

University of Alberta
Department of Civil &
Environmental Engineering



Masonry Chair Report No. 102–2011

CONCRETE MASONRY COMPRESSIVE STRENGTH USING THE UNIT STRENGTH METHOD

M. Gayed
Y. Korany

May 2011

Concrete Masonry Compressive Strength Using the Unit Strength Method

University of Alberta
Masonry Chair Report No. 102-2011

TABLE OF CONTENTS

BACKGROUND 2

DESCRIPTION OF THE DATABASE 2

RESULTS AND DISCUSSION 3

APPENDIX I 10

COMPRESSIVE STRENGTH OF HOLLOW BLOCK PRISMS 10

 REFERENCES 17

APPENDIX II..... 19

COMPRESSIVE STRENGTH OF GROUTED BLOCK PRISMS 19

 REFERENCES 22

Background

The current Canadian Masonry Design Standard (S304.1-2004) stipulates one of two methods to determine the compressive strength of concrete masonry for design. That is, testing of prisms built using materials representative of the actual construction materials or the use of tabulated values given in Table 4 of the Standard that are based on correlating the concrete unit compressive strength to the prism compressive strength based on research that was carried out in the 1970s and 1980s (Maurenbrecher, 1986). The objective of the analysis summarized in this report is to re-establish the correlations between unit strength and prism strength using recent test results. These correlations were examined using a large database of available test results of prism testing conducted mostly in North America, including a test program currently underway at the University of Alberta.

The tabulated values in Table 4 of the Canadian Standard were constructed from best-fit linear correlations between average concrete block compressive strength and average prism compressive strength values. Prism strength values were neither corrected for the prism height to thickness ratio nor for the effect of the mortar bedding type (full-bedded versus face-shell bedded). However, prism strength values were adjusted for the correct mortar bedding area resisting the load. A 20% reduction from the best-fit line was applied to the average prism strength values. These reduced values represent the basis for the current values in Table 4.

Description of the Database

For the analysis reported herein, a database was constructed for the compressive strength of both hollow and grouted concrete masonry construction. For hollow concrete block construction, 282 average/specified masonry compressive strength data points were computed from the test results of 1376 individual prisms. For grouted block construction, 89 data points from 310 individual prism tests were collected. Prism strength computations were performed according to CSA S304.1-04. The majority of the collected data ranged in sample size from 3 to 5 prisms. A full list of the collected data points and the references used in this analysis are given in Appendices I and II for hollow and grouted construction, respectively.

The database herein includes research subsequent to the research used in developing Table 4. Appropriate correction factors were applied to the computed masonry compressive strength values to take into account the effect of the following influential parameters:

- Prism height to thickness ratio— compressive strength values were multiplied by the correction factors given in Table D.1 of CSA S304.1-04 (see Table 1)
- Prism bedded area used for strength computation— where face-shell bedded prisms were tested and the reported masonry compressive strength was computed based on the average net area, strength values were increased by the area factors shown in Table 2. These factors represent the ratios between the average net area to the face-shell bedded area for different block sizes.
- Effect of type of mortar bedding— research has shown that fully bedded prisms and face-shell bedded prisms do not have direct strength correlation to load resisting areas. Two major investigations have

examined this parameter and have shown that face-shell bedded prisms have 10% (Maurenbrecher, 1986) to 15% (Gaynor et al., 1987) higher compressive strength than similar but fully bedded prisms. The more conservative value of 10% was used in this analysis to increase the strength of fully bedded prisms.

TABLE 1- Height to Thickness Correction Factors (CSA S304.1-04)

Correction factor			
Height-to-thickness ratio*	Solid units†	Hollow and semi-solid units	
		Concrete‡	Clay
1.4	—	1.00	0.85
2	0.80	1.00	0.85
3	0.90	1.00	0.90
4	0.95	1.00	0.95
5 to 10	1.00	1.00	1.00

*Linear interpolation is permitted.

†Including fully grouted hollow and semi-solid units.

‡For two-unit-high, hollow and semi-solid concrete block prisms, a correction factor of 0.90 shall be applied.

TABLE 2- Bedding Area Correction Factor for Strength Computation (Maurenbrecher, 1986)

Block Size (mm)	Area Factor (net/face-shell)
90	1.05
140	1.14
190	1.36
240	1.46
290	1.64

Results and Discussion

Using the data shown in Appendix I for hollow masonry prisms constructed using Type S and Type N mortars, best-fit correlations were developed between the average block compressive strength and the average prism compressive strength, Figures 1 and 2 respectively. A power correlation ($y = a \bullet x^b$) yielded the highest R^2 values. The correlation curve was lowered by a factor of 0.82 and 0.81 for Type S and Type N mortars so that 90% of the prism average compressive strength points fall above the correlation curve. This approach is similar to what was followed in developing Table 4 of CSA S304.1-04.

In addition, correlations were established between the average block strength and the specified prism compressive strength. These correlations are shown in Figures 3 and 4 for Type S and Type N mortars; respectively. This is a very conservative approach as a correlation between the average block strength and the specified prism strength yields lower prism strength value for a given designated/nominal block strength than a correlation between the specified block strength and specified prism strength would.

Based on these two sets of correlations (average block vs reduced average prism strength and specified block vs specified prism strength), updated tabulated values for the compressive strength of hollow masonry were derived and are given in Table 3.

Data for grouted masonry prisms were deemed insufficient to construct reliable correlations between block strength and prism strength. Further data is needed and a recently recruited Masters student at the University of Alberta is currently working on expanding the database for grouted masonry.

Hollow Block & Type S Mortar Average Block Strength vs Average Prism Strength

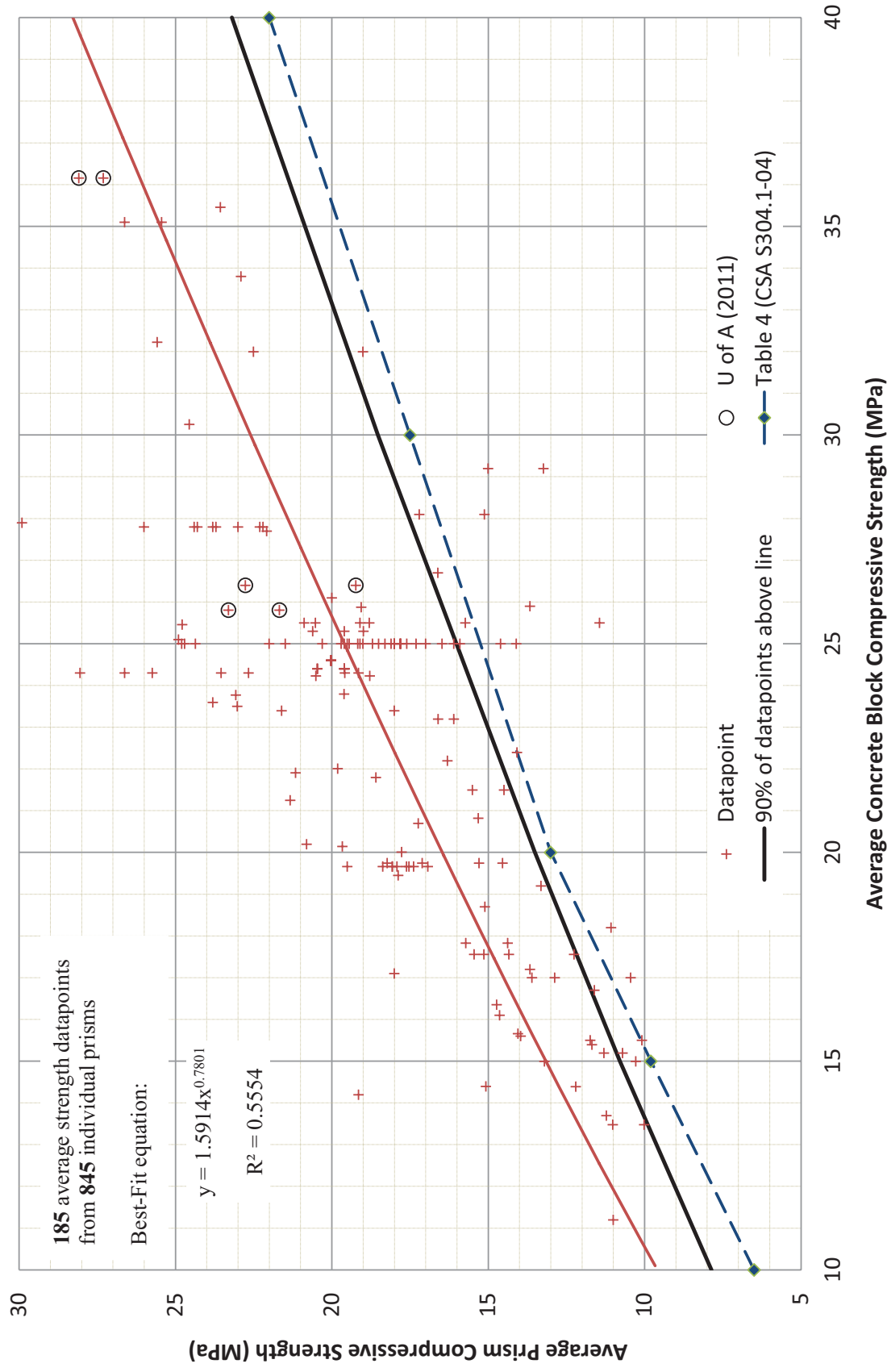


FIGURE 1- Correlation between Average Block and Average Prism Strength for Hollow Masonry with Type S Mortar

Hollow Block & Type N Mortar

Average Block Strength vs Average Prism Strength

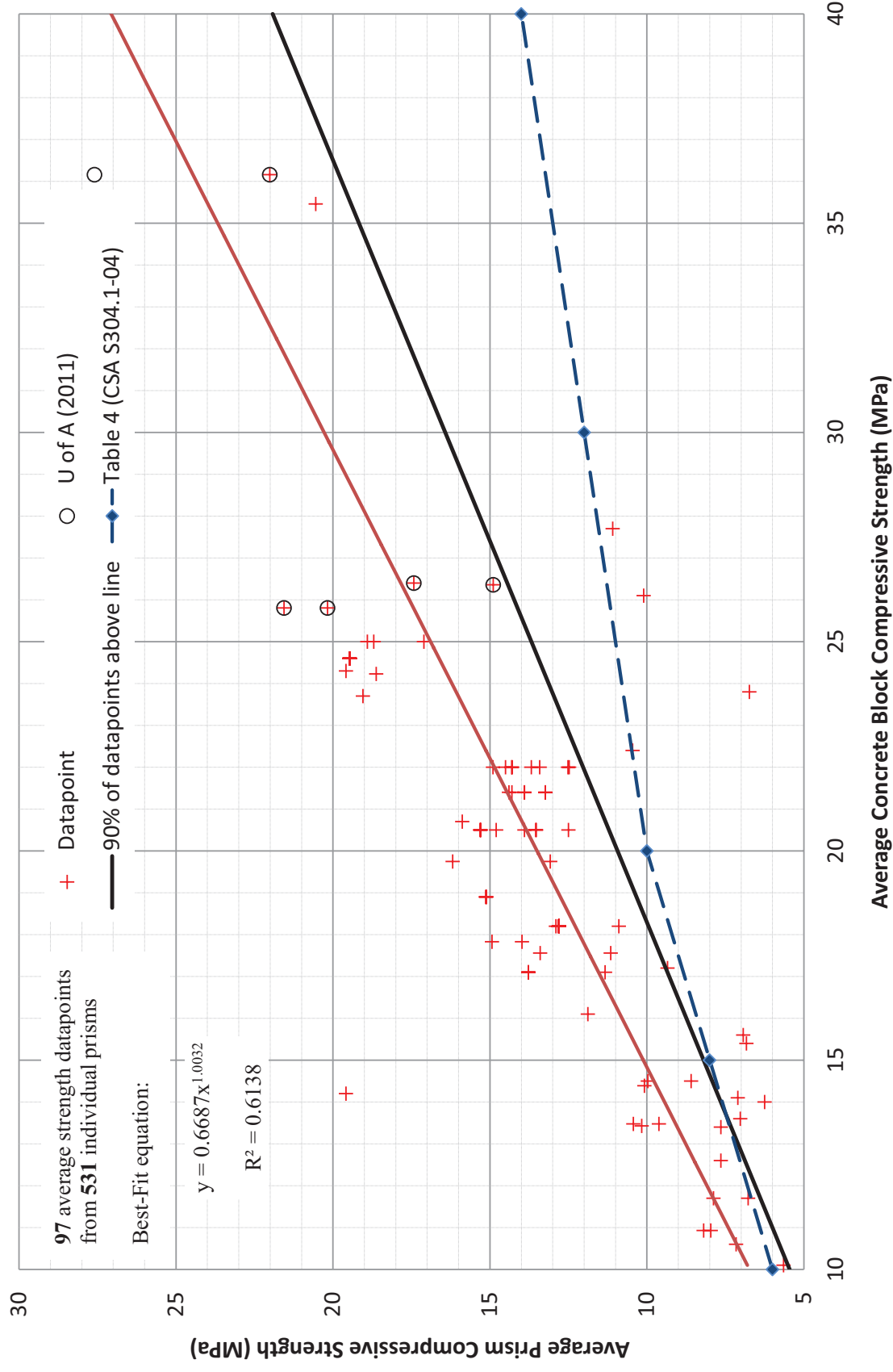


FIGURE 2- Correlation between Average Block and Average Prism Strength for Hollow Masonry with Type N Mortar

Hollow Block & Type S Mortar

Average Block Strength vs Specified Prism Strength

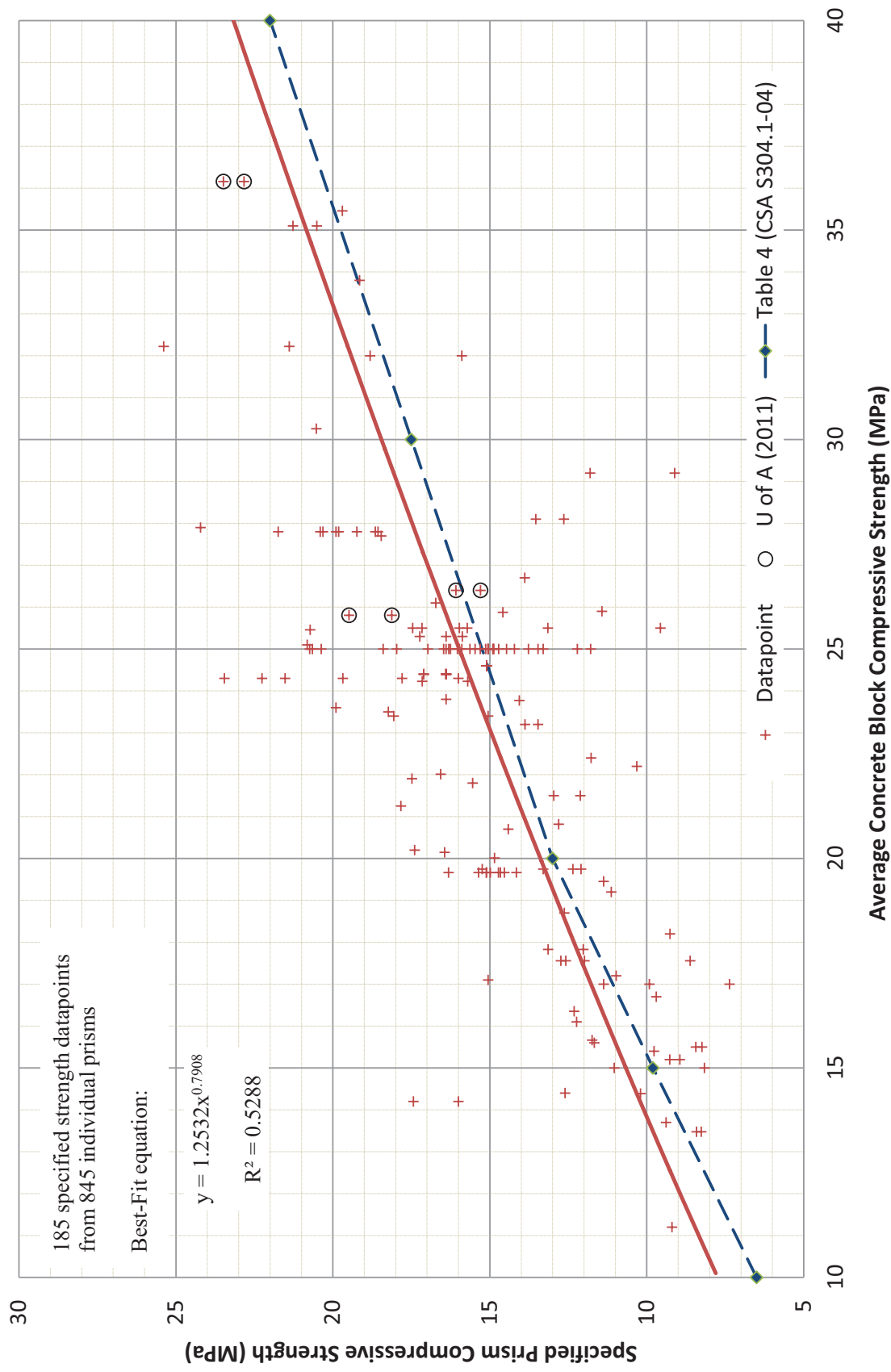


FIGURE 3- Correlation between Average Block and Specified Prism Strength for Hollow Masonry with Type S Mortar

Hollow Block & Type N Mortar Average Block Strength vs Specified Prism Strength

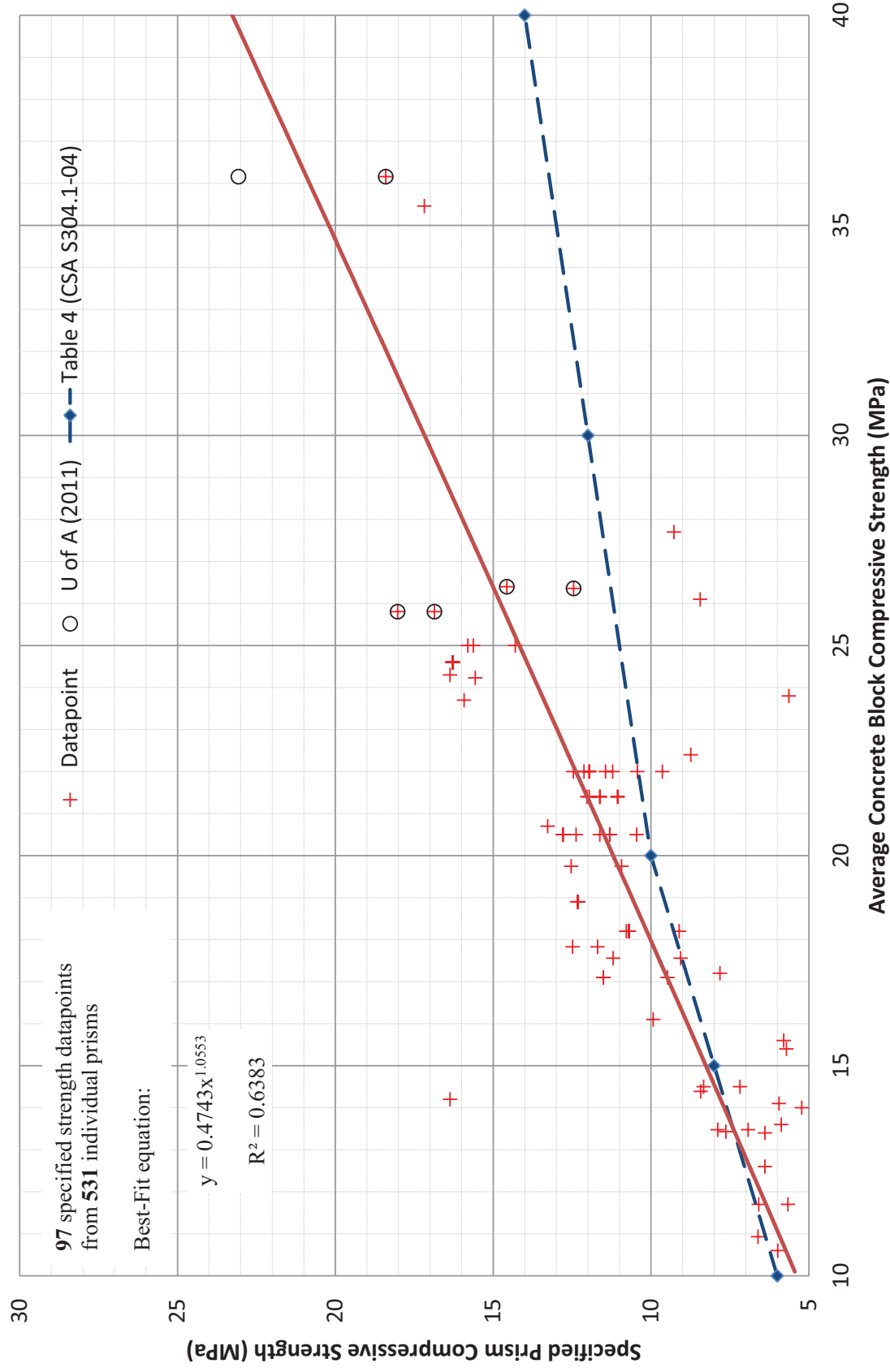


FIGURE 4- Correlation between Average Block and Specified Prism Strength for Hollow Masonry with Type N Mortar

Table 3- Summary of Proposed Updated Compressive Strength Values for Hollow Masonry

Hollow Concrete Masonry Compressive Strength (f'_m)												
Block Strength (MPa)	Type S Mortar						Type N Mortar					
	Current Value	90% Line (Average)	Best Fit (Specified)	Proposed Value	% Increase	f'_m/f'_u	Current Value	90% Line (Average)	Best Fit (Specified)	Proposed Value	% Increase	f'_m/f'_u
40 or more	22.0	23.2	23.2	23.0	4.5	0.58	14	21.9	23.3	18.0	28.6	0.45
30	17.5	18.5	18.5	18.5	5.7	0.62	12	16.4	17.2	15.0	25.0	0.50
20	13.0	13.5	13.4	13.5	3.8	0.68	10	10.9	11.2	11.0	10.0	0.55
15	9.8	10.8	10.7	10.5	7.1	0.70	8	8.2	8.3	8.5	6.3	0.57
10	6.5	7.9	7.7	7.5	15.4	0.75	6	5.5	5.4	6.0	0.0	0.60

Note: Test data for prisms constructed using 30 MPa and 40 MPa concrete blocks and Type N mortar is limited. This explains the caution exercised in proposing new values for these high strength blocks. An experimental program to determine the compressive strength of hollow and grouted masonry prisms constructed of concrete blocks having compressive strength from 10 MPa to 40 MPa and Type S or Type N mortar is currently ongoing at the University of Alberta. The test program includes both masonry cement mortar and PCL mortar.

APPENDIX I

COMPRESSIVE STRENGTH OF HOLLOW PRISMS

Reference	Prism Dimensions					Mortar					Block		Prism						
	Height (h)	Length (l)	Thickness (t)	h/t	Courses	Correction Factor	Type	Thickness	Strength	C.O.V	Bedding	Compressive Strength	St. Dev.	Average Strength	C.O.V.	Number of Tests	Bedding Area Factor	Bedding Type Factor	Calculated Specified Strength f _m
							(C:L:S)	(mm)	(MPa)	(%)	(MPa)	(MPa)	(MPa)	(%)					
1	397	397	194	2.05	2	0.9	S	9.5	14.9	8	Full	25.9	4.8	19.3	14.3	8	1.00	1.10	14.6
	397	397	194	2.05	2	0.9	S	12.7	14.9	8	Full	25.9	4.8	13.8	3.3	3	1.00	1.10	11.4
2	590	390	200	2.95	3	1.0	-	10.0	15.6	6	FS	19.8	2.3	13.4	9.3	6	1.36	1.00	15.2
	590	390	200	2.95	3	1.0	-	10.0	15.6	6	Full	19.8	2.3	13.9	11.7	6	1.00	1.10	12.3
	590	390	200	2.95	3	1.0	-	10.0	12.2	8	FS	19.8	2.3	12.6	13.6	6	1.36	1.00	13.3
	590	390	200	2.95	3	1.0	-	10.0	12.2	8	Full	19.8	2.3	13.2	10.3	6	1.00	1.10	12.1
	590	390	200	2.95	3	1.0	-	10.0	5.0	15	FS	19.8	2.3	11.9	13.8	6	1.36	1.00	12.5
	590	390	200	2.95	3	1.0	-	10.0	5.0	15	Full	19.8	2.3	11.9	7.7	6	1.00	1.10	10.9
	590	390	200	2.95	3	1.0	-	10.0	15.6	6	FS	17.6	1.4	11.4	10.7	6	1.36	1.00	12.7
	590	390	200	2.95	3	1.0	-	10.0	15.6	6	Full	17.6	1.4	13.8	10.3	6	1.00	1.10	12.6
	590	390	200	2.95	3	1.0	-	10.0	12.2	8	FS	17.6	1.4	10.5	9.4	6	1.36	1.00	12.0
	590	390	200	2.95	3	1.0	-	10.0	12.2	8	Full	17.6	1.4	11.1	18.1	6	1.00	1.10	8.6
	590	390	200	2.95	3	1.0	-	10.0	5.0	15	FS	17.6	1.4	9.9	9.9	6	1.36	1.00	11.2
	590	390	200	2.95	3	1.0	-	10.0	5.0	15	Full	17.6	1.4	10.1	11.4	6	1.00	1.10	9.1
	590	390	200	2.95	3	1.0	-	10.0	12.2	8	FS	13.5	1.4	8.1	14.4	6	1.36	1.00	8.4
	590	390	200	2.95	3	1.0	-	10.0	12.2	8	Full	13.5	1.4	9.1	10.7	6	1.00	1.10	8.3
	590	390	200	2.95	3	1.0	-	10.0	5.0	15	FS	13.5	1.4	7.7	14.9	6	1.36	1.00	7.9
	590	390	200	2.95	3	1.0	-	10.0	5.0	15	Full	13.5	1.4	8.7	17.0	6	1.00	1.10	6.9
3	590	390	200	2.95	3	1.0	-	10.0	5.0	15	FS	10.9	1.3	6.0	25.1	6	1.36	1.00	4.8
	590	390	200	2.95	3	1.0	-	10.0	5.0	15	Full	10.9	1.3	7.2	10.4	6	1.00	1.10	6.6
	600	390	143	4.20	3	1.0	S	9.5	15.1	-	Full	19.7	0.8	15.8	4.2	5	1.00	1.10	14.5
	600	390	143	4.20	3	1.0	S	9.5	16.7	-	Full	19.7	0.8	16.0	7.5	5	1.00	1.10	14.7
	600	390	143	4.20	3	1.0	S	9.5	17.3	-	Full	19.7	0.8	15.9	3.3	5	1.00	1.10	14.7
	600	390	143	4.20	3	1.0	S	9.5	14.7	-	Full	19.7	0.8	16.4	3.6	5	1.00	1.10	15.1
	600	390	143	4.20	3	1.0	S	9.5	14.2	-	Full	32.2	2.2	27.6	4.9	4	1.00	1.10	25.4
	600	390	143	4.20	3	1.0	S	19.1	14.2	-	Full	32.2	2.2	23.3	1.1	2	1.00	1.10	21.4
	600	390	143	4.20	3	1.0	S	9.5	14.2	-	Full	16.4	2.1	13.4	4.0	3	1.00	1.10	12.3
	600	390	143	4.20	3	1.0	S	9.5	14.2	-	Full	22.0	0.9	18.0	1.7	4	1.00	1.10	16.6
	600	390	143	4.20	3	1.0	S	9.5	14.2	-	Full	21.3	1.3	19.4	1.5	3	1.00	1.10	17.8
	600	390	143	4.20	3	1.0	S	9.5	14.2	-	Full	20.1	1.1	17.9	5.1	4	1.00	1.10	16.4
	600	390	143	4.20	3	1.0	S	9.5	14.2	-	Full	20.0	1.2	16.1	6.9	4	1.00	1.10	14.8
	600	390	143	4.20	3	1.0	S	9.5	14.2	-	Full	15.7	1.3	12.8	8.4	3	1.00	1.10	11.7
	600	390	143	4.20	3	1.0	S	9.5	12.8	-	Full	19.7	0.8	16.7	1.1	3	1.00	1.10	15.4
	600	390	143	4.20	3	1.0	S	9.5	12.8	-	Full	19.7	0.8	17.7	4.6	4	1.00	1.10	16.3
4	590	195	190	3.11	3	1.0	S	10.0	17.0	-	FS	25.1	-	24.9	6.8	4	1.00	1.00	20.8
	590	195	190	3.11	3	1.0	S	10.0	17.0	-	FS	17.1	-	18.0	7.3	3	1.00	1.00	15.0
	590	195	190	3.11	3	1.0	S	10.0	17.0	-	FS	27.9	-	29.9	11.6	3	1.00	1.00	24.2
	590	195	190	3.11	3	1.0	S	10.0	17.0	-	FS	20.2	-	20.8	1.5	3	1.00	1.00	17.4

	590	195	190	3.11	3	1.0	S	10.0	17.0	-	FS	22.2	-	16.3	22.4	3	1.00	1.00	10.3
	590	195	140	4.21	3	1.0	S	10.0	17.0	-	FS	23.6	-	23.8	3.6	3	1.00	1.00	19.9
	590	195	240	2.46	3	1.0	S	10.0	17.0	-	FS	23.4	-	21.6	8.9	3	1.00	1.00	18.1
5	587	390	190	3.09	3	1.0	1:1:6	10.0	9.2	-	Full	14.2	1.5	17.8	6.2	3	1.00	1.10	16.4
	587	390	190	3.09	3	1.0	1:0.5:4:5	10.0	15.4	-	Full	14.2	1.5	17.4	5.2	3	1.00	1.10	16.0
	587	390	190	3.09	3	1.0	1:0.5:4:5	10.0	15.4	-	Full	14.2	1.5	20.6	14.1	3	1.00	1.10	17.4
	602	395	194	3.10	3	1.0	N	10.0	-	-	FS	18.2	-	12.9	6.0	6	1.00	1.00	10.8
	602	100	240	2.51	3	1.0	S	10.0	-	-	FS	23.4	-	18.0	10.0	3	1.00	1.00	15.0
	599	396	142	4.22	3	1.0	S	10.0	-	-	FS	15.2	-	11.3	11.0	5	1.00	1.00	9.3
	599	792	142	4.22	3	1.0	S	10.0	-	-	FS	15.2	-	10.7	10.0	3	1.00	1.00	8.9
	398	397	194	2.05	2	0.9	S	10.0	-	-	Full	17.0	-	13.0	14.0	10	1.00	1.10	9.9
	398	397	194	2.05	2	0.9	S	10.0	-	-	FS	17.0	-	11.6	18.0	10	1.00	1.00	7.4
	1010	993	194	5.21	5	1.0	S	10.0	-	-	FS	17.0	-	13.6	10.0	2	1.00	1.00	11.4
	396	397	194	2.04	2	1.0	N	10.0	-	-	FS	22.0	1.8	14.9	4.0	12	1.00	1.00	12.5
	1005	397	194	5.18	5	1.0	N	10.0	-	-	FS	22.0	1.8	14.3	4.0	12	1.00	1.00	12.0
	396	397	194	2.04	2	0.9	N	10.0	-	-	FS	22.0	1.8	15.2	5.0	10	1.00	1.00	11.4
	396	397	194	2.04	2	0.9	N	10.0	-	-	FS	22.0	1.8	13.9	14.0	10	1.00	1.00	9.6
	396	397	194	2.04	2	0.9	N	10.0	-	-	Full	22.0	1.8	12.6	10.0	10	1.00	1.10	10.4
	386	391	140	2.76	2	0.9	N	10.0	-	-	FS	21.4	0.9	14.7	5.0	10	1.00	1.00	11.1
	386	391	140	2.76	2	0.9	N	10.0	-	-	Full	21.4	0.9	14.7	4.0	10	1.00	1.09	12.0
	782	391	140	5.59	4	1.0	N	10.0	-	-	FS	21.4	0.9	13.9	4.0	10	1.00	1.00	11.6
	790	391	140	5.64	4	1.0	N	10.0	-	-	FS	20.5	1.6	12.5	7.0	10	1.00	1.00	10.5
	790	391	140	5.64	4	1.0	N	10.0	-	-	Full	20.5	1.6	12.3	10.0	5	1.00	1.10	11.3
	790	391	140	5.64	4	1.0	N	10.0	-	-	Full	20.5	1.6	12.3	10.0	5	1.00	1.10	11.3
	794	391	140	5.67	4	1.0	N	10.0	-	-	FS	20.5	2.3	15.3	7.0	5	1.00	1.00	12.8
	794	391	140	5.67	4	1.0	N	10.0	-	-	FS	20.5	2.3	15.3	7.0	5	1.00	1.00	12.8
	794	391	140	5.67	4	1.0	N	10.0	-	-	FS	20.5	2.3	15.3	7.0	5	1.00	1.00	12.8
	794	391	140	5.67	4	1.0	N	10.0	-	-	FS	20.5	2.3	14.8	9.0	5	1.00	1.00	12.4
	1397	1173	140	9.98	7	1.0	N	10.0	-	-	FS	20.5	2.3	13.9	5.0	10	1.00	1.00	11.6
	392	391	140	2.80	2	0.9	N	10.0	-	-	FS	18.2	1.3	12.1	6.0	12	1.00	1.00	9.1
	392	391	140	2.80	2	0.9	S	10.0	-	-	FS	18.2	1.3	12.3	6.0	12	1.00	1.00	9.3
	398	397	92	4.33	2	0.9	S	10.0	-	-	Full	17.2	-	13.8	12.0	6	1.00	1.10	11.0
	398	397	92	4.33	2	0.9	N	10.0	-	-	Full	17.2	-	9.4	10.0	3	1.00	1.10	7.8
	398	397	92	4.33	2	0.9	S	10.0	-	-	Full	26.1	-	20.2	5.0	6	1.00	1.10	16.7
	398	397	92	4.33	2	0.9	N	10.0	-	-	Full	26.1	-	10.2	10.0	3	1.00	1.10	8.4
	398	397	143	2.78	2	0.9	S	10.0	-	-	Full	15.4	-	11.8	7.0	6	1.00	1.10	9.8
	398	397	143	2.78	2	0.9	N	10.0	-	-	Full	15.4	-	6.9	10.0	3	1.00	1.10	5.7
	398	397	143	2.78	2	0.9	S	10.0	-	-	Full	23.8	-	19.8	9.0	6	1.00	1.10	16.4
	398	397	143	2.78	2	0.9	N	10.0	-	-	Full	23.8	-	6.8	10.0	3	1.00	1.10	5.6
	398	397	194	2.05	2	0.9	S	10.0	-	-	Full	15.6	-	14.1	6.0	6	1.00	1.10	11.7
	398	397	194	2.05	2	0.9	N	10.0	-	-	Full	15.6	-	7.0	10.0	3	1.00	1.10	5.8
	398	397	194	2.05	2	0.9	S	10.0	-	-	Full	27.7	-	22.3	7.0	6	1.00	1.10	18.5
	398	397	194	2.05	2	0.9	N	10.0	-	-	Full	27.7	-	11.2	10.0	3	1.00	1.10	9.3
	398	397	143	2.78	2	1.0	S	10.0	-	-	Full	24.6	-	18.2	15.0	5	1.00	1.10	15.1
	398	397	143	2.78	2	1.0	S	10.0	-	-	Full	24.6	-	18.2	15.0	5	1.00	1.10	15.1
	398	397	143	2.78	2	1.0	S	10.0	-	-	Full	24.6	-	18.2	15.0	5	1.00	1.10	15.1
	398	397	143	2.78	2	1.0	S	10.0	-	-	Full	24.6	-	18.2	15.0	5	1.00	1.10	15.1
	398	397	143	2.78	2	1.0	S	10.0	-	-	Full	24.6	-	18.2	15.0	5	1.00	1.10	15.1
	398	397	143	2.78	2	1.0	S	10.0	-	-	Full	24.6	-	18.2	15.0	5	1.00	1.10	15.1
	398	397	143	2.78	2	1.0	S	10.0	-	-	Full	24.6	-	18.2	15.0	5	1.00	1.10	15.1
	398	397	143	2.78	2	1.0	S	10.0	-	-	Full	24.6	-	18.2	15.0	5	1.00	1.10	15.1
	398	397	143	2.78	2	1.0	S	10.0	-	-	Full	24.6	-	18.2	15.0	5	1.00	1.10	15.1
	398	397	143	2.78	2	1.0	S	10.0	-	-	Full	24.6	-	18.2	15.0	5	1.00	1.10	15.1
	398	397	143	2.78	2	1.0	S	10.0	-	-	Full	24.6	-	18.2	15.0	5	1.00	1.10	15.1
	398	397	143	2.78	2	1.0	S	10.0	-	-	Full	24.6	-	18.2	15.0	5	1.00	1.10	15.1
	398	397	143	2.78	2	1.0	S	10.0	-	-	Full	24.6	-	18.2	15.0	5	1.00	1.10	15.1

7	599	397	194	3.09	3	1.0	S	10.0	-	-	-	24.4	-	18.6	3.0	5	1.00	1.10	17.1
	599	397	194	3.09	3	1.0	S	10.0	-	-	-	24.4	-	18.6	3.0	5	1.00	1.10	17.1
	599	397	194	3.09	3	1.0	S	10.0	-	-	-	24.4	-	19.6	6.0	5	1.00	1.00	16.4
	599	397	194	3.09	3	1.0	S	10.0	-	-	-	24.4	-	19.6	6.0	5	1.00	1.00	16.4
	599	397	194	3.09	3	1.0	S	10.0	-	-	-	24.4	-	19.6	6.0	5	1.00	1.00	16.4
	599	397	194	3.09	3	1.0	S	10.0	-	-	-	24.4	-	19.6	6.0	5	1.00	1.00	16.4
	599	397	194	3.09	3	1.0	S	10.0	-	-	-	24.4	-	19.6	6.0	5	1.00	1.00	16.4
	599	397	194	3.09	3	1.0	S	10.0	-	-	-	24.4	-	19.6	6.0	5	1.00	1.00	16.4
	599	397	194	3.09	3	1.0	S	10.0	-	-	-	24.4	-	19.6	6.0	5	1.00	1.00	16.4
	599	397	194	3.09	3	1.0	S	10.0	-	-	-	24.4	-	19.6	6.0	5	1.00	1.00	16.4
8	600	178	143	4.20	3	1.0	S	9.5	14.5	8	-	19.7	0.8	16.4	3.6	5	1.00	1.10	15.1
	600	178	143	4.20	3	1.0	S	9.5	18.2	6	-	19.7	0.8	16.3	3.3	4	1.00	1.10	15.0
	600	178	143	4.20	3	1.0	N	9.5	5.7	5	-	19.7	0.8	15.4	5.5	4	1.00	1.10	14.2
	590	390	140	4.21	3	1.0	S	10.0	9.4	11	-	13.7	0.4	10.2	1.9	3	1.00	1.10	9.4
9	590	390	140	4.21	3	1.0	S	10.0	7.7	14	-	11.2	0.5	10.0	3.7	3	1.00	1.10	9.2
	590	390	140	4.21	3	1.0	S	10.0	15.5	2	-	15.0	0.3	12.0	4.8	3	1.00	1.10	11.0
	590	390	140	4.21	3	1.0	S	10.0	22.2	22	-	21.8	0.5	16.9	3.9	3	1.00	1.10	15.5
	590	390	190	3.11	3	1.0	cls	10.0	9.2	-	-	24.3	-	17.8	6.2	3	1.00	1.10	16.4
	590	390	190	3.11	3	1.0	cls	10.0	15.4	-	-	24.3	-	17.4	5.2	3	1.00	1.10	16.0
	590	390	190	3.11	3	1.0	cls	10.0	15.4	-	-	24.3	-	21.4	1.9	3	1.00	1.10	19.7
	590	390	190	3.11	3	1.0	cls	10.0	21.2	-	-	24.3	-	20.6	13.1	3	1.00	1.10	17.8
	590	390	190	3.11	3	1.0	cls	5.0	21.2	-	-	24.3	-	24.2	2.9	3	1.00	1.10	22.3
	610	390	190	3.21	3	1.0	cls	20.0	21.2	-	-	24.3	-	25.5	1.6	3	1.00	1.10	23.4
	390	195	190	2.05	2	0.9	cls	10.0	21.2	-	-	24.3	-	26.0	1.5	3	1.00	1.10	21.5
10	390	390	190	2.05	2	0.9	S	10.0	8.4	9	-	25.5	1.2	22.8	4.4	5	1.00	1.00	17.2
	390	390	190	2.05	2	0.9	S	10.0	8.4	9	-	25.5	1.2	23.2	2.4	5	1.00	1.00	17.5
	390	390	190	2.05	2	0.9	S	10.0	8.4	9	-	32.0	5.5	25.0	4.1	5	1.00	1.00	18.8
	390	390	190	2.05	2	0.9	S	10.0	8.4	9	-	21.5	6.2	16.1	4.2	5	1.00	1.00	12.1
	390	390	190	2.05	2	0.9	S	10.0	8.4	9	-	25.3	3.8	22.9	1.8	5	1.00	1.00	17.2
	390	390	190	2.05	2	0.9	S	10.0	8.4	9	-	25.3	3.8	21.1	3.7	5	1.00	1.00	15.9
	790	390	190	4.16	4	1.0	S	10.0	8.4	9	-	25.5	1.2	18.8	4.8	5	1.00	1.00	15.7
	790	390	190	4.16	4	1.0	S	10.0	8.4	9	-	25.5	1.2	19.1	1.6	5	1.00	1.00	16.0
	790	390	190	4.16	4	1.0	S	10.0	8.4	9	-	32.0	5.5	19.0	8.4	5	1.00	1.00	15.9
	790	390	190	4.16	4	1.0	S	10.0	8.4	9	-	21.5	6.2	15.5	6.4	5	1.00	1.00	13.0
11	790	390	190	4.16	4	1.0	S	10.0	8.4	9	-	25.3	3.8	19.6	3.0	5	1.00	1.00	16.4
	590	390	190	3.11	3	1.0	1:0:5	10.0	10.6	6	-	27.8	1.4	24.4	2.0	3	1.00	1.00	20.4
	590	390	190	3.11	3	1.0	1:0:6	10.0	10.6	6	-	27.8	1.4	26.0	1.0	3	1.00	1.00	21.7
	590	390	190	3.11	3	1.0	1:0:7	10.0	10.6	6	-	27.8	1.4	23.8	4.0	3	1.00	1.00	19.9
	590	390	190	3.11	3	1.0	1:0:8	10.0	10.6	6	-	27.8	1.4	24.3	2.0	3	1.00	1.00	20.3
	590	390	190	3.11	3	1.0	1:0:9	10.0	10.6	6	-	27.8	1.4	23.0	10.0	1	1.00	1.00	19.2
	590	390	190	3.11	3	1.0	1:0:10	10.0	10.6	6	-	27.8	1.4	23.7	10.0	1	1.00	1.00	19.8
	990	390	190	5.21	5	1.0	1:0:11	10.0	10.6	6	-	27.8	1.4	22.2	10.0	1	1.00	1.00	18.6
	990	390	190	5.21	5	1.0	1:0:12	10.0	10.6	6	-	27.8	1.4	22.3	10.0	1	1.00	1.00	18.6
	842	396	194	4.34	4	1.00	S	10.0	19.2	-	-	33.8	1.3	22.9	9.6	5	1.00	1.00	19.1
12	590	390	190	3.11	3	1.00	S	10.0	-	-	-	25.0	-	15.8	0.0	1	1.36	1.00	18.0
	590	390	190	3.11	3	1.00	(1:1:6)	10.0	-	-	-	23.7	-	14.0	0.0	1	1.36	1.00	15.9
	665	440	140	4.75	3	1.0	N	10.0	4.0	-	-	16.1	-	10.8	0.0	1	1.00	1.10	9.9
	665	440	140	4.75	3	1.0	S	10.0	-	-	-	16.1	-	13.3	0.0	1	1.00	1.10	12.2
13	665	440	190	3.50	3	1.0	N	10.0	4.0	-	-	22.4	-	9.5	0.0	1	1.00	1.10	8.7
	665	440	190	3.50	3	1.0	S	10.0	-	-	-	22.4	-	12.8	0.0	1	1.00	1.10	11.8
	-	-	-	2.80	2	0.9	N	-	-	-	-	17.1	1.7	15.3	6.7	5	1.00	1.00	11.5
	-	-	-	2.80	2	0.9	N	-	-	-	-	17.1	1.7	15.3	6.7	5	1.00	1.00	11.5
14	-	-	-	2.80	2	0.9	N	-	-	-	-	17.1	1.7	15.3	6.7	5	1.00	1.00	11.5
	-	-	-	2.80	2	0.9	N	-	-	-	-	17.1	1.7	15.3	6.7	5	1.00	1.00	11.5
	590	390	190	3.11	3	1.0	S	10.0	12.4	27	-	15.0	-	10.3	12.6	7	1.00	1.00	8.2
	-	-	-	-	2	0.9	S	10.0	17.9	-	-	25.0	-	21.6	8.8	5	1.00	1.00	16.3

	-	-	-	-	2	0.9	S	10.0	17.9	-	FS	25.0	-	18.3	5.1	5	1.00	1.00	13.8
	-	-	-	-	2	0.9	S	10.0	16.2	-	FS	25.0	-	21.3	2.6	5	1.00	1.00	16.0
	-	-	-	-	2	0.9	S	10.0	16.2	-	FS	25.0	-	19.8	6.1	5	1.00	1.00	14.9
	-	-	-	-	3	1.0	S	10.0	9.6	-	FS	25.0	-	19.0	8.9	5	1.00	1.00	15.9
	-	-	-	-	3	1.0	S	10.0	9.0	-	FS	25.0	-	18.3	3.8	5	1.00	1.00	15.3
	-	-	-	-	3	1.0	S	10.0	11.5	-	FS	25.0	-	19.5	6.1	5	1.00	1.00	16.3
	-	-	-	-	3	1.0	S	10.0	11.5	-	FS	25.0	-	18.5	5.1	5	1.00	1.00	15.5
	-	-	-	-	4	1.0	S	10.0	8.7	-	FS	25.0	-	17.8	4.4	10	1.00	1.00	14.9
	-	-	-	-	4	1.0	S	10.0	8.8	-	FS	25.0	-	18.0	5.9	10	1.00	1.00	15.0
	-	-	-	-	4	1.0	S	10.0	9.9	-	FS	25.0	-	18.0	2.8	5	1.00	1.00	15.0
	-	-	-	-	4	1.0	S	10.0	9.8	-	FS	25.0	-	18.0	4.9	10	1.00	1.00	15.0
	-	-	-	-	4	1.0	S	10.0	9.2	-	FS	25.0	-	20.3	6.1	5	1.00	1.00	17.0
	-	-	-	-	4	1.0	S	10.0	9.9	-	FS	25.0	-	19.6	6.5	5	1.00	1.00	16.4
	-	-	-	-	4	1.0	S	10.0	9.2	-	FS	25.0	-	19.1	5.0	5	1.00	1.00	16.0
	-	-	-	-	4	1.0	S	10.0	10.7	-	FS	25.0	-	17.8	5.1	5	1.00	1.00	14.9
	-	-	-	-	4	1.0	S	10.0	7.5	-	FS	25.0	-	17.6	5.6	5	1.00	1.00	14.7
	-	-	-	-	4	1.0	N	10.0	6.1	-	FS	25.0	-	18.9	4.5	5	1.00	1.00	15.8
	-	-	-	-	4	1.0	N	10.0	6.1	-	FS	25.0	-	17.1	4.1	5	1.00	1.00	14.3
	-	-	-	-	4	1.0	N	10.0	6.6	-	FS	25.0	-	18.7	2.4	5	1.00	1.00	15.6
	-	-	-	-	4	1.0	S	6.0	8.7	-	FS	25.0	-	18.0	2.5	5	1.00	1.00	15.0
18	-	-	-	-	4	1.0	S	6.0	9.8	-	FS	25.0	-	17.8	7.6	5	1.00	1.00	14.9
	-	-	-	-	4	1.0	S	15.0	9.0	-	FS	25.0	-	15.9	6.3	5	1.00	1.00	13.3
	-	-	-	-	4	1.0	S	15.0	9.0	-	FS	25.0	-	16.1	8.3	5	1.00	1.00	13.5
	-	-	-	-	4	1.0	S	10.0	9.9	-	FS	25.0	-	14.6	3.8	5	1.00	1.00	12.2
	-	-	-	-	4	1.0	S	10.0	9.9	-	FS	25.0	-	14.1	4.2	5	1.00	1.00	11.8
	-	-	-	-	4	1.0	S	10.0	10.9	-	FS	25.0	-	24.7	7.0	5	1.00	1.00	20.6
	-	-	-	-	4	1.0	S	10.0	10.9	-	FS	25.0	-	22.0	6.5	5	1.00	1.00	18.4
	-	-	-	-	4	1.0	S	10.0	10.0	-	FS	25.0	-	24.4	7.8	5	1.00	1.00	20.4
	-	-	-	-	4	1.0	S	10.0	10.9	-	FS	25.0	-	24.8	1.9	5	1.00	1.00	20.7
	-	-	-	-	4	1.0	S	10.0	10.7	-	FS	25.0	-	19.7	10.0	5	1.00	1.00	16.5
	-	-	-	-	4	1.0	S	10.0	10.7	-	FS	25.0	-	17.0	7.4	5	1.00	1.00	14.2
	-	-	-	-	4	1.0	S	10.0	7.5	-	FS	25.0	-	18.7	3.5	5	1.00	1.00	15.6
	-	-	-	-	5	1.0	S	10.0	8.5	-	FS	25.0	-	17.3	4.0	5	1.00	1.00	14.5
	-	-	-	-	5	1.0	S	10.0	8.5	-	FS	25.0	-	18.1	5.3	5	1.00	1.00	15.1
	-	-	-	-	5	1.0	S	10.0	8.5	-	Full	20.8	2.9	15.5	5.4	3	1.00	1.10	12.8
	97	99	48	2.00	2	0.9	N	10	6.76	-	Full	30.3	2.8	24.8	6.5	3	1.00	1.10	20.5
	97	99	48	3.07	3	1.0	N	10.0	11.9	-	FS	24.2	-	13.7	4.9	3	1.36	1.00	15.6
	596	397	194	3.07	3	1.0	S	10.0	17.7	-	FS	24.2	-	13.8	7.4	3	1.36	1.00	15.7
19	596	397	194	3.07	3	1.0	N	10.0	11.9	-	FS	17.8	-	10.3	4.2	3	1.36	1.00	11.7
	596	397	194	3.07	3	1.0	S	10.0	17.7	-	FS	17.8	-	10.6	6.1	3	1.36	1.00	12.0
	596	397	194	3.07	3	1.0	S	10.0	17.7	-	Full	24.2	-	18.6	5.4	3	1.00	1.10	17.1
	596	397	194	3.07	3	1.0	N	10.0	11.9	-	Full	17.8	-	13.6	3.1	3	1.00	1.10	12.5
	596	397	194	3.07	3	1.0	S	10.0	17.7	-	Full	17.8	-	14.3	4.0	3	1.00	1.10	13.1
	590	290	140	4.21	3	1.0	N	10.0	4.9	-	Full	13.4	2.1	9.2	15.2	5	1.00	1.10	7.6
	990	390	140	7.07	5	1.0	N	10.0	17.3	9	FS	23.2	2.7	16.6	3.7	3	1.00	1.00	13.9
	590	390	140	4.21	3	1.0	N	10.0	17.3	9	FS	23.2	2.7	16.1	8.1	3	1.00	1.00	13.5
	400	400	200	2.00	2	0.9	N	-	7.6	13	FS	18.9	10.3	16.8	11.3	6	1.00	1.00	12.3
	400	400	200	2.00	2	0.9	N	-	7.6	13	FS	18.9	10.3	16.8	11.3	6	1.00	1.00	12.3
	400	400	200	2.00	2	0.9	N	-	7.6	13	FS	18.9	10.3	16.8	11.3	6	1.00	1.00	12.3
	590	390	140	4.21	3	1.00	-	10.0	4.8	7	FS	14.4	-	10.1	10.0	3	1.00	1.00	8.4
	590	390	140	4.21	3	1.00	-	10.0	3.9	7	FS	20.7	-	15.9	10.0	3	1.00	1.00	13.3
	590	390	140	4.21	3	1.00	-	10.0	4.3	7	FS	35.5	-	20.6	10.0	3	1.00	1.00	17.2
	590	390	140	4.21	3	1.00	-	10.0	7.9	5	FS	14.4	-	12.2	10.0	3	1.00	1.00	10.2
23	97	99	48	2.00	2	0.9	N	10	6.76	-	Full	20.8	2.9	15.5	5.4	3	1.00	1.10	12.8
	97	99	48	3.07	3	1.0	N	10.0	11.9	-	FS	24.2	-	13.7	4.9	3	1.36	1.00	15.6
	596	397	194	3.07	3	1.0	S	10.0	17.7	-	FS	24.2	-	13.8	7.4	3	1.36	1.00	15.7
	596	397	194	3.07	3	1.0	N	10.0	11.9	-	FS	17.8	-	10.3	4.2	3	1.36	1.00	11.7
	596	397	194	3.07	3	1.0	S	10.0	17.7	-	FS	17.8	-	10.6	6.1	3	1.36	1.00	12.0
	596	397	194	3.07	3	1.0	S	10.0	17.7	-	Full	24.2	-	18.6	5.4	3	1.00	1.10	17.1
	596	397	194	3.07	3	1.0	N	10.0	11.9	-	Full	17.8	-	13.6	3.1	3	1.00	1.10	12.5
	596	397	194	3.07	3	1.0	S	10.0	17.7	-	Full	17.8	-	14.3	4.0	3	1.00	1.10	13.1
	590	290	140	4.21	3	1.0	N	10.0	4.9	-	Full	13.4	2.1	9.2	15.2	5	1.00	1.10	7.6
	990	390	140	7.07	5	1.0	N	10.0	17.3	9	FS	23.2	2.7	16.6	3.7	3	1.00	1.00	13.9
	590	390	140	4.21	3	1.0	N	10.0	17.3	9	FS	23.2	2.7	16.1	8.1	3	1.00	1.00	13.5
	400	400	200	2.00	2	0.9	N	-	7.6	13	FS	18.9	10.3	16.8	11.3	6	1.00	1.00	12.3
	400	400	200	2.00	2	0.9	N	-	7.6	13	FS	18.9	10.3	16.8	11.3	6	1.00	1.00	12.3
	400	400	200	2.00	2	0.9	N	-	7.6	13	FS	18.9	10.3	16.8	11.3	6	1.00	1.00	12.3
	590	390	140	4.21	3	1.00	-	10.0	4.8	7	FS	14.4	-	10.1	10.0	3	1.00	1.00	8.4
	590	390	140	4.21	3	1.00	-	10.0	3.9	7	FS	20.7	-	15.9	10.0	3	1.00	1.00	13.3
	590	390	140	4.21	3	1.00	-	10.0	4.3	7	FS	35.5	-	20.6	10.0	3	1.00	1.00	17.2
	590	390	140	4.21	3	1.00	-	10.0	7.9	5	FS	14.4	-	12.2	10.0	3	1.00	1.00	10.2

24	590	390	140	4.21	3	1.00	-	10.0	9.8	5	FS	20.7	-	17.2	10.0	3	1.00	1.00	14.4
	590	390	140	4.21	3	1.00	-	10.0	7.1	5	FS	35.5	-	23.6	10.0	3	1.00	1.00	19.7
	590	400	200	2.95	3	1.0	S	10.0	-	-	FS	18.7	2.0	15.1	10.0	5	1.00	1.00	12.6
	590	400	200	2.95	3	1.0	S	10.0	-	-	FS	16.7	1.1	11.6	10.0	5	1.00	1.00	9.7
25	-	-	-	-	3	1.0	S	-	-	-	FS	15.5	-	8.6	18.2	4	1.36	1.00	8.2
	-	-	-	-	3	1.0	S	-	-	-	FS	15.5	-	7.4	4.9	4	1.36	1.00	8.4
26	-	-	-	-	2	0.9	S	9.5	22.9	7	FS	23.8	3.1	17.0	19.7	5	1.36	1.00	14.1
	-	-	-	-	3	1.0	S	9.5	22.9	7	FS	23.5	2.4	16.9	12.7	5	1.36	1.00	18.2
	-	-	-	-	3	1.0	S	9.5	22.9	7	FS	25.5	3.9	18.2	7.7	5	1.36	1.00	20.7
	-	-	-	-	4	1.0	S	9.5	22.9	7	FS	21.9	1.1	15.6	10.6	5	1.36	1.00	17.5
	-	-	-	-	2	0.9	S	9.5	22.9	7	FS	19.5	2.5	13.1	17.9	5	1.36	1.00	11.4
	-	-	-	-	2	0.9	N	-	-	-	FS	13.6	0.7	5.7	6.8	10	1.36	1.00	5.9
27	390	390	140	2.79	2	0.9	N	10.0	6.6	-	FS	21.4	0.8	14.7	4.8	10	1.00	1.00	11.1
	590	390	140	4.21	3	1.0	N	10.0	6.6	-	FS	21.4	0.8	14.3	3.0	10	1.00	1.00	12.0
28	790	390	140	5.64	4	1.0	N	10.0	6.6	-	FS	21.4	0.8	13.9	4.3	10	1.00	1.00	11.6
	390	390	190	2.05	2	0.9	N	10.0	6.6	-	FS	22.0	1.9	14.9	3.6	10	1.00	1.00	11.2
	590	390	190	3.11	3	1.0	N	10.0	6.6	-	FS	22.0	1.9	14.5	5.4	10	1.00	1.00	12.1
	990	390	190	5.21	5	1.0	N	10.0	6.6	-	FS	22.0	1.9	14.3	3.9	10	1.00	1.00	12.0
29	590	390	190	3.11	3	1.0	PCL-N	10.0	7.4	12	FS	26.4	2.8	14.9	7	5	1.00	1.00	12.4
	590	390	190	3.11	3	1.0	MC-N	10.0	7.8	11	FS	26.4	2.8	17.4	2	5	1.00	1.00	14.6
	590	390	190	3.11	3	1.0	PCL-S	10.0	12.7	5	FS	26.4	2.8	19.2	10	5	1.00	1.00	16.1
	590	390	190	3.11	3	1.0	MC-S	10.0	13.8	19	FS	26.4	2.8	22.8	20	5	1.00	1.00	15.3
	590	390	190	3.11	3	1.0	PCL-N	10.0	7.4	12	FS	25.8	1.8	20.2	9	5	1.00	1.00	16.9
	590	390	190	3.11	3	1.0	MC-N	10.0	7.8	11	FS	25.8	1.8	21.6	10.0	5	1.00	1.00	18.0
	590	390	190	3.11	3	1.0	PCL-S	10.0	12.7	5	FS	25.8	1.8	23.3	3	5	1.00	1.00	19.5
	590	390	190	3.11	3	1.0	MC-S	10.0	13.8	19	FS	25.8	1.8	21.7	8	5	1.00	1.00	18.1
	590	390	190	3.11	3	1.0	PCL-N	10.0	7.4	12	FS	36.2	1.4	22.0	9	5	1.00	1.00	18.4
	590	390	190	3.11	3	1.0	MC-N	10.0	7.8	11	FS	36.2	1.4	27.6	7	4	1.00	1.00	23.1
	590	390	190	3.11	3	1.0	PCL-S	10.0	12.7	5	FS	36.2	1.4	27.3	8	5	1.00	1.00	22.8
	590	390	190	3.11	3	1.0	MC-S	10.0	13.8	19	FS	36.2	1.4	28.1	7	5	1.00	1.00	23.5

References

1. Cheema, T. S., & Klingner, R. E. (1984). Compressive Strength of Concrete Masonry Prisms. *American Concrete Institute Journal*, Nov./Dec., 88-97.
2. Ramamurthy, K., Sathish, V., & Ambalavanan, R. (2000). Compressive Strength Prediction of Hollow Concrete Block Masonry Prisms. *ACI Structural Journal*, 97(1), 61-67.
3. Drysdale, R. G., & Hamid, A. A. (1979). Behavior of Concrete Block Masonry Under Axial Compression. *ACI Journal*, June, 707-721.
4. Drysdale, R. G., & Hamid, A. A. (1983). Capacity of Concrete Block Masonry Prisms Under Eccentric Compressive Loading. *American Concrete Institute Journal*, Mar./Apr., 102-108.
5. Khalaf, F.M., Hendry, A.W., Fairbairn, D.R. (1994). Study of the Compressive Strength of Blockwork Masonry. *ACI Structural Journal*, 91(4), 367-376.
6. Maurenbrecher, A. H. P. (1986). Compressive Strength of Hollow Concrete Blockwork. *4th Canadian Masonry Symposium*, Fredericton, N.B., Canada., 2 997-1009.
7. Hamid, A.A., Drysdale, R.G., Heidebrecht, A.C. (1978). Effect of Grouting on the Strength Characteristics of Concrete Block Masonry. Proceedings of the North American Masonry Conference, Boulder, Colorado, 11-1 to 11-17.
8. Barbosa, C. S., Lourenco, P. B., & Hanai, J. B. (2009). On the compressive strength prediction for concrete masonry prisms. *Rilem: Materials and Structures*, doi:10.1617/s11527-009-9492-0
9. Khalaf, F. M. (1996). Factors Influencing Compressive Strength of Concrete Masonry Prisms. *Magazine of Concrete Research*, 48(174), 95-101.
10. Chahine, G. N., & Drysdale, R. G. (1989). Influence of Test Conditions on the Compressive Strength and Behaviour of Face Shell Mortar bedded Concrete Block Prisms. *5th Canadian Masonry Symposium*, Vancouver, B.C., Canada., 2 651-660.
11. Xie, H., Page, A. W., & Kleeman, P. W. (1992). An Investigation of the Compressive Failure Mechanism For Face-Shell Bedded Hollow Masonry. *6th Canadian Masonry Symposium*, Saskatoon, S.K., Canada. 97-108.
12. Duncan, L. J. (2008). Effect of Block Face Shell Geometry and Grouting on the Compressive Strength of Concrete Block Masonry. *MSc. Thesis to the Faculty of Graduate Studies*, University of Windsor.
13. Dhanasekar, M. (2004). Effect of Grout Confinement on the Compressive Strength of Masonry. *IE Journal*, 85, 25-30.
14. Phipps, M. E., Mirza, S. A., Bell, A. J., Pettit, G. J. L., Ormsher, M., & Lewis, N. G. (2001). Characteristic compressive strength of concrete block masonry. *The Structural Engineer*, 79(23/24), 31-38.

15. Maurenbrecher, A. H. P. (1985). Axial Compression Tests on Masonry Walls and Prisms. *Third North American Masonry Conference*, University of Texas Arlington. 19-1-19-14.
16. Paturova, A. (2006). The Influence of Vertical Reinforcement and Lateral Confinement on the Axial Capacity of Masonry Block Walls. *MSc. Thesis to the Faculty of Graduate Studies*, University of Saskatchewan.
17. Guo, P. (1991). Investigation and Modelling of the Mechanical Properties of Masonry. *PhD. Dissertation to the Faculty of Graduate Studies. McMaster University*.
18. Hamid, A. A., & Abboud, B. E. (1986). Effect of Block Geometry on the Compressive Strength of Concrete Block Masonry. *4th Canadian Masonry Symposium*, University of New Brunswick., 1 290-298.
19. Gaynor, P., Woodward, K., Scribner, C. (1987). Influence of Mortar Bedding on Masonry Prism Behavior. U.S. Department of Commerce, National Bureau of Standards, Report NBSIR 86-3467.
20. Andolfato, R. P., Camacho, J. S., & Ramalho, M. A. (2007). Brazilian Results on Structural Masonry Concrete Blocks. *American Concrete Institute Materials Journal*, 104(1), 33-39.
21. Hou, J. (2006). Strain Gradient Effect on the Behaviour and Strength of Masonry Prisms. *Master of Applied Science, Dalhousie University*.
22. Page, A.W., Shrive, N.G. (1990). Concentrated Loads on Hollow Concrete Masonry. *ACI Structural Journal*, July-August.
23. Roman, H.R., Romagna, R.H. (2002). Compressive Strength of Grouted and Un-grouted Concrete Block Masonry.
24. Yi, J. (2002). Design Rules for Hollow Concrete Masonry Walls Subjected to concentrated Loads. (Doctor of Philosophy, University of Calgary). *The University of Calgary*,
25. Olatunji, T.M., Warwaruk, J., Longworth, J. (1986). Behaviour and Strength of Masonry Wall/Slab Joints. University of Alberta Structural Engineering Report 139.
26. Hawk, McLean, Young. 1997.
27. Maurenbrecher, A.H.P. (1983). Compressive Strength of Eccentrically Loaded Masonry Prisms. Third Canadian Masonry Symposium. Edmonton, Alberta, Canada, 10-1 to 10-13.
28. Maurenbrecher, A. H. P. (1980). *Effect of Test Procedures on Compressive Strength of Masonry Prisms* No. NRCC-0018490). Ottawa, Canada: National Research Council of Canada.
29. Gayed, M., Korany, Y. (2011). Compressive Testing on Hollow Concrete Block Masonry Prisms. University of Alberta, Canada, Unpublished.

APPENDIX II

COMPRESSIVE STRENGTH OF GROUTED PRISMS

Reference	Prism Dimensions, mm					Mortar properties					Block		Grout		Prism		
	Height (h)	Length	Thickness (t)	h/t	Courses	Correction factor	Type	Thickness	Strength	St. Dev.	C.O.V	Average Compressive Strength	St. Dev.	Average Compressive Strength	C.O.V.	Number of Prisms	Calculated Specified Strength f'm
												(MPa)	(MPa)	(MPa)	(%)		
1	397	397	194	2.05	2	0.80	S	9.5	12.4	1.5	12	25.9	4.8	30.0	13.1	8	9.8
	397	397	194	2.05	2	0.80	S	9.5	12.1	1.7	14	25.9	4.8	24.6	13.7	3	11.4
	397	397	194	2.05	2	0.80	S	9.5	12.1	1.7	14	25.9	4.8	24.6	15.6	7	13.0
	397	397	194	2.05	2	0.80	S	9.5	12.1	1.7	14	25.9	4.8	24.6	15.4	11	12.6
	397	397	194	2.05	2	0.80	S	9.5	12.1	1.7	14	25.9	4.8	24.6	16.2	7	13.6
2	600	-	178	3.38	3	0.92	S	9.5	15.1	-	-	19.7	0.8	15.9	10.8	6	9.1
	600	-	178	3.38	3	0.92	S	9.5	16.7	-	-	19.7	0.8	15.3	11.2	6	9.3
	600	-	178	3.38	3	0.92	S	9.5	17.3	-	-	19.7	0.8	15.3	11.3	4	9.5
	600	-	178	3.38	3	0.92	S	9.5	14.2	-	-	19.7	0.8	15.3	11.3	14	8.8
	600	-	178	3.38	3	0.92	S	9.5	15.8	-	-	19.7	0.8	21.3	12.8	6	10.7
	600	-	178	3.38	3	0.92	S	9.5	13.5	-	-	19.7	0.8	17.4	12.1	3	10.1
	600	-	178	3.38	3	0.92	S	9.5	14.2	-	-	32.2	2.2	19.8	16.9	2	14.1
	600	-	178	3.38	3	0.92	S	9.5	14.2	-	-	22.0	0.9	22.0	13.2	4	11.0
	600	-	178	3.38	3	0.92	S	9.5	14.2	-	-	21.3	1.3	22.0	14.1	5	11.8
	600	-	178	3.38	3	0.92	S	9.5	14.2	-	-	20.1	1.1	19.8	12.1	1	10.2
	600	-	178	3.38	3	0.92	S	9.5	14.2	-	-	20.0	1.2	22.0	14.7	9	12.3
	600	-	178	3.38	3	0.92	S	9.5	14.2	-	-	15.7	1.3	21.4	9.2	3	7.7
	600	-	178	3.38	3	0.92	S	9.5	12.8	-	-	19.7	0.8	16.5	11.9	5	10.0
	600	-	178	3.38	3	0.92	S	9.5	12.8	-	-	19.7	0.8	16.5	13.3	5	11.1
	590	195	190	3.11	3	0.91	S	10.0	17.0	-	-	25.1	-	21.1	14.4	3	12.0
3	590	195	190	3.11	3	0.91	S	10.0	17.0	-	-	25.1	-	13.7	14.1	11	11.5
	590	195	190	3.11	3	0.91	S	10.0	17.0	-	-	17.1	-	21.1	11.0	16	8.1
	590	195	190	3.11	3	0.91	S	10.0	17.0	-	-	27.9	-	21.1	15.0	7	12.5
	590	195	190	3.11	3	0.91	S	10.0	17.0	-	-	20.2	-	21.1	14.1	2	11.8
	590	195	190	3.11	3	0.91	S	10.0	17.0	-	-	22.2	-	21.1	14.5	5	12.1
	590	195	140	4.21	3	0.96	S	10.0	17.0	-	-	23.6	-	21.1	13.8	7	11.5
	590	195	240	2.46	3	0.85	S	10.0	17.0	-	-	23.4	-	21.1	11.4	12	9.2
	600	178	143	4.20	3	0.96	S	9.5	14.5	-	8	19.7	0.8	12.4	11.3	14	8.8
	600	178	143	4.20	3	0.96	S	9.5	18.2	-	6	19.7	0.8	14.1	12.1	3	10.1
	600	178	143	4.20	3	0.96	N	9.5	5.7	-	5	19.7	0.8	14.1	10.4	3	8.7
4	600	178	143	4.20	3	0.96	S	9.5	14.5	-	8	19.7	0.8	17.3	12.8	6	10.7
	600	178	143	4.20	3	0.96	S	9.5	14.5	-	8	19.7	0.8	25.0	13.4	7	11.2
	600	178	143	4.20	3	0.96	S	9.5	14.5	-	8	19.7	0.8	14.1	12.1	3	10.1
	590	390	190	3.11	3	0.91	N	10.0	5.6	-	-	13.1	-	14.8	7.9	0	6.6
	590	390	190	3.11	3	0.91	N	10.0	5.6	-	-	13.1	-	20.3	9.1	0	1
	590	390	190	3.11	3	0.91	N	10.0	8.4	-	-	13.1	-	14.8	8.7	0	1
	590	390	190	3.11	3	0.91	N	10.0	8.4	-	-	13.1	-	20.3	9.9	0	1
	590	390	190	3.11	3	0.91	N	10.0	12.4	-	-	13.1	-	14.8	10.5	0	1
	590	390	190	3.11	3	0.91	S	10.0	12.4	-	-	13.1	-	20.3	11.2	0	1
	590	390	190	3.11	3	0.91	N	10.0	5.6	-	-	16.7	-	14.8	8.3	0	1
5	590	390	190	3.11	3	0.91	N	10.0	5.6	-	-	16.7	-	20.3	9.5	0	1
	590	390	190	3.11	3	0.91	N	10.0	8.4	-	-	16.7	-	14.8	9.2	0	1
	590	390	190	3.11	3	0.91	N	10.0	8.4	-	-	16.7	-	20.3	10.3	0	1
	590	390	190	3.11	3	0.91	S	10.0	12.4	-	-	16.7	-	14.8	11.2	0	1
	590	390	190	3.11	3	0.91	S	10.0	12.4	-	-	16.7	-	14.8	11.2	0	1
	590	390	190	3.11	3	0.91	S	10.0	12.4	-	-	16.7	-	14.8	11.2	0	1
	590	390	190	3.11	3	0.91	S	10.0	12.4	-	-	16.7	-	14.8	11.2	0	1

6	590	390	190	3.11	3	0.91	S	10.0	12.4	-		16.7	20.3	11.7	0	1	9.8	
	590	390	190	3.11	3	0.91	N	10.0	5.6	-		20.0	14.8	8.5	0	1	7.1	
	590	390	190	3.11	3	0.91	N	10.0	5.6	-		20.0	20.3	9.7	0	1	8.1	
	590	390	190	3.11	3	0.91	N	10.0	8.4	-		20.0	14.8	9.4	0	1	7.8	
	590	390	190	3.11	3	0.91	N	10.0	8.4	-		20.0	20.3	10.5	0	1	8.8	
	590	390	190	3.11	3	0.91	S	10.0	12.4	-		20.0	14.8	11.5	0	1	9.6	
	590	390	190	3.11	3	0.91	S	10.0	12.4	-		20.0	20.3	11.8	0	1	9.9	
	397	194	194	2.05	2	0.80	S	-	22.0			25.0	15.9	18.5	2	5	15.5	
	590	390	190	3.11	3	0.91	-	10.0	9.2	-	-	24.3	-	19.4	15.8	13	3	12.5
	590	390	190	3.11	3	0.91	-	10.0	13.5	-	-	24.3	-	32.0	17.9	3	3	15.0
7	590	390	190	3.11	3	0.91	-	10.0	15.4	-	-	24.3	-	8.6	13.8	9	3	11.5
	590	390	190	3.11	3	0.91	-	10.0	15.4	-	-	24.3	-	15.7	11.4	2	3	9.5
	590	390	190	3.11	3	0.91	-	10.0	20.2	-	-	24.3	-	23.5	13.4	8	3	11.2
	390	390	190	2.05	2	0.81	-	10.0	21.2	-	-	24.3	-	17.1	16.8	6	2	14.0
	390	195	190	2.05	2	0.81	-	10.0	21.2	-	-	24.3	-	17.1	23.2	2	2	19.4
	406	394	152	2.66	4	0.87	N(1:1:6)	-	11.6	-	10	24.7	-	29.2	28.2	10	5	23.6
	406	394	102	4.	4	0.95	N(1:1:6)	-	11.6	-	10	26.9	-	29.2	21.0	10	5	17.5
	406	394	203	2.	4	0.80	N(1:1:6)	-	11.6	-	10	21.6	-	29.2	27.9	10	5	23.3
	406	394	152	2.66	4	0.87	N(1:1:6)	-	11.6	-	10	24.7	-	29.2	25.0	10	5	20.9
	8	406	394	152	2.66	4	0.87	(1:1/2:4-1/2)	-	24.3	8	24.7	-	29.2	28.8	10	5	24.1
9	406	394	152	2.66	4	0.87	N(1:1:6)	-	11.6	10	24.7	-	30.6	29.0	10	5	24.2	
	406	394	152	2.66	4	0.87	N(1:1:6)	-	11.6	10	24.7	-	29.2	28.8	10	5	24.1	
	406	394	152	2.66	4	0.87	N(1:1:6)	-	11.6	10	24.7	-	29.2	24.1	10	5	20.1	
	416	406	203	2.05	2	0.80	S	10.0	11.2	-	-	24.5	-	15.5	17.1	6	3	14.3
	629	406	203	3.1	3	0.90	S	10.0	11.2	-	-	24.5	-	15.5	14.8	6	3	12.4
	842	406	203	4.14	4	0.96	S	10.0	11.2	-	-	24.5	-	15.5	13.2	6	3	11.0
	1055	406	203	5.19	5	1.00	S	10.0	11.2	-	-	24.5	-	15.5	12.6	6	3	10.5
	416	406	203	2.05	2	0.80	S	10.0	11.2	-	-	21.0	-	15.5	16.2	6	3	13.5
	629	406	203	3.1	3	0.90	S	10.0	11.2	-	-	21.0	-	15.5	15.0	6	3	12.5
	842	406	203	4.14	4	0.96	S	10.0	11.2	-	-	21.0	-	15.5	14.6	6	3	12.2
10	1055	406	203	5.19	5	1.00	S	10.0	11.2	-	-	21.0	-	15.5	14.8	6	3	12.4
	-	-	-	4.	4	0.95	S	-	10.9	-	-	25.0	-	10.2	12.9	5	5	10.8
	-	-	-	4.	4	0.95	S	-	10.9	-	-	25.0	-	11.6	14.0	5	5	11.7
	-	-	-	4.	4	0.95	S	-	11.3	-	-	25.0	-	34.9	14.8	11	5	12.2
	-	-	-	4.	4	0.95	S	-	11.3	-	-	25.0	-	37.4	13.6	8	5	11.4
11	990	390	140	7.07	5	1.00	N	10.0	17.3	1.6	9	23.2	2.7	15.3	10.6	2	3	8.9
	590	390	140	4.21	3	0.96	N	10.0	17.3	1.6	9	23.2	2.7	15.3	10.9	12	3	8.8
	590	390	140	4.21	3	0.96	-	10.0	7.9	-	5	14.4	-	12.5	13.1	10	3	11.0
	590	390	140	4.21	3	0.96	-	10.0	9.8	-	5	20.7	-	28.5	18.5	10	3	15.5
12	590	390	140	4.21	3	0.96	-	10.0	7.1	-	5	35.5	-	34.7	25.1	10	3	21.0
	-	-	-	3.16	3	0.91	S	-	-	-	-	15.5	-	11.4	10.7	10	4	9.0
	-	-	-	3.16	3	0.91	S	-	-	-	-	15.5	-	11.4	8.4	10	4	7.0

References

1. Cheema, T. S., & Klingner, R. E. (1984). Compressive Strength of Concrete Masonry Prisms. *American Concrete Institute Journal*, Nov./Dec., 88-97.
2. Drysdale, R. G., & Hamid, A. A. (1979). Behavior of Concrete Block Masonry Under Axial Compression. *ACI Journal*, June, 707-721.
3. Drysdale, R. G., & Hamid, A. A. (1983). Capacity of Concrete Block Masonry Prisms Under Eccentric Compressive Loading. *American Concrete Institute Journal*, Mar./Apr., 102-108.
4. Hamid, A.A., Drysdale, R.G., Heidebrecht, A.C. (1978). Effect of Grouting on the Strength Characteristics of Concrete Block Masonry. Proceedings of the North American Masonry Conference, Boulder, Colorado, 11-1 to 11-17.
5. Fahmy, E.H., Ghoneim, T.G.M. (1995). Behaviour of Concrete Block Masonry Prisms under Axial Compression. *Canadian Journal of Civil Engineering*, 898-915.
6. Thompson, Walloch, Thomas. (2002).
7. Khalaf, F. M. (1996). Factors Influencing Compressive Strength of Concrete Masonry Prisms. *Magazine of Concrete Research*, 48(174), 95-101.
8. Kingsley, G. R., Atkinson, R. H., Noland, J. L., & Hart, G. C. (1989). The effect of Height on Stress-Strain measurements on Grouted Concrete Masonry Prisms. *5th Canadian Masonry Symposium*, Vancouver, B.C., Canada. , 2 587-589.
9. Boul, B. F. (1979). Concrete Masonry Prism Testing. *ACI Journal*, April, 513-535.
10. Guo, P. (1991). Investigation and Modelling of the Mechanical Properties of Masonry. *PhD. Dissertation to the Faculty of Graduate Studies. McMaster University*.
11. Hou, J. (2006). Strain Gradient Effect on the Behaviour and Strength of Masonry Prisms. *Master of Applied Science, Dalhousie University*.
12. Roman, H.R., Romagna, R.H. (2002). Compressive Strength of Grouted and Un-grouted Concrete Block Masonry.
13. Olatunji, T.M., Warwaruk, J., Longworth, J. (1986). Behaviour and Strength of Masonry Wall/Slab Joints. University of Alberta Structural Engineering Report 139.