Exclusion Limit
<u>Plywood</u> <u>Waferboard</u>	0.65	0.66	1.43	1.40

Specific Gravity and Moisture Content Test Results (Edmonton)

Table 4.1 9.5 mm (3/8") Plywood

Property Type of Test	#	Specific Gravity		Moisture Content (%)	
		Average	5% Exclusion Limit	Average	5% Exclusion Limit
Overall Results	30	.411	.381	7.0	6.6
Panel #1	3	.420	.378	7.3	7.1
Panel #2	3	.392	.339	7.3	6.8
Panel #3	3	.418	.397	7.1	6.6
Panel #4	3	.402	.378	7.1	7.0
Panel #5	3	.419	.406	7.1	6.7
Panel #6	3	.395	.371	6.8	6.5
Panel #7	3	.408	.373	6.9	6.5
Panel #8	3	.408	.396	6.9	6.4
Panel #9	3	.424	.403	6.9	6.8
Panel #10	3	.420	.412	6.8	6.6

Table 4.2 11.1 mm (7/16") Waferboard

Property Type of Test	#	Specific Gravity		Moisture Content (%)	
		Average	5% Exclusion Limit	Average	5% Exclusion Limit
Overall Results	30	.633	.574	4.9	4.7
Panel #1	3	.625	.612	5.0	4.8
Panel #2	3	.630	.581	4.9	4.8
Panel #3	3	.598	.508	4.8	4.6
Panel #4	3	.634	.597	4.9	4.7
Panel #5	3	.628	.587	4.9	4.8
Panel #6	3	.635	.610	4.8	4.4
Panel #7	3	.658	.528	4.9	4.8
Panel #8	3	.658	.581	4.8	4.7
Panel #9	3	.618	.588	4.8	4.7
Panel #10	3	.648	.633	4.8	4.7

Post Flexure Test Results

Table 5.1 9.5 mm (3/8") Plywood

Moisture Content = 7.5% (See Table 6.1)

Property	#	EI (N·m ²)		MOE (GPa)		M.Ult. (N·m)		MOR (MPa)	
		Average	5% Exclusion Limit	Average	5% Exclusion Limit	Average	5% Exclusion Limit	Average	5% Exclusion Limit
All Parallel	20	200	163	9.67	7.66	157	83.5	35.4	18.1
Parallel & Up	10	199	157	9.83	8.30	150	78.5	34.6	17.3
Parallel & Down	10	202	166	9.51	7.06	164	86.4	36.2	18.0

Table 5.2 11.1 mm (7/16") Waferboard

Moisture Content = 3.1% (See Table 6.2)

Property	#	EI (N·m ²)		MOE (GPa)		M.Ult. (N·m)		MOR (MPa)	
		Average	5% Exclusion Limit	Average	5% Exclusion Limit	Average	5% Exclusion Limit	Average	5% Exclusion Limit
All Parallel	19	154	121	4.44	3.51	99.8	86.7	16.0	14.4
Parallel & Up	10	156	116	4.44	3.41	101	89.4	16.4	14.8
Parallel & Down	9	152	127	4.45	3.56	98.6	83.4	15.7	14.0

NOTE: All values are calculated on the basis of gross cross-sectional area.

Post Flexure Test Results

Table 5.3 9.5 mm (3/8") Plywood

Moisture Content = 7.5% (See Table 6.1)

Property	#	EI (N·m ²)		MOE (GPa)		M.Ult. (N·m)		MOR (MPa)	
		Average	5% Exclusion Limit	Average	5% Exclusion Limit	Average	5% Exclusion Limit	Average	5% Exclusion Limit
All Perpendicular	20	11.3	8.2	0.56	0.37	37.4	23.2	8.59	5.10
Perpendicular & Up	10	11.5	7.6	0.57	0.34	37.7	28.8	8.66	6.19
Perpendicular & Down	10	11.0	9.0	0.55	0.39	37.1	18.6	8.53	4.09

Table 5.4 11.1 mm (7/16") Waferboard

Moisture Content = 3.1% (See Table 6.2)

Property	#	EI (N·m ²)		MOE (GPa)		M.Ult. (N·m)		MOR (MPa)	
		Average	5% Exclusion Limit	Average	5% Exclusion Limit	Average	5% Exclusion Limit	Average	5% Exclusion Limit
All Perpendicular	19	143	125	4.11	3.46	90.8	79.6	14.5	12.6
Perpendicular & Up	9	143	129	4.20	3.42	92.6	82.1	15.0	12.9
Perpendicular & Down	10	143	122	4.03	3.52	89.2	77.6	14.0	12.5

NOTE: All values are calculated on the basis of gross cross-sectional area.

Post Flexure Ratios

Table 5.5 Ratio Comparison of Results
9.5 mm (3/8") Plywood versus 11.1 mm (7/16") Waferboard

	EI Ratio		MOE Ratio		M.Ult. Ratio		MOR Ratio	
	Average	5% Exclusion Limit	Average	5% Exclusion Limit	Average	5% Exclusion Limit	Average	5% Exclusion Limit
<u>Plywood</u> <u>Waferboard</u>	0.71		1.19		1.02		1.44	
<u>// Plywood</u> <u>// Waferboard</u>	1.30	1.34	2.18	2.18	1.57	0.96	2.27	1.25
<u>I Plywood</u> <u>I Waferboard</u>	0.08	0.07	0.14	0.11	0.41	0.29	0.59	0.41
<u>PLYWOOD</u>								
<u>// Plywood</u> <u>I Plywood</u>	17.78	19.84	17.30	20.79	4.19	3.59	4.12	3.54
<u>// U Plywood</u> <u>// D Plywood</u>	0.98	0.95	1.03	1.18	0.92	0.91	0.95	0.97
<u>I U Plywood</u> <u>I D Plywood</u>	1.04	0.85	1.05	0.87	1.01	1.55	1.02	1.52
<u>WAFFERBOARD</u>								
<u>// Waferboard</u> <u>I Waferboard</u>	1.08	0.97	1.08	1.01	1.10	1.09	1.11	1.15
<u>// U Waferboard</u> <u>// D Waferboard</u>	1.02	0.91	1.00	0.96	1.02	1.07	1.04	1.06
<u>I U Waferboard</u> <u>I D Waferboard</u>	1.00	1.06	1.04	0.97	1.04	1.06	1.07	1.04

NOTE: All values are calculated on the basis of gross cross-sectional area.

Specific Gravity and Moisture Content Test Results (Vancouver)

Table 6.1 9.5 mm (3/8") Plywood

Property Type of Test	#	Specific Gravity		Moisture Content (%)	
		Average	5% Exclusion Limit	Average	5% Exclusion Limit
Overall Results	40	.410	.376	7.5	5.5
Parallel & Up	10	.425	.377	8.4	6.2
Parallel & Down	10	.405	.386	7.8	6.6
Perpendicular & Up	10	.410	.383	7.1	5.3
Perpendicular & Down	10	.400	.377	6.9	4.8

Table 6.2 11.1 mm (7/16") Waferboard

Property Type of Test	#	Specific Gravity		Moisture Content (%)	
		Average	5% Exclusion Limit	Average	5% Exclusion Limit
Overall Results	40	.691	.621	3.1	1.1
Parallel & Up	10	.707	.677	3.9	2.6
Parallel & Down	10	.726	.649	3.7	2.0
Perpendicular & Up	10	.657	.612	2.2	0.5
Perpendicular & Down	10	.675	.613	2.6	0.9

Specific Gravity and Moisture Content Test Ratios (Vancouver)

Table 6.3 Ratio Comparison of Results

9.5 mm (3/8") Plywood versus 11.1 mm (7/16") Waferboard

Property	Specific Gravity Ratio		Moisture Content Ratio	
	Average	5% Exclusion Limit	Average	5% Exclusion Limit
<u>Plywood</u> <u>Waferboard</u>	0.59	0.61	2.44	4.94
PLYWOOD				
<u>// Plywood</u> <u>1 Plywood</u>	1.02	1.00	1.15	1.26
<u>// U Plywood</u> <u>// D Plywood</u>	1.05	0.98	1.08	0.94
<u>1 U Plywood</u> <u>1 D Plywood</u>	1.03	1.01	1.02	1.10
WAFERBOARD				
<u>// Waferboard</u> <u>1 Waferboard</u>	1.08	1.08	1.60	3.37
<u>// U Waferboard</u> <u>// D Waferboard</u>	0.97	1.04	1.06	1.32
<u>1 U Waferboard</u> <u>1 D Waferboard</u>	0.97	1.00	0.84	0.51

Concentrated Load Test Results

Span Between Joists = 600 mm

Table 7.1 9.5 mm (3/8") Plywood

Moisture Content = 7.5% (See Table 6.1)

Property Type of Test	#	Ultimate Load (N)		Deflection (mm) at 890 N	
		Average	5% Exclusion Limit	Average	5% Exclusion Limit
Supported with H-clips	22	3320	1720	10.2	8.4
Unsupported (No H-clips)	23	3140	1670	11.0	9.0
Interior Load Location	23	3710	2320	9.8	8.8
Exterior Load Location	22	2730	1510	11.4	9.4

Table 7.2 11.1 mm (7/16") Waferboard

Moisture Content = 3.1% (See Table 6.2)

Property Type of Test	#	Ultimate Load (N)		Deflection (mm) at 890 N	
		Average	5% Exclusion Limit	Average	5% Exclusion Limit
Supported with H-clips	40	2000	1620	7.9	6.1
Unsupported (No H-clips)	40	2340	1790	9.0	6.9
Interior Load Location	40	2240	1610	8.2	6.3
Exterior Load Location	40	2110	1670	8.7	6.4

Concentrated Load Test Ratios

Table 7.3 Ratio Comparison of Results
 9.5 mm (3/8") Plywood versus 11.1 mm (7/6") Waferboard

Property	P.Ult. Ratio		Deflection Ratio at 890 N	
	Average	5% Exclusion Limit	Average	5% Exclusion Limit
<u>Plywood</u> <u>Waferboard</u>	1.49	1.05	1.25	1.36
<u>Plywood Supported</u> <u>Waferboard Supported</u>	1.66	1.06	1.28	1.37
<u>Plywood Unsupported</u> <u>Waferboard Unsupported</u>	1.34	0.94	1.22	1.31
<u>Plywood Interior</u> <u>Waferboard Interior</u>	1.66	1.45	1.19	1.40
<u>Plywood Exterior</u> <u>Waferboard Exterior</u>	1.29	0.91	1.30	1.47
PLYWOOD				
<u>Plywood Interior Loading</u> <u>Plywood Exterior Loading</u>	1.36	1.53	0.87	0.93
<u>Plywood Supported</u> <u>Plywood Unsupported</u>	1.06	1.03	0.92	0.93
WAFERBOARD				
<u>Waferboard Interior Loading</u> <u>Waferboard Exterior Loading</u>	1.06	0.97	0.94	0.98
<u>Waferboard Supported</u> <u>Waferboard Unsupported</u>	0.86	0.90	0.88	0.89

Table 8

Comparison of Test Results for Waferboard and Values
Required in *CSA Standard CAN3-0188.2-M78

Property	Type of Test	Test Result Average	Test Result 5% Exclusion Limit	Minimum Requirement*
MOE (GPa)	Small Scale Flexure	3.60	2.46	2.70
	Compression	2.53	2.14	
	Post Flexure	4.28	2.86	
MOR (MPa)	Small Scale Flexure	18.9	12.2	14.0
	Post Flexure	15.3	9.01	
Bond (kPa)	Bond	496	290	280

From Table 8 it can be seen that different types of tests yield different values for MOE and MOR. The mean value for MOE, as determined by the post-flexure test was 16% higher than that determined by the small scale flexure test, and 40% higher than that determined by the compression tests. The mean value for MOR, as determined by the post-flexure test was 19% lower than that determined by the small scale flexure test.

4. ANALYSIS OF TEST METHODS

Because this was a pilot study, some of the test procedures were not as efficient as they could be. Some modifications would be desirable for future testing of large numbers of specimens. This section includes recommendations for improvement of the procedures followed. In addition estimates of approximate time requirements for the various tests are given.

4.1 Small Scale Tests

Most of the measurements of the small scale test specimens were taken using calipers with an accuracy of $\pm .01$ mm. As these measurements must be taken by hand, this procedure becomes very time consuming when large numbers of specimens are involved, especially if measurements are repeated for improved accuracy.

4.1.1 Flexural Tests

In the pilot study, three width measurements were taken per specimen. For future tests, it is recommended that only one width measurement be taken at the mid-span of each specimen.

Once the x-y plotter was calibrated and running smoothly, the testing rate was approximately ten specimens per hour. To save time, measurements were taken while tests were performed. This rate of testing does not include time

for cutting and labelling specimens, or additional time required for measuring specimens.

4.1.2 Compression Tests

Six thickness, two length, and two width measurements were taken for each specimen. For future tests, it is recommended that two thickness measurements be taken, one from either side of the specimen at mid-span. It is also recommended that one length and one width measurement be taken along the centreline of the specimen.

After the x-y plotter was calibrated and running smoothly, the test rate was about six specimens per hour. Measurements were taken while tests were performed. This test rate does not include time for cutting, labelling and additional time required for measuring specimens.

4.1.3 Bond Tests

The length of each of the four sides of the bond test specimens was measured prior to testing. It is recommended that only two measurements be taken, along the centreline of two adjacent sides.

For the bond tests, the rate determining step was the ten hour curing time of the glue. Twelve pairs of aluminum load blocks were used, so specimens were tested twelve at a time. The actual testing of twelve specimens took between an hour and an hour and a half. The time required to glue this number of specimens was about forty-five minutes. If

more aluminum load blocks were available, the total time for testing a given number of specimens could be decreased.

4.1.4 Density and Moisture Content Tests

The length of each of the four sides, and two thickness measurements were taken for each sample. These values were then used to calculate the volume of each sample. This method was more time consuming and less accurate than the water displacement method used at the laboratory of the Council of Forest Industries in Vancouver. Therefore, it is recommended that a method similar to that used in Vancouver be used for all density and moisture content tests in the future.

The rate determining step in this procedure was the oven drying time of twenty-four hours.

4.2 Large Scale Tests

For the large scale tests, the measuring of specimens did not create the same time problems as it did for the small scale tests. This is because no width or length measurements were taken after the specimen had been cut, and only one thickness measurement was taken per specimen.

4.2.1 Post Flexure Tests

The large scale post flexure test procedure employed in tests at the laboratory of the Council of Forest Industries in Vancouver was efficient and suited to handling large numbers of test specimens.

Although only one thickness measurement was taken per specimen, all but one of the values were acceptably close to the nominal thickness. For the specimen in question, a second thickness reading was taken and the two values were averaged to give a representative value for the entire specimen. One thickness reading per specimen should be adequate unless the value of that reading is in question.

Between twenty and twenty-five specimens were tested per day, excluding the time required for cutting, labelling and measuring specimens.

4.2.2 Density and Moisture Content Tests

The procedure for determining density and moisture content, as performed at the laboratory in Vancouver, was efficient and suited for handling large numbers of samples. No measurements were required, therefore the rate determining step was the oven drying time.

4.2.3 Concentrated Load Tests

The procedure used for performing concentrated load tests could be improved in a number of ways to facilitate testing large numbers of specimens. The following are a few suggestions:

1. A system of rollers and clamps could be introduced to facilitate the movement of the loading jack to various test locations within a grid.
2. An automatic pump in place of a hand pump would

ensure a uniform load rate.

3. Plotting load versus deflection curves on an x-y plotter rather than taking readings manually would decrease the testing and calculation time.

Weighing the specimens and taking thickness measurements was done for the purpose of calculating density. It is unnecessary for the load tests themselves.

Using the set-up presently available, the test rate is about two panels per day, for eight load locations per panel. This includes time to nail the panels in place and remove them. It does not include time for cutting and labelling specimens.

5. CONCLUSIONS

The procedures employed in conducting the standard tests for small scale flexure, compression and bond tests were considered satisfactory, and acceptable for a possible future extensive test program. However, the load capacity of the Baldwin machine was much larger than required for these tests. As a result, it was difficult to calibrate the x-y plotter for load versus deflection curves. For future testing, it would be desirable to use a smaller load capacity testing machine.

The procedures and equipment utilized in large scale post flexure tests and specific gravity and moisture content tests performed at the Council of Forest Industries laboratory are suited to efficient testing of large numbers of specimens.

The procedure and equipment used for the concentrated load tests were satisfactory for testing a small number of specimens but would have to be revised for testing a large number of specimens. Suggested revisions can be found in Section 4.2.3.

The type of failure observed in the H-clips indicates that their effectiveness is questionable. It may be desirable to do a separate study to further determine the behavior of H-clips in this type of construction.

For all tests, the number of individual specimens tested was insufficient to establish definitive values of

the various mechanical properties.

Summary Table of Test Results

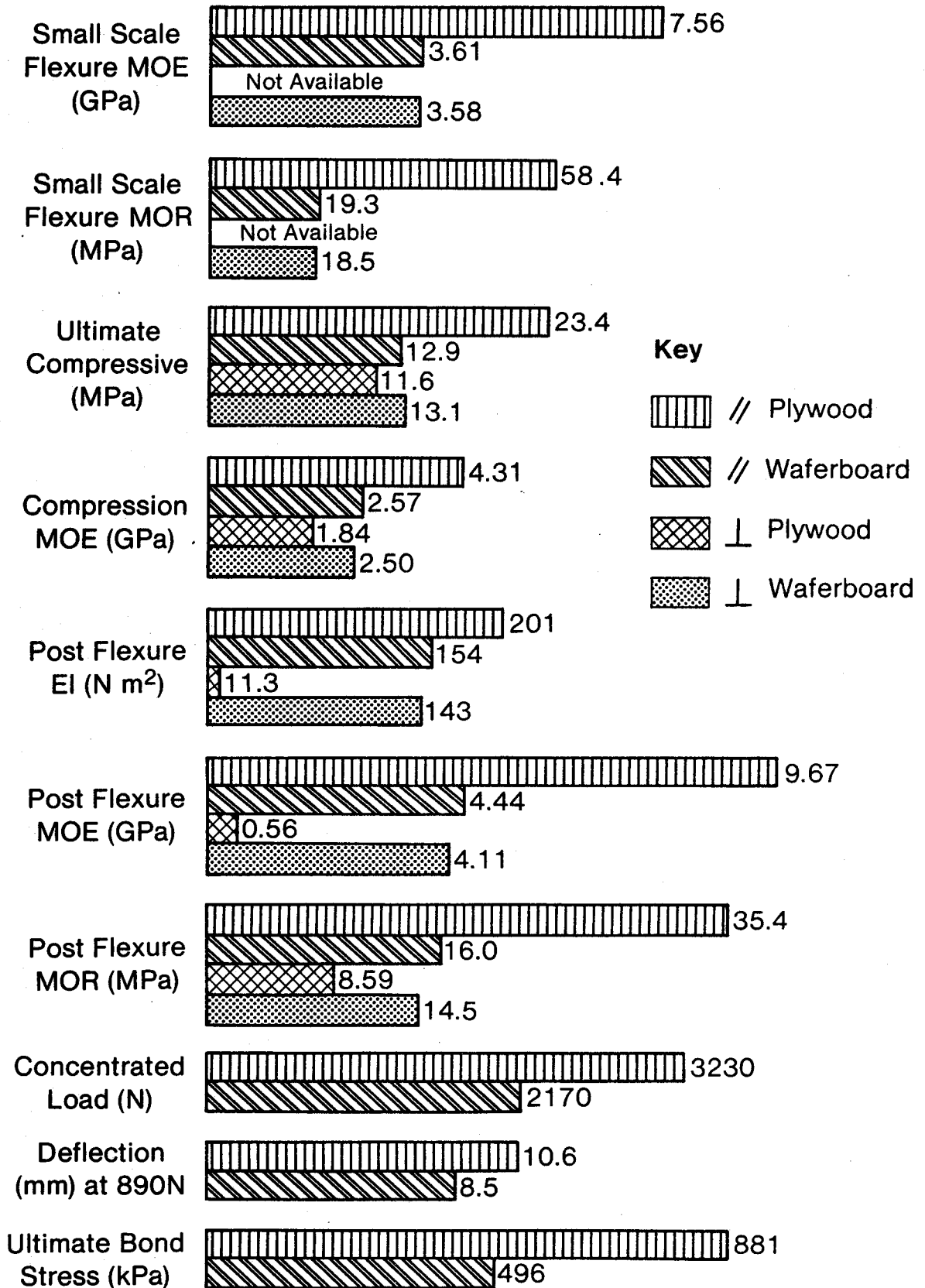
Type of Test	Face Grain Direction	Panel Type	Repli- cates	Test Results			
				Mean	Standard Deviation	CV (%)	5% Exclusion Limit
Small Scale Flexure MOE (GPa)	Parallel	Plywood	60	7.56	1.07	14.2	5.79
		Waferboard	58	3.61	0.69	19.0	2.48
	Perpendicular	Plywood	0	--	--	--	--
		Waferboard	59	3.58	0.69	19.3	2.44
Small Scale Flexure MOR (MPa)	Parallel	Plywood	60	58.4	13.1	22.4	36.8
		Waferboard	55	19.3	4.28	22.2	12.3
	Perpendicular	Plywood	0	--	--	--	--
		Waferboard	59	18.5	3.79	20.5	12.2
Ultimate Compressive Stress (MPa)	Parallel	Plywood	30	23.4	2.24	9.5	19.8
		Waferboard	30	12.9	1.31	10.1	10.7
	Perpendicular	Plywood	30	11.6	1.37	11.8	9.38
		Waferboard	29	13.1	1.53	11.7	10.6
Compression MOE (GPa)	Parallel	Plywood	30	4.31	0.32	7.4	3.8
		Waferboard	30	2.57	0.27	10.5	2.1
	Perpendicular	Plywood	30	1.84	0.28	15.3	1.38
		Waferboard	29	2.50	0.20	8.0	2.17
Post Flexure EI (N·m ²)	Parallel	Plywood	20	201	23.0	11.5	163
		Waferboard	20	154	19.8	12.9	121
	Perpendicular	Plywood	20	11.3	1.87	16.6	8.20
		Waferboard	19	143	10.9	7.6	125

continued

Summary Table of Test Results continued

Type of Test	Face Grain Direction	Panel Type	Repli-cates	Test Results			
				Mean	Standard Deviation	CV (%)	5% Exclusion Limit
Post Flexure MOE (GPa)	Parallel	Plywood	20	9.67	1.22	12.6	7.66
		Waferboard	20	4.44	0.57	12.7	3.51
	Perpendicular	Plywood	20	0.56	0.12	20.6	0.37
		Waferboard	19	4.11	0.39	9.5	3.46
Post Flexure MOR (MPa)	Parallel	Plywood	20	35.4	10.5	29.7	18.0
		Waferboard	19	16.0	0.99	6.19	14.4
	Perpendicular	Plywood	20	8.59	2.12	24.7	5.10
		Waferboard	19	14.5	1.17	8.09	12.6
Type of Test	Property	Panel Type	Repli-cates	Test Results			
				Mean	Standard Deviation	CV (%)	5% Exclusion Limit
Concentrated Load Test	Ultimate Load (N)	Plywood	45	3230	925	28.6	1700
		Waferboard	80	2170	334	15.4	1620
	Deflection (mm) at 890 N	Plywood	45	10.6	1.21	11.4	8.59
		Waferboard	79	8.5	1.32	15.6	6.30
Bond	Ultimate Bond Stress (kPa)	Plywood	57	881	384	43.6	248
		Waferboard	58	496	125	25.2	290

Bar Graph Summary of Test Results



References

1. Canadian Standards Association, Standard Test Methods for Mat-Formed Wood Particleboards and Waferboard, CSA Standard CAN3-0188.0-M78.
2. Longworth, J., Moisture-Strength Relations for Sheathing Grade Douglas Fir Plywood, Department of Civil Engineering, The University of Alberta, September, 1974.
3. American Society for Testing and Materials, Standard Methods for Testing Plywood in Flexure, ASTM Standard D3043-72.
4. American Society for Testing and Materials, Standard Test Method for Performance of Wood and Wood-Based Floor and Roof Sheathing Under Concentrated Static and Impact Loads, ASTM Standard E661-78.
5. American Society for Testing and Materials, Standard Test Methods for Specific Gravity of Wood and Wood-Base Materials, ASTM Standard D2395-69.

Appendix A

This appendix contains the computer printout of all test data, and statistical results. The statistical results include the numbers of tests, the average, standard deviation, coefficient of variation, five percent exclusion limit, maximum and minimum values.

The statistics were calculated as follows:

(i) Average

$$\bar{x} = \frac{\sum_{i=1}^n x_i}{n}$$

(ii) Standard Deviation

$$\sigma = \sqrt{\frac{\sum_{i=1}^n (\bar{x} - x_i)^2}{n - 1}}$$

(iii) Coefficient of Variation C.O.V.

$$\text{C.O.V.} = \frac{\sigma}{\bar{x}}$$

(iv) 5% Exclusion Limit

$$5\% \text{ ex. lt.} = \bar{x} - 1.65\sigma$$

The following are definitions of some of the terms used in the Appendix:

Parallel (//) - refers to specimens cut parallel to the longitudinal axis of the panel.

Perpendicular (⊥) - refers to specimens cut perpendicular to the longitudinal axis of the panel.

Up (U) - refers to specimens tested with the trademark side in tension.

Down (D) - refers to specimens tested with the trademark side in compression.

Supported - refers to a load location with H-clips.

Unsupported - refers to a load location without H-clips.

Interior - refers to a load location with a continuous span on both sides.

Exterior - refers to a load location with a continuous span on one side only.

Small Scale Flexural Test Results for Plywood

Panel #	1,3,5=up, 2,4,6=down	Avg. d (mm)	Avg. b (mm)	P ult. (N)	P/y (kN/mm)	M.O.E. (GPa)	M.O.R. (MPa)
Panel #1	1,3,5=up, 2,4,6=down	9.3200	75.530	1240.0	0.18340	8.9459	64.724
		9.3500	75.500	780.00	0.17570	8.4915	38.431
		9.5200	75.550	1350.0	0.20000	9.1224	87.376
		9.7800	75.570	970.00	0.19810	8.2738	45.956
		9.4000	75.700	1000.0	0.17950	8.5262	61.264
		9.2700	75.580	1060.0	0.18350	8.0904	55.890
Panel #2	1,3,5=up, 2,4,6=down	9.2300	75.580	1280.0	0.17570	8.8177	68.076
		9.3500	75.570	1070.0	0.16420	7.9284	55.463
		9.2500	75.550	1080.0	0.15280	8.1106	57.214
		9.3500	75.600	1080.0	0.15580	7.5297	58.033
		9.2800	75.600	500.00	0.12330	6.0949	28.334
		9.1500	75.620	1020.0	0.13750	7.0888	55.244
Panel #3	1,3,5=up, 2,4,6=down	9.5500	75.720	840.00	0.11030	4.9849	41.709
		9.4200	75.570	1300.0	0.12370	5.8407	66.387
		9.1200	75.530	1390.0	0.14580	7.5901	75.770
		9.0500	75.700	1410.0	0.13320	9.7511	77.882
		9.4200	75.750	1000.0	0.15840	7.4474	50.805
		9.3500	75.750	1280.0	0.14710	7.0952	65.243
Panel #4	1,3,5=up, 2,4,6=down	9.3000	75.550	1300.0	0.18090	7.8971	68.130
		9.3000	75.730	1190.0	0.17280	8.4722	62.298
		9.4200	75.730	1420.0	0.19720	8.2741	72.304
		9.4500	75.850	1570.0	0.17320	8.0882	78.657
		9.3200	75.730	1080.0	0.12770	8.2008	58.177
		9.3000	75.730	800.00	0.14550	7.1337	41.882
Panel #5	1,3,5=up, 2,4,6=down	9.3500	75.720	980.00	0.14670	7.0787	50.764
		9.2500	75.750	1000.0	0.14670	7.3079	52.906
		9.3800	75.700	1170.0	0.18320	8.7577	60.235
		9.2800	75.720	1430.0	0.17720	8.7454	75.196
		9.3800	75.750	1250.0	0.15290	7.3044	64.312
		9.5000	75.750	1440.0	0.15150	6.9667	72.227
Panel #6	1,3,5=up, 2,4,6=down	9.3700	75.700	1040.0	0.12630	6.0570	53.657
		9.3800	75.700	910.00	0.12500	5.9755	46.850
		9.5000	75.680	950.00	0.13240	6.0540	47.894
		9.4800	75.820	1070.0	0.14710	6.8190	53.988
		9.7500	75.730	650.00	0.14580	6.2036	31.436
		9.5000	75.720	1380.0	0.18400	8.1298	64.127
Panel #7	1,3,5=up, 2,4,6=down	9.3700	75.700	1500.0	0.17580	8.4309	77.390
		9.3000	75.570	790.00	0.15560	7.6349	41.391
		9.4200	75.730	900.00	0.13850	6.5343	45.924
		9.3800	75.530	1380.0	0.15580	7.4548	70.082
		9.2300	75.700	890.00	0.12770	6.4071	47.321
		9.4200	75.570	980.00	0.14520	6.8558	50.046
Panel #8	1,3,5=up, 2,4,6=down	9.5500	75.730	1330.0	0.15120	6.8461	66.030
		9.5700	75.700	730.00	0.13170	5.9282	36.105
		9.4200	75.580	1010.0	0.12940	6.1090	51.571
		9.3800	75.730	780.00	0.12280	5.8680	39.112
		9.2700	75.600	1320.0	0.15730	7.8008	69.672
		9.2500	75.580	1080.0	0.17910	8.9301	57.191
Panel #9	1,3,5=up, 2,4,6=down	9.3200	75.700	1260.0	0.15380	7.4952	65.707
		9.3700	75.570	940.00	0.16360	7.8488	48.517
		9.6400	75.650	1460.0	0.15380	6.6941	70.625
		9.7200	75.620	1120.0	0.16300	7.0100	53.755
		9.3600	75.780	1460.0	0.19480	9.3024	75.086
		9.4700	75.750	820.00	0.17580	8.1612	41.390
Panel #10	1,3,5=up, 2,4,6=down	9.6300	75.570	1070.0	0.18980	8.3881	52.285
		9.7800	75.770	1610.0	0.19440	8.1913	76.176
		9.1300	75.720	1400.0	0.15570	8.0693	75.058
		9.9300	75.700	1380.0	0.14440	7.9999	77.252
		9.6300	75.770	1450.0	0.18750	8.2755	70.760
		9.6200	75.780	1470.0	0.18180	8.0479	71.875

Small Scale Flexure Test Results for Waterboard

Panel #1, Parallel, 1,3,5=up, 2,4,6=down						
Avg. d (mm)	Avg. b (mm)	P ult. (N)	P/y (kN/mm)	M.O.E. (GPa)	M.O.R. (MPa)	
11.700	75.810	0.0	0.0	0.0	0.0	0.0
11.780	75.830	228.00	0.80300E-01	3.0840	8.8038	
11.880	75.850	328.00	0.70700E-01	2.8012	12.880	
11.840	75.880	488.00	0.88800E-01	3.4387	18.818	
11.080	75.780	418.00	0.58800E-01	2.8087	17.843	
11.230	75.850	500.00	0.51700E-01	2.2870	20.951	
Panel #1, Perpendicular, 1,3,5=up, 2,4,6=down						
Avg. d (mm)	Avg. b (mm)	P ult. (N)	P/y (kN/mm)	M.O.E. (GPa)	M.O.R. (MPa)	
11.310	75.600	535.00	0.89200E-01	3.8852	22.127	
11.310	75.850	553.00	0.70700E-01	3.0615	22.858	
11.460	75.810	380.00	0.13780	5.7155	14.060	
11.800	75.520	450.00	0.10170	4.1964	18.021	
11.320	75.480	410.00	0.67500E-01	2.8228	16.958	
11.310	75.660	460.00	0.61200E-01	2.6488	19.010	
Panel #2, Parallel, 1,3,5=up, 2,4,6=down						
Avg. d (mm)	Avg. b (mm)	P ult. (N)	P/y (kN/mm)	M.O.E. (GPa)	M.O.R. (MPa)	
11.070	75.610	250.00	0.84600E-01	3.8090	10.792	
11.160	75.620	470.00	0.87200E-01	3.9318	19.959	
11.390	75.890	420.00	0.88600E-01	3.7544	17.107	
11.190	75.620	460.00	0.80000E-01	3.5783	19.430	
11.730	75.780	600.00	0.11280	4.3708	23.015	
11.610	75.750	625.00	0.98100E-01	3.9220	24.482	
Panel #2, Perpendicular, 1,3,5=up, 2,4,6=down						
Avg. d (mm)	Avg. b (mm)	P ult. (N)	P/y (kN/mm)	M.O.E. (GPa)	M.O.R. (MPa)	
11.180	75.680	450.00	0.70800E-01	3.1843	18.893	
11.120	75.890	500.00	0.91000E-01	4.1438	21.367	
11.620	75.750	500.00	0.10050	4.0076	19.552	
11.560	75.640	510.00	0.10380	4.2210	20.215	
11.580	75.490	540.00	0.78600E-01	3.1778	21.336	
11.610	75.700	450.00	0.76500E-01	3.0604	17.639	
Panel #3, Parallel, 1,3,5=up, 2,4,6=down						
Avg. d (mm)	Avg. b (mm)	P ult. (N)	P/y (kN/mm)	M.O.E. (GPa)	M.O.R. (MPa)	
11.700	75.630	385.00	0.58700E-01	2.3358	14.873	
11.710	75.700	330.00	0.55800E-01	2.5658	12.715	
11.320	75.660	380.00	0.80200E-01	3.4633	14.851	
11.300	75.700	450.00	0.55800E-01	2.8463	18.620	
10.820	75.780	550.00	0.84300E-01	4.1620	22.785	
10.930	75.760	520.00	0.0	0.0	24.979	
Panel #3, Perpendicular, 1,3,5=up, 2,4,6=down						
Avg. d (mm)	Avg. b (mm)	P ult. (N)	P/y (kN/mm)	M.O.E. (GPa)	M.O.R. (MPa)	
10.850	75.530	410.00	0.71400E-01	3.5076	18.443	
10.840	75.780	430.00	0.74100E-01	3.6397	19.322	
11.120	75.730	500.00	0.78900E-01	3.5910	23.918	
11.060	75.730	0.0	0.93800E-01	4.3389	0.0	
11.060	75.630	280.00	0.63800E-01	2.9551	12.105	
11.220	75.660	320.00	0.77600E-01	3.4389	13.437	
Panel #4, Parallel, 1,3,5=up, 2,4,6=down						
Avg. d (mm)	Avg. b (mm)	P ult. (N)	P/y (kN/mm)	M.O.E. (GPa)	M.O.R. (MPa)	
11.480	75.700	460.00	0.88900E-01	3.5859	18.441	
11.570	75.650	490.00	0.83200E-01	3.3653	19.352	
11.080	75.710	0.0	0.65800E-01	3.0199	0.0	
11.070	75.480	0.0	0.70700E-01	3.2723	0.0	
11.180	75.630	410.00	0.82600E-01	3.7040	17.347	
11.180	75.780	510.00	0.58900E-01	2.6287	21.502	
Panel #4, Perpendicular, 1,3,5=up, 2,4,6=down						
Avg. d (mm)	Avg. b (mm)	P ult. (N)	P/y (kN/mm)	M.O.E. (GPa)	M.O.R. (MPa)	
11.390	75.770	470.00	0.93900E-01	3.9748	19.124	
11.280	75.680	420.00	0.90500E-01	3.9487	17.445	
10.950	75.780	500.00	0.80500E-01	3.8356	22.015	
10.940	75.620	350.00	0.70000E-01	3.3508	15.467	
11.210	75.530	450.00	0.84400E-01	3.7694	18.963	
11.280	75.680	400.00	0.58300E-01	2.5438	16.614	
Panel #5, Parallel, 1,3,5=up, 2,4,6=down						
Avg. d (mm)	Avg. b (mm)	P ult. (N)	P/y (kN/mm)	M.O.E. (GPa)	M.O.R. (MPa)	
11.810	75.690	460.00	0.78900E-01	2.9982	17.425	
11.820	75.700	425.00	0.96400E-01	3.6546	16.072	
11.880	75.780	400.00	0.10120	3.9736	15.481	
11.660	75.690	620.00	0.99600E-01	3.9442	24.139	
11.240	75.840	500.00	0.82500E-01	3.6305	20.872	
11.360	75.740	0.0	0.76200E-01	3.2524	0.0	
Panel #5, Perpendicular, 1,3,5=up, 2,4,6=down						
Avg. d (mm)	Avg. b (mm)	P ult. (N)	P/y (kN/mm)	M.O.E. (GPa)	M.O.R. (MPa)	
11.740	75.610	490.00	0.78000E-01	3.0503	18.805	
11.660	75.780	330.00	0.97600E-01	3.8520	12.815	
11.490	75.750	680.00	0.12630	5.2817	27.196	
11.420	75.830	600.00	0.13300	5.5812	24.266	
11.660	75.680	310.00	0.88800E-01	3.4298	12.054	
11.630	75.710	350.00	0.62800E-01	2.5031	13.670	

continued on next page

The statistics:

Small Scale Flexure Test Results for Waferboard

All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
M.D.E. (GPa)	117	3.5958	0.68646	0.19092	2.4630	5.9605	2.2570
P ult (N)	114	449.96	91.780	0.20397	298.53	680.00	225.00
M.D.R. (MPa)	114	18.896	4.0418	0.21389	12.227	28.875	8.6038

All parallel results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
M.D.E. (GPa)	58	3.6088	0.68692	0.19035	2.4752	5.9605	2.2570
P ult (N)	55	450.96	91.230	0.19791	310.43	680.00	225.00
M.D.R. (MPa)	55	18.340	4.2839	0.22150	12.272	28.875	8.6038

All perpendicular results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
M.D.E. (GPa)	59	3.5830	0.69167	0.19304	2.4417	5.7155	2.5031
P ult (N)	59	439.71	91.873	0.20894	288.12	680.00	240.00
M.D.R. (MPa)	59	18.482	3.7921	0.20517	12.226	28.567	11.022

All parallel and up results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
M.D.E. (GPa)	29	3.6837	0.74744	0.20291	2.4504	5.9605	2.3358
P ult (N)	27	451.86	92.434	0.20452	299.45	620.00	250.00
M.D.R. (MPa)	27	18.934	4.5852	0.24223	11.366	28.875	10.792

All parallel and down results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
M.D.E. (GPa)	29	3.5335	0.62468	0.17678	2.5028	5.0334	2.2570
P ult (N)	28	469.64	80.880	0.19351	319.69	680.00	225.00
M.D.R. (MPa)	28	18.732	4.0156	0.20351	13.106	28.864	8.6038

All perpendicular and up results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
M.D.E. (GPa)	30	3.6837	0.67352	0.18580	2.5137	5.7155	2.5357
P ult (N)	30	451.86	89.926	0.22719	274.85	680.00	240.00
M.D.R. (MPa)	30	18.934	4.1035	0.22251	11.671	27.196	11.022

All perpendicular and down results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
M.D.E. (GPa)	29	3.5395	0.71926	0.20321	2.3528	5.5812	2.5031
P ult (N)	29	439.59	84.513	0.19226	300.14	680.00	280.00
M.D.R. (MPa)	29	18.524	3.5134	0.18966	12.727	28.567	12.816

Small Scale Compression Test Results for Plywood

The Calculated Plywood Quantities:

Panel #1 1-3 parallel, 4-6 perpendicular

M.O.E. gross (GPa)	M.O.E. parallel (GPa)	Stress, gross (MPa)	Stress, parallel (MPa)
4.2735	6.4725	22.492	34.066
4.4803	7.0296	25.023	39.174
3.8004	5.7911	23.034	35.100
2.3032	6.9545	12.065	36.430
1.5810	5.2652	9.9205	33.044
1.7887	5.6980	10.343	32.764

Panel #2 1-3 parallel, 4-6 perpendicular

M.O.E. gross (GPa)	M.O.E. parallel (GPa)	Stress, gross (MPa)	Stress, parallel (MPa)
4.0347	6.3608	21.801	34.371
4.5955	7.3891	25.688	41.277
4.1579	6.3789	23.134	35.498
1.8905	5.0714	11.675	35.024
1.7590	5.3057	11.544	34.839
1.2081	3.6936	8.8516	26.330

Panel #3 1-3 parallel, 4-6 perpendicular

M.O.E. gross (GPa)	M.O.E. parallel (GPa)	Stress, gross (MPa)	Stress, parallel (MPa)
4.1937	6.5962	23.283	36.590
4.5957	7.2370	23.709	37.327
3.9036	6.0140	23.506	38.214
2.3804	7.4479	12.876	40.288
1.8773	5.8498	13.798	42.998
1.6070	4.4444	11.810	34.829

Panel #4 1-3 parallel, 4-6 perpendicular

M.O.E. gross (GPa)	M.O.E. parallel (GPa)	Stress, gross (MPa)	Stress, parallel (MPa)
4.6755	7.2881	22.357	34.745
4.6074	7.0355	23.873	36.454
4.1548	6.7127	19.706	31.838
1.8318	5.6053	10.893	33.333
1.7003	5.4237	10.739	34.254
1.6584	5.2404	11.909	37.632

Panel #5 1-3 parallel, 4-6 perpendicular

M.O.E. gross (GPa)	M.O.E. parallel (GPa)	Stress, gross (MPa)	Stress, parallel (MPa)
4.5280	7.0446	21.526	33.505
4.5293	7.0120	27.453	42.500
4.2545	8.4944	19.650	29.996
2.0766	6.7778	12.453	40.646
2.1465	6.7852	15.603	49.323
1.8209	5.8897	10.969	35.478

The statistics:

Small Scale Compression Test Results for Plywood

Results for All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	80	31419.	11238.	0.35771	12875.	49800.	15700.
M.O.E. par (GPa)	80	8.2142	0.85888	0.13823	4.7889	7.5189	3.5836
M.O.E. gro (GPa)	80	3.0766	1.2758	0.41470	0.87143	5.1776	1.2081
Stress par (MPa)	80	36.286	3.8303	0.10828	28.811	49.323	26.330
Stress gro (MPa)	80	17.545	6.2276	0.35486	7.2682	27.453	8.7168

All parallel results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	30	42049.	4131.3	0.98250E-01	35232.	49500.	31100.
M.O.E. par (GPa)	30	8.8510	0.45662	0.68655E-01	5.8976	7.5189	5.7811
M.O.E. gro (GPa)	30	4.3088	0.31745	0.73709E-01	3.7630	5.1776	3.6915
Stress par (MPa)	30	36.228	3.5691	0.98516E-01	30.338	42.500	28.417
Stress gro (MPa)	30	23.444	2.2388	0.95495E-01	19.750	27.453	17.687

All perpendicular results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	30	20789.	2475.4	0.11907	16705.	28000.	15700.
M.O.E. par (GPa)	30	5.7775	0.94763	0.16402	4.2140	7.4478	3.5836
M.O.E. gro (GPa)	30	1.8464	0.28234	0.15282	1.3805	2.3804	1.2081
Stress par (MPa)	30	36.364	4.3220	0.11885	28.233	48.323	26.330
Stress gro (MPa)	30	11.645	1.3730	0.11790	9.3798	15.603	8.7168

The statistics:

Small Scale Compression Test Results for Waferboard

Results for All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	58	27875.	3041.9	0.10874	22955.	34000.	21700.
M.O.E. (GPa)	58	2.5342	0.23878	0.94222E-01	2.1402	3.1177	2.0308
Stress (MPa)	58	12.992	1.4139	0.10883	10.659	15.568	9.9949

All parallel results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	30	27899.	2932.2	0.10510	23061.	34000.	22250.
M.O.E. (GPa)	30	2.5716	0.26998	0.10498	2.1261	3.1177	2.0308
Stress (MPa)	30	12.891	1.3068	0.10137	10.735	15.528	10.017

All perpendicular results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	29	28053.	3201.7	0.11413	22770.	33750.	21700.
M.O.E. (GPa)	29	2.4956	0.19892	0.79711E-01	2.1673	2.8831	2.1758
Stress (MPa)	29	13.096	1.5329	0.11705	10.567	15.568	9.9949

Small Scale Bond Test Results for Plywood.

The statistics:

Results For All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	57	2221.1	867.52	0.43560	824.73	4390.0	550.00
Stress (kPa)	57	881.27	384.03	0.43576	247.63	1741.2	218.27

Results For Each Group of 6 Specimens:

Panel #1	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	6	3141.7	667.34	0.21241	2040.6	4390.0	2450.0
Stress (kPa)	6	1247.6	264.00	0.21161	811.98	1741.2	974.44

Panel #2	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	5	2570.0	840.86	0.32718	1182.6	3420.0	1710.0
Stress (kPa)	5	1020.3	333.65	0.32701	489.78	1368.5	678.30

Panel #3	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	6	1553.3	936.32	0.60214	10.063	3000.0	550.00
Stress (kPa)	6	617.15	372.34	0.60332	2.7886	1193.6	218.27

Panel #4	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	5	2010.0	508.48	0.25287	1171.0	2670.0	1240.0
Stress (kPa)	5	796.61	201.53	0.25289	484.08	1058.0	481.27

Panel #5	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	6	2076.7	885.32	0.42632	615.88	3280.0	910.00
Stress (kPa)	6	823.46	351.28	0.42659	243.85	1299.5	359.39

Panel #6	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	6	2306.7	644.23	0.27828	1243.7	3270.0	1530.0
Stress (kPa)	6	915.62	256.63	0.28028	492.18	1299.5	606.05

Panel #7	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	5	1932.0	638.59	0.33105	876.88	2530.0	1130.0
Stress (kPa)	5	766.12	253.27	0.33059	348.23	1002.0	448.14

Panel #8	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	6	1830.0	559.84	0.30582	806.59	2650.0	1000.0
Stress (kPa)	6	725.30	222.10	0.30621	358.84	1050.6	385.20

Panel #9	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	6	2799.2	881.84	0.24359	1674.1	3500.0	1880.0
Stress (kPa)	6	1110.6	270.41	0.24349	664.40	1386.1	745.28

Panel #10	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	5	1966.7	793.41	0.40343	657.53	3360.0	1200.0
Stress (kPa)	5	779.89	313.54	0.40203	262.55	1331.2	477.99

Small Scale Bond Test Results for Waferboard.

The statistics:

Results For All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	58	1253.1	288.80	0.21275	813.24	1700.0	380.00
Stress (kPa)	58	496.08	125.13	0.25223	289.62	674.66	150.52

Results For Each Group of 6 Specimens:

Panel #1	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	6	1143.3	154.23	0.13488	888.85	1350.0	900.00
Stress (kPa)	6	452.32	60.826	0.13447	351.86	537.90	356.07

Panel #2	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	5	1448.0	200.17	0.13824	1117.7	1700.0	1220.0
Stress (kPa)	5	571.35	81.630	0.14287	436.88	674.66	484.12

Panel #3	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	6	1243.3	435.74	0.35046	524.37	1540.0	380.00
Stress (kPa)	6	492.50	172.65	0.35056	207.63	611.35	150.52

Panel #4	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	6	1162.5	177.53	0.15272	888.57	1375.0	950.00
Stress (kPa)	6	460.94	70.388	0.15270	344.80	546.28	377.09

Panel #5	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	6	1216.7	159.58	0.13116	953.36	1460.0	1000.0
Stress (kPa)	6	482.05	62.860	0.13040	378.34	577.00	395.74

Panel #6	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	6	1360.0	66.030	0.48552E-01	1251.1	1420.0	1250.0
Stress (kPa)	6	539.04	26.710	0.49551E-01	494.97	562.25	494.60

Panel #7	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	6	1215.0	152.02	0.12512	984.17	1420.0	1000.0
Stress (kPa)	6	481.37	60.227	0.12512	361.98	562.98	396.11

Panel #8	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	6	1255.0	120.79	0.96246E-01	1055.7	1410.0	1100.0
Stress (kPa)	6	496.94	48.020	0.96631E-01	417.71	558.73	435.46

Panel #9	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	6	1260.8	131.47	0.10427	1043.9	1505.0	1130.0
Stress (kPa)	5	498.76	57.834	0.11596	403.33	597.45	450.97

Panel #10	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
P ult. (N)	6	1259.2	262.31	0.20832	826.36	1495.0	910.00
Stress (kPa)	6	498.52	103.93	0.20847	327.04	592.01	359.31

Specific Gravity and Moisture Content for Plywood (Edmonton)

The Statistics:

Results For All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	30	0.41068	0.18226E-01	0.44381E-01	0.38061	0.44488	0.35987
Moisture Content	30	6.8999	0.23657	0.33786E-01	6.6086	7.5617	6.5979

Results For Each Group of 3 Specimens:

Panel #1

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.42017	0.25433E-01	0.60531E-01	0.37821	0.44488	0.39415
Moisture Content	3	7.2770	0.11082	0.15229E-01	7.0941	7.3709	7.1547

Panel #2

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.39163	0.32179E-01	0.82167E-01	0.33853	0.42421	0.35987
Moisture Content	3	7.2616	0.28178	0.40182E-01	6.7801	7.5617	6.9790

Panel #3

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.41812	0.12690E-01	0.30350E-01	0.39718	0.42795	0.40379
Moisture Content	3	7.0501	0.24616	0.34915E-01	6.6439	7.2263	6.7692

Panel #4

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.40228	0.14705E-01	0.36554E-01	0.37802	0.41811	0.38905
Moisture Content	3	7.0860	0.45767E-01	0.64588E-02	7.0105	7.1176	7.0335

Panel #5

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.41908	0.77217E-02	0.18425E-01	0.40634	0.42782	0.41318
Moisture Content	3	7.1077	0.22899	0.32217E-01	6.7299	7.3623	6.9185

Panel #6

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.39489	0.14537E-01	0.35812E-01	0.37090	0.40510	0.37825
Moisture Content	3	6.7749	0.16293	0.24050E-01	6.6061	6.9407	6.6149

Panel #7

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.40757	0.20875E-01	0.51484E-01	0.37296	0.42845	0.38763
Moisture Content	3	6.8520	0.20887	0.30630E-01	6.5058	7.0678	6.5486

Panel #8

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.40832	0.78665E-02	0.18776E-01	0.39587	0.41646	0.40125
Moisture Content	3	6.8488	0.25406	0.37086E-01	6.4296	7.1059	6.5979

Panel #9

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.42437	0.12980E-01	0.30586E-01	0.40295	0.43194	0.40938
Moisture Content	3	6.8956	0.42407E-01	0.61498E-02	6.8256	6.9382	6.8534

Panel #10

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.42040	0.50085E-02	0.11914E-01	0.41214	0.42406	0.41469
Moisture Content	3	6.8458	0.13019	0.19018E-01	6.6309	6.9325	6.6961

Specific Gravity and Moisture Content for Waferboard (Edmonton)

The Statistics:

Results For All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	30	0.83322	0.35929E-01	0.58740E-01	0.57394	0.71164	0.54401
Moisture Content	30	4.8605	0.10606	0.21820E-01	4.6855	5.0621	4.5770

Results For Each Group of 3 Specimens:

Panel #1

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.82472	0.79629E-02	0.12746E-01	0.51159	0.83392	0.51889
Moisture Content	3	4.8667	0.97033E-01	0.18529E-01	4.8086	5.0621	4.8664

Panel #2

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.83034	0.29837E-01	0.47335E-01	0.58111	0.64874	0.59591
Moisture Content	3	4.8213	0.73710E-01	0.14978E-01	4.7997	4.9742	4.8371

Panel #3

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.59826	0.54984E-01	0.91906E-01	0.50754	0.65395	0.54401
Moisture Content	3	4.8271	0.12308	0.25497E-01	4.6240	4.9638	4.7253

Panel #4

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.83404	0.22691E-01	0.35787E-01	0.59660	0.64722	0.60784
Moisture Content	3	4.8183	0.11002	0.22369E-01	4.7368	4.9988	4.7929

Panel #5

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.82810	0.24774E-01	0.39443E-01	0.58722	0.64486	0.59954
Moisture Content	3	4.8781	0.39868E-01	0.81319E-02	4.8127	4.9049	4.8325

Panel #6

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.83474	0.15104E-01	0.23795E-01	0.80982	0.84435	0.61733
Moisture Content	3	4.7731	0.21705	0.45473E-01	4.4150	5.0053	4.5770

Panel #7

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.65807	0.79134E-01	0.12025	0.52750	0.71164	0.56718
Moisture Content	3	4.8985	0.42346E-01	0.86445E-02	4.8287	4.9410	4.8553

Panel #8

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.65803	0.46959E-01	0.71364E-01	0.58055	0.70760	0.61421
Moisture Content	3	4.7921	0.58350E-01	0.12176E-01	4.6958	4.8423	4.7281

Panel #9

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.61820	0.18267E-01	0.28549E-01	0.58806	0.63816	0.60231
Moisture Content	3	4.7888	0.65263E-01	0.13628E-01	4.6811	4.8421	4.7160

Panel #10

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	3	0.64772	0.90984E-02	0.14047E-01	0.63270	0.65602	0.63799
Moisture Content	3	4.8392	0.59856E-01	0.12369E-01	4.7404	4.8905	4.7734

The statistics:

Large Scale Flexural Test Results For Plywood

All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
EI (Nm2) :	40	105.90	87.188	0.91754	-54.427	251.24	5.7340
M.O.E. (MPa) :	40	5114.5	4891.9	0.91738	-2827.2	11438.	305.38
M ult. (Nm) :	40	87.073	88.189	0.70225	-15.407	233.34	21.470
M.O.R. (kPa) :	40	21995.	15501.	0.70471	-3580.4	56174.	4502.4

All parallel results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
EI (Nm2) :	20	200.52	22.958	0.11454	162.63	251.24	155.97
M.O.E. (MPa) :	20	8670.2	1218.7	0.12582	7862.7	11438.	7356.6
M ult. (Nm) :	20	155.73	44.406	0.28333	83.461	233.34	93.903
M.O.R. (kPa) :	20	35399.	10512.	0.29695	18054.	56174.	20844.

All perpendicular results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
EI (Nm2) :	20	11.279	1.8684	0.16565	8.1961	14.912	5.7340
M.O.E. (MPa) :	20	558.82	115.28	0.20630	368.60	794.03	305.38
M ult. (Nm) :	20	37.414	8.6016	0.22990	23.222	54.240	21.470
M.O.R. (kPa) :	20	8592.5	2119.4	0.24686	5095.5	12156.	4502.4

All parallel and up results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
EI (Nm2) :	10	198.56	25.008	0.12595	157.30	251.24	155.97
M.O.E. (MPa) :	10	8227.1	824.19	0.94045E-01	8302.2	11000.	7985.2
M ult. (Nm) :	10	149.82	43.312	0.28891	78.452	217.30	93.903
M.O.R. (kPa) :	10	34569.	10443.	0.30209	17338.	51437.	21147.

All parallel and down results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
EI (Nm2) :	10	202.49	21.902	0.10816	166.35	238.23	170.91
M.O.E. (MPa) :	10	9513.3	1485.7	0.15649	7056.9	11438.	7356.6
M ult. (Nm) :	10	163.54	46.731	0.28574	86.439	233.34	93.903
M.O.R. (kPa) :	10	36228.	11077.	0.30575	17952.	56174.	20844.

All perpendicular and up results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
EI (Nm2) :	10	11.527	2.3849	0.20689	7.5922	14.912	5.7340
M.O.E. (MPa) :	10	571.29	138.29	0.24206	343.12	794.03	305.38
M ult. (Nm) :	10	37.685	5.4047	0.14342	28.768	44.522	29.606
M.O.R. (kPa) :	10	8657.3	1493.8	0.17255	6192.6	10770.	6053.8

All perpendicular and down results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
EI (Nm2) :	10	11.031	1.2429	0.11267	8.9798	13.000	8.8855
M.O.E. (MPa) :	10	548.35	92.672	0.16962	393.44	734.73	419.97
M ult. (Nm) :	10	37.183	11.262	0.30319	18.562	54.240	21.470
M.O.R. (kPa) :	10	8527.7	2691.1	0.31558	4067.3	12156.	4502.4

The statistics:

Large Scale Flexural Test Results For Waferboard

All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
EI (Nm ²) :	39	148.57	29.392	0.19783	100.07	204.54	114.88
M.O.E. (MPa) :	39	4280.9	862.24	0.20141	2858.2	5734.1	3502.5
M ult. (Nm) :	38	95.306	23.760	0.24930	56.102	117.68	81.227
M.O.R. (kPa) :	38	15266.	3788.8	0.24818	9014.6	17363.	12767.

All parallel results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
EI (Nm ²) :	20	153.92	19.814	0.12873	121.22	204.54	114.88
M.O.E. (MPa) :	20	4441.9	566.05	0.12743	3507.9	5734.1	3502.5
M ult. (Nm) :	19	99.777	7.9306	0.79483E-01	86.692	117.68	84.097
M.O.R. (kPa) :	19	16037.	991.97	0.61855E-01	14400.	17363.	14297.

All perpendicular results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
EI (Nm ²) :	19	142.94	10.858	0.75961E-01	125.03	188.24	127.02
M.O.E. (MPa) :	19	4111.5	392.52	0.95470E-01	3463.8	5266.3	3604.1
M ult. (Nm) :	19	90.834	6.7883	0.74711E-01	79.637	104.48	81.227
M.O.R. (kPa) :	19	14495.	1172.1	0.80860E-01	12561.	16923.	12767.

All parallel and up results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
EI (Nm ²) :	10	155.60	24.128	0.15506	115.79	204.54	114.88
M.O.E. (MPa) :	10	4434.7	823.37	0.14057	3406.1	5734.1	3502.5
M ult. (Nm) :	10	100.86	6.8245	0.68656E-01	89.433	110.79	88.402
M.O.R. (kPa) :	10	16360.	909.71	0.55640E-01	14848.	17363.	14650.

All parallel and down results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
EI (Nm ²) :	10	152.24	15.504	0.10184	126.65	188.11	127.02
M.O.E. (MPa) :	10	4449.1	536.39	0.12056	3564.1	5080.0	3726.1
M ult. (Nm) :	9	98.575	9.1915	0.93243E-01	83.409	117.68	84.097
M.O.R. (kPa) :	9	15690.	1012.3	0.64523E-01	14018.	16987.	14297.

All perpendicular and up results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
EI (Nm ²) :	9	142.69	8.5187	0.59701E-01	128.63	156.90	131.59
M.O.E. (MPa) :	9	4199.6	470.06	0.11193	3424.0	5266.3	3604.1
M ult. (Nm) :	9	92.644	6.4112	0.69203E-01	82.065	103.04	82.948
M.O.R. (kPa) :	9	14995.	1243.1	0.82901E-01	12944.	16923.	13515.

All perpendicular and down results:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
EI (Nm ²) :	10	143.18	13.083	0.91379E-01	121.69	166.24	127.02
M.O.E. (MPa) :	10	4032.2	311.42	0.77235E-01	3518.3	4565.7	3620.0
M ult. (Nm) :	10	89.206	7.0251	0.78751E-01	77.614	104.48	81.227
M.O.R. (kPa) :	10	14045.	947.60	0.67470E-01	12481.	16049.	12767.

Specific Gravity and Moisture Content for Plywood (Vancouver)

The statistics :

Results For All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	40	0.40988	0.20444E-01	0.49867E-01	0.37624	0.47631	0.37835
Moisture Cont. (%)	40	7.5475	1.2375	0.16396	5.5058	10.740	5.3673

Results For Each Group of 10 Panels:

#1 Ten Panels Tested Parallel and Up

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	10	0.42465	0.28718E-01	0.67628E-01	0.37726	0.47631	0.38176
Moisture Cont. (%)	10	8.3668	1.3331	0.15933	5.1672	10.740	5.6838

#2 Ten Panels Tested Perpendicular and Up

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	10	0.41038	0.16816E-01	0.40976E-01	0.36263	0.43392	0.37935
Moisture Cont. (%)	10	7.1120	1.1136	0.15658	5.2745	9.3908	5.6355

#3 Ten Panels Tested Parallel and Down

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	10	0.40461	0.11402E-01	0.28180E-01	0.36580	0.42683	0.39394
Moisture Cont. (%)	10	7.7718	0.72935	0.93848E-01	5.5684	9.1644	5.8865

#4 Ten Panels Tested Perpendicular and Down

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	10	0.40025	0.14055E-01	0.35114E-01	0.37707	0.42903	0.38127
Moisture Cont. (%)	10	6.9400	1.2900	0.18588	4.8115	9.2643	5.3673

Specific Gravity and Moisture Content for Waferboard (Vancouver)

The statistics :

Results For All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	40	0.69107	0.42517E-01	0.61524E-01	0.62091	0.78612	0.61111
Moisture Cont. (%)	40	3.0878	1.1984	0.38748	1.1138	5.7455	1.6216

Results For Each Group of 10 Panels:

#1 Ten Panels Tested Parallel and Up

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	10	0.70571	0.18237E-01	0.25808E-01	0.67682	0.74429	0.68911
Moisture Cont. (%)	10	3.9005	0.79091	0.20277	2.5955	5.7455	2.8834

#2 Ten Panels Tested Perpendicular and Up

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	10	0.66891	0.27223E-01	0.41442E-01	0.61189	0.69746	0.61111
Moisture Cont. (%)	10	2.1858	1.0357	0.47824	0.45672	4.9929	1.6216

#3 Ten Panels Tested Parallel and Down

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	10	0.72571	0.48539E-01	0.64129E-01	0.64892	0.78612	0.65901
Moisture Cont. (%)	10	3.6945	1.0438	0.28253	1.9722	5.6832	1.7591

#4 Ten Panels Tested Perpendicular and Down

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Specific Gravity	10	0.67485	0.37460E-01	0.55500E-01	0.61314	0.74976	0.64507
Moisture Cont. (%)	10	2.5899	1.0256	0.38599	0.89772	4.8780	1.6760

The statistics:

Concentrated Load Test Results for Plywood

Results for All Panels:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	45	5.3272	2.7658	0.51920	0.76354	11.176	0.29210
222.4 N:	45	2.8166	0.37261	0.13228	2.2018	3.8227	2.1844
444.8 N:	45	5.7226	0.94488	0.11269	4.6586	7.2263	4.5466
667.2 N:	45	8.2551	0.92026	0.11133	6.7477	10.312	6.6802
889.6 N:	45	10.580	1.2052	0.11391	8.5916	13.411	8.6487
P ult (N):	45	3229.3	824.87	0.25840	1703.3	5438.6	1707.1
Clip (N):	22	2607.3	467.88	0.17945	2442.7	3394.7	1756.1

Unsupported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	23	4.1634	2.4578	0.59034	0.10803	9.8933	0.29210
222.4 N:	23	2.9903	0.34023	0.11378	2.4280	3.8227	2.4511
444.8 N:	23	5.9966	0.56000	0.93386E-01	5.0726	7.0866	5.0419
667.2 N:	23	8.6164	0.88342	0.10021	7.1818	10.312	7.2888
889.6 N:	23	10.986	1.1979	0.10804	9.0093	13.411	9.2202
P ult (N):	23	3143.5	891.66	0.28365	1672.3	4761.6	1707.1

Supported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	22	6.5440	2.5818	0.39454	2.2839	11.176	2.6924
222.4 N:	22	2.6350	0.31940	0.12121	2.1080	3.8271	2.1844
444.8 N:	22	5.4362	0.61207	0.11258	4.4263	7.2263	4.5466
667.2 N:	22	7.9000	0.84768	0.10730	6.5013	10.312	6.6802
889.6 N:	22	10.156	1.0824	0.10658	8.3703	13.012	8.6487
P ult (N):	22	3319.0	971.00	0.29255	1718.9	5438.6	2047.4
Clip (N):	22	2607.3	467.88	0.17945	2442.7	3394.7	1756.1

Interior:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	23	5.1451	2.3424	0.45526	1.2803	10.592	1.0287
222.4 N:	23	2.7109	0.29970	0.11055	2.2164	3.3731	2.1844
444.8 N:	23	5.4925	0.48886	0.89006E-01	4.8558	6.3881	4.5466
667.2 N:	23	7.7926	0.56330	0.72286E-01	6.8532	8.8214	6.6802
889.6 N:	23	9.8267	0.63852	0.64912E-01	8.7532	11.044	8.6487
P ult (N):	23	3708.6	838.66	0.22814	2324.8	5438.6	1979.4
Clip (N):	11	2974.3	320.66	0.10781	2814.8	3394.7	2105.7

Exterior:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	22	5.5176	3.1948	0.57902	0.24620	11.176	0.29210
222.4 N:	22	2.9271	0.41446	0.14159	2.2433	3.8227	2.3114
444.8 N:	22	5.9632	0.70874	0.11885	4.7938	7.2263	4.8006
667.2 N:	22	8.7613	0.96933	0.11064	7.1619	10.312	7.1120
889.6 N:	22	11.358	1.1738	0.10335	9.4208	13.411	9.0932
P ult (N):	22	2728.2	735.35	0.26954	1514.9	4761.6	1707.1
Clip (N):	11	2240.2	245.86	0.10975	1834.5	2500.2	1756.1

Panel #3 1-4, unsupported, 5-8, supported

All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection							
in mm at :							
33.4 N:	8	4.3386	2.1850	0.50591	0.71694	8.1534	0.29210
222.4 N:	8	2.8956	0.31856	0.11818	2.1699	3.1115	2.1844
444.8 N:	8	5.5277	0.59415	0.10749	4.5473	6.3627	4.5486
667.2 N:	8	8.0169	0.84869	0.10566	6.8165	9.3345	6.6802
889.6 N:	8	10.273	1.0817	0.10530	8.4879	11.874	8.6487
P ult (N):	8	2989.3	829.70	0.27756	1620.3	4267.0	1821.0
Clip (N):	4	2674.1	622.14	0.23265	1647.6	3394.7	1756.1

Supported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection							
in mm at :							
33.4 N:	4	5.5499	1.9528	0.35186	2.3278	8.1534	2.8194
222.4 N:	4	2.4384	0.20080	0.82351E-01	2.1071	2.6924	2.1844
444.8 N:	4	5.0673	0.39247	0.77451E-01	4.4187	5.8134	4.5486
667.2 N:	4	7.4104	0.54042	0.72927E-01	6.5187	8.2042	6.6802
889.6 N:	4	9.6234	0.80363	0.83506E-01	8.2874	10.871	8.6487
P ult (N):	4	3395.5	643.71	0.18956	2333.4	4267.0	2726.4
Clip (N):	4	2674.1	622.14	0.23265	1647.6	3394.7	1756.1

Unsupported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection							
in mm at :							
33.4 N:	4	3.1274	1.6994	0.54341	0.32330	4.4704	0.29210
222.4 N:	4	2.9527	0.17425	0.58012E-01	2.6852	3.1115	2.6670
444.8 N:	4	5.9880	0.35792	0.59772E-01	5.3975	6.3627	5.3975
667.2 N:	4	8.6233	0.64264	0.74523E-01	7.5629	9.3345	7.6708
889.6 N:	4	10.922	0.92256	0.84468E-01	9.3998	11.874	8.8901
P ult (N):	4	2583.1	795.25	0.30787	1927.0	3836.8	1821.0

Panel #4 1-4, unsupported, 5-8, supported

All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection							
in mm at :							
33.4 N:	8	5.1563	2.9580	0.48049	1.2756	11.176	1.2065
222.4 N:	8	2.7241	0.30114	0.11054	2.2273	3.3528	2.4003
444.8 N:	8	5.5626	0.62366	0.11212	4.5336	6.9723	4.8006
667.2 N:	8	8.0407	0.88939	0.11061	6.5732	10.020	7.1120
889.6 N:	8	10.318	1.1849	0.11487	8.3604	12.916	8.0932
P ult (N):	8	2617.5	610.01	0.23305	1611.0	3823.9	1756.1
Clip (N):	4	2359.0	333.30	0.14129	1809.0	2928.1	2105.7

Supported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection							
in mm at :							
33.4 N:	4	5.6738	2.7181	0.40728	2.1890	11.176	4.0513
222.4 N:	4	2.5178	0.15486	0.61507E-01	2.2623	2.7613	2.4003
444.8 N:	4	5.1975	0.32570	0.62664E-01	4.8601	5.8261	4.8006
667.2 N:	4	7.5374	0.40724	0.54029E-01	6.8655	7.9756	7.1120
889.6 N:	4	9.6996	0.47878	0.49464E-01	8.9080	10.376	8.0932
P ult (N):	4	2661.9	347.20	0.13043	2089.0	3221.2	2305.3
Clip (N):	4	2359.0	333.30	0.14129	1809.0	2928.1	2105.7

Unsupported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection							
in mm at :							
33.4 N:	4	5.6388	3.0945	0.54879	0.53285	9.8933	1.2065
222.4 N:	4	2.9305	0.26871	0.91695E-01	2.4871	3.3528	2.6416
444.8 N:	4	5.9277	0.63555	0.10738	4.8774	6.9723	5.3594
667.2 N:	4	8.5439	0.85278	0.11163	6.9702	10.020	7.6835
889.6 N:	4	10.932	1.3488	0.12338	8.7061	12.916	8.6266
P ult (N):	4	2573.2	787.24	0.30594	1823.7	3823.9	1756.1

continued on next page

Concentrated Load Test Results for Waferboard

Panel #1 1-4, unsupported, 5-8, supported

Deflection in mm at various values of load:

33.4 N (7.5 lbs)	222.4 N (50 lbs)	444.8 N (100 lbs)	667.2 N (150 lbs)	889.6 N (200 lbs)	Pult (N)	P clip (N)
6.5532	1.9304	3.8957	6.8040	8.7630	2945.0	0.0
7.0231	2.7859	5.7277	8.6360	11.897	1846.8	0.0
6.0452	2.0320	4.8514	7.7597	10.480	2153.1	0.0
6.2892	2.4892	5.2324	7.8962	10.033	2844.9	0.0
7.2136	1.8383	3.5814	5.7150	7.7724	2060.3	1671.1
9.2328	2.1483	4.5593	6.8929	8.6995	1886.0	1380.2
5.1435	1.7145	3.8227	5.8528	7.9375	1690.7	1501.2
4.6101	1.7907	3.9487	6.0833	8.2931	2105.7	1478.1

Panel #2 1-4, unsupported, 5-8, supported

Deflection in mm at various values of load:

33.4 N (7.5 lbs)	222.4 N (50 lbs)	444.8 N (100 lbs)	667.2 N (150 lbs)	889.6 N (200 lbs)	Pult (N)	P clip (N)
4.9784	1.9304	4.1910	6.3373	8.4201	2241.3	0.0
3.6830	1.4986	3.4798	5.4610	7.5946	2701.7	0.0
5.1181	1.8288	4.1021	6.4843	8.9281	2079.9	0.0
3.4925	2.0701	4.2545	6.2484	8.1407	2548.7	0.0
3.7084	1.3716	3.1242	5.0800	7.0104	1886.0	2031.4
6.5913	1.4361	3.2004	4.8768	6.6329	2306.3	2079.9
6.4008	1.8415	3.7719	5.6642	7.5565	2235.1	1874.2
5.6769	1.4859	3.3401	5.2070	7.0485	1943.8	2209.3

Panel #3 1-4, unsupported, 5-8, supported

Deflection in mm at various values of load:

33.4 N (7.5 lbs)	222.4 N (50 lbs)	444.8 N (100 lbs)	667.2 N (150 lbs)	889.6 N (200 lbs)	Pult (N)	P clip (N)
6.3373	2.2987	4.8895	7.2771	9.7155	1866.4	0.0
7.5057	2.0574	4.5212	6.9723	8.5631	2691.5	0.0
4.0386	2.1082	4.6990	7.2898	9.7282	2073.2	0.0
3.2385	4.3053	6.3627	8.4455	10.490	2416.2	0.0
7.1755	1.2827	2.7559	4.3942	6.1087	2289.8	2118.6
5.3594	1.3970	3.3020	4.9022	6.6548	2354.8	1950.4
5.1816	1.5240	3.4798	5.3875	7.3152	2293.4	1592.8
7.6454	1.4986	3.3655	5.3340	7.2898	2260.9	1723.6

Panel #4 1-4, unsupported, 5-8, supported

Deflection in mm at various values of load:

33.4 N (7.5 lbs)	222.4 N (50 lbs)	444.8 N (100 lbs)	667.2 N (150 lbs)	889.6 N (200 lbs)	Pult (N)	P clip (N)
6.8342	2.2860	4.8280	7.3533	9.5504	1966.5	0.0
6.2484	2.3241	5.0038	7.7878	10.530	2073.2	0.0
4.5893	2.4257	4.8641	7.0231	8.9788	2367.7	0.0
11.125	2.0447	4.3307	6.4516	8.3820	2921.4	0.0
5.7404	1.7907	3.5576	5.7404	-5.7404	1934.4	2095.9
6.2738	1.4478	3.4290	5.3086	7.2390	2070.1	2454.9
7.1120	1.7526	3.9878	6.2230	8.4074	1641.8	1625.3
3.7718	1.5367	3.4417	5.4356	7.5057	2111.9	1950.4

Panel #5 1-4, unsupported, 5-8, supported

Deflection in mm at various values of load:

33.4 N (7.5 lbs)	222.4 N (50 lbs)	444.8 N (100 lbs)	667.2 N (150 lbs)	889.6 N (200 lbs)	Pult (N)	P clip (N)
8.0010	1.6256	2.2088	3.5814	5.5118	2632.8	0.0
9.3726	1.3462	3.2512	4.7498	6.8226	2629.7	0.0
6.4770	2.3368	5.3340	8.3820	11.252	2118.6	0.0
3.5814	2.4892	5.4102	7.8740	10.338	2184.0	0.0
6.8580	1.4478	3.4290	5.4356	7.3406	1882.4	2083.0
3.3020	1.4986	3.4798	5.4102	7.2544	2409.5	1853.5
9.7028	1.8542	4.1148	6.3246	8.3820	1891.2	1366.9
6.2992	1.9304	4.2672	6.4770	8.5868	1599.5	1429.1

The statistics:

Concentrated Load Test Results for Waferboard

Results for All Panels:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	80	4.5514	3.1042	0.66738	-0.47062	13.540	0.38100E-01
222.4 N:	80	1.8156	0.47148	0.25970	1.0376	4.3053	0.62230
444.8 N:	80	4.1308	0.82092	0.19873	2.7783	6.3627	1.9558
667.2 N:	80	6.3377	1.1196	0.17665	4.4905	8.6360	2.9464
889.6 N:	78	8.4826	1.3221	0.15586	6.3011	11.697	4.8133
P ult (N):	80	2172.2	334.02	0.15377	1621.1	3128.3	1592.8
Clip (N):	40	1758.4	245.32	0.13951	1694.4	2454.9	1366.9

Unsupported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	40	4.5841	3.1259	0.68190	-0.57361	13.540	0.27940
222.4 N:	40	1.9818	0.53585	0.27039	1.0876	4.3053	0.92710
444.8 N:	40	4.4251	0.80060	0.18092	3.1041	6.3627	2.2098
667.2 N:	40	6.7867	1.0852	0.15989	4.9862	8.6360	3.5814
889.6 N:	40	9.0399	1.3037	0.14422	6.8888	11.697	5.5118
P ult (N):	40	2341.2	336.26	0.14320	1788.0	3128.3	1768.4

Supported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	40	4.7187	3.1208	0.66136	-0.43053	10.541	0.38100E-01
222.4 N:	40	1.8493	0.32836	0.19787	1.1108	2.1844	0.62230
444.8 N:	40	3.8366	0.73932	0.19270	2.8187	6.2992	1.9558
667.2 N:	40	5.8889	0.87365	0.14934	4.2823	8.3820	2.9464
889.6 N:	38	7.9110	1.0889	0.13739	6.1176	10.439	4.8133
P ult (N):	40	2003.2	234.56	0.11709	1616.2	2408.5	1592.8
Clip (N):	40	1758.4	245.32	0.13951	1694.4	2454.9	1366.9

Interior:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	40	4.4391	3.0775	0.69327	-0.63878	11.125	0.38100E-01
222.4 N:	40	1.8583	0.54908	0.29547	0.95230	4.3053	0.92710
444.8 N:	40	4.1013	0.82337	0.20076	2.7428	6.3627	1.9558
667.2 N:	40	6.2035	1.0817	0.17437	4.4187	8.4455	2.9464
889.6 N:	40	8.2456	1.2048	0.14612	6.2577	10.490	4.8133
P ult (N):	40	2237.3	361.53	0.17053	1807.8	3128.3	1641.8
Clip (N):	20	1758.7	252.77	0.14405	1661.5	2454.9	1366.9

Exterior:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	40	4.8638	3.1554	0.64875	-0.34256	13.540	0.35560
222.4 N:	40	1.7728	0.38092	0.21487	1.1443	2.7559	0.62230
444.8 N:	40	4.1603	0.82789	0.19900	2.7943	6.2992	2.4892
667.2 N:	40	6.4721	1.1541	0.17831	4.5879	8.6360	4.3842
889.6 N:	38	8.7256	1.4066	0.16120	6.4048	11.697	6.1087
P ult (N):	40	2107.1	257.85	0.12712	1665.2	2701.7	1592.8
Clip (N):	20	1762.1	244.15	0.13856	1359.2	2209.3	1429.1

Panel #3 1-4, unsupported, 5-8, supported

All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	8	5.8102	1.5303	0.26338	3.2852	7.8454	3.2385
222.4 N:	8	2.0590	0.81835	0.44802	0.54371	4.3053	1.2827
444.8 N:	8	4.1719	1.0858	0.26265	2.3639	6.3827	2.7559
667.2 N:	8	6.2516	1.3372	0.21390	4.0452	8.4455	4.3942
889.6 N:	8	8.3582	1.5775	0.18873	5.7553	10.490	6.1087
P ult (N):	8	2260.8	225.81	0.99007E-01	1908.2	2891.5	1886.4
Clip (N):	4	1846.4	202.66	0.10976	1512.0	2118.6	1592.8

Supported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	4	6.3405	1.0846	0.17106	4.5508	7.8454	5.1816
222.4 N:	4	1.4266	0.95198E-01	0.66779E-01	1.2685	1.5240	1.2827
444.8 N:	4	3.2258	0.27868	0.85390E-01	2.7680	3.4788	2.7559
667.2 N:	4	5.0070	0.40185	0.80258E-01	4.3439	5.3975	4.3942
889.6 N:	4	6.8421	0.49930	0.72975E-01	6.0183	7.3152	6.1087
P ult (N):	4	2299.7	34.183	0.14864E-01	2243.3	2354.8	2260.9
Clip (N):	4	1846.4	202.66	0.10976	1512.0	2118.6	1592.8

Unsupported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	4	5.2800	1.7161	0.32502	2.4434	7.5057	3.2385
222.4 N:	4	2.6924	0.93554	0.34748	1.1438	4.3053	2.0574
444.8 N:	4	5.1181	0.73028	0.14269	3.9131	6.3827	4.5212
667.2 N:	4	7.4962	0.56264	0.75057E-01	6.5678	8.4455	6.9723
889.6 N:	4	9.8742	0.36151	0.36611E-01	9.2778	10.490	9.5631
P ult (N):	4	2261.8	316.38	0.13988	2000.8	2891.5	1886.4

Panel #4 1-4, unsupported, 5-8, supported

All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	8	6.4706	2.0570	0.31789	3.0766	11.125	3.7719
222.4 N:	8	1.9510	0.34819	0.17898	1.3749	2.4257	1.4478
444.8 N:	8	4.1926	0.61281	0.14617	3.1814	5.0038	3.4290
667.2 N:	8	6.4167	0.85432	0.13314	5.0070	7.7878	5.3086
889.6 N:	7	8.6705	1.0867	0.12534	6.8774	10.630	7.2390
P ult (N):	8	2135.9	352.33	0.16496	1654.5	2921.4	1641.8
Clip (N):	4	2031.6	297.88	0.14662	1540.1	2454.9	1625.3

Supported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	4	5.7245	1.2288	0.21465	3.6970	7.1120	3.7719
222.4 N:	4	1.5319	0.14382	0.88130E-01	1.3848	1.7907	1.4478
444.8 N:	4	3.6290	0.22618	0.62326E-01	3.2558	3.8878	3.4290
667.2 N:	4	5.6789	0.35218	0.62038E-01	5.0958	6.2230	5.3086
889.6 N:	3	7.7174	0.49983	0.64780E-01	6.8925	8.4074	7.2390
P ult (N):	4	1939.5	184.02	0.94879E-01	1635.8	2111.9	1641.8
Clip (N):	4	2031.6	297.88	0.14662	1540.1	2454.9	1625.3

Unsupported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at :							
33.4 N:	4	7.2168	2.4164	0.33483	3.2287	11.125	4.5593
222.4 N:	4	2.2701	0.13881	0.61586E-01	2.0394	2.4257	2.0447
444.8 N:	4	4.7561	0.25440	0.53488E-01	4.3384	5.0038	4.3307
667.2 N:	4	7.1564	0.49109	0.68623E-01	6.3461	7.7878	6.4516
889.6 N:	4	9.3853	0.82886	0.88315E-01	8.0177	10.630	6.3820
P ult (N):	4	2332.2	370.58	0.15680	2026.5	2921.4	1866.5

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Panel #7 1-4, unsupported, 5-8, supported

All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at:							
33.4 N:	8	1.8256	1.5848	0.86263	-0.95639	5.0038	0.38100E-01
222.4 N:	8	1.5700	0.47484	0.30231	0.78889	2.0574	0.62230
444.8 N:	8	3.9973	0.81085	0.20280	2.8597	4.9887	2.4882
667.2 N:	8	8.1755	1.1174	0.13685	4.3348	7.8867	4.4577
889.6 N:	8	8.3518	1.3790	0.16511	6.0765	10.516	6.5405
P ult (N):	8	2196.6	383.28	0.17448	1564.2	3128.3	1837.0
Clip (N):	4	1759.4	187.82	0.10675	1448.5	1988.9	1494.5

Supported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at:							
33.4 N:	4	0.87630	0.66907	0.76352	-0.22767	1.7018	0.38100E-01
222.4 N:	4	1.2859	0.49288	0.38331	0.47262	1.8034	0.62230
444.8 N:	4	3.4163	0.72528	0.21230	2.2195	4.2164	2.4892
667.2 N:	4	5.4229	0.78960	0.14560	4.1201	8.2982	4.4577
889.6 N:	4	7.4612	0.88247	0.11827	6.0052	8.5344	6.5405
P ult (N):	4	1987.5	175.57	0.88337E-01	1697.8	2286.7	1837.0
Clip (N):	4	1759.4	187.82	0.10675	1448.5	1988.9	1494.5

Unsupported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at:							
33.4 N:	4	2.3749	1.8240	0.76803	-0.63468	5.0038	0.27940
222.4 N:	4	1.8542	0.21478	0.11583	1.4988	2.0574	1.5240
444.8 N:	4	4.5783	0.33631	0.73457E-01	4.0234	4.9657	4.1783
667.2 N:	4	6.9342	0.85539	0.12336	5.5228	7.8867	5.9309
889.6 N:	4	9.2424	1.1982	0.12975	7.2637	10.516	7.9758
P ult (N):	4	2405.8	418.91	0.17412	2060.2	3128.3	2118.6

Panel #8 1-4, unsupported, 5-8, supported

All Tests:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at:							
33.4 N:	8	1.1128	0.93061	0.83625	-0.42268	2.8448	0.35560
222.4 N:	8	1.8669	0.20218	0.12129	1.3333	1.9812	1.2573
444.8 N:	8	3.9624	0.39727	0.10026	3.3069	4.4450	3.1877
667.2 N:	8	6.1849	0.45485	0.73557E-01	5.4342	8.8326	5.6261
889.6 N:	8	8.2836	0.51087	0.60837E-01	7.5408	9.2984	7.7470
P ult (N):	8	2167.5	337.84	0.15578	1610.3	2888.1	1739.6
Clip (N):	4	1666.1	135.08	0.81078E-01	1443.2	1886.0	1527.4

Supported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at:							
33.4 N:	4	1.0541	0.87002	0.82537	-0.38143	2.5146	0.35560
222.4 N:	4	1.7621	0.14124	0.80155E-01	1.5291	1.9812	1.8002
444.8 N:	4	4.1053	0.30445	0.74161E-01	3.6029	4.4450	3.7592
667.2 N:	4	6.3182	0.49134	0.77785E-01	5.5075	8.8326	5.7658
889.6 N:	4	8.4836	0.64182	0.75654E-01	7.4245	9.2984	7.7470
P ult (N):	4	1994.8	247.88	0.12425	1585.8	2403.3	1739.6
Clip (N):	4	1666.1	135.08	0.81078E-01	1443.2	1886.0	1527.4

Unsupported:

	#	Average	Std. Dev.	Coef. of Var.	5% Ex Lt	Maximum	Minimum
Deflection in mm at:							
33.4 N:	4	1.1716	0.84400	0.83989	-0.45202	2.8448	0.38100
222.4 N:	4	1.5716	0.20895	0.13295	1.2269	1.8415	1.2573
444.8 N:	4	3.8195	0.42676	0.11173	3.1154	4.2418	3.1877
667.2 N:	4	6.0515	0.37010	0.61158E-01	5.4409	8.5024	5.6261
889.6 N:	4	8.2836	0.30005	0.36222E-01	7.7885	8.7376	7.9502
P ult (N):	4	2340.1	327.04	0.13975	2070.3	2888.1	2047.4

continued on next page

Appendix B

This appendix contains the computer programs used to calculate material properties and perform statistical analysis.


```
C      This program was written to manipulate data from small
C      scale flexural tests performed on plywood and waferboard
C      specimens.
C
C      The data file should be set up as follows:
C
C      1.  MAIN TITLE
C      2.  T, NPOINTS, SKIP
C          NOTE: NPOINTS will default to 120 if left blank,
C              and if all the values are parallel, let
C              SKIP be equal to one. Otherwise, leave it
C              blank.
C      3.  First group of 6 title
C      4.  Dbar, Bbar, Pult, P/y
C      5.-8. Repeat line 4.
C          NOTE: Repeat lines 3 - 8 for as many groups of
C              6 as you have. If you have less than
C              20, change NPOINTS, and if you have more
C              than 20, change the dimensioning of the
C              vectors and arrays.
C
C      Dimension the various vectors and arrays. They are thus:
C
C      DBAR - - The average d.
C      BBAR - - The average b.
C      PULT - - The ultimate load.
C      POVERY - The slope of the load deflection curve,
C              i.e., P/y.
C      MOE - - The modulus of Elasticity.
C      MDR - - The modulus of Rupture.
C      TITLE - The overall title for the run.
C      TITLEA - The titles of the groups of six. Each line
C              is one title.
C
C      REAL DBAR(120), BBAR(120), PULT(120), POVERY(120),
C      * MOE(120), MDR(120), TITLE(30), TITLEA(20,30)
C
C      Define some logical (T/F) indicators for later.
C      PARA is true for parallel values, DOWN true for down
C      values, and POPPAR will be true if there are no
C      parallel values, and POPPER if there are no perpendicular
C      values. This is the case for plywood. To set POPPER
C      to be true (for plywood), let SKIP (from the third line
C      of the data file) be greater than zero. i.e., let SKIP=1.
C
C      LOGICAL*1 PARA /.FALSE./, DOWN /.TRUE./, POPPER /.FALSE./,
C      * POPPAR /.FALSE./
C
C      Read in the main title and the wood thickness. ELL
C      is the length of the specimens, and is equal to 24 T.
C
C      READ(5,500)(TITLE(I),I=1,20)
C      FORMAT(30A4)
C      CALL FREAD(5,'R,2I:',T,NPOINT,SKIP)
C
C      We assign the number of points to be equal to 120,
C      but we can assign some other number if necessary.
C
C      IF(NPOINT.LE.0)NPOINT = 120
C
C      N6 is the number of groups of 6.
C
C      N6 = NPOINT / 6
C
C      Decide whether everything is parallel. By default, it
C      is not.
C
C      IF(SKIP.GT.0)POPPER = .TRUE.
C
C      Find the length.
C
C      ELL = 24. * T
C
C      Read in the first group of 6 title:
C
C      READ(5,500)(TITLEA(I,J),J=1,20)
C
C      The loop will read in all the other data, and do
C      some calculations for M.O.E. and M.O.R.
C
C      DO 10 I=1,NPOINT
C
C          Find out when 5 READ statements have gone by, in order
C          that we may read in another group of 6 title.
C
C          A = I / 6
C          I6 = A * 6
C          NTIT = I6 / 6 + 1
C
C          Read in the information.
C
C          CALL FREAD(5,'4R:',DBAR(I),BBAR(I),PULT(I),POVERY(I))
C
C          If 6 READ statements have gone by, read in a new title.
C          NTIT is the title number.
C
C          IF(NTIT.GT.N6)GOTO 11
C          IF(I6.EQ.I)READ(5,500)(TITLEA(NTIT,J),J=1,20)
C          CONTINUE
C
C      11
C
```

```
C
PEDEMx = -1E10
PEDEMN = 1E10
PEDRMx = -1E10
PEDRMN = 1E10
PEDPMx = -1E10
PEDPMN = 1E10
C
PAAEMx = -1E10
PAAEMN = 1E10
PAARMx = -1E10
PAARMN = 1E10
PAAPMx = -1E10
PAAPMN = 1E10
C
PEAEMx = -1E10
PEAEMN = 1E10
PEARMx = -1E10
PEARMN = 1E10
PEAPMx = -1E10
PEAPMN = 1E10
EVEEMx = -1E10
EVEEMN = 1E10
EVERMx = -1E10
EVERMN = 1E10
EVEPMx = -1E10
EVEPMN = 1E10
C
C C C C
      And now start a DO loop to calculate the maximum and
      minimum values.
C C C C
DO 20 I=1,NPOINT
C C C C
      First, see if the range is parallel, and set a T/F
      indicator.
C C C C
      II = I - 1
      IAS = II / 6
      IAS2 = IAS / 2
      IAS22 = IAS2 * 2
      PARA = .FALSE.
      IF(IAS22.EQ.IAS)PARA = .TRUE.
C C C C
      And next, whether it is odd or even.
C C C C
      IO2 = I / 2
      IO22 = IO2 * 2
      DOWN = .FALSE.
      IF(IO22.EQ.I)DOWN = .TRUE.
C C C C
      Having established line ranges, check out what to do.
      IS refers to the group of six, I2 to alternating values.
C C C C
      IF PARA and DOWN, refers to PARDN
      IF PARA and not DOWN, refers to PARUP
      IF not PARA and DOWN, refers to PERDN
      IF not PARA and not DOWN, refers to PERUP
      IF PARA, refers to PARAL
      IF not PARA, refers to PERAL
C C C C
      Now find the maximum and minimum values.
C C C C
      If everything is parallel (POPPER = .TRUE.) then make
      sure PARA is .TRUE.
C C C C
      IF(POPPER) PARA = .TRUE.
C C C C
      Get the various values.
C C C C
      IF(MDE(I).LE.O.O)GOTO 800
      IEVER1 = IEVER1 + 1
      EVERYE = EVERYE + MOE(I)
      IF( MOE(I).GT.EVEEMX)EVEEMX = MOE(I)
      IF( MOE(I).LT.EVEEMN)EVEEMN = MOE(I)
800 CONTINUE
      IF(PULT(I).LE.O.O)GOTO 810
      IEVER2 = IEVER2 + 1
      EVERYP = EVERYP + PULT(I)
      IF(PULT(I).GT.EVEPMX)EVEPMX = PULT(I)
      IF(PULT(I).LT.EVEPMN)EVEPMN = PULT(I)
810 CONTINUE
      IF(MDR(I).LE.O.O)GOTO 820
      IEVER3 = IEVER3 + 1
      EVERYR = EVERYR + MOR(I)
      IF(MDR(I).GT.EVERMX)EVERMX = MOR(I)
      IF(MDR(I).LT.EVERMN)EVERMN = MOR(I)
820 CONTINUE
      IF(PARA)GOTO 31
      IF(MOE(I).LE.O.O)GOTO 80
      IPERP1 = IPERP1 + 1
      PERALE = PERALE + MOE(I)
      IF( MOE(I).GT.PEAEMX)PEAEMX = MOE(I)
      IF( MOE(I).LT.PEAEMN)PEAEMN = MOE(I)
80 CONTINUE
      IF(PULT(I).LE.O.O)GOTO 81
      IPERP2 = IPERP2 + 1
      PERALP = PERALP + PULT(I)
      IF(PULT(I).GT.PEAPMX)PEAPMX = PULT(I)
      IF(PULT(I).LT.PEAPMN)PEAPMN = PULT(I)
81 CONTINUE
```

```
GOTO 40
C
C      Perpendicular and down.
C
43  CONTINUE
    IF(MOE(I).LE.0.0)GOTO 95
    IPERD1 = IPERD1 + 1
    PERDNE = PERDNE + MOE(I)
    IF( MOE(I).GT.PEDEMNX)PEDEMNX = MOE(I)
    IF( MOE(I).LT.PEDEMNX)PEDEMNX = MOE(I)
95  CONTINUE
    IF(PULT(I).LE.0.0)GOTO 96
    IPERD2 = IPERD2 + 1
    PERDNP = PERDNP + PULT(I)
    IF(PULT(I).GT.PEDPMNX)PEDPMNX = PULT(I)
    IF(PULT(I).LT.PEDPMNX)PEDPMNX = PULT(I)
96  CONTINUE
    IF(MOR(I).LE.0.0)GOTO 97
    IPERD3 = IPERD3 + 1
    PERDNR = PERDNR + MOR(I)
    IF( MOR(I).GT.PEDRMNX)PEDRMNX = MOR(I)
    IF( MOR(I).LT.PEDRMNX)PEDRMNX = MOR(I)
97  CONTINUE
40  CONTINUE
20  CONTINUE
C
C      Initialize the averages.  If any is not changed, then
C      it will have a value of -0.0.
C
PARAVE = -0.0
PARAVP = -0.0
PARAVR = -0.0
PERAVE = -0.0
PERAVP = -0.0
PERAVR = -0.0
PAUAVE = -0.0
PAUAVP = -0.0
PAUAVR = -0.0
PADAVE = -0.0
PADAVP = -0.0
PADAVR = -0.0
PEUAVE = -0.0
PEUAVP = -0.0
PEUAVR = -0.0
PEDAVE = -0.0
PEDAVP = -0.0
PEDAVR = -0.0
EVEAVE = -0.0
EVEAVP = -0.0
EVEAVR = -0.0
C
C      Calculate the averages.  If any counter is equal to zero,
C      i.e., no values have been read, skip over it.
C
C      Everything
C
IF(IEVER1.LE.0)GOTO 1001
EVEAVE = EVERVE / IEVER1
1001 CONTINUE
IF(IEVER2.LE.0)GOTO 1011
EVEAVP = EVERVP / IEVER2
1011 CONTINUE
IF(IEVER3.LE.0)GOTO 1021
EVEAVR = EVERVR / IEVER3
1021 CONTINUE
C
C      All the parallel.
C
IF(IPARA1.LE.0)GOTO 100
PARAVE = PARALE / IPARA1
100  CONTINUE
IF(IPARA2.LE.0)GOTO 101
PARAVP = PARALP / IPARA2
101  CONTINUE
IF(IPARA3.LE.0)GOTO 102
PARAVR = PARALR / IPARA3
102  CONTINUE
C
C      All the perpendicular.
C
IF(IPERP1.LE.0)GOTO 103
PERAVE = PERALE / IPERP1
103  CONTINUE
IF(IPERP2.LE.0)GOTO 104
PERAVP = PERALP / IPERP2
104  CONTINUE
IF(IPERP3.LE.0)GOTO 105
PERAVR = PERALR / IPERP3
105  CONTINUE
C
C      All the parallel and up.
C
IF(IPARU1.LE.0)GOTO 106
PAUAVE = PARUPE / IPARU1
106  CONTINUE
IF(IPARU2.LE.0)GOTO 107
PAUAVP = PARUPP / IPARU2
107  CONTINUE
IF(IPARU3.LE.0)GOTO 108
```

```
C
C   If everything is parallel (POPPER = .TRUE.) then make
C   sure PARA is .TRUE.
C
C   IF(POPPER) PARA = .TRUE.
C
C   Everything
C
C   IF(MOE(I).LE.O.O)GOTO 1801
1801  EVEES = EVEES + (( MOE(I) - EVEAVE)**2)
      CONTINUE
      IF(PULT(I).LE.O.O)GOTO 1811
      EVEPS = EVEPS + ((PULT(I) - EVEAVP)**2)
1811  CONTINUE
      IF(MOR(I).LE.O.O)GOTO 1821
      EVERS = EVERS + (( MOR(I) - EVEAVR)**2)
1821  CONTINUE
C
C   All Perpendicular.
C
C   IF(PARA)GOTO 131
      IF(MOE(I).LE.O.O)GOTO 180
      PEAES = PEAES + (( MOE(I) - PERAVE)**2)
180  CONTINUE
      IF(PULT(I).LE.O.O)GOTO 181
      PEAPS = PEAPS + ((PULT(I) - PERAVP)**2)
181  CONTINUE
      IF(MOR(I).LE.O.O)GOTO 182
      PEARS = PEARS + (( MOR(I) - PERAVR)**2)
182  CONTINUE
      GOTO 130
C
C   All Parallel.
C
131  CONTINUE
      IF(MOE(I).LE.O.O)GOTO 183
      PAAES = PAAES + (( MOE(I) - PARAVE)**2)
183  CONTINUE
      IF(PULT(I).LE.O.O)GOTO 184
      PAAPS = PAAPS + ((PULT(I) - PARAVP)**2)
184  CONTINUE
      IF(MOR(I).LE.O.O)GOTO 185
      PAARS = PAARS + (( MOR(I) - PARAVR)**2)
185  CONTINUE
130  CONTINUE
C
C   And now for the quantities involving multiple IF's.
C
C   IF(PARA.AND.DOWN)GOTO 141
C   IF(.NOT.DOWN.AND.PARA)GOTO 142
C   IF(.NOT.PARA.AND.DOWN)GOTO 143
C
C   Perpendicular and up.
C
C   IF(MOE(I).LE.O.O)GOTO 186
186  PEUES = PEUES + (( MOE(I) - PEUAVE)**2)
      CONTINUE
      IF(PULT(I).LE.O.O)GOTO 187
      PEUPS = PEUPS + ((PULT(I) - PEUAVP)**2)
187  CONTINUE
      IF(MOR(I).LE.O.O)GOTO 188
      PEURS = PEURS + (( MOR(I) - PEUAVR)**2)
188  CONTINUE
      GOTO 140
C
C   Parallel and down.
C
141  CONTINUE
      IF(MOE(I).LE.O.O)GOTO 189
      PADES = PADES + (( MOE(I) - PADAVE)**2)
189  CONTINUE
      IF(PULT(I).LE.O.O)GOTO 190
      PADPS = PADPS + ((PULT(I) - PADAVP)**2)
190  CONTINUE
      IF(MOR(I).LE.O.O)GOTO 191
      PADRS = PADRS + (( MOR(I) - PADAVR)**2)
191  CONTINUE
      GOTO 140
C
C   Parallel and up.
C
142  CONTINUE
      IF(MOE(I).LE.O.O)GOTO 192
      PAUES = PAUES + (( MOE(I) - PAUAVE)**2)
192  CONTINUE
      IF(PULT(I).LE.O.O)GOTO 193
      PAUPS = PAUPS + ((PULT(I) - PAUAVP)**2)
193  CONTINUE
      IF(MOR(I).LE.O.O)GOTO 194
      PAURS = PAURS + (( MOR(I) - PAUAVR)**2)
194  CONTINUE
      GOTO 140
C
C   Perpendicular and down.
C
143  CONTINUE
      IF(MOE(I).LE.O.O)GOTO 195
      PEDES = PEDES + (( MOE(I) - PEDAVE)**2)
195  CONTINUE
      IF(PULT(I).LE.O.O)GOTO 196
```

```
EVERCO = EVERSD / EVEAVR
AN = FLOAT(EVERS)
EVERSP = EVEAVR - (1.650 * (EVERSD ))
902 CONTINUE
C
C      All the parallel.
C
IF(IPARA1.LE.0)GOTO 1100
PAESD = SORT(PAAS / (IPARA1-1))
PAECC = PAESD / PARAVE
AN = FLOAT(IPARA1)
PAESP = PARAVE - (1.650 * (PAESD ))
1100 CONTINUE
IF(IPARA2.LE.0)GOTO 1101
PAAPSD = SORT(PAAPS / (IPARA2-1))
PAAPCC = PAAPSD / PARAVP
AN = FLOAT(IPARA2)
PAAPSP = PARAVP - (1.650 * (PAAPSD ))
1101 CONTINUE
IF(IPARA3.LE.0)GOTO 1102
PAARSD = SORT(PAARS / (IPARA3-1))
PAARCC = PAARSD / PARAVR
AN = FLOAT(IPARA3)
PAARSP = PARAVR - (1.650 * (PAARSD ))
1102 CONTINUE
C
C      All the perpendicular.
C
IF(IPERP1.LE.0)GOTO 1103
PEAESD = SORT(PEAES / (IPERP1-1))
PEAECC = PEAESD / PERAVE
AN = FLOAT(IPERP1)
PEAESP = PERAVE - (1.650 * (PEAESD ))
1103 CONTINUE
IF(IPERP2.LE.0)GOTO 1104
PEAPSD = SORT(PEAPS / (IPERP2-1))
PEAPCC = PEAPSD / PERAVP
AN = FLOAT(IPERP2)
PEAPSP = PERAVP - (1.650 * (PEAPSD ))
1104 CONTINUE
IF(IPERP3.LE.0)GOTO 1105
PEARSD = SORT(PEARS / (IPERP3-1))
PEARCC = PEARSD / PERAVR
AN = FLOAT(IPERP3)
PEARSP = PERAVR - (1.650 * (PEARSD ))
1105 CONTINUE
C
C      All the parallel and up.
C
IF(IPARU1.LE.0)GOTO 1106
PAUESD = SORT(PAUES / (IPARU1-1))
PAUECC = PAUESD / PAUAVE
AN = FLOAT(IPARU1)
PAUESP = PAUAVE - (1.650 * (PAUESD ))
1106 CONTINUE
IF(IPARU2.LE.0)GOTO 1107
PAUPSD = SORT(PAUPS / (IPARU2-1))
PAUPCC = PAUPSD / PAUAVP
AN = FLOAT(IPARU2)
PAUPSP = PAUAVP - (1.650 * (PAUPSD ))
1107 CONTINUE
IF(IPARU3.LE.0)GOTO 1108
PAURSD = SORT(PAURS / (IPARU3-1))
PAURCC = PAURSD / PAUAVR
AN = FLOAT(IPARU3)
PAURSP = PAUAVR - (1.650 * (PAURSD ))
1108 CONTINUE
C
C      All the perpendicular and up.
C
IF(IPERU1.LE.0)GOTO 1109
PEUESD = SORT(PEUES / (IPERU1-1))
PEUECC = PEUESD / PEUAVE
AN = FLOAT(IPERU1)
PEUESP = PEUAVE - (1.650 * (PEUESD ))
1109 CONTINUE
IF(IPERU2.LE.0)GOTO 1110
PEUPSD = SORT(PEUPS / (IPERU2-1))
PEUPCC = PEUPSD / PEUAVP
AN = FLOAT(IPERU2)
PEUPSP = PEUAVP - (1.650 * (PEUPSD ))
1110 CONTINUE
IF(IPERU3.LE.0)GOTO 1111
PEURSD = SORT(PEURS / (IPERU3-1))
PEURCC = PEURSD / PEUAVR
AN = FLOAT(IPERU3)
PEURSP = PEUAVR - (1.650 * (PEURSD ))
1111 CONTINUE
C
C      All the parallel and down.
C
IF(IPARD1.LE.0)GOTO 1112
PAESD = SORT(PADES / (IPARD1-1))
PADECC = PAESD / PADAVE
AN = FLOAT(IPARD1)
PADESP = PADAVE - (1.650 * (PAESD ))
1112 CONTINUE
IF(IPARD2.LE.0)GOTO 1113
PADPSD = SORT(PADPS / (IPARD2-1))
PADPCO = PADPSD / PADAVP
```

```
* IEVER3, EYEAVR, EYERSD, EVERCO, EVERSP, EVERMX, EVERMN
632 FORMAT(20X, 'M.O.E. (GPa) ', I3, 6(2X, G12.5)/
* 20X, 'P ul t (N) ', I3, 6(2X, G12.5)/
* 20X, 'M.O.R. (MPa) ', I3, 6(2X, G12.5)/)
WRITE(6, 621)
621 FORMAT(////20X, 'All parallel results:')
WRITE(6, 666)
WRITE(6, 622) IPARA1, PARAVE, PAESD, PAECO, PAESP,
* PAEMX, PAEMN, IPARA2, PARAVP,
* PAAPSD, PAAPCO, PAAPSP, PAAPMX, PAAPMN,
* IPARA3, PARAVR, PAARSD, PAARCO, PAARSP, PAARMX, PAARMN
622 FORMAT(20X, 'M.O.E. (GPa) ', I3, 6(2X, G12.5)/
* 20X, 'P ul t (N) ', I3, 6(2X, G12.5)/
* 20X, 'M.O.R. (MPa) ', I3, 6(2X, G12.5)/)
IF (POPPER) GO TO 630
WRITE(6, 623)
623 FORMAT(////20X, 'All perpendicular results:')
WRITE(6, 666)
WRITE(6, 622) IPERP1, PERAVE, PEASD, PEACO, PEASP,
* PEAMX, PAEMN, IPERP2, PERAVP,
* PEAPSD, PEAPCO, PEAPSP, PEAPMX, PEAPMN,
* IPERP3, PERAVR, PEARSD, PEARCO, PEARSP, PEARMX, PEARMN
630 CONTINUE
WRITE(6, 624)
624 FORMAT(////20X, 'All parallel and up results:')
WRITE(6, 666)
WRITE(6, 622) IPARU1, PAUAVE, PAUESD, PAUECO, PAUESP,
* PAUEMX, PAUEMN, IPARU2, PAUAVP,
* PAUPSD, PAUPCO, PAUPSP, PAUPMX, PAUPMN,
* IPARU3, PAUAVR, PAURSD, PAURCO, PAURSP, PAURMX, PAURMN
WRITE(6, 625)
625 FORMAT(////20X, 'All parallel and down results:')
WRITE(6, 666)
WRITE(6, 622) IPARD1, PADAVE, PADES, PADECO, PADESP,
* PADEM, PADEM, IPARD2, PADAVP,
* PADPSD, PADPCO, PADPSP, PADPMX, PADPMN,
* IPARD3, PADAVR, PADRS, PADRCO, PADRSP, PADRMX, PADRMN
IF (POPPER) GO TO 651
WRITE(6, 626)
626 FORMAT(////20X, 'All perpendicular and up results:')
WRITE(6, 666)
WRITE(6, 622) IPERU1, PAUAVE, PEUESD, PEUECO, PEUESP,
* PEUEMX, PEUEMN, IPERU2, PAUAVP,
* PEUPSD, PEUPCO, PEUPSP, PEUPMX, PEUPMN,
* IPERU3, PAUAVR, PEURSD, PEURCO, PEURSP, PEURMX, PEURMN
WRITE(6, 627)
627 FORMAT(////20X, 'All perpendicular and down results:')
WRITE(6, 666)
WRITE(6, 622) IPERD1, PEDAVE, PEDES, PEDECO, PEDESP,
* PEDEM, PEDEM, IPERD2, PEDAVP,
* PEDPSD, PEDPCO, PEDPSP, PEDPMX, PEDPMN,
* IPERD3, PEDAVR, PEDRS, PEDRCO, PEDRSP, PEDRMX, PEDRMN
651 CONTINUE
99999 CONTINUE
STOP
END
```

```
C
12 CONTINUE
CALL FREAD(5,'4R:',LENGTH(I),AREAGR(I),PULT(I),POVERY(I))
13 CONTINUE
C
C If 6 READ statements have gone by, read in a new title.
C Unless, of course, it is the last one, in which case, don't.
C NTIT is the title number.
C
11 IF(NTIT.GT.N6)GOTO 11
IF(16.EQ.I)READ(6,500)(TITLEA(NTIT,J),J=1,20)
CONTINUE
C
C And calculate the M.O.E's and stress quantities.
C
SIGGR(I) = PULT(I) / AREAGR(I)
MOEGR(I) = POVERY(I) * LENGTH(I) / AREAGR(I)
IF(WAFER) GOTO 14
SIGPAR(I) = PULT(I) / AREAPA(I)
MOEPAR(I) = POVERY(I) * LENGTH(I) / AREAPA(I)
14 CONTINUE
10 CONTINUE
C
C And now calculate the averages.
C
C Getting some things straight:
C
C For I = 4, 10, 16, ... it is perpendicular.
C For I = 1, 7, 13, ... it is parallel.
C
C We want the average of:
C
C a) sigma parallel (name) SIGP
C b) sigma gross SIGG
C c) M.O.E. parallel MOEP
C d) M.O.E. gross MOEG
C e) PULT PULT
C
C with PA,PE,TO endings to establish whether they are
C parallel, perpendicular, or total quantities. The 'gross'
C quantities (SIGG, MOEG) will be use for the waferboard,
C along with PULT.
C
C Initialize these quantities. These will be divided by
C the counters to find the averages.
C
SIGPPA = 0.0
SIGPPE = 0.0
SIGPTO = 0.0
SIGGPA = 0.0
SIGGPE = 0.0
SIGGTO = 0.0
MOEPPA = 0.0
MOEPPE = 0.0
MOEPTO = 0.0
MOEGPA = 0.0
MOEGPE = 0.0
MOEGTO = 0.0
PULTPA = 0.0
PULTPE = 0.0
PULTTO = 0.0
C
C And initialize some counter quantities. These are needed
C to find the averages.
C
ISIGPT = 0
ISIGPP = 0
ISIGPE = 0
ISIGGT = 0
ISIGGP = 0
ISIGGE = 0
IMOEPT = 0
IMOEPP = 0
IMOEPE = 0
IMOEGT = 0
IMOEGP = 0
IMOEGE = 0
IPULTT = 0
IPULTP = 0
IPULTE = 0
C
C And some values to find maximum and minimum quantities.
C
PULPMX = -1E10
PULPMN = 1E10
PULEMX = -1E10
PULEMN = 1E10
PULTMX = -1E10
PULTMN = 1E10
C
PMEPMX = -1E10
PMEPMN = 1E10
PMEEMX = -1E10
PMEEMN = 1E10
PMETMX = -1E10
PMETMN = 1E10
C
GMEPMX = -1E10
GMEPMN = 1E10
GMEEMX = -1E10
```

```
IF(MOEPAR(I).GT.PMEEMX)PMEEMX = MOEPAR(I)
IF(MOEPAR(I).LT.PMEEMN)PMEEMN = MOEPAR(I)
73 CONTINUE
IF(PULT(I).LE.O.O)GOTO 74
IPULTE = IPULTE + 1
PULTE = PULTE + PULT(I)
IF(PULT(I).GT.PULEMX)PULEMX = PULT(I)
IF(PULT(I).LT.PULEMN)PULEMN = PULT(I)
74 CONTINUE
GOTO 30
31 CONTINUE
IF(SIGGR(I).LE.O.O)GOTO 80
ISIGGP = ISIGGP + 1
SIGGPA = SIGGPA + SIGGR(I)
IF(SIGGR(I).GT.SGGPMX)SGGPMX = SIGGR(I)
IF(SIGGR(I).LT.SGGPMN)SGGPMN = SIGGR(I)
80 CONTINUE
IF(WAFER)GOTO 81
IF(SIGPAR(I).LE.O.O)GOTO 81
ISIGPP = ISIGPP + 1
SIGPPA = SIGPPA + SIGPAR(I)
IF(SIGPAR(I).GT.SPGPMX)SPGPMX = SIGPAR(I)
IF(SIGPAR(I).LT.SPGPMN)SPGPMN = SIGPAR(I)
81 CONTINUE
IF(MOEGRO(I).LE.O.O)GOTO 82
IMOEGP = IMOEGP + 1
MOEGPA = MOEGPA + MOEGRO(I)
IF(MOEGRO(I).GT.GMEPMX)GMEPMX = MOEGRO(I)
IF(MOEGRO(I).LT.GMEPMN)GMEPMN = MOEGRO(I)
82 CONTINUE
IF(WAFER)GOTO 83
IF(MOEPAR(I).LE.O.O)GOTO 83
IMOEP = IMOEP + 1
MOEPPA = MOEPPA + MOEPAR(I)
IF(MOEPAR(I).GT.PMEPMX)PMEPMX = MOEPAR(I)
IF(MOEPAR(I).LT.PMEPMN)PMEPMN = MOEPAR(I)
83 CONTINUE
IF(PULT(I).LE.O.O)GOTO 84
IPULTP = IPULTP + 1
PULTPA = PULTPA + PULT(I)
IF(PULT(I).GT.PULPMX)PULPMX = PULT(I)
IF(PULT(I).LT.PULPMN)PULPMN = PULT(I)
84 CONTINUE
30 CONTINUE
20 CONTINUE
C
C Initialize the averages. If any is not changed, then
C it will have a value of -0.0.
C
ASIGPT = -0.0
ASIGPP = -0.0
ASIGPE = -0.0
ASIGGT = -0.0
ASIGGP = -0.0
ASIGCE = -0.0
AMOEP = -0.0
AMOEP = -0.0
AMOEP = -0.0
AMOEP = -0.0
AMOEP = -0.0
AMOEP = -0.0
AMOEP = -0.0
AMOEP = -0.0
AMOEP = -0.0
APULTT = -0.0
APULTE = -0.0
C
C Calculate the averages. If any counter is equal to zero,
C i.e., no values have been read, skip over it.
C
C The overall averages.
C
IF(WAFER)GOTO 90
IF(ISIGPT.LE.O)GOTO 90
ASIGPT = SIGPTO / ISIGPT
90 CONTINUE
IF(ISIGGT.LE.O)GOTO 91
ASIGGT = SIGGTO / ISIGGT
91 CONTINUE
IF(WAFER)GOTO 92
IF(IMOEP.LE.O)GOTO 92
AMOEP = MOEPTO / IMOEP
92 CONTINUE
IF(IMOEGT.LE.O)GOTO 93
AMOEGT = MOEGTO / IMOEGT
93 CONTINUE
IF(IPULTT.LE.O)GOTO 94
APULTT = PULTTO / IPULTT
94 CONTINUE
C
C And the averages for the perpendicular.
C
IF(WAFER)GOTO 95
IF(ISIGPP.LE.O)GOTO 95
ASIGPP = SIGPPA / ISIGPP
95 CONTINUE
IF(ISIGGP.LE.O)GOTO 96
ASIGGP = SIGGPA / ISIGGP
96 CONTINUE
IF(WAFER)GOTO 97
IF(IMOEP.LE.O)GOTO 97
AMOEP = MOEPPA / IMOEP
```



```
IF(MDEPAR(I).LE.0.0)GOTO 173
PMEES = PMEES + ((MDEPAR(I) - AMDEPE)**2)
173 CONTINUE
IF(PULT(I).LE.0.0)GOTO 174
PULES = PULES + ((PULT(I) - APULTE)**2)
174 CONTINUE
GOTO 130
131 CONTINUE
IF(SIGGRD(I).LE.0.0)GOTO 180
SGGPS = SGGPS + ((SIGGRD(I) - ASIGGP)**2)
180 CONTINUE
IF(WAFER)GOTO 181
IF(SIGPAR(I).LE.0.0)GOTO 181
SPGPS = SPGPS + ((SIGPAR(I) - ASIGPP)**2)
181 CONTINUE
IF(MDEGRD(I).LE.0.0)GOTO 182
GMEPS = GMEPS + ((MDEGRD(I) - AMOEGP)**2)
182 CONTINUE
IF(WAFER)GOTO 183
IF(MDEPAR(I).LE.0.0)GOTO 183
PMEPS = PMEPS + ((MDEPAR(I) - AMDEPP)**2)
183 CONTINUE
IF(PULT(I).LE.0.0)GOTO 184
PULPS = PULPS + ((PULT(I) - APULTP)**2)
184 CONTINUE
130 CONTINUE
120 CONTINUE
C
C Initialize the statistics. If any is not changed, then
C it will have a value of -0.0.
C
SGGPSD = -0.0
SGGPCO = -0.0
SGGPSP = -0.0
SGGESD = -0.0
SGGECO = -0.0
SGGESP = -0.0
SGGTSO = -0.0
SGGTSD = -0.0
SGGTSP = -0.0
C
SPGPSD = -0.0
SPGPCO = -0.0
SPGPSP = -0.0
SPGESD = -0.0
SPGECO = -0.0
SPGESP = -0.0
SPGTSO = -0.0
SPGTSD = -0.0
SPGTSP = -0.0
C
GMEPSD = -0.0
GMEPCO = -0.0
GMEPSP = -0.0
GMEESD = -0.0
GMEECO = -0.0
GMEESP = -0.0
GMETS O = -0.0
GMETSD = -0.0
GMETCO = -0.0
GMETSP = -0.0
C
PMEPSD = -0.0
PMEPCO = -0.0
PMEPSP = -0.0
PMEESD = -0.0
PMEECO = -0.0
PMEESP = -0.0
PMETS O = -0.0
PMETSD = -0.0
PMETCO = -0.0
PMETSP = -0.0
C
PULPSD = -0.0
PULPCO = -0.0
PULPSP = -0.0
PULES D = -0.0
PULECO = -0.0
PULESP = -0.0
PULTSD = -0.0
PULTCO = -0.0
PULTSP = -0.0
C
C Calculate the statistics. If any counter is equal to zero,
C i.e., no values have been read, skip over it.
C
IF(WAFER)GOTO 190
IF(ISIGPT.LE.0)GOTO 190
SPGTSO = SORT(SPGTS / (ISIGPT-1))
SPGTSD = SPGTSO / ASIGPT
AN = FLOAT(ISIGPT)
SPGTSP = ASIGPT - (1.850 * (SPGTSO ))
190 CONTINUE
IF(ISIGGT.LE.0)GOTO 191
SGGTSO = SORT(SGGTS / (ISIGGT-1))
SGGTSD = SGGTSO / ASIGGT
AN = FLOAT(ISIGGT)
SGGTSP = ASIGGT - (1.850 * (SGGTSO ))
191 CONTINUE
IF(WAFER)GOTO 192
IF(IMOEP T.LE.0)GOTO 192
PMETS O = SORT(PMETS / (IMOEP T-1))
```

```
WRITE(6,602)
602 FORMAT(27X,'Length',8X,'parallel area',5X,'gross area',
* 5X,'P ult.',12X,'P/y',/, 28X,'(mm)', 13X,'(mm2)',
* 11X,'(mm2)', 13X,'(N)', 12X,'(kN/mm)',/)
GOTO 111
CONTINUE
WRITE(6,603)
603 FORMAT(27X,'Length',12X,'Area',12X,'P ult.',
* 12X,'P/y',13X,'M.O.E.',11X,'Stress',/, 28X,'(mm)',
* 13X,'(mm2)', 13X,'(N)', 11X,'(kN/mm)',11X,
* '(GPa)', 12X,'(MPa)',/)
111 CONTINUE
C
C The loop will write out all the data as a little
C check.
C
C DD 50 I=1,NPPOINT
C
C Find out when 6 WRITE statements have gone by.
C
C A = I / 6
C IS = A * 6
C NTIT = (IS / 6) + 1
C
C Write out the information.
C
C IF(WAFER)GOTO 112
C WRITE(6,615) LENGTH(I),AREAPA(I),AREAGR(I),PULT(I),POVERY(I)
615 FORMAT(20X,6(5X,G12.5))
GOTO 113
112 CONTINUE
C WRITE(6,604) LENGTH(I),AREAGR(I),PULT(I),POVERY(I),
* MOEGRD(I), SIGGRD(I)
604 FORMAT(20X,6(5X,G12.5))
113 CONTINUE
C
C If 6 WRITE statements have gone by, write out the next
C title.
C
C IF(NTIT.GT.N6)GOTO 52
C IF(IS.EQ.1)GOTO 51
52 CONTINUE
50 CONTINUE
GOTO 53
C
C A little outside piece for doing things on an IF statement.
C
C 51 CONTINUE
C WRITE(6,601)(TITLEA(NTIT,J),J=1,20)
C IF(WAFER)WRITE(6,603)
C IF(.NOT.WAFER)WRITE(6,602)
C GOTO 52
53 CONTINUE
C IF(WAFER) GOTO 57
C
C The loop will write out the calculated values for
C the plywood.
C
C Write out the initial title, and then start the loop.
C
C WRITE(6,600)(TITLE(I),I=1,20)
C WRITE(6,606)
606 FORMAT(4(//),20X,'The Calculated Plywood Quantities:',/)
C WRITE(6,699)(TITLEA(I,J),J=1,20)
699 FORMAT(6(//),20X,30A4,/)
C WRITE(6,615)
C DD 54 I=1,NPPOINT
C
C Find out when 6 WRITE statements have gone by.
C
C A = I / 6
C IS = A * 6
C NTIT = (IS / 6) + 1
C
C Write out the information.
C
C WRITE(6,617) MOEGRD(I),MOEPAR(I),SIGGRD(I),SIGPAR(I)
617 FORMAT(20X,4(5X,G12.5))
C
C If 6 WRITE statements have gone by, write out the next
C title.
C
C IF(NTIT.GT.N6)GOTO 56
C IF(IS.EQ.1)GOTO 55
56 CONTINUE
54 CONTINUE
GOTO 57
C
C A little outside piece for doing things on an IF statement.
C
C 55 CONTINUE
C WRITE(6,699)(TITLEA(NTIT,J),J=1,20)
C WRITE(6,615)
615 FORMAT(/25X,'M.O.E. gross',3X,'M.O.E. parallel',3X,
* 'Stress, gross',3X,'Stress, parallel',/, 28X,'(GPa)',
* 12X,'(GPa)', 12X,'(MPa)', 12X,'(MPa)',/)
C GOTO 56
57 CONTINUE
```

```

C      This program was written for the purpose of
C      manipulating data from bond tests performed
C      on plywood and waferboard specimens.
C
C      The data file should be set up as follows:
C
C      1. MAIN TITLE
C      2. NPOINTS,
C         NOTE: NPOINTS will default to 120 if left blank,
C         and if the values are for plywood, let
C         SKIP be equal to one. Otherwise, leave it
C         blank. This will then assume waferboard.
C      3. First group of 6 title
C      4. Width 1, 2, Length 1, 2, Area, Pult, Stress
C      5.-9. Repeat line 4.
C         NOTE: Repeat lines 3 - 9 for as many groups of
C         6 as you have. If you have less than
C         20, change NPOINTS, and if you have more
C         than 20, change the dimensioning of the
C         vectors and arrays.
C
C      Dimension the various vectors and arrays. They are thus:
C
C      TITLE - The overall title for the run.
C      TITLEA - The titles of the groups of six. Each line
C               is one title.
C
C      REAL PULT(120), SIGMA(120), TITLE(20), TITLEA(20,20)
C      REAL PULTME(20), PULTSD(20),
C      * PULTCO(20), PULTSP(20), PULTMX(20), PULTMN(20)
C      REAL SIGMME(20), SIGMSD(20), SIGMCO(20), SIGMSP(20),
C      * SIGMMX(20), SIGMMN(20)
C
C      Some vectors for counting.
C
C      INTEGER IPULT(20), ISIGM(20)
C
C      Read in the main title.
C
C      READ(5,500)(TITLE(I),I=1,20)
C      FORMAT(20A4)
C      CALL FREAD(5,'1:',NPOINT)
C
C      We assign the number of points to be equal to 120,
C      but we can assign some other number if necessary.
C
C      IF(NPOINT.LE.0)NPOINT = 120
C
C      N6 is the number of groups of 6.
C
C      N6 = NPOINT / 6
C
C      Read in the first group of 6 title:
C
C      READ(5,500)(TITLEA(I,J),J=1,20)
C
C      The loop will read in all the other information.
C
C      DO 10 I=1,NPOINT
C
C      Find out when 6 READ statements have gone by, in order
C      that we may read in another group of 6 title.
C
C      A = I / 6
C      I6 = A * 6
C      NTIT = I6 / 6 + 1
C
C      Read in the information. Check which type to read.
C
C      CALL FREAD(5,'2R:',PULT(I),SIGMA(I))
C
C      If 6 READ statements have gone by, read in a new title.
C      NTIT is the title number.
C
C      IF(NTIT.GT.N6)GOTO 11
C      IF(I6.EQ.I)READ(5,500)(TITLEA(NTIT,J),J=1,20)
C      CONTINUE
C      CONTINUE
C
C      And now calculate the various statistical quantities.
C
C      a) PULT (name)
C      b) Stress PULT
C              SIGM
C
C      with ME, SD, CO, SP, MX, MN to establish whether they
C      are mean, standard deviation, coefficient of variation,
C      5 % confidence limit, maximum, or minimum for that group
C      of 6.
C
C      Initialize these quantities. These will be divided by
C      the counters to find the averages for the entire run.
C
C      EPUL = 0.0
C      ESIG = 0.0
C      EPULMX = -1.0E+10
C      EPULMN = 1.0E+10
C      ESIGMX = -1.0E+10
C      ESIGMN = 1.0E+10

```

```
83 CONTINUE
IF(IESIG.LE.0)GOTO 84
ESGSD = ESGSD + ((SIGMA(K) - AESIG)**2)
84 CONTINUE
31 CONTINUE
C
C The calculations for standard deviation, coefficient
C of variation, and 5% exclusion limit.
C
IF(IPULT(J).LE.0)GOTO 70
PULTSD(J) = SQRT(PULSD / (IPULT(J)-1))
PULTCO(J) = PULTSD(J) / PULTME(J)
AN = FLOAT(IPULT(J))
PULTSP(J) = PULTME(J) - (1.650 * PULTSD(J) )
70 CONTINUE
IF(ISIGM(J).LE.0)GOTO 71
SIGMSD(J) = SQRT(SIGSD / (ISIGM(J)-1))
SIGMCO(J) = SIGMSD(J) / SIGMME(J)
AN = FLOAT(ISIGM(J))
SIGMSP(J) = SIGMME(J) - (1.650 * SIGMSD(J) )
71 CONTINUE
21 CONTINUE
IF(IEPUL.LE.0)GOTO 72
EPULSD = SQRT(EPLSD / (IEPUL-1))
EPULCO = EPULSD / AEPUL
AN = FLOAT(IEPUL)
EPULSP = AEPUL - (1.650 * EPULSD )
72 CONTINUE
IF(IESIG.LE.0)GOTO 73
ESIGSD = SQRT(ESGSD / (IESIG-1))
ESIGCO = ESIGSD / AESIG
AN = FLOAT(IESIG)
ESIGSP = AESIG - (1.650 * ESIGSD )
73 CONTINUE
C
C Start to write out the results.
C
WRITE(6,600)(TITLE(I),I=1,20)
800 FORMAT('1',8(/),40X,30A4,/)
C
C Write out the first title.
C
WRITE(6,601)(TITLEA(I,J),J=1,20)
601 FORMAT(/45X,30A4)
C
C Write out the header:
C
WRITE(6,603)
603 FORMAT(56X,'P ult.',11X,'Stress',/, 57X,'(N)',
*14X,'(kPa)',/)
C
C The loop will write out all the data as a little
C check.
C
DO 50 I=1,NPDINT
C
C Find out when 6 WRITE statements have gone by.
C
A = I / 6
IB = A * 6
NTIT = (IB / 6) + 1
C
C Write out the information.
C
WRITE(6,616) PULT(I),SIGMA(I)
616 FORMAT(50X,2(SX,G12.5))
C
C If 6 WRITE statements have gone by, write out the next
C title.
C
IF(NTIT.GT.N6)GOTO 52
IF(IB.EQ.I)GOTO 51
52 CONTINUE
50 CONTINUE
GOTO 53
C
C A little outside piece for doing things on an IF statement.
C
51 CONTINUE
WRITE(6,601)(TITLEA(NTIT,J),J=1,20)
WRITE(6,603)
GOTO 52
53 CONTINUE
C
C The loop will write out the calculated values.
C
C Write out the initial title, and then start the loop.
C
WRITE(6,606)(TITLE(I),I=1,20)
606 FORMAT('1',8(/),20X,20A4,4(/),
*20X,'The statistics:',4(/))
C
C Write out the information.
C
616 FORMAT(20X,'P ult. (N) ',I2, 6(2X, G12.5)/
*20X, 'Stress (kPa) ',I2, 6(2X, G12.5))
WRITE(6,617)
617 FORMAT(20X,'Results For All Tests:',/)
```

```

C      This program was written for the purpose of
C      manipulating data from small scale SPECIFIC GRAVITY
C      and MOISTURE CONTENT tests performed on plywood and
C      waferboard samples.
C
C      The data file should be set up as follows:
C
C      1. MAIN TITLE
C      2. NPDINTS,
C      3. First group of 3 title
C      4. Specific Gravity, Moisture Content
C      5.-9. Repeat line 4.
C          NOTE: Repeat lines 3 - 9 for as many groups of
C                3 as you have. If you have less than
C                10, change NPDINTS, and if you have more
C                than 10, change the dimensioning of the
C                vectors and arrays.
C
C      Dimension the various vectors and arrays. They are thus:
C
C      TITLE - The overall title for the run.
C      TITLEA - The titles of the groups of three. Each line
C                is one title.
C
C      Define some real variables.
C
C      REAL SPGR(30), MASS1(30), MASSDR(30), VOL(30),
C      * MOIST(30), TITLE(20), TITLEA(10,20)
C      REAL SPGRME(10), SPGRSD(10),
C      * SPGRCD(10), SPGRES(10), SPGRMX(10), SPGRMN(10)
C      REAL MOISME(10), MOISSD(10), MOISCO(10), MOISSP(10),
C      * MOISMX(10), MOISMN(10), MDI, MOISD
C
C      Some vectors for counting.
C
C      INTEGER ISPGR(10), IMOIS(10)
C
C      Read in the main title.
C
C      READ(5,500)(TITLE(I),I=1,20)
C      FORMAT(20A4)
C      CALL FREAD(5,'1:',NPDINT)
C
C      N3 is the number of groups of 3.
C
C      N3 = NPDINT / 3
C
C      Read in the first group of 3 title:
C
C      READ(5,500)(TITLEA(I,J),J=1,20)
C
C      The loop will read in the data.
C
C      DO 10 I=1,NPDINT
C
C      Find out when 3 READ statements have gone by, in order
C      that we may read in another group of 3 title.
C
C      A = I / 3
C      I3 = A * 3
C      NTIT = I3 / 3 + 1
C
C      Read in the information. Check which type to read.
C
C      CALL FREAD(5,'3R:',MASS1(I),MASSDR(I),VOL(I))
C
C      Calculate the specific gravity and moisture content.
C
C      SPGR(I) = MASSDR(I)/VOL(I)
C      MOIST(I) = 100*(MASS1(I) - MASSDR(I))/MASSDR(I)
C
C      If 3 READ statements have gone by, read in a new title.
C      Unless, of course, it is the last one, in which case, don't.
C      NTIT is the title number.
C
C      IF(NTIT.GT.N3)GOTO 11
C      IF(I3.EQ.I)READ(5,500)(TITLEA(NTIT,J),J=1,20)
C      CONTINUE
C      CONTINUE
C
C      And now calculate the various statistical quantities.
C
C      (name)
C      a) Specific Gravity      SPGR
C      b) Moisture Content      MOIS
C
C      with ME, SD, CO, SP, MX, MN to establish whether they
C      are mean, standard deviation, coefficient of variation,
C      5 % confidence limit, maximum, or minimum for that group
C      of 3.
C
C      Initialize these quantities. These will be divided by
C      the counters to find the maximums and minimums for the
C      entire run.
C
C      ESPG = 0.0
C      EMDI = 0.0
C      ESPGMX = -1.0E+10
C      ESPGMN = 1.0E+10
C      EMOISX = -1.0E+10
C      EMOISN = 1.0E+10

```

```
64 CONTINUE
31 CONTINUE
C
C The calculations for standard deviation, coefficient
C of variation, and 5% exclusion limit.
C
IF(ISPGR(J).LE.0)GOTO 70
SPGRSD(J) = SQRT(SPGRD / FLOAT(ISPGR(J)-1))
SPGRCD(J) = SPGRSD(J) / SPGRME(J)
AN = FLOAT(ISPGR(J))
SPGRSP(J) = SPGRME(J) - (1.650 * SPGRSD(J) )
70 CONTINUE
IF(IMOIS(J).LE.0)GOTO 71
MOISSD(J) = SQRT(MOISD / FLOAT(IMOIS(J)-1))
MOISCO(J) = MOISSD(J) / MOISME(J)
AN = FLOAT(IMOIS(J))
MOISSP(J) = MOISME(J) - (1.650 * MOISSD(J) )
71 CONTINUE
21 CONTINUE
IF(IESPG.LE.0)GOTO 72
ESPGRD = SQRT(ESGSD / FLOAT(IESPG-1))
ESPGCO = ESPGRD / AESPG
AN = FLOAT(IESPG)
ESPGSP = AESPG - (1.650 * ESPGRD )
72 CONTINUE
IF(IEMDI.LE.0)GOTO 73
EMOISD = SQRT(EMCSD / FLOAT(IEMDI-1))
EMDICO = EMOISD / AEMDI
AN = FLOAT(IEMDI)
EMDISP = AEMDI - (1.650 * EMOISD )
73 CONTINUE
C
C Start to write out the results.
C
WRITE(6,600)(TITLE(I),I=1,20)
FORMAT('1',8(/),30X,30A4,5(/))
C
C Write out the first title.
C
WRITE(6,601)(TITLEA(1,J),J=1,20)
601 FORMAT(3(/),40X,30A4,2(/))
C
C Write out the header.
C
WRITE(6,603)
603 FORMAT(40X,'Specific Gravity',17X,'Moisture Content',
* /79X, '(%)', /)
C
C The loop will write out all the data as a little
C check.
C
DO 50 I=1,NPOINT
C
C Find out when 3 WRITE statements have gone by.
C
A = I / 3
I3 = A * 3
NTIT = (I3 / 3) + 1
C
C Write out the information.
C
WRITE(6,616) SPGR(I),MOIST(I)
616 FORMAT(43X, G12.5, 21X, G12.5)
C
C If 3 WRITE statements have gone by, write out the title
C of the next little bit.
C
IF(NTIT.GT.N3)GOTO 52
IF(I3.EQ.1)GOTO 51
CONTINUE
52 CONTINUE
50 CONTINUE
GOTO 53
C
C A little outside piece for doing things on an IF statement.
C
51 CONTINUE
WRITE(6,601)(TITLEA(NTIT,J),J=1,20)
WRITE(6,603)
GOTO 52
53 CONTINUE
C
C The loop will write out the calculated values.
C
C Write out the initial title, and then start the loop.
C
WRITE(6,699)(TITLE(I),I=1,20)
699 FORMAT('1',8(/),20X,30A4,5(/))
WRITE(6,606)
606 FORMAT(3(/),20X,'The Statistics:',5(/), 20X,
* 'Results For All Tests:',3(/))
C
C Write out the information.
C
WRITE(6,686)
686 FORMAT(37X, '#', 2X, 'Average', 7X, 'Std. Dev.',2X,
* 'Coef. of Var.', 1X, '5% Ex Lt', 6X, 'Maximum', 6X,
* 'Minimum', /)
WRITE(6,616) IESPG, AESPG, ESPGRD, ESPGCO, ESPGSP, ESPGMX, ESPGMN,
* IEMDI, AEMDI, EMOISD, EMDICO, EMDISP, EMOISX, EMOISN
618 FORMAT(20X, 'Specific Gravity ', I2, 6(1X, G12.5) /
* 20X, 'Moisture Content ', I2, 6(1X, G12.5), 3(/))
```

C This program was written for the purpose of manipulating
C data for large scale flexural tests performed on plywood
C and waferboard specimens.
C

C The data file should be set up as follows:

- C 1. MAIN TITLE
- C 2. T, NPOINTS
- C 3. First group of 10 title
- C 4. EI, MOE, MULT, MOR
- C 5.-9. Repeat line 4.

C NOTE: Repeat lines 3 - 9 for as many groups of
C 10 as you have. If you have less than
C 4, change NPOINTS, and if you have more
C than 4, change the dimensioning of the
C vectors and arrays.

C Dimension the various vectors and arrays. They are thus:

- C EI - - The stiffness
- C MULT - - The ultimate moment
- C MOE - - The modulus of Elasticity.
- C MOR - - The modulus of Rupture.
- C TITLE - The overall title for the run.
- C TITLEA - The titles of the groups of ten. Each line
C is one title.

C REAL EI(120), MOE(120), MULT(120),
C *MOR(120), TITLE(30), TITLEA(20,30)
C REAL PARCOE, PARSDI, PARS2I, PARSPE, PARCOR, PARSDR, PARS2R,
C * PARSPR, PARCOM, PARSDM, PARS2M, PARS5M,
C * PARCOI, PARSDI, PARS2I, PARS5I

C Some logical quantities.

C LOGICAL*1 DOWN /.FALSE./, PARA /.TRUE./, PERP /.FALSE./

C Read in the main title and the wood thickness.

C READ(5,500)(TITLE(I),I=1,20)
C FORMAT(30A4)
C CALL FREAD(5,'R,11:',T,NPOINT)

C N10 is the number of groups of 10.

C N10 = NPOINT / 10

C Read in the first group of 10 title:

C READ(5,500)(TITLEA(I,J),J=1,20)

C The loop will read in all the data.

C DO 10 I=1,NPOINT

C Find out when 10 READ statements have gone by, in order
C that we may read in another group of 10 title.

C A = 1 / 10
C I10 = A * 10
C NTIT = I10 / 10 + 1

C Read in the information.

C CALL FREAD(5,'4R:',EI(I),MOE(I),MULT(I),MOR(I))

C Convert units from Imperial to metric.

C EI(I) = EI(I)*4.448*645.2/1000**2
C MOE(I) = MOE(I)*6.895
C MULT(I) = MULT(I)*1.356/12
C MOR(I) = MOR(I)*6.895

C If 10 READ statements have gone by, read in a new title.
C Unless, of course, it is the last one, in which case, don't.
C NTIT is the title number.

C IF(NTIT.GT.N10)GOTO 11
C IF(I10.EQ.I)READ(5,500)(TITLEA(NTIT,J),J=1,20)
C CONTINUE
C CONTINUE

C Calculate the averages.

C Getting some things straight:

- C For I = 1 - 10, ... it is parallel up.
- C For I = 11 - 20, ... it is parallel down.
- C For I = 21 - 30, ... it is perpendicular up.
- C For I = 31 - 40, ... it is perpendicular down.

C We want the average of:

- C a) parallel up. (name) PARUP
- C b) parallel down. PARDN
- C c) perpendicular up. PERUP
- C d) perpendicular down. PERDN
- C e) all parallel. PARAL
- C f) all perpendicular. PERAL
- C g) everything EVERY

```
C
C      And initialize some counter quantities.  These are needed
C      to find the maximums and minimums.
C
C      Parallel
IPARA1 = 0
IPARA2 = 0
IPARA3 = 0
IPARA4 = 0
C
C      Perpendicular
IPERP1 = 0
IPERP2 = 0
IPERP3 = 0
IPERP4 = 0
C
C      Parallel and Down
IPARD1 = 0
IPARD2 = 0
IPARD3 = 0
IPARD4 = 0
C
C      Parallel and Up
IPARU1 = 0
IPARU2 = 0
IPARU3 = 0
IPARU4 = 0
C
C      Perpendicular and Down
IPERD1 = 0
IPERD2 = 0
IPERD3 = 0
IPERD4 = 0
C
C      Perpendicular and Up
IPERU1 = 0
IPERU2 = 0
IPERU3 = 0
IPERU4 = 0
C
C      Everything
IEVER1 = 0
IEVER2 = 0
IEVER3 = 0
IEVER4 = 0
C
C      And now start a DO loop to find the maximums and minimums.
C
C      DO 20 I=1,NPOINT
C
C      Find out some things about the number.
C
C      First, see if the range is parallel, and set a T/F
C      indicator.
C
C      PARA = .FALSE.
C      IF(I.LE.20)PARA = .TRUE.
C
C      And next, whether it is up or down.
C
C      DOWN = .FALSE.
C      IF(I.LE.20.AND.I.GE.11)DOWN = .TRUE.
C      IF(I.GE.31)DOWN = .TRUE.
C
C      Having established line ranges, check out what to do.
C      I10 refers to the group of ten, I2 to alternating values.
C
C      IF PARA and DOWN, refers to PARDN
C      IF PARA and not DOWN, refers to PARUP
C      IF not PARA and DOWN, refers to PERDN
C      IF not PARA and not DOWN, refers to PERUP
C      IF PARA, refers to PARAL
C      IF not PARA, refers to PERAL
C
C      Find the maximums and minimums.
C
C      Perpendicular
C
C      IF(PARA)GOTO 31
C      IF(EI(I).LE.0.0)GOTO 80
C      IF(EI(I).GT.PERMXI)PERMXI=EI(I)
C      IF(EI(I).LT.PERMNI)PERMNI=EI(I)
C      IPERP1 = IPERP1 + 1
C      PERALI = PERALI + EI(I)
80  CONTINUE
C      IF(MOE(I).LE.0.0)GOTO 81
C      IF(MOE(I).GT.PERMXE)PERMXE=MOE(I)
C      IF(MOE(I).LT.PERMNE)PERMNE=MOE(I)
C      IPERP2 = IPERP2 + 1
C      PERALE = PERALE + MOE(I)
81  CONTINUE
C      IF(MULT(I).LE.0.0)GOTO 82
C      IF(MULT(I).GT.PERMXM)PERMXM=MULT(I)
C      IF(MULT(I).LT.PERMNM)PERMNM=MULT(I)
C      IPERP3 = IPERP3 + 1
C      PERALM = PERALM + MULT(I)
82  CONTINUE
C      IF(MOR(I).LE.0.0)GOTO 182
C      IF(MOR(I).GT.PERMXR)PERMXR=MOR(I)
C      IF(MOR(I).LT.PERMNR)PERMNR=MOR(I)
C      IPERP4 = IPERP4 + 1
C      PERALR = PERALR + MOR(I)
182 CONTINUE
```



```
IF(MOE(I).LE.O.O)GOTO 93
IF(MOE(I).GT.PAUMXE)PAUMXE=MOE(I)
IF(MOE(I).LT.PAUMNE)PAUMNE=MOE(I)
IPARU2 = IPARU2 + 1
PARUPE = PARUPE + MOE(I)
93 CONTINUE
IF(MULT(I).LE.O.O)GOTO 94
IF(MULT(I).GT.PAUMXM)PAUMXM=MULT(I)
IF(MULT(I).LT.PAUMNM)PAUMNM=MULT(I)
IPARU3 = IPARU3 + 1
PARUPM = PARUPM + MULT(I)
94 CONTINUE
IF(MOR(I).LE.O.O)GOTO 194
IF(MOR(I).GT.PAUMXR)PAUMXR=MOR(I)
IF(MOR(I).LT.PAUMNR)PAUMNR=MOR(I)
IPARU4 = IPARU4 + 1
PARUPR = PARUPR + MOR(I)
194 CONTINUE
GOTO 40
C
C Perpendicular and down.
C
43 CONTINUE
IF(EI(I).LE.O.O)GOTO 95
IF(EI(I).GT.PEDMXI)PEDMXI=EI(I)
IF(EI(I).LT.PEDMNI)PEDMNI=EI(I)
IPERD1 = IPERD1 + 1
PERDNI = PERDNI + EI(I)
95 CONTINUE
IF(MOE(I).LE.O.O)GOTO 96
IF(MOE(I).GT.PEDMXE)PEDMXE=MOE(I)
IF(MOE(I).LT.PEDMNE)PEDMNE=MOE(I)
IPERD2 = IPERD2 + 1
PERDNE = PERDNE + MOE(I)
96 CONTINUE
IF(MULT(I).LE.O.O)GOTO 97
IF(MULT(I).GT.PEDMXM)PEDMXM=MULT(I)
IF(MULT(I).LT.PEDMNM)PEDMNM=MULT(I)
IPERD3 = IPERD3 + 1
PERDNM = PERDNM + MULT(I)
97 CONTINUE
IF(MOR(I).LE.O.O)GOTO 197
IF(MOR(I).GT.PEDMXR)PEDMXR=MOR(I)
IF(MOR(I).LT.PEDMNR)PEDMNR=MOR(I)
IPERD4 = IPERD4 + 1
PERDNR = PERDNR + MOR(I)
197 CONTINUE
40 CONTINUE
C
C Everything
C
IF(EI(I).LE.O.O)GOTO 195
IF(EI(I).GT.EVEMXI)EVEMXI=EI(I)
IF(EI(I).LT.EVEMNI)EVEMNI=EI(I)
IEVER1 = IEVER1 + 1
EVERTI = EVERTI + EI(I)
195 CONTINUE
IF(MOE(I).LE.O.O)GOTO 196
IF(MOE(I).GT.EVEMXE)EVEMXE=MOE(I)
IF(MOE(I).LT.EVEMNE)EVEMNE=MOE(I)
IEVER2 = IEVER2 + 1
EVERTI = EVERTI + MOE(I)
196 CONTINUE
IF(MULT(I).LE.O.O)GOTO 198
IF(MULT(I).GT.EVEMXM)EVEMXM=MULT(I)
IF(MULT(I).LT.EVEMNM)EVEMNM=MULT(I)
IEVER3 = IEVER3 + 1
EVERTM = EVERTM + MULT(I)
198 CONTINUE
IF(MOR(I).LE.O.O)GOTO 199
IF(MOR(I).GT.EVEMXR)EVEMXR=MOR(I)
IF(MOR(I).LT.EVEMNR)EVEMNR=MOR(I)
IEVER4 = IEVER4 + 1
EVERTR = EVERTR + MOR(I)
199 CONTINUE
20 CONTINUE
C
C Initialize the averages. If any is not changed, then
C it will have a value of -0.0.
C
C
C Parallel
PARAVE = -0.0
PARAVM = -0.0
PARAVI = -0.0
PARAVR = -0.0
C Perpendicular
PERAVE = -0.0
PERAVM = -0.0
PERAVI = -0.0
PERAVR = -0.0
C Parallel and Up
PAUAVE = -0.0
PAUAVM = -0.0
PAUAVI = -0.0
PAUAVR = -0.0
C Parallel and Down
PADAVE = -0.0
PADAVM = -0.0
PADAVI = -0.0
PADAVR = -0.0
```

```
118 CONTINUE
    IF(IPERD3.LE.0)GOTO 117
    PEDAYM = PERDNM / IPERD3
117 CONTINUE
    IF(IPERD4.LE.0)GOTO 217
    PEDAVR = PERDNR / IPERD4
217 CONTINUE
C
C     The averages of everything.
C
    IF(IEVER1.LE.0)GOTO 118
    EVERY1 = EVERT1 / IEVER1
118 CONTINUE
    IF(IEVER2.LE.0)GOTO 119
    EVERYE = EVERSE / IEVER2
119 CONTINUE
    IF(IEVER3.LE.0)GOTO 120
    EVERYM = EVERTM / IEVER3
120 CONTINUE
    IF(IEVER4.LE.0)GOTO 220
    EVERYR = EVERTR / IEVER4
220 CONTINUE
C
C     Calculate the statistics.
C
C     Initialize.
C
    PARSDI = 0.0
    PARUDE = 0.0
    PARSDM = 0.0
    PARSDR = 0.0
C
    PERSDI = 0.0
    PERSDE = 0.0
    PERSDM = 0.0
    PERSDR = 0.0
C
    PAUSDI = 0.0
    PAUSDE = 0.0
    PAUSDM = 0.0
    PAUSDR = 0.0
C
    PEUSDI = 0.0
    PEUSDE = 0.0
    PEUSDM = 0.0
    PEUSDR = 0.0
C
    PADSDI = 0.0
    PADSDE = 0.0
    PADSDM = 0.0
    PADSDR = 0.0
C
    PEDSDI = 0.0
    PEDSDE = 0.0
    PEDSDM = 0.0
    PEDSDR = 0.0
C
    EVESDI = 0.0
    EVESDE = 0.0
    EVESDM = 0.0
    EVESDR = 0.0
C
    DD 32 I = 1, NPOINT
C
    PERP = .TRUE.
    PARA = .FALSE.
    IF(I.LE.20)PARA = .TRUE.
    IF(I.LE.20)PERP = .FALSE.
    DOWN = .FALSE.
    IF(I.LE.20.AND.I.GE.11)DOWN = .TRUE.
    IF(I.GE.31)DOWN = .TRUE.
C
C     Change the index here instead of a11 through the following.
C
    K = I
    IF(PERP)GOTO 33
C
C     All the parallel
C
    IF(EI(K).LE.0)GOTO 61
    PARSDI = PARSDI + ((EI(K) - PARAVI)**2)
    CONTINUE
61 IF(MOE(K).LE.0)GOTO 161
    PARUDE = PARUDE + ((MOE(K) - PARAVE)**2)
    CONTINUE
161 IF(MULT(K).LE.0)GOTO 261
    PARSDM = PARSDM + ((MULT(K) - PARAVM)**2)
    CONTINUE
261 IF(MOR(K).LE.0)GOTO 361
    PARSDR = PARSDR + ((MOR(K) - PARAVR)**2)
    CONTINUE
361 CONTINUE
    GOTO 34
C
C     All the perpendicular
C
33 CONTINUE
    IF(EI(K).LE.0)GOTO 62
    PERSDI = PERSDI + ((EI(K) - PERAVI)**2)
    CONTINUE
62 CONTINUE
```

```
C
C      The calculations for standard deviation, coefficient of
C      variation, and 5% exclusion limit.
C
C      All parallel
C
70  IF(IPARA1.LE.0)GOTO 70
    PARS2I = SORT(PARSDI / (IPARA1-1))
    PARCOI = PARS2I / PARAVI
    AN = FLOAT(IPARA1)
    PARSPI = PARAVI - (1.650 * PARS2I)
    CONTINUE
170 IF(IPARA2.LE.0)GOTO 170
    PARS2E = SORT(PARSDE / (IPARA2-1))
    PARCOE = PARS2E / PARAVE
    AN = FLOAT(IPARA2)
    PARSPE = PARAVE - (1.650 * PARS2E)
    CONTINUE
270 IF(IPARA3.LE.0)GOTO 270
    PARS2M = SORT(PARSDM / (IPARA3-1))
    PARCOM = PARS2M / PARAVM
    AN = FLOAT(IPARA3)
    PARS2M = PARAVM - (1.650 * PARS2M)
    CONTINUE
370 IF(IPARA4.LE.0)GOTO 370
    PARS2R = SORT(PARSDR / (IPARA4-1))
    PARCOR = PARS2R / PARAVR
    AN = FLOAT(IPARA4)
    PARS2R = PARAVR - (1.650 * PARS2R)
    CONTINUE
C
C      All perpendicular
C
71  IF(IPERP1.LE.0)GOTO 71
    PERS2I = SORT(PERSDI / (IPERP1-1))
    PERCOI = PERS2I / PERAVI
    AN = FLOAT(IPERP1)
    PERSPI = PERAVI - (1.650 * PERS2I)
    CONTINUE
171 IF(IPERP2.LE.0)GOTO 171
    PERS2E = SORT(PERSDE / (IPERP2-1))
    PERCOE = PERS2E / PERAVE
    AN = FLOAT(IPERP2)
    PERSPE = PERAVE - (1.650 * PERS2E)
    CONTINUE
271 IF(IPERP3.LE.0)GOTO 271
    PERS2M = SORT(PERSDM / (IPERP3-1))
    PERCOM = PERS2M / PERAVM
    AN = FLOAT(IPERP3)
    PERS2M = PERAVM - (1.650 * PERS2M)
    CONTINUE
371 IF(IPERP4.LE.0)GOTO 371
    PERS2R = SORT(PERSDR / (IPERP4-1))
    PERCOR = PERS2R / PERAVR
    AN = FLOAT(IPERP4)
    PERS2R = PERAVR - (1.650 * PERS2R)
    CONTINUE
C
C      All parallel up
C
72  IF(IPARU1.LE.0)GOTO 72
    PAUS2I = SORT(PAUSDI / (IPARU1-1))
    PAUCOI = PAUS2I / PAUAVI
    AN = FLOAT(IPARU1)
    PAUSPI = PAUAVI - (1.650 * PAUS2I)
    CONTINUE
172 IF(IPARU2.LE.0)GOTO 172
    PAUS2E = SORT(PAUSDE / (IPARU2-1))
    PAUCOE = PAUS2E / PAUAVE
    AN = FLOAT(IPARU2)
    PAUSPE = PAUAVE - (1.650 * PAUS2E)
    CONTINUE
272 IF(IPARU3.LE.0)GOTO 272
    PAUS2M = SORT(PAUSDM / (IPARU3-1))
    PAUCOM = PAUS2M / PAUAVM
    AN = FLOAT(IPARU3)
    PAUSPM = PAUAVM - (1.650 * PAUS2M)
    CONTINUE
372 IF(IPARU4.LE.0)GOTO 372
    PAUS2R = SORT(PAUSDR / (IPARU4-1))
    PAUCOR = PAUS2R / PAUAVR
    AN = FLOAT(IPARU4)
    PAUSPR = PAUAVR - (1.650 * PAUS2R)
    CONTINUE
C
C      All perpendicular up
C
73  IF(IPERU1.LE.0)GOTO 73
    PEUS2I = SORT(PEUSD1 / (IPERU1-1))
    PEUCOI = PEUS2I / PEUAVI
    AN = FLOAT(IPERU1)
    PEUSPI = PEUAVI - (1.650 * PEUS2I)
    CONTINUE
173 IF(IPERU2.LE.0)GOTO 173
    PEUS2E = SORT(PEUSDE / (IPERU2-1))
    PEUCOE = PEUS2E / PEUAVE
    AN = FLOAT(IPERU2)
    PEUSPE = PEUAVE - (1.650 * PEUS2E)
    CONTINUE
273 IF(IPERU3.LE.0)GOTO 273
    PEUS2M = SORT(PEUSDM / (IPERU3-1))
    PEUCOM = PEUS2M / PEUAVM
    AN = FLOAT(IPERU3)
```

```
C
C      Write out the thickness.
C
C      WRITE(6,601)T
601  FORMAT(/30X,'Thickness (mm) = ',G12.5)
C
C      Write out the first title.
C
C      WRITE(6,602)(TITLEA(I,J),J=1,20)
602  FDRMAT(/////30X,30A4,/)
C
C      Write out the header:
C
C      WRITE(6,603)
603  FORMAT(/,39X,'EI',14X,'MDE',13X,'M ult.',
* 12X,'MDR',/, 38X,'(Nm2)',11X,'(MPa)',
* 13X,'(Nm)', 12X,'(kPa)',/)
C
C      The loop will write out all the data as a little
C      check.
C
C      DO 50 I=1,NPDINT
C
C      Find out when 10 WRITE statements have gone by.
C
C      A = I / 10
C      I10 = A * 10
C      NTIT = (I10 / 10) + 1
C
C      Write out the information.
C
C      WRITE(6,604) EI(I),MDE(I),MULT(I),MDR(I)
604  FORMAT(30X,4(5X,G12.5))
C
C      If 10 WRITE statements have gone by, write out the title
C      of the next little bit.
C
C      IF(NTIT.GT.N10)GOTO 52
C      IF(I10.EQ.1)GOTO 51
52  CONTINUE
50  CONTINUE
C      GOTO 53
C
C      A little outside piece for doing things on an IF statement.
C
C      CONTINUE
51  WRITE(6,602)(TITLEA(NTIT,J),J=1,20)
C      WRITE(6,603)
C      GOTO 52
C      CONTINUE
C
C      Write out the statistics. If none were calculated
C      then don't write them out.
C
C      566  FORMAT(/35X,' #', 4X,'Average', 7X,'Std. Dev.',2X,
* 'Coef. of Var.', 4X,'5% Ex Lt', 6X,'Maximum', 7X,
* 'Minimum',/)
610  FORMAT(20X,'EI (Nm2) : ', 12, 6(2X,G12.5),/20X,
* 'M.O.E. (MPa) : ', 12, 6(2X,G12.5),/20X,
* 'M ult. (Nm) : ', 12, 6(2X,G12.5),/20X,
* 'M.O.R. (kPa) : ', 12, 6(2X,G12.5),/)
C
C      And the statistics.
C
C      WRITE(6,620)(TITLE(I),I=1,20)
620  FORMAT('1',8(/),20X,'The statistics:',///20X,20A4)
C
C      WRITE(6,628)
628  FORMAT(///20X,'A11 Tests:',/)
C      WRITE(6,666)
C      WRITE(6,610)IEVER1, EVERY1, EVES21, EVECO1, EVESP1,
* EVEMX1, EVEMN1, IEVER2, EVERYE,
* EVES2E, EVECOE, EVESPE, EVEMXE, EVEMNE,
* IEVER3, EVERYM, EVES2M, EVECOM, EVESPM, EVEMXM, EVEMNM,
* IEVER4, EVERYR, EVES2R, EVECOR, EVESPR, EVEMXR, EVEMNR
C
C      WRITE(6,621)
621  FORMAT(///20X,'A11 parallel results:',/)
C      WRITE(6,666)
C      WRITE(6,610)IPARA1, PARAV1, PARS21, PARCO1, PARSP1,
* PARMX1, PARMN1, IPARA2, PARAVE,
* PARS2E, PARCOE, PARSPE, PARMXE, PARMNE,
* IPARA3, PARAVM, PARS2M, PARCOM, PARSPM, PARMXM, PARMNM,
* IPARA4, PARAVR, PARS2R, PARCOR, PARSPR, PARMXR, PARMNR
C
C      WRITE(6,623)
623  FORMAT(///20X,'A11 perpendicular results:',/)
C      WRITE(6,666)
C      WRITE(6,610)IPERP1, PERAV1, PERS21, PERCO1, PERSP1,
* PERMX1, PERMN1, IPERP2, PERAVE,
* PERS2E, PERCOE, PERSPE, PERMXE, PERMNE,
* IPERP3, PERAVM, PERS2M, PERCOM, PERSPM, PERMXM, PERMNM,
* IPERP4, PERAVR, PERS2R, PERCOR, PERSPR, PERMXR, PERMNR
C
C      WRITE(6,624)
624  FORMAT(///20X,'A11 parallel and up results:',/)
C      WRITE(6,666)
C      WRITE(6,610)IPARU1, PAUAV1, PAUS21, PAUCO1, PAUSP1,
* PAUMX1, PAUMN1, IPARU2, PAUAVE,
* PAUS2E, PAUCOE, PAUSPE, PAUMXE, PAUMNE,
* IPARU3, PAUAVM, PAUS2M, PAUCOM, PAUSPM, PAUMXM, PAUMNM,
* IPARU4, PAUAVR, PAUS2R, PAUCOR, PAUSPR, PAUMXR, PAUMNR
```

```
C      This program was written to manipulate data
C      from large scale SPECIFIC GRAVITY and
C      MOISTURE CONTENT tests performed on
C      plywood and waferboard specimens.
C
C      The data file should be set up as follows:
C
C      1. MAIN TITLE
C      2. NPPOINTS,
C      3. First group of 10 title
C      4. Original Weight, Oven Dry Weight, Volume
C      5.-8. Repeat line 4.
C          NOTE: Repeat lines 3 - 8 for as many groups of
C                10 as you have. If you have less than
C                4, change NPPOINTS, and if you have more
C                than 4, change the dimensioning of the
C                vectors and arrays.
C
C      Dimension the various vectors and arrays. They are thus:
C
C      TITLE - The overall title for the run.
C      TITLEA - The titles of the groups of ten. Each line
C               is one title.
C
C      Define some real variables.
C
C      REAL SPGR(40), MASS1(40), MASSDR(40), VOL(40),
C      * MOIST(40), TITLE(20), TITLEA(4,20)
C      REAL SPGRME(4), SPGRSD(4),
C      * SPGRCD(4), SPGRSP(4), SPGRMX(4), SPGRMN(4)
C      REAL MOISME(4), MOISSD(4), MOISCO(4), MOISSP(4),
C      * MOISMX(4), MOISMN(4), MOI, MOISD
C
C      Some vectors for counting.
C
C      INTEGER ISPGR(4), IMDIS(4)
C
C      Read in the main title.
C
C      500 READ(5,500)(TITLE(I),I=1,20)
C      FORMAT(20A4)
C      CALL FREAD(5,'1:',NPPOINT)
C
C      N10 is the number of groups of 10.
C
C      N10 = NPPOINT / 10
C
C      Read in the first group of 10 title:
C
C      READ(5,500)(TITLEA(I,J),J=1,20)
C
C      The loop will read in all the data.
C
C      DO 10 I=1,NPPOINT
C
C      Find out when 10 READ statements have gone by, in order
C      that we may read in another group of 10 title.
C
C      A = I / 10
C      I10 = A * 10
C      NTIT = I10 / 10 + 1
C
C      Read in the information. Check which type to read.
C
C      CALL FREAD(5,'3R:',MASS1(I),MASSDR(I),VOL(I))
C
C      Calculate the specific gravity and the moisture content.
C
C      SPGR(I) = MASSDR(I)/VOL(I)
C      MOIST(I) = 100*(MASS1(I) - MASSDR(I))/MASSDR(I)
C
C      If 10 READ statements have gone by, read in a new title.
C      NTIT is the title number.
C
C      IF(NTIT.GT.N10)GOTO 11
C      IF(I10.EQ.I)READ(5,500)(TITLEA(NTIT,J),J=1,20)
C      CONTINUE
C      CONTINUE
C
C      11 And now calculate the various statistical quantities.
C
C      (name)
C      a) Specific Gravity      SPGR
C      b) Moisture Content      MOIS
C
C      with ME, SD, CO, SP, MX, MN to establish whether they
C      are mean, standard deviation, coefficient of variation,
C      5 % confidence limit, maximum, or minimum for that group
C      of 10.
C
C      Initialize these quantities. These will be divided by
C      the counters to find the maximums and minimums for the
C      entire run.
C
C      ESPG = 0.0
C      EMOI = 0.0
C      ESPGMX = -1.0E+10
C      ESPGMN = 1.0E+10
C      EMOISX = -1.0E+10
C      EMOISH = 1.0E+10
```

```
83 CONTINUE
   IF(IEMOI.LE.0)GOTO 84
   EMCSD = EMCSD + ((MOIST(K) - AEMOI)**2)
84 CONTINUE
31 CONTINUE
C
C   The calculations for standard deviation, coefficient of
C   variation, and 5% confidence limit.
C
   IF(ISPR(J).LE.0)GOTO 70
   SPGRSD(J) = SORT(SPCR / FLOAT(ISPR(J)-1))
   SPCR(J) = SPCRSD(J) / SPGRME(J)
   AN = FLOAT(ISPR(J))
   SPGRSP(J) = SPGRME(J) - (1.650 * SPGRSD(J) )
70 CONTINUE
   IF(IMOIS(J).LE.0)GOTO 71
   MOISSD(J) = SORT(MOISD / FLOAT(IMOIS(J)-1))
   MOISCO(J) = MOISSD(J) / MOISME(J)
   AN = FLOAT(IMOIS(J))
   MOISSP(J) = MOISME(J) - (1.650 * MOISSD(J) )
71 CONTINUE
21 CONTINUE
   IF(IESPG.LE.0)GOTO 72
   ESPGRD = SORT(ESGSD / FLOAT(IESPG-1))
   ESPGCO = ESPGRD / AESPG
   AN = FLOAT(IESPG)
   ESPGSP = AESPG - (1.650 * ESPGRD )
72 CONTINUE
   IF(IEMOI.LE.0)GOTO 73
   EMOISD = SORT(EMCSD / FLOAT(IEMOI-1))
   EMOICO = EMOISD / AEMOI
   AN = FLOAT(IEMOI)
   EMOISP = AEMOI - (1.650 * EMOISD )
73 CONTINUE
C
C   Start to write out the results.
C
   WRITE(6,600)(TITLE(I),I=1,20)
600 FORMAT('1',8(/),30X,30A4,5(/))
C
C   Write out the first title.
C
   WRITE(6,601)(TITLEA(1,J),J=1,10)
601 FORMAT(7(/),40X,30A4,2(/))
C
C   Write out the header.
C
   WRITE(6,603)
603 FORMAT(/,43X,'Specific Gravity',12X,'Moisture Content',/,
   = 78X, '(%)', /)
C
C   The loop will write out all the data as a little
C   check.
C
   DO 50 I=1,NPPOINT
C
C   Find out when 10 WRITE statements have gone by.
C
   A = I / 10
   I10 = A * 10
   NTIT = (I10 / 10) + 1
C
C   Write out the information.
C
   WRITE(6,616) SPGR(I),MOIST(I)
616 FORMAT(47X,G12.5,15X,G12.5)
C
C   If 10 WRITE statements have gone by, write out the title
C   of the next little bit.
C
   IF(NTIT.GT.N10)GOTO 52
   IF(I10.EQ.1)GOTO 51
52 CONTINUE
50 CONTINUE
   GOTO 53
C
C   A little outside piece for doing things on an IF statement.
C
51 CONTINUE
   WRITE(6,601)(TITLEA(NTIT,J),J=1,20)
   WRITE(6,603)
   GOTO 52
53 CONTINUE
C
C   The loop will write out the calculated values.
C
C   Write out the initial title, and then start the loop.
C
   WRITE(6,699)(TITLE(I),I=1,20)
699 FORMAT('1',8(/),20X,30A4,5(/))
   WRITE(6,606)
606 FORMAT(4(/),20X,'The statistics :',5(/),20X,
   = 'Results For All Tests:',2(/))
```

This program was written for the purpose of manipulating data from large scale concentrated load tests performed on plywood and waferboard panels.

The data file should be set up as follows:

1. MAIN TITLE
2. NPOINTS
NOTE: NPOINTS will default to 120 if left blank, and if all the values are parallel, let SKIP be equal to one. Otherwise, leave it blank.
3. First group of 8 title
4. Data
- 5.-11. Repeat line 4.
NOTE: Repeat lines 3 - 11 for as many groups of 8 as you have.

Dimension the various vectors and arrays. They are thus:

ASU### - Average supported values.
 AV### - Average deflection values.
 AUN### - Average unsupported deflections.
 AVPULT - Average ultimate load per panel.
 AVCLIP - Average clip failure load per panel.
 CLIP - The clip load.
 SUPULT - Average ultimate supported load.
 UNPULT - Average ultimate unsupported load.
 LB### - Deflection for that load.
 PULT - Ultimate load.
 TITLE - Individual titles.
 TITLEA - Titles of the groups of eight. Each line is one title.

```

REAL LB75(100), LB50(100), LB100(100), LB150(100),
* LB200(100), PULT(100), CLIP(100), AV75(12), AV50(12),
* AV100(12), AV150(12), AV200(12), AVPULT(12), AVCLIP(12),
* AUN75(12), AUN50(12), AUN100(12), AUN150(12), AUN200(12),
* UNPULT(12), ASU75(12), ASU50(12), SUCLIP(12),
* ASU100(12), ASU150(12), ASU200(12), SUPULT(12),
* O75(12), O50(12),
* O100(12), O150(12), O200(12), OPULT(12), OCLIP(12),
* OUN75(12), OUN50(12), OUN100(12), OUN150(12), OUN200(12),
* OUNPU(12), OSU75(12), OSU50(12), OSCLIP(12),
* OSU100(12), OSU150(12), OSU200(12), OSUPU(12),
* C75(12), C50(12),
* C100(12), C150(12), C200(12), CPULT(12), CCLIP(12),
* CUN75(12), CUN50(12), CUN100(12), CUN150(12), CUN200(12),
* CUNPU(12), CSU75(12), CSU50(12), CSCLIP(12),
* CSU100(12), CSU150(12), CSU200(12), CSUPU(12).

```

```

REAL P75(12), P50(12),
* P100(12), P150(12), P200(12), PPULT(12), PCLIP(12),
* PUN75(12), PUN50(12), PUN100(12), PUN150(12), PUN200(12),
* PUNPU(12), PSU75(12), PSU50(12), PSCLIP(12),
* PSU100(12), PSU150(12), PSU200(12), PSUPU(12),
* TITLE(20), TITLEA(12,20)

```

```

REAL P75MX(12), P75MN(12), P50MX(12), P50MN(12),
* P10MX(12), P15MX(12), P20MX(12), PPUMX(12), PCLMX(12),
* P10MN(12), P15MN(12), P20MN(12), PPUMN(12), PCLMN(12),
REAL P75MX(12), P75MN(12), P50MX(12), P50MN(12),
* P10MX(12), P15MX(12), P20MX(12), PSPUMX(12), PSCLMX(12),
* P10MN(12), P15MN(12), P20MN(12), PSPUMN(12), PSCLMN(12),
REAL PU75MX(12), PU75MN(12), PU50MX(12), PU50MN(12),
* PU10MX(12), PU15MX(12), PU20MX(12), PUPUMX(12),
* PU10MN(12), PU15MN(12), PU20MN(12), PUPUMN(12)

```

```

INTEGER I75(12), I50(12),
* I100(12), I150(12), I200(12), IPULT(12), ICLIP(12),
* IUN75(12), IUN50(12), IUN100(12), IUN150(12), IUN200(12),
* IUNPU(12), ISU75(12), ISU50(12), ISUCL(12),
* ISU100(12), ISU150(12), ISU200(12), ISUPU(12)

```

Read in the main title.

```

READ(5,500)(TITLE(I),I=1,20)
FORMAT(20A4)
CALL FREAD(5,'1',NPOINT)

```

N8 is the number of groups of 8.

N8 = NPOINT / 8

Read in the first group of 8 title:

```

READ(5,500)(TITLEA(1,J),J=1,20)

```

The loop will read in all the other stuff.

DO 10 I=1,NPOINT

Find out when 8 READ statements have gone by, in order that we may read in another group of 8 title.

```

A = I / 8
I8 = A * 8
NTIT = I8 / 8 + 1

```

```
C
S75SMU = 0.0
S50SMU = 0.0
S10SMU = 0.0
S15SMU = 0.0
S20SMU = 0.0
SPUSMU = 0.0
SCLSMU = 0.0
I75SMU = 0
I50SMU = 0
I10SMU = 0
I15SMU = 0
I20SMU = 0
IPUSMU = 0
ICLSMU = 0

C
S75SME = 0.0
S50SME = 0.0
S10SME = 0.0
S15SME = 0.0
S20SME = 0.0
SPUSME = 0.0
SCLSME = 0.0
I75SME = 0
I50SME = 0
I10SME = 0
I15SME = 0
I20SME = 0
IPUSME = 0
ICLSME = 0

C
S75MXS = -1.0E10
S50MXS = -1.0E10
S10MXS = -1.0E10
S15MXS = -1.0E10
S20MXS = -1.0E10
SPUMXS = -1.0E10
SCLMXS = -1.0E10

C
S75MNS = 1.0E10
S50MNS = 1.0E10
S10MNS = 1.0E10
S15MNS = 1.0E10
S20MNS = 1.0E10
SPUMNS = 1.0E10
SCLMNS = 1.0E10

C
S75MXU = -1.0E10
S50MXU = -1.0E10
S10MXU = -1.0E10
S15MXU = -1.0E10
S20MXU = -1.0E10
SPUMXU = -1.0E10
SCLMXU = -1.0E10

C
S75MNU = 1.0E10
S50MNU = 1.0E10
S10MNU = 1.0E10
S15MNU = 1.0E10
S20MNU = 1.0E10
SPUMNU = 1.0E10
SCLMNU = 1.0E10

C
S75MXE = -1.0E10
S50MXE = -1.0E10
S10MXE = -1.0E10
S15MXE = -1.0E10
S20MXE = -1.0E10
SPUMXE = -1.0E10
SCLMXE = -1.0E10

C
S75MNE = 1.0E10
S50MNE = 1.0E10
S10MNE = 1.0E10
S15MNE = 1.0E10
S20MNE = 1.0E10
SPUMNE = 1.0E10
SCLMNE = 1.0E10

C
Now, start the loop to run through the groups of 8.
C
DO 20 J=1, N8
C
Initialize the quantities for the eight.
C
DEF75 = 0.0
DEF50 = 0.0
DEF100 = 0.0
DEF150 = 0.0
DEF200 = 0.0
PULTTD = 0.0
CLIP75 = 0.0
I75(J) = 0
I50(J) = 0
I100(J) = 0
I150(J) = 0
I200(J) = 0
IPULT(J) = 0
ICLIP(J) = 0
```



```
82 CONTINUE
   IF(LB150(K).LE.O.O)GOTO 83
   IEX150 = IEX150 + 1
   AEX150 = AEX150 + LB150(K)
83 CONTINUE
   IF(LB200(K).LE.O.O)GOTO 84
   IEX200 = IEX200 + 1
   AEX200 = AEX200 + LB200(K)
84 CONTINUE
   IF(PULT(K).LE.O.O)GOTO 320
   IEXPUL = IEXPUL + 1
   AEXPUL = AEXPUL + PULT(K)
320 CONTINUE
   IF(CLIP(K).LE.O.O)GOTO 321
   IEXCLI = IEXCLI + 1
   AEXCLI = AEXCLI + CLIP(K)
321 CONTINUE
   GOTO 71
C
C Interior.
C
70 CONTINUE
   IF(LB75(K).LE.O.O)GOTO 65
   IIN75 = IIN75 + 1
   AIN75 = AIN75 + LB75(K)
65 CONTINUE
   IF(LB50(K).LE.O.O)GOTO 66
   IIN50 = IIN50 + 1
   AIN50 = AIN50 + LB50(K)
66 CONTINUE
   IF(LB100(K).LE.O.O)GOTO 67
   IIN100 = IIN100 + 1
   AIN100 = AIN100 + LB100(K)
67 CONTINUE
   IF(LB150(K).LE.O.O)GOTO 68
   IIN150 = IIN150 + 1
   AIN150 = AIN150 + LB150(K)
68 CONTINUE
   IF(LB200(K).LE.O.O)GOTO 69
   IIN200 = IIN200 + 1
   AIN200 = AIN200 + LB200(K)
69 CONTINUE
   IF(PULT(K).LE.O.O)GOTO 322
   IINPUL = IINPUL + 1
   AINPUL = AINPUL + PULT(K)
322 CONTINUE
   IF(CLIP(K).LE.O.O)GOTO 323
   IINCLI = IINCLI + 1
   AINCLI = AINCLI + CLIP(K)
323 CONTINUE
71 CONTINUE
C
C Now, for the unsupported and supported parts.
C
C IF(I.LT.5)GOTO 72
C
C Supported.
C
   IF(LB75(K).LE.O.O)GOTO 80
   ISU75(J) = ISU75(J) + 1
   SU75 = SU75 + LB75(K)
   I75SMS = I75SMS + 1
   S75SMS = S75SMS + LB75(K)
80 CONTINUE
   IF(LB50(K).LE.O.O)GOTO 81
   ISU50(J) = ISU50(J) + 1
   SU50 = SU50 + LB50(K)
   ISOSMS = ISOSMS + 1
   SSOSMS = SSOSMS + LB50(K)
81 CONTINUE
   IF(LB100(K).LE.O.O)GOTO 82
   ISU100(J) = ISU100(J) + 1
   SU100 = SU100 + LB100(K)
   I10SMS = I10SMS + 1
   S10SMS = S10SMS + LB100(K)
82 CONTINUE
   IF(LB150(K).LE.O.O)GOTO 83
   ISU150(J) = ISU150(J) + 1
   SU150 = SU150 + LB150(K)
   I15SMS = I15SMS + 1
   S15SMS = S15SMS + LB150(K)
83 CONTINUE
   IF(LB200(K).LE.O.O)GOTO 84
   ISU200(J) = ISU200(J) + 1
   SU200 = SU200 + LB200(K)
   I20SMS = I20SMS + 1
   S20SMS = S20SMS + LB200(K)
84 CONTINUE
   IF(PULT(K).LE.O.O)GOTO 85
   ISUPU(J) = ISUPU(J) + 1
   SUPU = SUPU + PULT(K)
   IPUSMS = IPUSMS + 1
   SPUSMS = SPUSMS + PULT(K)
85 CONTINUE
   IF(CLIP(K).LE.O.O)GOTO 86
   ISUCL(J) = ISUCL(J) + 1
   SUCL = SUCL + CLIP(K)
   ICLSMS = ICLSMS + 1
   SCLSMS = SCLSMS + CLIP(K)
86 CONTINUE
72 GOTO 73
CONTINUE
```

```
108 CONTINUE
    IF(IUN100(J).LE.0)GOTO 109
    AUN100(J) = UN100 / IUN100(J)
109 CONTINUE
    IF(IUN150(J).LE.0)GOTO 110
    AUN150(J) = UN150 / IUN150(J)
110 CONTINUE
    IF(IUN200(J).LE.0)GOTO 111
    AUN200(J) = UN200 / IUN200(J)
111 CONTINUE
    IF(IUNPU(J).LE.0)GOTO 112
    UNPULT(J) = UNPU / IUNPU(J)
112 CONTINUE
C
C      All the supported quantites.
C
    IF(ISU75(J).LE.0)GOTO 113
    ASU75(J) = SU75 / ISU75(J)
113 CONTINUE
    IF(ISU50(J).LE.0)GOTO 114
    ASU50(J) = SU50 / ISU50(J)
114 CONTINUE
    IF(ISU100(J).LE.0)GOTO 115
    ASU100(J) = SU100 / ISU100(J)
115 CONTINUE
    IF(ISU150(J).LE.0)GOTO 116
    ASU150(J) = SU150 / ISU150(J)
116 CONTINUE
    IF(ISU200(J).LE.0)GOTO 117
    ASU200(J) = SU200 / ISU200(J)
117 CONTINUE
    IF(ISUPU(J).LE.0)GOTO 118
    SUPULT(J) = SUPU / ISUPU(J)
118 CONTINUE
    IF(ISUCL(J).LE.0)GOTO 119
    SUCLIP(J) = SUCL / ISUCL(J)
119 CONTINUE
20 CONTINUE
C
C      And now find the overall averages.
C
C      Initialize the averages for interior and exterior.
C
    AVI75 = -0.0
    AVI50 = -0.0
    AVI100 = -0.0
    AVI150 = -0.0
    AVI200 = -0.0
    AVIPUL = -0.0
    AVICLI = -0.0
    AVE75 = -0.0
    AVE50 = -0.0
    AVE100 = -0.0
    AVE150 = -0.0
    AVE200 = -0.0
    AVEPUL = -0.0
    AVECLI = -0.0
C
C      Initialize the averages for everything.
C
    S75AVS = -0.0
    S50AVS = -0.0
    S10AVS = -0.0
    S15AVS = -0.0
    S20AVS = -0.0
    SPUAVS = -0.0
    SCLAVS = -0.0
C
    S75AVU = -0.0
    S50AVU = -0.0
    S10AVU = -0.0
    S15AVU = -0.0
    S20AVU = -0.0
    SPUAVU = -0.0
C
    S75AVE = -0.0
    S50AVE = -0.0
    S10AVE = -0.0
    S15AVE = -0.0
    S20AVE = -0.0
    SPUAVE = -0.0
    SCLAVE = -0.0
C
C      Everything.
C
    IF(I75SME.LE.0)GOTO 130
    S75AVE = S75SME / I75SME
130 CONTINUE
    IF(I50SME.LE.0)GOTO 131
    S50AVE = S50SME / I50SME
131 CONTINUE
    IF(I10SME.LE.0)GOTO 132
    S10AVE = S10SME / I10SME
132 CONTINUE
    IF(I15SME.LE.0)GOTO 133
    S15AVE = S15SME / I15SME
133 CONTINUE
    IF(I20SME.LE.0)GOTO 134
    S20AVE = S20SME / I20SME
```

```
C
C
C      And now, the statistics.
STI75 = 0.0
STI80 = 0.0
STI100 = 0.0
STI150 = 0.0
STI200 = 0.0
STIPUL = 0.0
STICLI = 0.0
C
C
C      And the exterior average running total counters.
STE75 = 0.0
STE80 = 0.0
STE100 = 0.0
STE150 = 0.0
STE200 = 0.0
STEPUL = 0.0
STECLI = 0.0
C
C
C      Maximum and minimum values, Initiation of.
PE75MX = -1E+10
PE75MN = 1E+10
PE80MX = -1E+10
PE80MN = 1E+10
PE10MX = -1E+10
PE10MN = 1E+10
PE15MX = -1E+10
PE15MN = 1E+10
PE20MX = -1E+10
PE20MN = 1E+10
PEPUMX = -1E+10
PEPUMN = 1E+10
PECLMX = -1E+10
PECLMN = 1E+10
C
C
C      P175MX = -1E+10
P175MN = 1E+10
P180MX = -1E+10
P180MN = 1E+10
P110MX = -1E+10
P110MN = 1E+10
P115MX = -1E+10
P115MN = 1E+10
P120MX = -1E+10
P120MN = 1E+10
PIPUMX = -1E+10
PIPUMN = 1E+10
PICLMX = -1E+10
PICLMN = 1E+10
C
C
C      S75SE = 0.0
S80SE = 0.0
S10SE = 0.0
S15SE = 0.0
S20SE = 0.0
SPUSE = 0.0
SCLSE = 0.0
C
C
C      S75SS = 0.0
S80SS = 0.0
S10SS = 0.0
S15SS = 0.0
S20SS = 0.0
SPUSS = 0.0
SCLSS = 0.0
C
C
C      S75SU = 0.0
S80SU = 0.0
S10SU = 0.0
S15SU = 0.0
S20SU = 0.0
SPUSU = 0.0
C
C
C      Now, start the loop to run through the groups of 8.
DO 21 J=1, N8
C
C
C      Initialize the quantities for the eight.
S75 = 0.0
S80 = 0.0
S100 = 0.0
S180 = 0.0
S200 = 0.0
SPULT = 0.0
SCLIP = 0.0
C
C
C      Initialize the quantities for the unsupported four.
SUN75 = 0.0
SUN80 = 0.0
SUN100 = 0.0
SUN150 = 0.0
SUN200 = 0.0
SUNPU = 0.0
```

```
244 CONTINUE
IF(PULT(K).LE.O.O)GOTO 245
SPULT = SPULT + ((PULT(K) - AVPULT(J))*2)
SPUSE = SPUSE + ((PULT(K) - SPUAVE)**2)
IF(PULT(K).GT.PPUMX(J))PPUMX(J) = PULT(K)
IF(PULT(K).LT.PPUMN(J))PPUMN(J) = PULT(K)
IF(PULT(K).GT.SPUMXE)SPUMXE = PULT(K)
IF(PULT(K).LT.SPUMNE)SPUMNE = PULT(K)
245 CONTINUE
IF(CLIP(K).LE.O.O)GOTO 246
SCLIP = SCLIP + ((CLIP(K) - AVCLIP(J))*2)
SCLSE = SCLSE + ((CLIP(K) - SCLAVE)**2)
IF(CLIP(K).GT.PCLMX(J))PCLMX(J) = CLIP(K)
IF(CLIP(K).LT.PCLMN(J))PCLMN(J) = CLIP(K)
IF(CLIP(K).GT.SCLMXE)SCLMXE = CLIP(K)
IF(CLIP(K).LT.SCLMNE)SCLMNE = CLIP(K)
246 CONTINUE
C
C      And now for the overall quantities.
C
C      IF(I.EQ.1.OR.I.EQ.4.OR.I.EQ.6.OR.I.EQ.7)GOTO 74
C
C      Exterior.
C
IF(LB75(K).LE.O.O)GOTO 260
STE75 = STE75 + ((LB75(K) - AVE75)**2)
IF(LB75(K).GT.PE75MX)PE75MX = LB75(K)
IF(LB75(K).LT.PE75MN)PE75MN = LB75(K)
260 CONTINUE
IF(LB50(K).LE.O.O)GOTO 261
STE50 = STE50 + ((LB50(K) - AVE50)**2)
IF(LB50(K).GT.PE50MX)PE50MX = LB50(K)
IF(LB50(K).LT.PE50MN)PE50MN = LB50(K)
261 CONTINUE
IF(LB100(K).LE.O.O)GOTO 262
STE100 = STE100 + ((LB100(K) - AVE100)**2)
IF(LB100(K).GT.PE10MX)PE10MX = LB100(K)
IF(LB100(K).LT.PE10MN)PE10MN = LB100(K)
262 CONTINUE
IF(LB150(K).LE.O.O)GOTO 263
STE150 = STE150 + ((LB150(K) - AVE150)**2)
IF(LB150(K).GT.PE15MX)PE15MX = LB150(K)
IF(LB150(K).LT.PE15MN)PE15MN = LB150(K)
263 CONTINUE
IF(LB200(K).LE.O.O)GOTO 264
STE200 = STE200 + ((LB200(K) - AVE200)**2)
IF(LB200(K).GT.PE20MX)PE20MX = LB200(K)
IF(LB200(K).LT.PE20MN)PE20MN = LB200(K)
264 CONTINUE
IF(PULT(K).LE.O.O)GOTO 328
STEPUL = STEPUL + ((PULT(K) - AVEPUL)**2)
IF(PULT(K).GT.PEPUMX)PEPUMX = PULT(K)
IF(PULT(K).LT.PEPUMN)PEPUMN = PULT(K)
328 CONTINUE
IF(CLIP(K).LE.O.O)GOTO 329
STECLI = STECLI + ((CLIP(K) - AVECLI)**2)
IF(CLIP(K).GT.PECLMX)PECLMX = CLIP(K)
IF(CLIP(K).LT.PECLMN)PECLMN = CLIP(K)
329 CONTINUE
GOTO 75
C
C      Interior.
C
74 CONTINUE
IF(LB75(K).LE.O.O)GOTO 265
STI75 = STI75 + ((LB75(K) - AVI75)**2)
IF(LB75(K).GT.PI75MX)PI75MX = LB75(K)
IF(LB75(K).LT.PI75MN)PI75MN = LB75(K)
265 CONTINUE
IF(LB50(K).LE.O.O)GOTO 266
STI50 = STI50 + ((LB50(K) - AVI50)**2)
IF(LB50(K).GT.PI50MX)PI50MX = LB50(K)
IF(LB50(K).LT.PI50MN)PI50MN = LB50(K)
266 CONTINUE
IF(LB100(K).LE.O.O)GOTO 267
STI100 = STI100 + ((LB100(K) - AVI100)**2)
IF(LB100(K).GT.PI10MX)PI10MX = LB100(K)
IF(LB100(K).LT.PI10MN)PI10MN = LB100(K)
267 CONTINUE
IF(LB150(K).LE.O.O)GOTO 268
STI150 = STI150 + ((LB150(K) - AVI150)**2)
IF(LB150(K).GT.PI15MX)PI15MX = LB150(K)
IF(LB150(K).LT.PI15MN)PI15MN = LB150(K)
268 CONTINUE
IF(LB200(K).LE.O.O)GOTO 269
STI200 = STI200 + ((LB200(K) - AVI200)**2)
IF(LB200(K).GT.PI20MX)PI20MX = LB200(K)
IF(LB200(K).LT.PI20MN)PI20MN = LB200(K)
269 CONTINUE
IF(PULT(K).LE.O.O)GOTO 330
STIPUL = STIPUL + ((PULT(K) - AVIPUL)**2)
IF(PULT(K).GT.PIPUMX)PIPUMX = PULT(K)
IF(PULT(K).LT.PIPUMN)PIPUMN = PULT(K)
330 CONTINUE
IF(CLIP(K).LE.O.O)GOTO 331
STICLI = STICLI + ((CLIP(K) - AVICLI)**2)
IF(CLIP(K).GT.PICLMX)PICLMX = CLIP(K)
IF(CLIP(K).LT.PICLMN)PICLMN = CLIP(K)
331 CONTINUE
```

```
318 CONTINUE
IF (ISU150(J).LE.0)GOTO 318
OSU150(J) = SORT(SSU150 / ISU150(J))
CSU150(J) = OSU150(J) / ASU150(J)
AN = FLOAT(ISU150(J))
PSU150(J) = ASU150(J) - (1.650 * (OSU150(J) ))
318 CONTINUE
IF (ISU200(J).LE.0)GOTO 317
OSU200(J) = SORT(SSU200 / ISU200(J))
CSU200(J) = OSU200(J) / ASU200(J)
AN = FLOAT(ISU200)
PSU200(J) = ASU200(J) - (1.650 * (OSU200(J) ))
317 CONTINUE
IF (ISUPU(J).LE.0)GOTO 318
OSUPU(J) = SORT(SSUPU / ISUPU(J))
CSUPU(J) = OSUPU(J) / SUPULT(J)
AN = FLOAT(ISUPU(J))
PSUPU(J) = SUPULT(J) - (1.650 * (OSUPU(J) ))
318 CONTINUE
IF (ISUCL(J).LE.0)GOTO 318
OSCLIP(J) = SORT(SSUCL / ISUCL(J))
CSCLIP(J) = OSCLIP(J) / SUCLIP(J)
AN = FLOAT(ISUCL(J))
PSCLIP(J) = SUCLIP(J) - (1.650 * (OSCLIP(J) ))
318 CONTINUE
21 CONTINUE
C
C Initialize some statistical quantities.
C
DIN75 = -0.0
DIN50 = -0.0
DIN100 = -0.0
DIN150 = -0.0
DIN200 = -0.0
DINPUL = -0.0
DINCLI = -0.0
C
CIN75 = -0.0
CIN50 = -0.0
CIN100 = -0.0
CIN150 = -0.0
CIN200 = -0.0
CINPUL = -0.0
CINCLI = -0.0
C
PIN75 = -0.0
PIN50 = -0.0
PIN100 = -0.0
PIN150 = -0.0
PIN200 = -0.0
PINPUL = -0.0
PINCLI = -0.0
C
DEX75 = -0.0
DEX50 = -0.0
DEX100 = -0.0
DEX150 = -0.0
DEX200 = -0.0
DEXPUL = -0.0
DEXCLI = -0.0
C
CEX75 = -0.0
CEX50 = -0.0
CEX100 = -0.0
CEX150 = -0.0
CEX200 = -0.0
CEXPUL = -0.0
CEXCLI = -0.0
C
PEX75 = -0.0
PEX50 = -0.0
PEX100 = -0.0
PEX150 = -0.0
PEX200 = -0.0
PEXPUL = -0.0
PEXCLI = -0.0
C
S75SDE = -0.0
S50SDE = -0.0
S100SDE = -0.0
S150SDE = -0.0
S200SDE = -0.0
SPUSDE = -0.0
SCLSDE = -0.0
C
S75COE = -0.0
S50COE = -0.0
S100COE = -0.0
S150COE = -0.0
S200COE = -0.0
SPUCOE = -0.0
SCLCOE = -0.0
C
S75SPE = -0.0
S50SPE = -0.0
S100SPE = -0.0
S150SPE = -0.0
S200SPE = -0.0
SPUSPE = -0.0
SCLSPE = -0.0
```

```
416 CONTINUE
IF(IEK50.LE.0)GOTO 416
DEX50 = SORT(STE50 / (IEK50-1))
CEX50 = DEX50 / AVE50
AN = FLOAT(IEK50)
PEX50 = AVE50 - (1.650 * (DEX50 ))
418 CONTINUE
IF(IEK100.LE.0)GOTO 417
DEX100 = SORT(STE100 / (IEK100-1))
CEX100 = DEX100 / AVE100
AN = FLOAT(IEK100)
PEX100 = AVE100 - (1.650 * (DEX100 ))
417 CONTINUE
IF(IEK150.LE.0)GOTO 418
DEX150 = SORT(STE150 / (IEK150-1))
CEX150 = DEX150 / AVE150
AN = FLOAT(IEK150)
PEX150 = AVE150 - (1.650 * (DEX150 ))
418 CONTINUE
IF(IEK200.LE.0)GOTO 419
DEX200 = SORT(STE200 / (IEK200-1))
CEX200 = DEX200 / AVE200
AN = FLOAT(IEK200)
PEX200 = AVE200 - (1.650 * (DEX200 ))
419 CONTINUE
IF(IEXPUL.LE.0)GOTO 420
DEXPUL = SORT(STEPUL / (IEXPUL-1))
CEXPUL = DEXPUL / AVEPUL
AN = FLOAT(IEXPUL)
PEXPUL = AVEPUL - (1.650 * (DEXPUL ))
420 CONTINUE
IF(IEXCLI.LE.0)GOTO 421
DEXCLI = SORT(STECLI / (IEXCLI-1))
CEXCLI = DEXCLI / AVECLI
AN = FLOAT(IEXCLI)
PEXCLI = AVECLI - (1.650 * (DEXCLI ))
421 CONTINUE
C
C      Everything.
C
IF(I75SME.LE.0)GOTO 430
S75SDE = SORT(S75SE / (I75SME-1))
S75CDE = S75SDE / S75AVE
AN = FLOAT(I75SME)
S75SPE = S75AVE - (1.650 * (S75SDE ))
430 CONTINUE
IF(I50SME.LE.0)GOTO 431
S50SDE = SORT(S50SE / (I50SME-1))
S50CDE = S50SDE / S50AVE
AN = FLOAT(I50SME)
S50SPE = S50AVE - (1.650 * (S50SDE ))
431 CONTINUE
IF(I10SME.LE.0)GOTO 432
S10SDE = SORT(S10SE / (I10SME-1))
S10CDE = S10SDE / S10AVE
AN = FLOAT(I10SME)
S10SPE = S10AVE - (1.650 * (S10SDE ))
432 CONTINUE
IF(I15SME.LE.0)GOTO 433
S15SDE = SORT(S15SE / (I15SME-1))
S15CDE = S15SDE / S15AVE
AN = FLOAT(I15SME)
S15SPE = S15AVE - (1.650 * (S15SDE ))
433 CONTINUE
IF(I20SME.LE.0)GOTO 434
S20SDE = SORT(S20SE / (I20SME-1))
S20CDE = S20SDE / S20AVE
AN = FLOAT(I20SME)
S20SPE = S20AVE - (1.650 * (S20SDE ))
434 CONTINUE
IF(IPUSME.LE.0)GOTO 435
SPUSDE = SORT(SPUSE / (IPUSME-1))
SPUCDE = SPUSDE / SPUAVE
AN = FLOAT(IPUSME)
SPUSPE = SPUAVE - (1.650 * (SPUSDE ))
435 CONTINUE
IF(ICLSME.LE.0)GOTO 436
SCLSDE = SORT(SCLSE / (ICLSME-1))
SCLCDE = SCLSDE / SCLAVE
AN = FLOAT(ICLSME)
SCLSPE = SCLAVE - (1.650 * (SCLSDE / SORT(AN)))
436 CONTINUE
C
C      Supported.
C
IF(I75SMS.LE.0)GOTO 440
S75SDS = SORT(S75SS / (I75SMS-1))
S75CDS = S75SDS / S75AVS
AN = FLOAT(I75SMS)
S75SPS = S75AVS - (1.650 * (S75SDS ))
440 CONTINUE
IF(I50SMS.LE.0)GOTO 441
S50SDS = SORT(S50SS / (I50SMS-1))
S50CDS = S50SDS / S50AVS
AN = FLOAT(I50SMS)
S50SPS = S50AVS - (1.650 * (S50SDS ))
441 CONTINUE
IF(I10SMS.LE.0)GOTO 442
S10SDS = SORT(S10SS / (I10SMS-1))
S10CDS = S10SDS / S10AVS
AN = FLOAT(I10SMS)
S10SPS = S10AVS - (1.650 * (S10SDS ))
```

```
C
C      Write out the information.
C
603  WRITE(6,603) LB75(I),LB80(I),LB100(I),LB150(I),
      * LB200(I), PULT(I), CLIP(I)
      FORMAT(20X,7(3X,G12.5))
C
C      If 8 WRITE statements have gone by, write out the next
C      title.
C
      IF(NTIT.GT.N8)GOTO 52
      IF(I8.EQ.I)GOTO 51
52  CONTINUE
50  CONTINUE
      GOTO 53
C
C      A little outside piece for doing things on an IF statement.
C
51  CONTINUE
      WRITE(6,601)(TITLEA(NTIT,J),J=1,20)
      WRITE(6,602)
      GOTO 52
C
C      Write out the statistics.
C
53  CONTINUE
      WRITE(6,604)(TITLE(I),I=1,20)
      FORMAT('1',8(//),20X,'The statistics:',
      * //20X,20A4,/)
      WRITE(6,628)
      FORMAT(//20X,'Results for All Panels:',/)
      WRITE(6,666)
      FORMAT(//22X,'#',3X,'Average',6X,'Std. Dev.',3X,
      * 'Coef. of Var.',4X,'5X Ex Lt',6X,'Maximum',7X,
      * 'Minimum',/)
      WRITE(6,620)I75SME,S75AVE,S75SDE,S75CDE,S75SPE,S75MXE,S75MNE,
      * I50SME,S50AVE,S50SDE,S50CDE,S50SPE,S50MXE,S50MNE,
      * I10SME,S10AVE,S10SDE,S10CDE,S10SPE,S10MXE,S10MNE,
      * I15SME,S15AVE,S15SDE,S15CDE,S15SPE,S15MXE,S15MNE,
      * I20SME,S20AVE,S20SDE,S20CDE,S20SPE,S20MXE,S20MNE,
      * IPUSME,SPUAVE,SPUSDE,SPUCDE,SPUSPE,SPUMXE,SPUMNE,
      * ICLSME,SCLAVE,SCLSDE,SCLCDE,SCLSPE,SCLMXE,SCLMNE
C
C      WRITE(6,626)
      FORMAT(//20X,'Unsupported:')
      WRITE(6,666)
      WRITE(6,621)I75SMU,S75AVU,S75SDU,S75CDU,S75SPU,S75MXU,S75MNU,
      * I50SMU,S50AVU,S50SDU,S50CDU,S50SPU,S50MXU,S50MNU,
      * I10SMU,S10AVU,S10SDU,S10CDU,S10SPU,S10MXU,S10MNU,
      * I15SMU,S15AVU,S15SDU,S15CDU,S15SPU,S15MXU,S15MNU,
      * I20SMU,S20AVU,S20SDU,S20CDU,S20SPU,S20MXU,S20MNU,
      * IPUSMU,SPUAVU,SPUSDU,SPUCDU,SPUSPU,SPUMXU,SPUMNU
C
C      WRITE(6,627)
      FORMAT(//20X,'Supported:')
      WRITE(6,666)
      WRITE(6,620)I75SMS,S75AVS,S75SDS,S75CDS,S75SPS,S75MXS,S75MNS,
      * I50SMS,S50AVS,S50SDS,S50CDS,S50SPS,S50MXS,S50MNS,
      * I10SMS,S10AVS,S10SDS,S10CDS,S10SPS,S10MXS,S10MNS,
      * I15SMS,S15AVS,S15SDS,S15CDS,S15SPS,S15MXS,S15MNS,
      * I20SMS,S20AVS,S20SDS,S20CDS,S20SPS,S20MXS,S20MNS,
      * IPUSMS,SPUAVS,SPUSDS,SPUCDS,SPUSPS,SPUMXS,SPUMNS,
      * ICLSMS,SCLAVS,SCLSDS,SCLCDS,SCLSPS,SCLMXS,SCLMNS
C
C      WRITE(6,605)
      FORMAT(//20X,'Interior:')
      WRITE(6,666)
620  FORMAT(20X,'Deflection',//20X,'in mm at :',/
      * 21X,'33.4 N: ',I3,6(2X,G12.5)/
      * 21X,'222.4 N: ',I3,6(2X,G12.5)/
      * 21X,'444.8 N: ',I3,6(2X,G12.5)/
      * 21X,'667.2 N: ',I3,6(2X,G12.5)/
      * 21X,'889.6 N: ',I3,6(2X,G12.5)/
      * 20X,'P ult (N): ',I3,6(2X,G12.5)/
      * 20X,'CLIP (N): ',I3,6(2X,G12.5)/)
621  FORMAT(20X,'Deflection',//20X,'in mm at :',/
      * 21X,'33.4 N: ',I3,6(2X,G12.5)/
      * 21X,'222.4 N: ',I3,6(2X,G12.5)/
      * 21X,'444.8 N: ',I3,6(2X,G12.5)/
      * 21X,'667.2 N: ',I3,6(2X,G12.5)/
      * 21X,'889.6 N: ',I3,6(2X,G12.5)/
      * 20X,'P ult (N): ',I3,6(2X,G12.5)/)
      WRITE(6,620)IIN75,AVI75,OIN75,CIN75,PIN75,
      * PI75MX,PI75MN,
      * IIN50,AVI50,OIN50,CIN50,PIN50,
      * PI50MX,PI50MN,
      * IIN100,AVI100,OIN100,CIN100,PIN100,
      * PI10MX,PI10MN,
      * IIN150,AVI150,OIN150,CIN150,PIN150,
      * PI15MX,PI15MN,
      * IIN200,AVI200,OIN200,CIN200,PIN200,
      * PI20MX,PI20MN,
      * IINPUL,AVIPUL,OINPUL,CINPUL,PINPUL,
      * PIPUMX,PIPUMN,
      * IINCLI,AVICLI,OINCLI,CINCLI,PINCLI,
      * PICLMX,PICLMN
```

Appendix C

This appendix contains the formulas used in the calculation of material properties for each of the tests. For all tests, section properties were calculated on the basis of gross cross-sectional area.

C.1 Small Scale Flexural Tests

The modulus of elasticity (MOE) and modulus of rupture (MOR) were calculated in accordance with CSA Standard CAN3-0188.0-M78, as follows:

$$\text{MOE (GPa)} = \frac{L^3}{4bd^3} \times \frac{P}{Y}$$

$$\text{MOR (MPa)} = \frac{3PL}{2bd^2}$$

where b = width (mm)

d = average thickness (mm)

L = length of span (mm)

P = maximum load (N)

P/y = slope of the load-deflection curve (kN/mm)

C.2 Small Scale Compression Tests

The following formulas were used to calculate ultimate compressive stress (σ) and modulus of elasticity (MOE):

$$\sigma \text{ (MPa)} = \frac{P}{bd}$$

$$\text{MOE (GPa)} = \frac{P}{y} \times \frac{L}{bd}$$

where P = ultimate load (N)

b = width (mm)

d = thickness (mm)

L = length (mm)

P/y = slope of load deflection curve (kN/m)

C.3 Bond Tests

$$\sigma = \frac{P}{bl}$$

where σ = bond stress (kPa)

P = ultimate load (N)

b = width (mm)

l = length (mm)

C.4 Specific Gravity and Moisture Content (Edmonton)

The formula used to calculate moisture content is in accordance with CSA Standard CAN3-0188.0-M78:

$$\text{M.C. (\%)} = \frac{100 (M - F)}{F}$$

where M = mass at the time of test

F = oven dry mass

Specific gravity was calculated instead of density so the density formula in the above mentioned standard was not used. Specific gravity was calculated as follows:

$$\text{Sp.Gr.} = \frac{F}{V} \frac{1}{\text{Sp.Gr. H}_2\text{O}}$$

where F = oven dry mass (gm)

V = volume (cm³)

Sp.Gr. H₂O = specific gravity of water
= 1 gm/cm³

C.5 Post Flexure Test

For the post flexure test, all values were calculated in Imperial units and then converted to metric units. Section properties were calculated on the basis of full cross-sectional area. Calculations were made as follows:

Section Properties for 12 inch Width

$$A = t \times b$$

$$I = \frac{bh^3}{12}$$

$$c = \frac{t}{2}$$

$$S = \frac{I}{c}$$

where A = area (in.²)

t = gross thickness (in.)

b = width (set equal to 12 in.)

Mechanical Properties for 12 inch Width

i) Ultimate moment (M.Ult.)

$$\text{M.Ult. (for 12" width)} = \frac{\text{M.Ult. (recorded)}}{\text{Full panel width}} \times 12" \text{ width}$$

ii) Stiffness (EI)

$$EI = MR$$

where M = moment at the proportional limit (p.l.)

R = radius of curvature.

M (for 12" width) = (y axis value on graph at P.L.) x (Scale factor on Load Cell) x (y setting on x-y recorder) x 12" width/full panel width

$$R = \frac{L^2}{8h} + \frac{h}{2}$$

where h = (x axis value on graph at P.L.) x (scale factor) x (x setting on x-y recorder)

iii) $\text{MOE} = \frac{EI}{I}$

iv) $\text{MOR} = \frac{\text{M.Ult.}}{S}$

Conversion to Metric

i) M.Ult. (lb·in) x $\left(\frac{1.356}{12}\right)$ → N·m

ii) EI (lb·in²) x $\left[\frac{4.448 \times 645.2}{(1000)^2}\right]$ → N·m²

iii) MOE (ksi) x (0.00689476) → GPa

iv) MOR (psi) x (0.00689476) → MPa

C.6 Specific Gravity and Moisture Content

$$\text{Sp.Gr.} = \frac{F}{m_{\text{H}_2\text{O}}}$$

where f = oven dry mass of wood

$m_{\text{H}_2\text{O}}$ = mass of water displaced

$$\text{M.C. (\%)} = \frac{100 (M - F)}{F}$$

where M = mass at time of test

F = oven dry mass

C.7 Concentrated Load Test

No calculations were necessary for these tests as all values were measured directly.