Effect of High Pressure CO2 Treatment on the Moisture Sorption Isotherm

and

Physicochemical Properties of Beef Jerky

by

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Abstract

High pressure carbon dioxide (HPCD) treatment is a promising non-thermal pasteurization technique, targeting the enhancement of food safety by inactivating microorganisms without sacrificing quality. Even though this technique is effective for high moisture foods, research on products with a low water activity (a_w) is limited. Beef jerky, as a low a_w ready-to-eat snack, has become more popular because of the growing trend of high-protein and low-carb diets. The objective of this thesis research was to investigate the effects of HPCD treatment on the moisture sorption behavior and physicochemical properties of beef jerky.

Moisture sorption isotherms (MSIs), monolayer water content (M_0) and net isosteric heat of sorption (q_{st}) were determined under air and CO₂ environments at ambient pressure, as well as HPCD environment. MSI data were described mathematically by fitting into six isotherm equations. The deviation of the models used to fit the data increased under CO₂ atmosphere at ambient pressure and HPCD conditions. At ambient pressure, compared to the air environment, samples in CO₂ environment had higher a_w at a given moisture content. Under HPCD environment, the shape of MSIs changed from type II to type III and the isotherms became very steep at a_w levels of 0.73 and 0.70 at high pressures of 57 and 200 bar, respectively. Monolayer water content decreased with temperature, but pressure did not have a significant effect on M_0 . Net isosteric heat of sorption in CO₂ environment was higher than that in air environment and the differential between the two environments decreased when the moisture content was increased.

The effects of HPCD processing parameters, including pressure, temperature, processing time and depressurization rate, on the physicochemical properties, including, a_w, surface color,

fat content, and Warner-Bratzler shear force, of beef jerky were studied by response surface methodology (RSM). Water activity decreased after HPCD treatment and temperature had a significant effect. In terms of surface color profile, L, a, b values increased after HPCD treatment and pressure had a significant effect on L value, no processing parameter showed a significant effect on a value, and pressure, quadratic pressure and depressurization rate had a significant effect on b value. After HPCD treatment, fat content of beef jerky was reduced slightly but no processing parameter had a significant effect. Warner-Bratzler shear force was either increased or decreased after HPCD treatment, where quadratic depressurization rate and linear temperature had a significant effect. An optimum HPCD treatment condition, that is, pressure of 92.9 bar, temperature of 59.1°C, processing time of 35.9 min and depressurization rate of 56.3 bar/min, was determined via the RSM model to minimize the changes in responses.

The results obtained from this thesis research provide valuable information on further understanding of moisture sorption behavior during HPCD treatment that would contribute to elucidation of the microbial inactivation mechanism and the impact of HPCD treatment on the quality attributes of a low a_w food product like beef jerky.

Preface

This thesis is an original work by Yanzhao Ren under the supervision of Dr. Feral Temelli. There are a total five chapters in the thesis: Chapter 1 provides introduction and the overall objectives of this thesis study; Chapter 2 is a literature review on topics related to this research; Chapter 3 focuses on the effect of high pressure CO₂ environment on the moisture sorption isotherm of beef jerky; Chapter 4 investigates the effect of high pressure CO₂ treatment on the physicochemical properties of beef jerky; and Chapter 5 provides the overall conclusions and recommendations. These works were carried out by Yanzhao Ren by developing the specific experimental designs, experimental protocols, conducting experiments, performing data analysis and writing the first drafts and editing of the manuscripts under the guidance of Dr. Temelli. Of course, all of these works cannot be done without help from the people mentioned in the acknowledgements.

Manuscripts based on Chapters 3 and 4 are in preparation for submission to peer-reviewed journals for consideration for publication. Results of Chapter 3 were presented as a poster at the 17th European Meeting on Supercritical Fluids as "Effect of high pressure and CO₂ environment on the moisture sorption isotherm of beef jerky" by Yanzhao Ren and Feral Temelli in Ciudad Real, Spain on April 8-11, 2019.

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List of Abbreviations

| а | Hunter color index a, red-green |
|----------|---|
| А, В, С | Constants |
| ANOVA | Analysis of variance |
| a_{w} | Water activity |
| AWM | a _w measurement |
| b | Hunter color index b, blue-yellow |
| CCRD | Central composite rotatable design |
| CO_2 | Carbon dioxide |
| d | Desirability |
| DR | Depressurization rate |
| Ε | Mean relative percentage deviation |
| HH | Hailwood and Horrobin equation |
| H-IC | Halsey-Iglesias and Chirife equation |
| HPCD | High pressure carbon dioxide |
| IC | Iglesias and Chrife equation |
| GAB | Guggenheim, Anderson and de Boer equation |
| k | Number of independent parameters |
| L | Hunter color index L, lightness |
| M_0 | Monolayer water content |
| M, MC | Moisture content |
| MSI | Moisture sorption isotherm |
| Ν | Newtons |
| Р | Pressure |
| Pc | Critical pressure |
| q_{st} | Heat of sorption |
| R | Gas constant R=8.314 J/(mol-K) |
| RSM | Response surface methodology |
| SDS-PAGE | Sodium dodecyl sulfate-polyacrylamide gel electrophoresis |

| - |
|--|
| Processing time |
| Temperature |
| Critical temperature |
| Warner-Bratzler shear force |
| Molar volume of the liquid |
| Mole fraction of H ₂ O |
| Coded process variables |
| Responses of untreated sample |
| Responses of treated sample |
| Response differences |
| Constant |
| The first degree coded input parameters |
| The second degree coded input parameters |
| The interaction of linear parameters |
| Error term |
| |

Chapter 1: Introduction and objectives

Generally, low water activity (a_w) foods (a_w<0.85) are considered as shelf-stable at ambient temperature because low a_w places osmotic stress on bacteria and less water is available for bacterial growth (Borowski, Ingham, and Ingham, 2009; Kimber, Kaur, Wang, Danyluk, and Harris, 2012; FAO. WHO, 2015). Normally, low a_w foods like nuts may have a year or more of shelf life. However, numerous studies have demonstrated that *Escherichia coli* and *Salmonella* can survive on low a_w foods (Hiramatsu, Matsumoto, Sakae and Miyazaki, 2005; Gruzdew, Pinto and Sela Saldinger, 2012). These microorganisms can grow and cause infections upon reaching the gastrointestinal tract after ingestion of a contaminated product and seriously threaten the health of consumers (Aviles, Klotz, Smith, Williams and Ponder, 2013).

CO₂ has been used as an antimicrobial agent for more than 100 years because of its natural characteristics, including microbial inhibition effect near atmospheric pressure, being non-toxic and that it can be easily removed from food products (Valley and Rettger, 1927; Jones and Greenfield, 1982; Eklund, 1984; Dixon and Kell, 1989). More recently, it has been found that pressurised CO₂ is no longer bacteriostatic, but bactericidal (Nakamura et al., 1994; Enomoto et al., 1997; Erkmen, 2000; Calvo and Balcones, 2001; Garcia-Gonzalez et al. 2007). High pressure CO₂ (HPCD) treatment as a food processing technique was found to show a microbial inactivation effect. However, microbial inactivation strongly depends on a_w of the food where low a_w products are more challenging to treat. Haas et al. (1989) even suggested that a HPCD treatment would not be applicable to dry substances. On the contrary, Dillow, Dehghani, Hrkach, Foster and Langer (1999) reported that *E. coli* cells were inactivated by HPCD in the absence of water. According to Statistica (2019), there is a growing demand for beef jerky due to its convenience, nutritional value as a protein source, and the popularity of low-carb and low-fat diets. Schultze (2019) found that *E. coli* AW 1.7, MG1655 and the Shiga toxin-producing *E. coli* cocktail inoculated onto beef jerky were inactivated successfully by treatment with CO₂ saturated with water at 65 °C and 57 bar for 15 min. Therefore, for beef jerky, HPCD is a promising non-thermal pasteurisation technology to extend its shelf life and enhance its safety with a minimal change in its nutritional value. However, some studies reported that HPCD treatment can lead to a change in physicochemical properties, including surface colour and tenderness of meat products (Cappelletti, Ferrentino and Spilimbergo, 2015). Nevertheless, available literature focusing on the effects of HPCD treatment on the physicochemical quality of meat products is limited to provide guidance in this regard.

Moisture plays an important role in microbial inactivation by HPCD and HPCD treatment can have an impact on the physicochemical properties of a food product. However, the literature lacks information on these aspects. Therefore, it was hypothesized that:

- 1) HPCD environment affects the moisture sorption behavior of beef jerky; and
- 2) HPCD treatment affects the physicochemical properties of beef jerky.

The objectives of this thesis research were to:

1) study the moisture sorption behavior of beef jerky under HPCD conditions (Chapter 3); and

2) investigate the influence of HPCD treatment parameters on the physicochemical properties of beef jerky (Chapter 4).

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Chapter 2: Literature review

2.1 High pressure carbon dioxide (HPCD) treatment and microbial inactivation

2.1.1 HPCD treatment

High pressure CO_2 (HPCD) technique refers to treating foods with either sub- or supercritical CO₂ for a certain period of time in a batch, semi-continuous or continuous manner. Supercritical CO₂ is CO₂ at a temperature and pressure above its critical point ($T_c=31.1$ °C, $P_c=73.8$ bar), and exhibits the unique ability to diffuse through solids like a gas, and dissolve different solutes like a liquid. Subcritical CO_2 is CO_2 at a temperature or pressure below its critical point values (Garcia-Gonzalez et al., 2007). HPCD has antimicrobial effects in various liquid and solid food systems (Garcia-Gonzalez et al., 2007). For example, Wei, Balaban, Fernando and Peplow (1991) found that HPCD could reduce Listeria in shrimp, orange juice and egg yolk and Salmonella in chicken and egg yolk effectively. As a solvent, CO₂ is relatively inert, inexpensive, non-toxic, non-flammable, recyclable, readily available in high purity, and leaves no residue (Choi et al., 2007). Additionally, HPCD technique is classified as a cold pasteurization method because application of relatively low temperatures can result in inhibition of microorganisms. Compared to heat treatment, HPCD is believed to involve fewer changes in taste, color, texture and nutritional quality in foods (Damar and Balaban, 2006). As a result, HPCD can be applied as a processing aid to foods. According to Health Canada, a processing aid is defined as "a substance that is used for a technical effect during food processing or manufacture but, unlike food additives, its use does not affect the intrinsic characteristics of the food and it results in no or negligible residues of the substance or its by-products in or on the finished food" (Health Canada, 2018). Therefore, HPCD is a promising clean-label technology to

extend food shelf life with minimal changes in quality because processing aids do not need to be disclosed on labels (Health Canada, 2018).

2.1.2 Mechanism of microbial inactivation

As an alternative non-thermal pasteurization technique for foods, the pressures employed during HPCD treatment, compared to high hydrostatic pressure (HHP) technique, are much lower (generally <200 bar) than that used in HHP (~3000-6000 bar). However, the exact inactivation mechanisms still remain to be unraveled. Garcia-Gonzalez et al. (2007) summarized comprehensively how HPCD exerts its lethal action on bacteria in the following steps. Garcia-Gonzalez et al. (2007) emphasized that these steps will not occur consecutively but rather take place simultaneously in a complex and interrelated manner.

2.1.2.1 Solubilization of CO₂ in the external liquid phase

In foods with a high water content, CO_2 can dissolve in the water to form carbonic acid, which dissociates into bicarbonate (HCO₃⁻), carbonate (CO₃²⁻) and hydrogen (H⁺) ion species according to the following equilibria (Eq. 2.1-2.4) (Garcia-Gonzalez et al., 2007):

$$CO_{2}(g) \bigoplus CO_{2}(aq)$$

$$[CO_{2}]_{aq} = H * p_{CO2} \text{ with } H = 3.3*10^{-2} \text{ mol}/(L \text{ atm}) (25 °C)$$
(2.1)

$$CO_{2}(aq) + H_{2}O \bigoplus H_{2}CO_{3}$$

$$[H_{2}CO_{3}]/[CO_{2}]_{aq} = 1.7 * 10^{-3} \text{mol}/L (25 °C)$$
(2.2)

$$H_{2}CO_{3} \bigoplus H^{+} + HCO_{3}^{-}$$

$$[HCO_{3}^{-}] [H^{+}]/[H_{2}CO_{3}] = 2.5 * 10^{-4} \text{ mol}/L (25 °C)$$
(2.3)

 $HCO_3^- \rightarrow H^+ + CO_3^{2-}$

$$[CO_3^{2-}] [H^+]/[HCO_3^{-}] = 5.61 * 10^{-11} \text{ mol/L } (25 \text{ °C})$$
(2.4)

As a consequence, external water in contact with HPCD becomes acidic due to the formation and dissociation of H₂CO₃. The decrease in external pH may inhibit microbial growth (Hutkins and Nannen, 1993) and increase energy consumption by bacteria to maintain homeostasis (Hong, Park and Pyun, 1999). However, the reduction of external pH cannot fully explain the inactivation effect of HPCD because stronger acids like hydrochloric acid or phosphoric acid cannot exert a comparable reduction (Haas et al., 1989; Wei, Balaban, Fernando, and Peplow, 1991; Lin et al., 1993; Debs-Louka, Louka, Abraham, Chabot and Allaf, 1999).

2.1.2.2 Cell membrane modification

Because of the high affinity between CO_2 and the plasma membrane, CO_2 can be dissolved in the phospholipids of a model cell membrane to a high extent (Spilimbergo, 2002). Jones and Greenfield (1982) also suggested that the HCO_3^- ion may act on the charged phospholipid head groups and the proteins on the membrane. Due to the presence of dissolved CO_2 and HCO_3^- , the cell membrane can be modified structurally and functionally (Jones and Greenfield, 1982; Isenschmid, Marison and Von Stockar, 1995).

2.1.2.3 Intracellular pH decrease

With CO_2 penetrating through the bacterial cell membrane, more CO_2 accumulates in the cytoplasm of the cells. Inside the cell, CO_2 acts as a reactant and shifts the equilibrium to the products, resulting in the formation of carbonic acid and carbonate, bicarbonate and hydrogen ions (Eq. 2.1-2.4). At the beginning, the cell attempts to maintain homeostasis using pH

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buffering systems, including cytoplasmic buffering, proton pumps, membrane-bound H⁺-ATPases, and the production of acids or bases (Booth, 1985; Hutkins and Nannen, 1993). However, the intracellular pH would start decreasing after the buffering ability is exceeded (Damar and Balaban, 2006; Garcia-Gonzalez et al., 2007). According to Spilimbergo, Bertucco, Basso and Bertoloni (2005), intracellular pH of *Bacillus subtilis* decreased to 3.3 upon HPCD exposure (8 MPa, 30 °C, 5 min).

2.1.2.4 Key enzyme inactivation/cellular metabolism inhibition

According to Hutkins and Nanen (1993), the lowering of the cytosolic pH might significantly impact the activity of key enzymes, involved in essential metabolic and regulating processes for the bacteria cell, such as glycolysis, amino acid and peptide transport, active transport of ions and proton translocation. According to Hong and Pyun (2001), some enzymes lost their activities significantly by HPCD treatment in *Lactobacillus plantarum*. Spilimbergo (2002) also found that several enzymes were inactivated by HPCD treatment in *B. subtilis*.

In addition to pH, the concentrations of CO_2 and HCO_3^- are also important in the regulation of enzymatic activity by either promoting or inhibiting carboxylation and decarboxylation reactions (Jones and Greenfield, 1982). Specifically, CO_2 is a substrate in the carboxylation reaction and a product in the decarboxylation reaction. As a result, cell metabolism is affected with increasing concentration of CO_2 by regulating equilibrium balance of these metabolic reactions (Jones and Greenfield, 1982).

2.1.2.5 Disordering of the intracellular electrolyte balance

According to Lin et al. (1993), intracellular inorganic electrolytes, including Ca^{2+} and Mg^{2+} could precipitate in the presence of CO_3^{2-} . These inorganic electrolytes play important roles

not only in a large number of cell activities but also in maintaining the osmotic relationships between cells and their surrounding media. Additionally, collapse of the proton motive force across the membrane disorders cytosolic Ca^{2+} levels, because Ca^{2+} extrusion is catalyzed by a Ca^{2+}/H^+ antiporter driven by the proton motive force (Gangola and Rosen, 1987).

2.1.2.6 Removal of vital constituents

Last but not least, the physical disruption of cells was the first explanation for the bacterial inactivation after release of CO₂. HPCD treatment involving rapid depressurization results in the expansion of CO₂ in the cells, leading to cellular disruption (Damar and Balaban, 2006). Besides, Kmihira, Taniguchi and Kobayashi (1987) and Lin et al. (1992, 1993) reported that CO₂ could extract vital constituents from the cell or cell membranes because of its relatively high solvating power, especially under supercritical conditions. The removal of constituents not only disturbs the structure of the bio-membrane but also alters the balance of the biological system, and as a result, promoting inactivation (Lin et al., 1992, 1993).

2.1.3 Importance of water

2.1.3.1 Effect of moisture content

Different studies have shown that foods with a low moisture content were poorly inactivated by HPCD (Haas, Prescott, Dudley, Dik, Hintlian, and Keane, 1989; Nakamura, Enomoto, Fukushima, Nagai and Hakoda, 1994; Kumagai, Hata and Nakamura, 1997; Debs-Louka, Louka, Abraham, Chabot and Allaf, 1999; Schmidt, Beermann, Bach and Schollmeyer, 2005). For example, Kumugai et al. (1997) found the first order sterilization rate constant to be almost zero at a moisture content below 0.2 g/g of dry matter, and the sterilization rate tended to increase with increasing moisture content of up to 1 g/g of dry matter. The reason for why dry microbial cells are more challenging to be inactivated by HPCD is probably the result of a decrease in the amount of CO₂ solubilized in the dry cell (Steps 1 and 3 in mechanism of inactivation). The acidification of the extra- and intra-cellular environment through dissociation reaction is dependent on the presence of water. An increased amount of formation and dissociation of H₂CO₃ would release more H⁺ ions that reduce the pH of the external suspending medium (Step 1 of the mechanism of inactivation). Additionally, Lin, Yang and Chen (1993) attributed the synergistic effect of water to swollen cell walls and membranes so that these biological barriers become more penetrable by CO₂.

2.1.3.2 Water-CO₂ interactions

To better understand the impact of HPCD treatment on low a_w products, it is also necessary to understand how water behaves under HPCD environment. The solubility of water in HPCD was studied by different researchers (Chrastil, 1982; King, Mubarak, Kim and Bott, 1992; Bamberger, Sieder, and Maurer, 2004; Tabasinejad et al., 2011; Ahmad, Gersen, and Wilbers, 2014; Comak et al., 2016). Recently, Wang, Zhou, Guo, Yang, and Lu (2018) determined the water solubility in supercritical CO₂ from 40 to 200 °C and from 100 to 500 bar by in-situ quantitative Raman spectroscopy (Fig. 2.1). Wang et al. (2018) found that at constant pressure, water solubility in HPCD increases exponentially with increasing temperature. At low temperatures (40-100 °C), water solubility increases with increasing pressure, but at high temperatures (140-200 °C), water solubility decreases with increasing pressure. From 100 to 140 °C, water solubility first decreases with increasing pressure (pressure < 20 bar), and then increases with increasing pressure (pressure > 20 bar).

The intermolecular interaction of water in HPCD as a solvent was studied by some authors (Tucker, 1999; Kajimoto, 1999) but they reached different conclusions. Clarke, Harrison, Johnston, and Howdle (1997) concluded that water is almost free in HPCD (T=32 °C, P=156 bar) environment. In contrast, Bowman et al. (1996) argued that the rotation of water in CO₂ was hindered because of dipole-quadrupole interaction between water and CO₂. Tassaing, Oparin, Danten, and Besnard (2005) studied water-CO₂ interaction in supercritical CO₂ by infrared spectroscopy and vibrational frequency shift calculation. Tassaing et al. (2005) found that dispersive and dipole-quadrupole interactions are dominant in the stabilisation energy of water-CO₂ pair, and that water acts as an attractive solute (the attractive forces between water and CO₂ leading to the clustering of solvent molecules around water) in the hyper-compressible regime in the vicinity of the critical point of the solvent.



Figure 2.1. Water solubility in CO₂ (x_{H2O}) as a function of pressure (*P*). ●, 40 °C; ■, 60 °C; ◆, 80 °C; ▲, 100 °C; ×, 120 °C, Predictions from Duan, Hu, and Sun (2003): —, 40 °C; —, 60 °C; ----, 80 °C; -----, 100 °C; ==, 120 °C. Prediction from Aavatsmark and Kaufmann (2015):, 40 °C; ----, 60 °C;, 80 °C; ----, 120 °C. Reprinted from Wang et al. (2018) with permission from Elsevier.

According to Ferrentino, Calix, Poletto, Ferrari and Balaban (2012), CO₂ solubility in water also increases with pressure and temperature. As a result of CO₂ solubilization in H₂O, the volume of liquid water phase was found to increase (Fig. 2.2) in HPCD environment and the relative volumetric expansion of water increased up to 14.4%, 12.3% and 10.2% at 40, 50 and 60 °C, respectively, at 300 bar (Zhao, Temelli, Curtis and Chen, 2015).



Figure 2.2. Relative volumetric expansion of water in equilibrium with CO_2 as a function of pressure at different temperatures. Reprinted from Zhao, Temelli, Curtis and Chen (2018) with permission from Elsevier.

2.2 Moisture sorption isotherm (MSI)

2.2.1 Water in a food matrix and classification of MSI

In biological systems such as foods, water exists with unhindered or hindered mobility and is colloquially referred to as free water and bound water, respectively (Fig. 2.3). Free water behaves similar to liquid water, whereas bound water is defined as sorbent- or solute-associated water that differs thermodynamically from pure water (Berlin, 1978). The bound water is reported to be bound to stronger hydrogen bond acceptors than liquid water as well as water-solvating nonpolar groups. Bound water has a reduced solubility for other compounds, and it is not freezable, not available for chemical reactions or for microbial growth or as plasticizer, and it shows a decrease in its diffusion coefficient with decreasing moisture content (Luck, 1981; Al-Muhtaseb et al., 2002; Rao et al., 2014).



Figure 2.3. Strongly associated, perturbated, and "free" water in a food matrix. Reprinted from Labuza and Albunakar (2007) with permission from Wiley Books.

To investigate the reasons behind why low a_w food products are poorly inactivated by HPCD, it is essential to understand the role water plays in food. Moisture sorption isotherm (MSI) is a useful tool to understand the thermodynamic properties involved in the sorption behavior of water in foods; however, such information is missing for foods placed in a HPCD environment. The knowledge of thermodynamic properties can provide insights into the microstructure associated with a food, as well as theoretical interpretations of the physical phenomena occurring at food-water interfaces (Rao, Rizvi, Datta and Ahmed, 2014).

MSI represents the relationship between total moisture content (MC) and the corresponding a_w of a food over a range of values at a constant temperature and pressure. The a_w of food is defined as the ratio of the water vapor pressure in food (P_w) to the vapor pressure exerted by pure water (P°_w) at the same temperature, as shown in Eq. (2.5)

$$a_w = P_w / P^\circ_w \tag{2.5}$$

Adsorption isotherms are generated by placing a dry material into atmospheres of high relative humidity and measuring the weight gain due to water uptake, which can be considered as physical adsorption referring to the adherence of molecules of a gas on a surface at a lower pressure than the pressure of steam (Nieto, 2010). The isotherms, product of the physical adsorption, can be grouped into five types (Fig. 2.4) according to Brunauer, Deming, Deming and Teller (1940). Types II and III are closely related to types IV and V, except that the maximum adsorption occurs at some pressure lower than the vapor pressure of the gas. In other words, types IV and V suggest that the complete or almost complete filling of the pores and capillaries of the adsorbent occurs at a pressure lower than the vapor pressure of the gas, sometimes at a considerably lower pressure. Interpretation of the different types of isotherms is shown in Table 2.1.



Figure 2.4. Five types of moisture sorption isotherms. Reprinted from Brunauer et al. (1940) with permission from American Chemical Society.

Table 2.1. Classification of physical adsorption isotherms. Reprinted from Condon (2006) with permission from Elsevier.

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| Туре | Type interpretation |
|------|--|
| Ι | This is characteristic of either a chemisorption isotherm (in which case the final upswing at high pressure may not be present) or physisorption on a material that has extremely fine pores (micropores). |
| II | This is characteristic of a material, which is not porous, or possibly microporous, and has a high energy of adsorption. |
| III | This is characteristic of a material, which is not porous, or possibly microporous, and has a low energy of adsorption. |
| IV | This is characteristic of a material, which contains mesoporosity and has a high energy of adsorption. These often contain hysteresis attributed to the mesoporosity. |
| V | This is characteristic of a material, which contains mesoporosity and has a low energy of adsorption. These often contain hysteresis attributed to the mesoporosity. |

MSIs of most foods are nonlinear, generally sigmoidal in shape, and have been classified as type II isotherm. According to Labuza and Albunakar (2007), the sigmoidal shape is caused by the additive effects of Raoult's law, capillary effect and surface-water interactions. In a typical type II isotherm, there are two bending regions, one around an aw of 0.2-0.4 and another at 0.6-0.7. According to Al-Muhtaseb, McMinn and Magee (2002), most of the water in fresh foods exert a vapor pressure very close to that of pure water and this vapor pressure level is maintained until the moisture content of food decreases to about 22%. Then, the moisture level is no longer able to sustain the vapor pressure of food at unity, and therefore, begins to show a lowered vapor pressure. The changes with atmosphere humidity of this last fraction of water in dehydrated foods result in the characteristic sigmoidal shape of MSI.

Foods rich in soluble components, such as sugar or salt, display type III behavior (Rao, Rizvi, Datta and Ahmed, 2014). However, if the solid is porous so that it has an internal surface, then the thickness of the adsorbed layer on the wall of the pores is necessarily limited by the width of the pores and the form of the isotherm is modified accordingly (Table 2.1).

2.2.2 Measurement of MSI

Commonly, MSI is determined by the saturated salt slurry (SSS) method, where the food material is placed over saturated salt slurries with specific a_w values in closed chambers and stored until the food reaches the same a_w as the saturated salt slurry. However, this method has disadvantages in terms of requiring cumbersome labor, microbial deterioration of sample at $a_w>0.6$ and the need for a long time (normally from weeks to months) to reach equilibrium.

An alternative approach is the a_w measurement (AWM) method, which can be used to generate the MSIs in a relatively short period of time. AWM method was proposed by Bell and

Labuza (2000) and the basic principle is measuring the water activity of a sample when the water content is fixed. Specifically, a real test by AWM requires the following steps for generating an adsorption isotherm (Zhang, Sun and Zhang, 2017):

- Moisture adjustment: change the amount of water in the target samples to several levels by mild dehydration;
- Moisture adsorption: wet the sample by spraying water directly or by exposing to humid atmosphere;
- 3. Moisture redistribution: samples with various water contents need to be sealed separately and stored for a period time for complete moisture redistribution in samples; and
- Measurement of a_w and water content: a_w and water content are measured and thus one data point is generated.

Compared with the SSS method, AWM method expedites the experimental process to as low as tens of minutes and hours (Demarchi et al., 2013; Argyropoulos and Muller, 2014). In addition, a large number of data points can be generated by simply adjusting the rewetting time.

2.2.3 Effects of processing parameters on MSI

Because the a_w is an equilibrium concept, any single or combined processing effect might change the adsorbing sites. In this section, the effects of temperature, pressure, and combined temperature-pressure on moisture sorption isotherms are discussed (Labuza and Albunakar, 2007).

2.2.3.1 Temperature effect on MSI

During measuring and describing the MSI, the temperature has to be specified and held constant because temperature affects the mobility of water molecules and the dynamic equilibrium between the vapor and adsorbed phases (Labuza, 1971; Kapsalis, 1981). In general, temperature has an increasing effect on a_w at constant moisture content and this effect is greatest at lower to intermediate water activities (Fig. 2.5). This is because of the nature of water binding; at constant a_w, foods that follow the type II isotherm hold less water at higher temperatures than at lower temperatures (Labuza and Albunakar, 2007). Additionally, at high a_w and temperature, some new solutes may dissolve causing a crossover of isotherms at high a_w (Fig. 2.5). Above an a_w value of 0.8, no temperature effect was observed.

Labuza (1968), Loncin (1980), and Iglesias and Chirife (1976a) have shown that the Clausius-Clapeyron equation can be applied to predict the a_w value at any temperature if the corresponding excess heat of sorption is known at constant moisture content. The effect of temperature follows the Clausius-Clapeyron equation (Eq. (2.6)):

$$\ln\frac{a_{w2}}{a_{w1}} = \frac{q_{st}}{R}\left(\frac{1}{T_1} - \frac{1}{T_2}\right)$$
(2.6)

where a_{w2} and a_{w1} are the a_w at temperatures T_2 and T_1 , respectively; q_{st} is the heat of sorption in J/mol (as a function of moisture content), and *R* equals 8.314 J/(mol K).



Figure 2.5. Water activity change for a food subjected to a temperature shift (Labuza, 1984). Reprinted from Labuza and Altunakar (2007) with permission from Wiley Books.

2.2.3.2 Pressure effect on MSI

Pressure also has an effect on the a_w of a food system, but the effect is small compared with the temperature effect (Labuza and Albunakar, 2007). In most cases, the pressure effect can be neglected unless elevated pressures are used. According to Labuza and Albunakar (2007), the utility of a_w as a system descriptor under high pressure has not been demonstrated and methods of measurement have not been developed. The thermodynamic effect of pressure on water activity was discussed by Glasstone and Lewis (1960), who showed that a change in the total pressure of a system will affect the vapor pressure. The effect of pressure on a_w can be described by Eq. (2.7)

$$\ln \frac{a_{W2}}{a_{W1}} = \frac{\overline{V}_L}{RT} (P_2 - P_1) \tag{2.7}$$

where \bar{V}_L is the molar volume of the liquid (water in this case); P_1 and P_2 are pressures for initial and final pressure, respectively.

2.2.3.3 Combined temperature-pressure effect on MSI

In some cases, a_w is influenced by the combination effect of temperature and pressure. Depending on the severity of each factor, neglecting the pressure effect could be an effective solution; however, in some cases, the combined effect of temperature and pressure on moisture sorption isotherms is estimated by using Eq. (2.8) (Labuza and Albunakar, 2007):

$$\ln \frac{a_{w2}}{a_{w1}} = \frac{-q_{st}}{R} \left[\frac{1}{T_2} - \frac{1}{T_1} \right] + \frac{\bar{V}_L \Delta P}{RT_2}$$
(2.8)

2.2.4 Mathematical description of MSI

To obtain basic information, such as some energy terms related to the level of interaction between water and food molecules, MSI needs to be described mathematically. Although there are about 77 different equations with varying degrees of fundamental validity (Bruin and Luyben, 1980; Rao et al., 2014), none provide accurate results in the full range of water activity for all types of food products (Al-Muhtaseb et al., 2002). The reason is that the water is associated in the solid food matrix with different mechanisms in different a_w regions (Labuza, 1974, Azuara and Beristain, 2006).

The equations used most commonly to describe MSI are BET (Brunauer, Emmett, and Teller) and GAB (Guggenheim, Anderson and De Boer) equations. The two equations allow the calculation of the monolayer adsorbed water value (M_0), which is the amount of water needed to form a layer of molecules that cover the food surface (Labuza, 1974; Iglesia and Chirife, 1984; Al-Muhtaseb et al., 2002). M_0 is often stated to represent the moisture content at which the water attached to each polar and ionic group starts to behave as a liquid-like phase and corresponds with the optimal moisture content for stability of low-moisture foods (Bell and Labuza, 2000;

Labuza, 1980). However, one of the assumptions behind the BET theory and GAB is that the sorption of molecules occurs on a surface whose structural and chemical characteristics are uniform, and that there are no lateral interactions between the molecules sorbed, which is not valid due to the heterogeneity of food materials (Nieto, 2010). Among the large number of models available, the equations that were used in this research are discussed below. These equations were selected because they have been shown to display a good fit for animal protein products (Basu, Shivhare and Mujumdar, 2006; Delgado and Sun, 2001).

2.2.4.1 Different isotherm equations

The Brunauer-Emmett-Teller (BET) equation

The BET equation (Brunauer, Emmett, and Teller, 1938) is used to fit MSI data over the range 0.05<aw<0.35-0.5 (Chirife and Iglesias, 1984). It provides an estimate of the monolayer value of moisture adsorbed on the surface and has been approved by the commission on Colloid and Surface Chemistry of the IUPAC (International Union of Pure and Applied Chemistry) (IUPAC, 1985) for standard evaluation of monolayer and specific area of sorbates. The BET equation can be written as Eq. (2.9)

$$\frac{a_w}{M(1-a_w)} = \frac{1}{CM_0} + \frac{C-1}{CM_0}(a_w)$$
(2.9)

where *M* is the moisture content (kg/kg dry solid), the constants defined as $b=(C-1)/(M_0C)$ and $c=1/(M_0C)$ are obtained from the slope and intercept, respectively, of the straight line generated by plotting $a_w/(1-a_w)*M$ against a_w . Then, the value of monolayer can be obtained from $M_0=1/(b+c)$.

The Henderson equation

Henderson equation (Henderson, 1952) is one of the most widely used models and can be written as Eq. (2.10):

$$M = \left[\frac{\ln(1-a_w)}{-A}\right]^{\frac{1}{B}}$$
(2.10)

where *M* is the moisture content (kg/kg dry solid) and *A* and *B* are constants. A linearized plot of $\ln[-\ln(1-a_w)]$ versus moisture content has been reported to give rise to three" localized isotherms," which do not necessarily provide any precise information on the physical state of water, as was originally thought (Henderson, 1952; Rockland, 1969).

The Oswin equation

Oswin (1946) developed an empirical model, which is a series expansion of Pearson's equation for sigmoid shaped curves (type II), and can be written as Eq. (2.11):

$$M = A \left(\frac{a_w}{1 - a_w}\right)^B \tag{2.11}$$

where *M* is the moisture content (kg/kg dry solid) and *A* and *B* are constants. This equation was used by Labuza et al. (1972) to relate the moisture contents of non-fat dry milk up to $a_w=0.5$.

The Guggenheim-Anderson-de Boer (GAB) equation

The three-parameter GAB equation derived independently by Guggenhem (1966), Anderson (1946) and de Boer (1953) has been suggested to be the most versatile sorption model available in the literature. It represents a refined extension of Langmuir and BET theories, with three parameters having physical meanings. It can be written as Eq. (2.12):

$$M = ABC \frac{a_w}{(1 - Ba_w)[1 + (A - 1)Ba_w]}$$
(2.12)

where *M* is the moisture content (kg/kg dry solid) and *A*, *B* and *C* are constants.

The Halsey-Iglesias and Chirife (H-IC) equation

Iglesias and Chirife (1976b) simplified the original Halsey equation and H-IC equation can be written as Eq. (2.13):

$$M = \left[-\frac{A}{\ln(a_w)} \right]^{\frac{1}{B}}$$
(2.13)

where *M* is the moisture content (kg/kg dry solid) and *A* and *B* are constants. Iglesias, Chirife and Lombardi (1975) and Iglesias and Chirife (1976b) reported that the Halsey equation could be used to describe 220 experimental sorption isotherms of 69 different foods in the range of $0.1 < a_w < 0.8$. Sorption behavior of dried milk products (Linko, Pollari, Harju and Heikonen, 1982) have been well described by this equation.

The Hailwood and Horrobin equation

Hailwood and Horrobin (1946) generated a simple model to describe the absorption of water by polymers. Hailwood and Horrobin equation can be written as Eq. (2.14):

$$M = \left(\frac{A}{a_w} + B - Ca_w\right)^{-1} \tag{2.14}$$

where M is the moisture content (kg/kg dry solid) and A, B and C are constants.

Iglesias and Chirife (1976c) modified Fenkel-Halsey-Hill equation empirically and the equation can be written as Eq. (2.15)

$$a_w = \exp(-e^{AT+B}M^{-C})$$
(2.15)

where M is the moisture content (kg/kg dry solid) and A, B and C are constants.

2.2.4.2 Calculation of the net isosteric heat of sorption from MSI

The net isosteric heat of sorption (q_{st}) (also called excess heat of sorption) can be calculated by Eq. (2.6). The isosteric heat of sorption was determined from the slope after plotting $\ln(a_w)$ versus 1/T at constant moisture content. This approach assumes that isosteric heat of sorption does not change with temperature. Accurate estimation of q_{st} using Eq. (2.6) requires measurement of water activities at several temperatures in the range of interest although a minimum of only two temperatures are needed.

Fig. 2.6 shows the behavior of the isosteric heat of sorption as a function of moisture content for desorption of water from pear (Iglesias and Chirife, 1976a). The plot shows the characteristic sharp decline in q_{st} with increasing moisture. The slope of the line (q_{st}/R) decreases to zero as moisture content increases. This is indicative of reduced water interactions (less binding energy) with the surface for adsorption, behaving more like pure water. The effect of temperature with respect to moisture content is shown to be the greatest at low moisture contents (Labuza and Albunakar, 2007).



Figure 2.6. Net isosteric heat of sorption (q_{st}) for pear at 20 °C. Reprinted from Iglesias and Chirife (1976a) with permission from Taylor and Francis.

2.3 Effects of HPCD treatment on physicochemical properties of meat products

To date, the literature focusing on the effects of HPCD treatment on the physicochemical properties of meat products is quite limited (Wei, Balaban, Fernando and Peplow, 1991; Sirisee, 1998; Meurehg and Arturo, 2006; Choi et al., 2008; Ferrentino and Spilimbergo, 2011; Choi et al., 2013; Cappelletti, Ferrentino and Spilimbergo, 2015; Rahman, Seo, Choi, Gul and Yang, 2018). In this section, HPCD treatment's influence on meat color and texture is summarised. HHP treatment effects are also included for comparison purposes to help understand the influences of high pressure and HPCD.

2.3.1 Factors that influence meat color

Wei et al. (1991) reported a change in the color of chicken meat and shrimp, which turned whitish after HPCD treatment. Sirisee et al. (1998) found that ground beef looked like cooked ground beef after HPCD treatment. Brown and Mebine (1969) stated that high
concentration of CO₂ could cause darkening in meat tissues by combining with myoglobin to form metmyoglobin. Choi et al. (2008; 2013) found an increased lightness and lower redness value of meat following HPCD treatment. To explain the effect of HPCD on meat color, Choi et al. (2008) investigated the denaturation of the porcine muscle proteins with HPCD treatment. HPCD treatment had no effect on myofibrillar protein solubility, including myosin, while the SDS-PAGE analysis revealed denaturation of sarcoplasmic proteins (phosphorylase b, creatine kinase, triosephosphate isomerase and one unknown protein), which masked the red color of the sarcoplasm, causing the muscle to become pale. Cappelletti et al. (2015) stated that the HPCD treatment of raw pork meat resulted in an increase in lightness, decrease in redness, and the sample turned whitish and looked like "cooked" meat.

HHP treatment was also reported to lead to modifications of meat color (Szerman et al., 2011; Rodrigues et al., 2016). According to Marcos and Mullen (2014), HHP treatment induced strong modification of protein solubility and sarcoplasmic proteins (p<0.001) were more susceptible to HHP effect than myofibrillar proteins (p>0.05) in beef muscle proteome. Ferrini, Comapossada, Arnau and Guo (2012) found that the changes in the color of cured meat products depended on the water content and a_w . Ferrini et al. (2012) stated that HHP treatment increased L and reduced a and b values in raw cured ham with high water content but the effects were negligible on the low water content sample.

2.3.2 Factors that influence meat texture

Meurehg (2006) found the tenderness of ground beef to be higher after HPCD treatment. Choi et al. (2008) showed that HPCD treatment did not have an effect on the tenderness of porcine muscle. Choi et al. (2013) also found that HPCD treatment improved meat tenderness

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when samples were treated at a relatively low pressure and temperature (150 bar and 31.1 $^{\circ}$ C) in comparison to the HHP treatment (3000 bar). Choi et al. (2013) reported that treated hot-pepper paste marinated pork samples were significantly more tender than the control samples (p<0.05). The majority of the studies showed that HHP treatment is associated with the tenderizing of meat due to structural changes of the myofibrils (Schumann et al., 1982; Suzuki et al., 1992; Cheftel and Culioli, 1997). Suzuki et al. (1992) reported that bovine semitendinosus muscle became more tender when pressurized to 3000 bar at 10 $^{\circ}$ C.

For both color and texture, the extent of the changes observed depends on the processing parameters (temperature, pressure, and time) applied, and the specific products used. More research is needed to better understand and minimize these changes during processing, especially for low aw products.

Chapter 3: Effects of high pressure and CO₂ environment on the moisture sorption isotherm of beef jerky

3.1 Introduction

Beef jerky has been used for centuries as a processed dried meat product. The typical a_w range of the beef jerky products on the market is 0.77-0.82. High pressure carbon dioxide (HPCD) treatment is well known as a low temperature pasteurization technique but mainly for high a_w foods. It has been shown to be effective for microbial reduction in meat products, including chicken (Wei, Balaban, Fernando and Peplow, 1991) and ground beef (Sirisee, Hsieh, and Huff, 1998). In addition, an extended shelf life can be achieved without sacrificing nutritional and organoleptic quality of food since it is performed at relatively low temperatures. However, there are also some drawbacks associated with this technology, including the lack of a clear understanding of the microbial inactivation mechanism especially under low a_w environment, extraction of some food components, the need for high pressure equipment and the need for optimization of processing conditions for each case, depending on the type of food product and the type of microorganism targeted (Garcia-Gonzalez et al., 2007). Several studies (Haas et al., 1989; Nakamura, Enomoto, Fukushima, Nagai and Kakoda, 1994; Kumagai, Hata and Nakamura, 1997; Schmidt, Beermann, Bach and Schollmeyer, 2005) have shown that inactivation efficiency is reduced when HPCD is applied to low a_w food products.

Because moisture plays a critical role in microbial inactivation by HPCD treatment, it is necessary to understand the moisture sorption behavior in a CO₂ environment; however, the literature lacks information in this aspect. Moisture sorption isotherm (MSI) is a graphical expression of the relationship between total moisture content (MC) and the a_w of a food product

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at a constant temperature and pressure within a defined surrounding atmosphere, typically air. MSI can be used to study the thermodynamics of water adsorption on a food material via measurement and modeling of the sorption isotherm. Comprehensive reviews on sorption behavior in foods and widely used mathematical sorption models have been published previously (Rizvi, 1986; Bell and Labuza, 2000; Al-Muhtaseb, McMinn, and Magee, 2002; Basu, Shivhare, and Mujumdar, 2006; Iglesias, 2012). However, how the MSI is affected in a CO₂ environment has not been reported even though such information would be valuable for further understanding of microbial inactivation mechanism during HPCD treatment of low a_w products. Therefore, the objective of this study was to determine the experimental data of MSI for beef jerky under different conditions: 1) air atmosphere at 23, 35, and 45 °C; 2) CO₂ atmosphere at 23 and 45 °C; and 3) high pressure CO₂ atmosphere at 45 °C and 57 bar and 200 bar. MSIs were generated by fitting experimental data into different mathematical models. Finally, the amount of monolayer of adsorbed water (M_0) for each isotherm and the net isosteric heat of sorption (q_{st}) were calculated.

3.2 Materials and methods

3.2.1 Materials

The beef jerky sample used in this study was prepared in the meat wing in Agri-Food Discovery Place located in the south campus of the University of Alberta. Two beef inside rounds were obtained from a federally inspected facility. Frozen beef stored at -20 °C was thawed in a cooler until slightly frozen. Then, beef was cut into 6 mm thick slices with a Berkel Model X13 meat slicer (Berkel, Chicago, IL, USA) at a speed setting of 30. Sliced beef was marinated overnight at 4 °C with cover brine, which consisted of beef jerky seasoning (without monosodium glutamate) (Unipac, Edmonton, AB, Canada) and cure COOAE1 (Newly Weds Foods, Chicago, IL, USA) added according to the manufacturer's recommendations for the preparation of a marinated product. Marinated beef slices were placed on racks and transferred into a processing oven and smokehouse (ALKAR-RapidPak Inc., Lodi, WI, USA). Table 3.1 shows the treatment conditions used in the preparation of beef jerky. Sample a_w was measured 0.5 h after the first hour to get a final a_w of around 0.75 with Aqualab CX-2 water activity meter (Aqualab by Meter, Pullman, WA, USA). Finally, beef jerky samples were double bagged in 3 mm and 4 mm vacuum bags (Unipac, Edmonton, AB, Canada) with 5 slices per bag and sealed using a vacuum packager (Multivac Inc., Model C200, Kansas, MO, USA). Packed samples were stored at 0 °C until further use.

| Step | Step | DB | WB | %RH | Exhaust | Exhaust | Smoke |
|------------|-------|-------|-------|-----|---------|---------|---------|
| | Time | Temp. | Temp. | | Fan | Damper | Preheat |
| | | (°C) | (°C) | | | | |
| Cook | 00:30 | 35 | 25 | 45 | On | Auto | 10 |
| Smoke cook | 01:00 | 35 | 24 | 40 | Off | Closed | |
| Smoke cook | 01:00 | 45 | 29 | 30 | Off | Closed | |
| Cook | 01:00 | 55 | 34 | 25 | On | Auto | |
| Cook | 02:00 | 80 | 48 | 20 | On | Auto | |

 Table 3.1. Treatment conditions used for beef jerky processing.

DB, dry bulb T; WB, wet bulb T; RH, relative humidity.

3.2.2 Proximate analysis

Proximate analysis was performed on the beef jerky sample to determine its protein, fat,

water and ash contents. All measurements were performed in triplicate.

3.2.2.1 Protein content

The total protein content was determined by the Dumas combustion method (Buckee, 1994). A beef jerky sample $(0.1\pm0.02 \text{ g})$ was sealed into a pellet, and the nitrogen content was measured with a TruSpec CN analyzer (Leco Corp., St Joseph, MI, USA). The protein content was calculated by multiplying the total nitrogen content with the conversion factor of 6.25.

3.2.2.2 Fat content

Total fat content was analyzed according to Hara and Radin (1978) with some modifications. A beef jerky sample (0.5±0.05 g) was chopped into small pieces and mixed with 10 mL hexane in a 16 mm * 125 mm screw cap culture tube. The samples were allowed to sit for 24 h in a fume hood with occasional shaking to ensure complete extraction of the fat. Then, the supernatant was transferred into a pre-weighed tube, dried under a gentle stream of nitrogen and weighed before and after drying.

3.2.2.3 Moisture content

The MC was determined according to the AOAC method 3.003 (AOAC, 1984). A beef jerky sample (0.5±0.05 g) was dried in an oven (Model 655G, Isotemp Oven, Fisher Scientific, Ottawa, ON, Canada) at 105 °C for 1 day. To generate MSIs, it is standard practice to express moisture content on dry basis, which was calculated using the following equation (Eq. 3.1):

$$MC\% = \frac{(Fresh sample weight - Dried sample weight)}{Dried sample weight} * 100\%$$
(3.1)

3.2.2.4 Ash content

The ash content was determined according to the AOAC method 7.009 (AOAC, 1984). A beef jerky sample (0.5±0.05 g) was burnt in a muffle furnace (Barnstead/Thermolyne® Muffle Furnace, Waltham, MA, USA) at 550 °C to constant weight. The ash content was calculated using the following equation (Eq. 3.2):

$$As \hbar \% = \frac{Burnt \ sample \ weight}{Fresh \ sample \ weight} * 100\%$$
(3.2)

3.2.3 Moisture sorption isotherm generation

In this study, a_w measurement method as described in Chapter 2 (section 2.2.2) was used to generate the MSI for beef jerky. All experiments were performed in triplicate. First, beef jerky was cut into 2.3*0.9*0.3 cm pieces and heated at 60 °C for 24 h resulting in dry beef jerky ($a_w = 0.1 \pm 0.05$).

A glass container (20*16*8 cm) with a tight lip was filled to half height with distilled water so that the overhead space could generate a 100% relative humidity atmosphere. The dry beef jerky samples were placed in the overhead space in the glass container without any contact with water. The system was maintained at different temperatures (T=23, 35, 45±1 °C) by placing the glass containers in ambient conditions (23 °C) or in an oven (Model 655G, Isotemp Oven, Fisher Scientific, Ottawa, ON, Canada) set at 35 or 45 °C. The samples were removed from the container at different time intervals (up to 65, 50, 25 h at 23, 35, 45 °C, respectively) so that they would adsorb different amounts of water. Then, the treated sample was stored in a refrigerator (~4 °C) for one week to allow the moisture to distribute uniformly throughout the sample. Finally, the aw of the sample was determined using a water activity meter (Aqualab by Meter, Pullman,

WA, USA) at the same temperature of the treatment applied and the moisture content was determined as described above (section 3.2.2.3).

For those treatments performed in a CO_2 environment and ambient pressure, CO_2 atmosphere was created in the glass container by filling the overhead space with CO_2 gas, and the remaining steps were kept the same with treatment times of up to 40 and 20 h at 23 and 45 °C, respectively.

For those treatments performed under high pressure CO₂ environment, a phase equilibrium apparatus (SITEC-Sieber Engineering AG, Maur/Zurich, Switzerland) was used for creating the HPCD environment and the schematic diagram of the experimental apparatus is shown in Fig. 3.1. The apparatus mainly consisted of a 10 mL high pressure view cell connected to an ISCO 500D syringe pump (Teledyne Isco, Lincoln, NE, USA). A heating jacket was used to regulate the cell temperature, which was filled with circulating water connected to a water bath (Model 260, Thermo Fisher Scientific Inc., Waltham, MA, USA). A micrometering valve was connected to the exit to depressurize the vessel.

The cell was pre-heated to 45 °C. To create a high relative humidity environment in the cell, 500 μ L water was added to the cell. The amount of added water was determined based on the solubility of water in CO₂ at the targeted temperature and pressure conditions to ensure saturation of CO₂ and to create 100% relative humidity environment in the cell (Wang et al., 2018). In addition, the added liquid water did not contact the beef jerky sample and expansion of liquid water phase within the HPCD environment was taken into consideration (Zhao et al., 2015). Custom designed glassware with holes at the bottom was used to hold the beef jerky sample to avoid contact with water in the bottom while allowing CO₂ circulation around the

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sample. Then, the dried sample was placed into the cell followed by sealing the cell with its lid. The pre-heated cell (45 °C) was pressurized to the desired pressure (57 or 200 bar) with CO₂ and the magnetic stirrer was turned on. The dried sample was kept in the cell set at the desired temperature and pressure for different periods of time (up to 45 h at 57 bar; up to 9 h at 200 bar). Finally, the cell was depressurized at a rate of 60 bar/min. Treated samples were sealed and stored in a refrigerator for one week to allow the moisture to distribute uniformly throughout, prior to determination of a_w and MC.



Figure 3.1. Schematic flow diagram of the high pressure system. (A) CO₂ tank; (B and E) on/off valves; (C) ISCO syringe pump; (D) refrigeration bath; (F) micrometering valve; (G) water bath; (H) high pressure view cell; (I) magnetic stirrer; (J) pressure gauge; (K) thermocouple.

3.2.4 Mathematical modelling

The experimental data were fitted to the moisture sorption isotherm equations (Eqs. (3.3)-(3.8)) shown in Table 3.2. A non-linear regression analysis was used to calculate the best value of the constants in each equation using the R software (R Core Team, 2018). All data points represent means of triplicate tests. The goodness of fit was evaluated by a mean relative percentage deviation (*E*) (Eq. 3.9) between the predicted (*Mp_i*) and experimental (*M_i*) moisture content values. Coefficient of determination (*R*²) for best fit equation was also determined.

| Model | Equation | |
|--|--|-------|
| Oswin (1946) | $M = A \left(\frac{a_w}{1 - a_w}\right)^B$ | (3.3) |
| Halsey-Iglesias and Chirife (H-IC) (1976b) | $M = \left[-\frac{A}{\ln(a_w)} \right]^{\frac{1}{B}}$ | (3.4) |
| Hailwood and Horrobin (HH) (1946b) | $M = \left(\frac{A}{a_w} + B - Ca_w\right)^{-1}$ | (3.5) |
| Guggenheim (1966), Anderson (1946) and de Boer (1953)- (GAB) | $M = ABC \frac{a_w}{(1 - Ba_w)[1 + (A - 1)Ba_w]}$ | (3.6) |
| Henderson (1952) | $M = \left[\frac{\ln(1-a_w)}{-A}\right]^{\frac{1}{B}}$ | (3.7) |
| Iglesias and Chirife (IC) (1976c) | $a_w = \exp(-e^{AT+B}M^{-C})$ | (3.8) |

| Table 3.2. | Moisture so | rption | isotherm ec | mations | used for | fitting ex | xnerimental | data. |
|-------------|-------------|--------|-------------|---------|----------|------------|-------------|-------|
| 1 abic 0.2. | monstare so | puon | | Junions | | muning of | apermientar | uutu. |

M is the moisture content (dry basis); *A*, *B*, *C* are constants; and *T* is temperature in °C.

$$E = \frac{100}{n} \sum_{i=1}^{n} \frac{|M_i - M_{p_i}|}{M_i}$$
(3.9)

3.2.5 Determination of monolayer water content (M_{θ})

The monolayer water content (M_0) was obtained from Brunauer, Emmett and Teller (BET) plots (Brunauer, Emmett, and Teller, 1938). The linearized form (Eq. 3.10) of this isotherm was plotted in terms of a_w . This function was applied within the linear range of the isotherm ($a_w < 0.5$).

$$\frac{a_w}{M(1-a_w)} = \frac{1}{CM_0} + \frac{C-1}{CM_0}(a_w)$$
(3.10)

Finally, M_0 was calculated from the slope (S) and intercept (I) of the line $a_w/M(1-a_w)$ as a function of a_w according to Eq. (3.11).

$$M_0 = \frac{1}{I+S}$$
(3.11)

The M_0 results obtained under the seven conditions tested were analyzed by one-way analysis of variance (ANOVA), and multiple comparison of the means was performed using the Tukey's test at a significance level of p < 0.05.

3.2.6 Determination of net isosteric heat of sorption (q_{st})

Net isosteric heat of sorption (q_{st}) was calculated at different moisture content levels by using the Clausius-Clapeyron equation (Eq. 2.6) (section 2.2.3.1), employing the MSIs obtained at 23 and 45 °C in air and CO₂ atmospheres at 1 bar.

3.3 Results and Discussion

3.3.1 Composition of beef jerky

The proximate composition of the beef jerky samples used in this study are presented in Table 3.3.

| Composition | %, w/w* |
|-------------|-------------------|
| Protein | 47.65±0.49 |
| Fat | 2.04 ± 0.89 |
| Moisture | 38.07 ± 2.69 |
| Ash | 12.49 ± 0.010 |

Table 3.3. Chemical composition of beef jerky samples.

* Mean±standard deviation based on triplicate analysis.

3.3.2 Moisture sorption isotherms

The experimental data points of MSIs are presented in Fig. 3.2 together with the curves obtained by using the best fitted model for each data set.

3.3.2.1 Mathematical modeling of the moisture sorption isotherms

Eqs. (3.3)-(3.8) were used to fit the MSI for beef jerky sample. The mean relative percentage deviation (*E*) for the different models is reported in Table 3.4. An equation is considered a good fit for data when E<10. Table 3.5 shows the parameters of the best fit equations for beef jerky MSIs at each condition, and the R^2 values for the best fit equations.

Table 3.4 shows that under air atmosphere and ambient pressure, HH and GAB models gave the best fit of experimental MSI data at 23 °C; GAB provided the best fit at 35 °C; and IC fit 45 °C data the best. However, none of these models gave a good fit (E>10) for the

experimental data under CO_2 atmosphere either at ambient pressure or high pressure with *E* values reaching as high as 80. This finding highlights the need for additional research to improve the available models to describe MSI data obtained under CO_2 atmosphere better.



Figure 3.2. Moisture sorption isotherms of beef jerky under different conditions (n=3). The following curves were obtained using the GAB model (Eq. (3.6)): 23 °C (air/1 bar); 35 °C (air/1 bar); 45 °C ($CO_2/57$ bar); the curve for 45 °C (air/1 bar) was obtained using the IC model (Eq. (3.8)); the curve for 23 °C ($CO_2/1$ bar) was obtained using the Oswin model (Eq. (3.3)); the curve for 45 °C ($CO_2/1$ bar) was obtained using the H-IC model (Eq. (3.4)); the curve for 45 °C ($CO_2/200$ bar) was obtained using the HH model (Eq. (3.5)).

| | | Oswin | H-IC | НН | GAB | Henderson | IC |
|------------------------|---------|-------|-------|-------|-------|-----------|-------|
| Air/1 bar | 23°C | 5.17 | 19.48 | 4.67 | 4.67 | 12.81 | 40.99 |
| | 35°C | 34.55 | 53.42 | 11.89 | 9.37 | 11.94 | 12.82 |
| | 45°C | 21.44 | 27.68 | 26.28 | 13.76 | 23.24 | 6.03 |
| CO ₂ /1 bar | 23°C | 11.72 | 23.74 | 14.93 | 13.60 | 12.77 | 56.94 |
| | 45°C | 20.04 | 10.92 | 19.05 | 19.04 | 30.34 | 80.04 |
| HPCD/45°C | 57 bar | 36.11 | 32.41 | 12.17 | 12.16 | 39.30 | 81.15 |
| | 200 bar | 51.79 | 50.06 | 27.54 | 77.71 | 52.92 | 79.91 |

Table 3.4. Accuracy of fit of different models expressed as mean relative percentage deviation *(E)*.

Table 3.5. Parameters of the best fit equations for beef jerky.

| | | Best fit equation | Α | В | С | R ² |
|------------------------|---------|----------------------|----------|----------|---------|-----------------------|
| Air/1 bar | 23 °C | HH | 3.6321 | 2.9841 | 0.3576 | 0.998 |
| | 23 °C | GAB | 0.26631 | 1.11439 | 0.92773 | 0.998 |
| | 35 °C | GAB | 13.8122 | 0.022494 | 0.62172 | 0.981 |
| | 45 °C | IC | 0.00633 | -2.06049 | 0.87631 | 0.980 |
| CO ₂ /1 bar | 23 °C | Oswin | 0.20435 | 0.81148 | N/A | 0.975 |
| | 45 °C | H-IC | -0.12946 | 0.75489 | N/A | 0.995 |
| HPCD/45 °C | 57 bar | GAB | 0.03214 | 158.9 | 1.269 | 0.977 |
| | 200 bar | HH | -0.9234 | 56.375 | 74.5234 | 0.902 |

According to Brunauer, Deming, Deming and Teller (1940), sorption isotherms are classified into 5 types as described in Chapter 2 (section 2.2.1). The MSIs under ambient pressure in both air and CO₂ environments showed sigmoid (type II) characteristics, but under HPCD condition the isotherms changed to type III as discussed below. Comaposada, Gou, Pakowski and Arnau (2000) used the Mujica model to describe a type III isotherm. However, use of the Mujica model for the MSIs obtained in this study did not improve the *E* value.

3.3.2.2 Effect of temperature

Isotherms of the beef jerky at 23, 35 and 45 °C in air at ambient pressure are shown in Fig. 3.2. The MC decreased as temperature increased at a given a_w. Similar observations were also reported by Igobeka and Blasidell (1982) for a meat product, and Delgado and Sun (2001) on cooked and cured beef. According to Palipane and Driscoll (1992), and Hossain, Bala, Hossain and Mondol (2001), as temperature increases, water molecules move to higher energy levels, which results in water molecules breaking away from water binding sites on the solid particles. Therefore, at a constant MC, the a_w increased with temperature, indicating a decrease in bound water and an increase in the level of free water. A similar trend was also apparent in CO₂ atmosphere at ambient pressure with increasing temperature.

3.3.2.3 Effect of CO2 and HPCD environment

When the isotherms obtained under air and CO₂ atmospheres at 23 °C and ambient pressure were compared (Fig. 3.2), the MC at a given a_w was lower in CO₂ atmosphere; however, at 45 °C, the two isotherms were very close and even overlapped in the high a_w range. According to Jakobsen and Bertelsen (2002), CO₂ can be adsorbed onto proteins so that there would be less surface available for water adsorption and therefore less water was adsorbed to achieve similar a_w at 23 °C. However, at 45 °C, with increased volatilization of CO₂, less CO₂ would be adsorbed onto the proteins, diminishing the difference between the isotherms obtained in CO₂ and air atmospheres. In addition, the solubility of CO₂ in muscle tissue decreases with increasing temperature (Jakobsen and Bertelsen, 2002), which explains the smaller gap between the two isotherms (under air and CO₂ environment at ambient pressure) at the higher temperature of 45 °C.

Under HPCD conditions, the isotherms became very steep (J-like shape) at a_w level of 0.73 and 0.70 at 57 and 200 bar, respectively (Fig. 3.2). J-like shaped isotherms were also reported for osmotically dehydrated and smoked Atlantic bonito muscle (Hubinger, Vivanco-Pezantes, Kurozawa and Sobral, 2009), and cod fish (Martins, Martins and da Silva Pena, 2015). Products containing soluble crystalline components, e.g., salts, often have J-shape isotherms. The effect of soluble components on MSI was studied by other authors, including but not limited to Chinachoti and Steinberg (1984), Comaposada et al., (2000), and Martins et al. (2015). Comaposada et al. (2000) and Martins et al. (2015) observed that MSIs were stabilized at a level of 0.75 a_w, which is the a_w of a saturated NaCl solution at 25 °C (36 g NaCl/100 g H₂O) (Greenspan, 1977; Lioutas, Bechtel and Steinberg, 1984). According to Lioutas et al. (1984), the NaCl solution crystallises below water activity of 0.75, and the crystallised NaCl adsorbs little or no water. When $a_w > 0.75$, a solution was produced by adsorbing a large amount of water rapidly with small increases in a_w. Therefore, the a_w of the inflection point is determined by the solubility of NaCl under different conditions. According to Gibson (1938), and Owen and Brinkley (1941), the solubility of NaCl in water increases with pressure while higher concentrations correspond to lower a_w. This could be one possible reason for the isotherms at high pressure CO₂ environment turning steep at a_w level of 0.73 and 0.70 at 57 bar and 200 bar, respectively. Martins (2015) reported that the isotherms of cod fish changed from type II to type III with an increase in salt content. On the other hand, Bando, Takemura, Nishio, Hihara and Akai (2003) demonstrated that the CO₂ solubility in water decreased with increasing NaCl concentration. Therefore, in the present study, HPCD treatment may have an effect on protein-salt bonding and make salt more available. As a result, the change in the shape of the isotherms showed similar behavior to that when there was an increase in salt content. Regardless,

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further research is needed to better understand the changes in water-salt-protein-CO₂ interactions under high pressure.

3.3.3 Monolayer water content (M_{θ})

The results for determination of M_0 under different conditions were presented in Fig. 3.3. M_0 value decreased (p<0.05) with an increase in temperature but pressure did not have a significant effect (p>0.05). Different dehydrated food products show that M_0 decreases with increasing temperature (Chen and Clayton, 1971; Iglesias, Chirife and Lombardi, 1975; Al-Mahasneh, Alkoaik, Khalil, Fulleros and El-Waziry, 2014). According to Rao, Rizvi, Datta and Ahmed (2014), a reduction in the number of active sites due to chemical and physical changes induced by temperature is the reason for this behavior. In other words, samples with the same water content, would have more free water with an increase in temperature.



Figure 3.3. Monolayer water content (M_0) under different conditions (n=3). Bars with different superscripts are significantly different (p < 0.05).

3.3.4 Net isosteric heat of sorption (q_{st})

Net isosteric heat of sorption (q_{st}) of beef jerky at 34 °C (average temperature between 23 and 45 °C) in air and CO₂ environments at ambient pressure as a function of moisture content is presented in Fig. 3.4. It is important to note that q_{st} plus latent heat of vaporisation of pure water makes up the total isosteric heat of sorption. Fig. 3.4 shows a comparison between the air and CO₂ environments, where the q_{st} value in CO₂ environment is higher and the differential between the two environments decreases when the moisture content is increased. The highest q_{st} value was 4,034 kJ/kg and 17,474 kJ/kg for beef jerky under air and CO₂ environments, respectively, at 10% moisture level and approached zero at the high moisture levels. The highest q_{st} value for cured beef obtained by Delgado and Sun (2002) was 3,780 kJ/kg, which is in agreement with the value obtained for beef jerky in this study. The decrease in the q_{st} with the increase in moisture content can be qualitatively explained by the fact that sorption initially occurs on the most active sites, giving rise to the greatest interaction energy, but as the moisture content increases, there are fewer sorption sites available for water, resulting in a lower value of q_{st} (Tsami, Maroulis, Marinos-Kouris and Saravacos, 1990).



Figure 3.4. Net isosteric heat of desorption (q_{st}) of water in beef jerky under air and CO₂ environments at ambient pressure.

3.4 Conclusions

The influence of temperature, CO₂ atmosphere at ambient pressure and HPCD environment on MSIs of beef jerky was evaluated. The deviation of the mathematical models used to fit the data increased under CO₂ atmosphere at ambient pressure and HPCD conditions. With an increase in temperature and switching from air atmosphere to CO₂, the a_w increased at a given moisture content, indicating higher level of free water. However, under CO₂ atmosphere at high pressures of 57 and 200 bar, the isotherms became very steep at a_w of 0.73 and 0.70, respectively, displaying J-shaped, type III isotherms. Monolayer water content decreased with temperature, but pressure did not have a significant effect on M_0 . Net isosteric heat of sorption in CO₂ environment was higher than that in an air environment and the differential between the two environments decreased when the moisture content was increased.

Chapter 4: Effect of high pressure CO₂ treatment on the physicochemical properties of beef jerky

4.1 Introduction

In recent years, there has been a growing demand for the minimally processed Ready-To-Eat (RTE) meat products, free of chemical additives (Decker and Park, 2010; Zhang, Xiao, Samaraweera, Lee and Ahn, 2010). Among the RTE meat products, beef jerky is a popular choice in North America and its consumption has increased by 20% from 2011 to 2018 in the USA (Statistica, 2019). However, safety of the final product depends on the quality of the raw beef material and contamination of the beef can happen during slaughter and processing (Wheeler, Kalchayanand and Bosilevac, 2014; McCarty, 2016).

High pressure CO₂ (HPCD) treatment has been known as a non-thermal process for extending the shelf-life and safety of RTE meat products due to its microbial inactivation effect. HPCD was shown to be effective at reducing specific bacteria, including *Listeria monocytogenes*, *Staphylococcus aureus* and *Escherichia coli*, in beef and other meat products (Wei, Balaban, Fernando and Peplow, 1991; Sirisee, Hsieh and Huff, 1998). However, HPCD treatment can affect the physicochemical properties of meat. For example, the color of chicken meat became whiter, while that of ground beef became darker with an increase in tenderness after HPCD treatment (Wei et al., 1991; Sirisee et al., 1998; Meurehg and Arturo, 2006). Nevertheless, there are only very limited reports to date on the effect of HPCD treatment on the physicochemical properties of meat and none specifically on beef jerky. Since the majority of the studies on HPCD treatment deals with high moisture products, it is also worthwhile to demonstrate its impact on the quality attributes of a product with a low water activity like beef jerky.

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Therefore, the objective of this study was to investigate the combined effects of different HPCD processing parameters, including pressure (P), temperature (T), treatment time (t), and depressurization rate (DR), on the physicochemical characteristics of HPCD-treated beef jerky. Physicochemical characteristics evaluated in this study include water activity (a_w), surface color profile, crude fat content and Warner-Bratzler shear force (WBSF).

4.2 Materials and methods

4.2.1 Materials

The preparation of beef jerky was described in Chapter 3 (section 3.2.1).

4.2.2 HPCD treatment

Beef jerky was cut into 2.3*0.9*0.3 cm pieces so that it could fit into the high pressure treatment cell. The schematic diagram of the high pressure apparatus used for HPCD processing (Phase equilibria apparatus, SITEC-Sieber Engineering AG, Maur/Zurich, Switzerland) was presented in Chapter 3 (Fig. 3.1).

The unit was pre-heated to the desired temperature and the beef jerky sample was placed into the cell. The cell was sealed with its lid and pressurized to the desired pressure. Treatment time was started once the pressure reached the desired value. Treatment times reported in this study do not include pressurization and depressurization times. Finally, the cell was depressurized at different rates, *DR*, controlled manually by a micrometering valve.

4.2.3 Characterization of physicochemical properties

The following analyses were performed before and after the HPCD treatment under different conditions. All measurements were performed in triplicate.

4.2.3.1 Water activity

Sample a_w was determined by an Aqualab CX-2 water activity meter (Aqualab by Meter, Pullman, WA, USA) set at measurement temperature of 25 °C.

4.2.3.2 Surface color profile

Surface color was measured with the Chroma Meters CR-410 (Konica Minolta Sensing America Inc, Ramsey, NJ, USA). Color profile was presented by L, a, and b values. L represents lightness with L=0 referring to black and L=100 referring to white; a value going from low to high represents color change from green to red; and b value going from low to high indicates color change from blue to yellow.

4.2.3.3 Fat content

Total fat content was analyzed according to Hara and Radin (1978) with some modifications as described in Chapter 3 (section 3.2.2.2).

4.2.3.4 Warner-Bratzler shear force

WBSF was measured by shearing once through the centre of the beef jerky sample (2.3*0.9*0.3 cm) with a WBSF device attached to an Universal Instron apparatus (Model 5967, Instron Ltd, Buckinghamshire, UK) fitted with a 5k N tension/compression load cell at a crosshead speed of 200 mm/min. Force at rupture was recorded in Newtons (N).

4.2.4 Experimental design

4.2.4.1 Central composite rotatable design

A five-level, four-variable, central composite rotatable design (CCRD) was employed using a commercial statistical package, MINITAB version 18 (Minitab Inc., State College, PA, USA). The independent variables were pressure (P), temperature (T), treatment time (t), and depressurization rate (DR) and these variables were coded at levels of -1.414, -1, 0, +1, and +1.414. Uncoded and coded independent variables are given in Table 4.1. Design of experiments was based on coded levels of the independent variables in the CCRD, which resulted in 31 experimental runs, including 7 replications at the central point as shown in Table 4.2. Experiments were randomized to minimize the systematic bias in the observed responses due to extraneous factors and to increase precision.

| Coded | P [bar] | <i>T</i> [°C] | <i>t</i> [min] | DR [bar/min] |
|-----------|----------------|---------------|----------------|--------------|
| variables | | | | |
| -1.414 | 58.6 | 30.9 | 6.7 | 33.4 |
| -1 | 100 | 35 | 15 | 50 |
| 0 | 200 | 45 | 35 | 90 |
| +1 | 300 | 55 | 55 | 130 |
| +1.414 | 341.4 | 59.14 | 63.28 | 146.56 |

Table 4.1. Uncoded and coded levels of independent variables used in the central composite rotatable design.

| No. of experiments | Р | Т | t | DR |
|--------------------|--------|--------|--------|--------|
| 1 | 0 | 0 | 0 | 0 |
| 2 | -1 | -1 | 1 | -1 |
| 3 | -1 | 1 | 1 | 1 |
| 4 | 0 | 0 | 0 | 0 |
| 5 | 1 | 1 | 1 | -1 |
| 6 | 0 | -1.414 | 0 | 0 |
| 7 | 1 | -1 | -1 | 1 |
| 8 | -1 | 1 | -1 | 1 |
| 9 | 1 | -1 | 1 | 1 |
| 10 | -1 | -1 | 1 | 1 |
| 11 | -1 | -1 | -1 | 1 |
| 12 | -1 | -1 | -1 | -1 |
| 13 | 1 | 1 | 1 | 1 |
| 14 | 1 | 1 | -1 | 1 |
| 15 | 1 | -1 | -1 | -1 |
| 16 | 0 | 0 | 0 | 0 |
| 17 | -1.414 | 0 | 0 | 0 |
| 18 | 0 | 0 | 0 | 0 |
| 19 | 1 | 1 | -1 | -1 |
| 20 | 0 | 1.414 | 0 | 0 |
| 21 | 0 | 0 | 1.414 | 0 |
| 22 | 0 | 0 | 0 | 0 |
| 23 | -1 | 1 | -1 | -1 |
| 24 | 0 | 0 | 0 | 0 |
| 25 | 0 | 0 | 0 | 0 |
| 26 | 0 | 0 | -1.414 | 0 |
| 27 | 1.414 | 0 | 0 | 0 |
| 28 | 1 | -1 | 1 | -1 |
| 29 | -1 | 1 | 1 | -1 |
| 30 | 0 | 0 | 0 | -1.414 |
| 31 | 0 | 0 | 0 | 1.414 |

 Table 4.2. Central composite rotatable design with coded variables.

4.2.4.2 Fitting the model and data analysis

The data obtained from the experiments were analyzed by fitting a mathematical equation (Eq. 4.1) to describe the behavior of the responses according to the levels of studied values. With the objective of minimizing the quality changes due to HPCD treatment, the response variable used for modeling was the difference (ΔY , Eqs. 4.1 and 4.2) in the physicochemical properties determined (a_w , *L*, *a*, *b*, fat content, WBSF) between the treated and untreated samples. Least square method (LSM) was used to perform the regression analysis and determine the coefficients of Eq. (4.1). The achieved mathematical model was evaluated by the application of analysis of variance (ANOVA). The significance of each coefficient was assessed by *p*-value and model terms with *p*<0.05 were considered as significant.

$$\Delta Y = \beta_0 + \sum_{i=1}^k \beta_i X_i + \sum_{i=1}^k \beta_{ii} X_i^2 + \sum_i \sum_j^k \beta_{ij} X_i X_j + \in$$
(4.1)

$$\Delta Y = Y' - Y \tag{4.2}$$

where ΔY is the difference in responses between treated and untreated sample, Y' is the response of sample after HPCD treatment, Y is the response of sample before HPCD treatment, $X_i X_j$ refer to coded process variables, β_0 is a constant, β_i , β_{ii} are the first and second degree coded input parameters, β_{ij} is the parameter for interactions of linear, quadratic and 2-way interaction terms, k is the number of independent parameters (k=4 in this study) and \in is the error term.

4.2.4.3 Optimization of HPCD treatment conditions

The optimum condition was obtained by using the MINITAB software by targeting minimum changes in the four responses, which were weighted equally. The change in each response factor, comparing before and after HPCD treatment (ΔY), was minimized in the optimization function. For confirmation, samples were treated at the optimum condition and the responses (a_w, *L*, *a*, *b*, fat content, WBSF) were measured.

According to Schultze (2019), P=57 bar, T=65°C, t=15 min, DR=60 bar/min with the addition of water was the condition that resulted in the best microbial inactivation using the same beef jerky sample. Therefore, additional HPCD treatments were performed under the condition defined by Schultze (2019) with and without the addition of 500 µL water and the responses were determined for comparison to the sample obtained under the optimum condition determined in this study.

4.2.5 Morphology analysis

Four samples (untreated, treated under the optimum condition obtained by MINITAB software, treated under the condition reported by Schultze (2019) without and with the addition of 500 μ L water into the high pressure chamber) were prepared and their morphology was observed under a light microscope (ZEISS AXIO Scope.A1, Oberkochen, Germany).

4.3 Results

4.3.1 Fitting the model and analysis of experimental data

The results for the observed responses are summarized in Table 4.3. The experimental data in Table 4.3 were used to calculate the coefficients of the quadratic polynomial equation (Eq. (4.1)) by the LSM technique.

| No. of | aw | Surface color profile | | | Fat content | WBSF |
|-------------|----------|-----------------------|----------|--------|-------------|----------|
| experiments | | L | a | b | (%) | (N) |
| 1 | -0.02343 | 1.0900 | 0.53666 | 1.2100 | -0.638 | 17.6213 |
| 2 | -0.00825 | 1.2948 | 0.36142 | 1.4225 | -2.163 | -14.3559 |
| 3 | -0.03935 | 2.2889 | 0.16142 | 1.4650 | -3.445 | 0.6579 |
| 4 | -0.02823 | 0.8233 | 0.30333 | 0.7800 | 0.366 | -5.1075 |
| 5 | -0.02105 | 1.5723 | 0.29142 | 2.0175 | -3.325 | -4.1675 |
| 6 | -0.02152 | 0.7405 | 0.58791 | 2.2183 | -1.060 | -19.6039 |
| 7 | -0.02425 | 1.9072 | 0.25000 | 1.9250 | -0.807 | -11.3377 |
| 8 | -0.02355 | 1.6500 | 0.42555 | 1.8319 | -1.267 | -3.0656 |
| 9 | -0.00545 | 1.2723 | 0.26142 | 2.1525 | -3.665 | -8.6661 |
| 10 | -0.02872 | 1.1905 | 0.37000 | 1.6138 | -1.641 | -13.3384 |
| 11 | -0.01345 | 0.1223 | 0.34142 | 1.2425 | -1.148 | -16.3595 |
| 12 | -0.01955 | 0.8516 | 0.17666 | 1.4016 | -0.509 | -10.7875 |
| 13 | -0.02695 | 2.5100 | 0.49055 | 3.0344 | -1.070 | -1.8708 |
| 14 | -0.04275 | 2.4773 | 0.27142 | 1.8275 | -2.900 | -13.3640 |
| 15 | -0.01495 | 0.6898 | 0.35642 | 1.7000 | -2.980 | -0.2185 |
| 16 | -0.03153 | 1.2533 | -0.04333 | 0.8466 | -2.799 | 7.2873 |
| 17 | -0.02066 | 1.1283 | 0.22777 | 0.7183 | -2.294 | -8.8892 |
| 18 | -0.03353 | 0.8233 | 0.30333 | 0.7800 | -1.892 | 9.4921 |
| 19 | -0.02825 | 2.7750 | 0.14555 | 1.5627 | -0.905 | -1.0332 |
| 20 | -0.02765 | 2.9550 | 0.32555 | 2.6194 | -2.178 | 8.9227 |
| 21 | -0.01275 | 3.2527 | 0.28888 | 2.7494 | -2.995 | -10.7348 |
| 22 | -0.03543 | 1.9200 | 0.25666 | 1.1600 | -2.686 | 11.0696 |
| 23 | -0.03155 | 2.0448 | 0.34476 | 1.5366 | -2.767 | 1.8599 |
| 24 | -0.04053 | 0.4233 | 0.23666 | 0.8966 | -2.316 | -8.3420 |
| 25 | -0.04853 | 0.8961 | 0.45222 | 1.0261 | -2.416 | 14.1964 |
| 26 | -0.03153 | 1.1838 | 0.19444 | 1.2372 | -2.385 | -4.8852 |
| 27 | -0.02973 | 2.0283 | 0.27777 | 1.6605 | -2.224 | 1.6365 |
| 28 | -0.02979 | 1.3527 | 0.34000 | 1.6383 | -1.686 | -17.3897 |
| 29 | -0.02835 | 1.2866 | 0.19555 | 1.2294 | 0.175 | -13.8393 |
| 30 | -0.01708 | 2.2716 | 0.27222 | 1.7038 | -2.424 | -12.9828 |
| 31 | -0.01329 | 1.6961 | 0.32555 | 2.4894 | -1.083 | -7.2968 |

| Table 4.3. Recorded ΔY response value | es. |
|--|-----|
|--|-----|

4.3.1.1 Effect on aw

The significance of each factor was determined by the standardized Pareto chart, as shown in Fig. 4.1. The length of each bar is proportional to the impact of each corresponding effect on the response. Any bar extending beyond the vertical line indicated that the variable is statistically significant at p<0.05. The results for a_w indicated that the linear *T* term was significant (p<0.05), whereas all the other first-order terms, quadratic terms and interaction terms did not have an effect on a_w. Therefore, the model was simplified to include only the significant terms and the regression coefficients of the predicted model for a_w are summarized in Table 4.4. The proposed mathematical model is shown in Eq. (4.3).

$$\Delta Y_{aw} = 0.1015 - 0.00287 T \tag{4.3}$$

The responses, ΔY for a_w obtained under different conditions were all negative, which indicated that the HPCD treatment resulted in a decrease in sample a_w . From Eq. (4.3), it can be seen that ΔY_{aw} decreases with an increase in treatment *T*.



Figure 4.1. Pareto chart of the standardized effects for the response a_w (α =0.05).

| Term | Coefficient | SE Coef. | P-Value |
|----------|-------------|----------|---------|
| Constant | -0.03204 | 0.00353 | 0 |
| Т | -0.00613 | 0.00234 | 0.019 |

Table 4.4. Regression coefficients of the model for a_w for coded coefficients.

The fitted model was analyzed via the analysis of variance (ANOVA) as shown in Table 4.5. The model shows that the lack-of-fit error is insignificant, indicating that the fitted model is accurate enough to predict the response a_w.

Table 4.5. ANOVA for aw model.

| Source | DF | Adj SS | Adj MS | F-Value | P-Value |
|-------------|----|----------|----------|----------------|----------------|
| Model | 14 | 0.001834 | 0.000131 | 1.2 | 0.363 |
| Т | 1 | 0.00075 | 0.00075 | 6.85 | 0.019 |
| Error | 16 | 0.001754 | 0.00011 | | |
| Lack-of-Fit | 10 | 0.001451 | 0.000145 | 2.88 | 0.104 |
| Pure Error | 6 | 0.000302 | 0.00005 | | |
| Total | 30 | 0.003588 | | | |

Residual plots for a_w are shown in Fig. 4.2. The probability plot and histogram of residuals, Figs. 4.2 (a, c), can be used to verify the normality assumption. Therefore, ideally, a histogram chart displays a normal distribution. Fig. 4.2 (c) shows that the data somewhat resembled the normal distribution, except for the high frequency at -0.015 residual. Figs. 4.2 (b, d) show that the residuals fall in a horizontal band with no systematic pattern. This implies that the model proposed is adequate and there is no reason to suspect any violation of the independence or constant variance assumption.



Figure 4.2. Residual plots for a_w: (a) Normal probability plot for standardized residuals, (b) versus fits for standardized residuals, (c) histogram of standardized residuals, and (d) versus order for standardized residuals.

4.3.1.2 Effect on surface color

Pareto charts for *L*, *a*, *b* values are shown in Figs. 4.3, 4.4, and 4.5, respectively. The results indicated that the linear *P* term was significant (p<0.05) on *L* whereas all the other first-order terms, quadratic terms and interaction terms had no effect on *L* value. None of the linear, quadratic or interaction terms showed any significant effect on *a* value. In terms of the *b* value, linear *P*, quadratic *P* and linear *DR* terms showed a significant (p<0.05) effect.



Figure 4.3. Pareto chart of the standardized effects for response *L* value (α =0.05).







Figure 4.5. Pareto chart of the standardized effects for response *b* value (α =0.05).

The regression coefficients of the predicted simplified models for L and b are summarized in Tables 4.6 and 4.7, respectively. Proposed mathematical models are given in Eqs. (4.4) and (4.5), respectively, for L and b values.

$$\Delta Y_L = 1.56 + 0.0155 P \tag{4.4}$$

 $\Delta Y_{b} = -0.62 + 0.01633 P + 0.0138 DR - 0.000027 P^{*}P$ (4.5)

Table 4.6. Regression coefficients of the model for *L* value for coded coefficients.

| Term | Coefficient | SE Coef. | P-Value |
|----------|-------------|----------|---------|
| Constant | 1.602 | 0.215 | 0 |
| Р | 0.363 | 0.143 | 0.022 |

| Term | Coefficient | SE Coef. | P-Value |
|----------|-------------|----------|----------------|
| Constant | 1.694 | 0.124 | 0 |
| Р | 0.3972 | 0.0822 | 0 |
| DR | 0.1808 | 0.0822 | 0.043 |
| P*P | -0.274 | 0.12 | 0.036 |

Table 4.7. Regression coefficients of the model for b value for coded coefficients.

ANOVA results for L and b models are shown in Tables 4.8, 4.9, respectively. For the model of L value, the results show that the p-value is 0.276 and lack-of-fit error is 0.986, indicating that the fitted model is accurate enough to predict the response L value. For the model of b value, it is clear that p-value is 0.008, showing the model is significant at 95% confidence level. This model shows that lack-of-fit error is 0.97, indicating that the fitted model is accurate enough to predict the response b value.

| Source | DF | Adj SS | Adj MS | F-Value | P-Value |
|-------------|----|---------|---------|---------|---------|
| Model | 14 | 7.7416 | 0.55297 | 1.36 | 0.276 |
| Р | 1 | 2.6416 | 2.64162 | 6.49 | 0.022 |
| Error | 16 | 6.5149 | 0.40718 | | |
| Lack-of-Fit | 10 | 1.6501 | 0.16501 | 0.2 | 0.986 |
| Pure Error | 6 | 4.8648 | 0.8108 | | |
| Total | 30 | 14.2565 | | | |

 Table 4.8. ANOVA results for L value model.

| Source | DF | Adj SS | Adj MS | F-Value | P-Value |
|-------------|----|---------|---------|----------------|----------------|
| Model | 14 | 6.82091 | 0.48721 | 3.61 | 0.008 |
| Р | 1 | 3.15534 | 3.15534 | 23.35 | 0 |
| DR | 1 | 0.65393 | 0.65393 | 4.84 | 0.043 |
| P*P | 1 | 0.70963 | 0.70963 | 5.25 | 0.036 |
| Error | 16 | 2.16211 | 0.13513 | | |
| Lack-of-Fit | 10 | 0.65568 | 0.06557 | 0.26 | 0.97 |
| Pure Error | 6 | 1.50643 | 0.25107 | | |
| Total | 30 | 8.98302 | | | |

Table 4.9. ANOVA results for *b* value model.

Residual plots for *L* and *b* values are shown in Figs. 4.6 and 4.7, respectively. For *L* value, Fig. 4.6 (c) shows that the data resembled normal distribution between the residual range from -1 to 1 but showing a residual at 1.5. As for the residual plot for *b* value, the results show that the majority of residuals are located in the range from -0.2 to 0.2 (Fig. 4.7 (c)). Figs. 4.6 (b, d) and 4.7 (b, d) for the two responses show that the residuals fall in a horizontal band with no systematic patterns.



Figure 4.6. Residual plots for *L* value: (a) Normal probability plot for standardized residuals, (b) versus fits for standardized residuals, (c) histogram of standardized residuals, and (d) versus order for standardized residuals.

Considering the second-order model for response b value (Eq. (4.5)), response surfaces were generated as presented in Fig. 4.8. The surface plots for b value versus DR and P displayed a convex shape. The biggest change in *b* value was observed close to P=250 bar and DR=120 bar/min condition. For *b* value, the most desirable area is in the lower left corner, which represents low *P* and *DR*.



Figure 4.7. Residual plots for *b* value: (a) Normal probability plot for standardized residuals, (b) versus fits for standardized residuals, (c) histogram of standardized residuals, and (d) versus order for standardized residuals.

Photographs were taken during experiments to visualize how the HPCD treatment affects the color of samples. Fig. 4.9 shows some selected photographs. In all photographs, the left three

samples were treated under the various conditions specified and the right three samples were untreated. The change in appearance was substantial at the more extreme treatment conditons.



Figure 4.8. (a) Response contour and (b) surface plot (holding values: T = 45 °C, t = 35 min) for the effect of pressure (bar) and depressurization rate (bar/min) on *b* value.


200 bar, 45°C, 63 min, 90 bar/min

341 bar, 45°C, 35 min, 90 bar/min



200 bar, 45°C, 35 min, 90 bar/min



58.6 bar, 45°C, 35 min, 90 bar/min



57 bar, 65°C, 15 min, 60 bar/min



57 bar, 65°C, 15 min, 60 bar/min (with water added)



93 bar, 59 °C, 36 min, 56 bar/min (optimum condition)

Figure 4.9. Photographs comparing surface color of treated and untreated beef jerky. (57 bar, 65 °C, 15 min, 60 bar/min is the condition reported by Schultze (2019)).

4.3.1.3 Effect on fat content

Pareto chart of fat content is shown in Fig 4.10. None of the linear, quadratic or interaction terms showed a significant effect on fat content. Therefore, further modeling was not performed.



Figure 4.10. Pareto chart of the standardized effects for the response fat content (α =0.05).

4.3.1.4 Effect on WBSF

In terms of WBSF, the quadratic *DR* and linear *T* terms showed a significant (p < 0.05)

effect as shown in the Pareto chart (Fig. 4.11).



Figure 4.11. Pareto chart of the standardized effects for the response WBSF (α =0.05).

The regression coefficients of the predicted second-order polynomial model for WBSF were summarized in Table 4.10 and the proposed mathematical model is given in Eq. (4.6).

 $\Delta Y_{\text{WBSF}} = -170.6 + 4.90 T - 0.00451 DR*DR$ (4.6)

The ANOVA results for the simplified WBSF model are shown in Table 4.11. The *p*-value of the model is 0.045, showing the model is significant at 95% confidence level. Lack-of-fit error is 0.49, indicating that the fitted model is accurate enough to predict the response of WBSF.

Table 4.10. Regression coefficients of the model for WBSF for coded coefficients.

| Term | Coefficient | SE Coef. | P-Value |
|----------|-------------|----------|----------------|
| Constant | 12.12 | 3.35 | 0.002 |
| Т | 4.9 | 2.22 | 0.042 |
| DR*DR | -7.21 | 3.24 | 0.04 |

| Source | DF | Adj SS | Adj MS | F-Value | P-Value |
|-------------|----|---------|---------|----------------|----------------|
| Model | 14 | 3368.89 | 240.635 | 2.44 | 0.045 |
| Τ | 1 | 479.91 | 479.907 | 4.86 | 0.042 |
| DR*DR | 1 | 490.76 | 490.764 | 4.97 | 0.04 |
| Error | 16 | 1579.07 | 98.692 | | |
| Lack-of-Fit | 10 | 1010.75 | 101.075 | 1.07 | 0.49 |
| Pure Error | 6 | 568.32 | 94.72 | | |
| Total | 30 | 4947.96 | | | |

Table 4.11. ANOVA results for WBSF.

Residual plots for WBSF are shown in Fig 4.12. Fig. 4.12 (c) shows that the data somewhat resembled normal distribution. Figs. 4.12 (b, d) show that the residuals fall in a horizontal band with no systematic pattern.



Figure 4.12. Residual plots for WBSF: (a) Normal probability plot for standardized residuals, (b) versus fits for standardized residuals, (c) histogram of standardized residuals, and (d) versus order for standardized residuals.

Response contour and surface plots for WBSF are presented in Fig. 4.13. As shown in the surface plot, ΔY_{WBSF} increased the most in the center circle area. Contour plot shows that the desirable area of WBSF is located on the junction line between the first and second light green areas. Inside the junction circle line between the first and second light green areas, ΔY_{WBSF} is positive, indicating that there is an increase in the WBSF. Outside the junction line, ΔY_{WBSF} is negative, which represents a decrease in the WBSF.



(a)



(b)

Figure 4.13. (a) Response contour and (b) surface plots (hold values: P = 200 bar, t = 35 min) for the effects of depressurization rate (bar/min) and temperature (°C) on WBSF.

4.3.2 Optimization of HPCD treatment conditions

The desirability function technique was used for the parameter optimization. According to this function, the measured quality characteristics of every predicted response is transformed to a dimensionless desirability (d) value ranging between d=0 and d=1. The value of d increases as the desirability of the corresponding response increases. In this study, four responses were set at d=1 equally. To make the color profile weight equal to 1, *L*, *a* and *b* value responses were all set at d=0.33 with an equal weight among the three color parameters. Table 4.12 shows the optimum condition obtained using the Minitab software.

 Table 4.12. Optimum HPCD condition generated by Minitab software.

| P(bar) | T(°C) | <i>t</i> (min) | DR(bar/min) |
|--------|-------|----------------|-------------|
| 92.88 | 59.14 | 35.86 | 56.3 |

Table 4.13 shows the comparison between the experimental results and predicted values under the optimum condition, which were in agreement. Table 4.14 shows the comparison of experimental results and predicted values under the condition: P=57 bar, $T=65^{\circ}$ C, t=15 min, DR=60 bar/min with the addition of water, which was established by Schultze (2019) to maximize microbial inactivation.

| Response | Experimental result (ΔY) | Predicted value | <i>Y</i> ' |
|----------------|------------------------------------|-----------------|------------|
| a _w | -0.018 | -0.021 | 0.77 |
| L | 0.008 | 0.007 | 79.74 |
| a | 0.260 | 0.384 | 2.09 |
| b | 0.220 | 0.659 | -0.85 |
| Fat content | -0.011 | -0.013 | 3.69% |
| WBSF | -6.62 | -1.11 | 32.04 N |

Table 4.13. Comparison between experimental and predicted results under the optimum condition: P=93 bar, T=59 °C, t=36 min, DR=56 bar/min.

Table 4.14. Comparison between experimental and predicted results under the condition: P=57 bar, T=65 °C, t=15 min, DR=60 bar/min with the addition of water, established by Schultze (2019).

| Response | Experimental result (ΔY) | Predicted value | <i>Y</i> ' |
|-------------|------------------------------------|-----------------|------------|
| $a_{ m w}$ | -0.0145 | -0.010 | 0.78 |
| L | 0.794 | -1.287 | 84.68 |
| a | 0.268 | 0.171 | 2.47 |
| b | 0.090 | -0.132 | -1.02 |
| Fat content | -0.022 | -0.020 | 2.65% |
| WBSF | 5.649 | -11.718 | 39.10 N |

4.3.3 Morphology analysis

As shown in Fig. 4.14, untreated and treated under the optimum condition samples showed similar morphologies of compact muscle fibres. Fig. 4.14 (c) shows that the sample treated under P=57 bar, T=65°C, t=15 min, DR=60 bar/min condition, which was the best condition in terms of microbial inactivation (Schultze, 2019), showed larger spaces between muscle fibre tissues. Fig. 4.14 (d) demonstrates that adding water under the same condition could minimize the effect and shows moderate space between muscle fibres.



Figure 4.14. Light microscopy images (scale bars represent 100 μ m) for (a) untreated sample; (b) treated under the optimum condition: *P*=93 bar, *T*=59 °C, *t*=36 min, *DR*=56 bar/min; (c) treated under: *P*=57 bar, *T*=65°C, *t*=15 min, *DR*=60 bar/min (Schultze, 2019); (d) treated under: *P*=57 bar, *T*=65°C, *t*=15 min, *DR*=60 bar/min with the addition of water (Schultze, 2019).

4.4 Discussion

The a_w of beef jerky samples decreased after the HPCD treatment at different conditions. Since the CO₂ used during processing was dry CO₂ (< 3 ppm H₂0), free water in the sample would solubilize into the CO₂ phase, in an effort to reach equilibrium of water. According to Wang, Zhou, Guo, Yang and Lu (2018), the water solubility (the mole fraction of H₂O in the homogeneous supercritical CO₂ phase, x_{H2O}) in supercritical CO₂ is 0.0093 and 0.0129 at 40 and 60 °C at 200 bar, respectively. Wang et al. (2018) demonstrated that the solubility of water in HPCD increases exponentially with increasing temperature at constant pressure. In addition, available free water content in beef jerky also increases with temperature, as was reported in Chapter 3 (section 3.3.4). As a result of both reasons, increasing *T* would accelerate free water moving into the CO₂ phase, and therefore *T* showed a significant influence on a_w reduction (Lewicki, 2004).

There was an increase in L and b values of beef jerky samples to different extents, depending on the conditions applied. Cappelletti, Ferrentino and Spilimbergo (2015) found higher L and b values but a lower a value for raw pork meat treated with HPCD. Choi et al. (2013) also reported a higher L value, lower a value and no significant change in b value after HPCD treatment. According to Choi et al. (2013), one of the pork products marinated with soy sauce that was treated at 152 bar, 31.1°C for 10 min showed a significantly paler surface color than the control. In the present study, a similar result was found for beef jerky samples treated under different conditions, i.e. 200 bar, 45°C, 63 min, 90 bar/min (Fig. 4.9) An increasing L value after HPCD treatment is the result of the changes in proteins. After HPCD treatment, an increase in denatured proteins was detected, especially the sarcoplasmic proteins in fresh pork meat (Choi et al., 2008). The changes in L and a, and paler surface color are believed to be related to the denaturation of sarcoplasmic proteins (phosphorylase b, creatine kinase, triosephophate isomerase and one unknown protein) in meat (Choi et al., 2008). It is worth to mention that meat samples treated with high hydrostatic pressure (HHP) treatment also showed an increase in L value (Campus, Flores, Martinez and Toldra, 2008; Yi et al., 2013). HHP

treatment leads to coagulation of the protein, increasing light reflection and creating a whitened color. It is well known that myoglobin and its oxidative state are responsible for the red color of meat. Cava, Ladero, Gonzalez, Carrasco and Ramirez (2009) reported that discoloration of meat with HPP treatment was caused by the oxidation of ferrous myoglobin to ferric myoglobin. Moller and Skibsted (2006) reported that globin denaturation, heme displacement or release may also result in meat discoloration through the HHP process. It is possible that similar changes can occur during the HPCD treatment; however, the literature lacks such information. On the other hand, the HHP process changes the structure (mainly depolymerization) of the protein, which creates an increase in the ratio of the light reflected and absorbed by the material (Rodrigues et al., 2016). In terms of the *a* value, HHP treatment is believed to lead to a lower *a* value when P > 3000 bar, and there was no significant change or even a slight increase when P < 3000 bar (Carles, Veciana-Nogues, and Cheftel, 1995). Apparently, the pressure levels used in this study were substantially lower than 3000 bar, but regardless there was a change in the *L* and *b* values.

The change in the fat content of the majority of the samples was small, and none of the input variables had a significant effect on the reduction of fat content. This is due to the fact that the studied processing conditions were too mild to show a difference. Rahman, Seo, Choi, Gul, and Yang (2018) extracted bovine heart (~15.42% fat) using a CO₂ flow rate of 30-50 g/min at 400 bar and 40°C for 5 h to get a defatted bovine heart (~1% fat). Based on the equation generated by Güçlü-Üstündağ and Temelli (2000), the solubility of triolein in HPCD phase is 0.9675 g/L at 50 °C and 200 bar. The low solubility of triglycerides in HPCD under the conditions tested contributes to the small change in the fat content of the beef jerky in this study.

In terms of texture, beef jerky was either tenderized or toughened after the HPCD treatment under different conditions. Firstly, *T* showed a significant effect on WBSF instead of *P*.

According to Rastogi, Raghavarao, Balasubramaniam, Niranjan, and Knorr (2007), pressure-induced denaturation of proteins is normally reversible when P < 3000 bar. Therefore, Pdoes not have a significant effect on the texture of meat. Different from high P, increased T can cause destruction of hydrogen and covalent bonds, which leads to the variation in meat texture (Sun and Holley, 2010). The tenderizing effect of HHP treatment on meat products is because HHP results in structural changes in the myofibrils (Cheftel and Culioli, 1997; Suzuki, Kim, Homma, Ikeuchi, and Saito, 1992). The toughening effect could be associated with muscle fibre elongation induced by HHP treatment (Vaudagna et al., 2012). In terms of HPCD treatment, a higher tenderness of ground beef and marinated pork was reported after HPCD treatment (Meurehg, 2006; Choi et al., 2013).

4.5 Conclusions

In this study, response surface methodology (RSM) was employed to model the effects of HPCD treatment on the physicochemical properties of beef jerky as a function of temperature, pressure, time and depressurization rate. *T* showed a significant effect on a_w ; *P*, *P*² and *DR* exerted a significant effect on surface color; no input variable had a significant effect on fat content, while *DR*² and *T* showed a significant effect on WBSF of beef jerky sample after HPCD treatment. An optimum HPCD treatment condition was determined via RSM model to minimize the changes in responses, which was *P*=92.9 bar, *T*=59.1°C, *t*=35.9 min and *DR*=56.3 bar/min. Such a treatment shows potential for the use of HPCD treatment to enhance the safety of beef jerky products while minimizing changes in its quality attributes.

Chapter 5: Conclusions and Recommendations

5.1 Summary of key findings

In this thesis research, the influence of high-pressure carbon dioxide (HPCD) treatment on the moisture sorption isotherm and physicochemical properties of beef jerky was studied in an effort to contribute to further development of HPCD treatment to enhance the safety and quality of low water activity (aw) food products. Compared to either air or CO₂ environment at ambient pressure, the shape of the moisture sorption isotherm under HPCD environment changed from type II to type III, which was demonstrated for the first time (Chapter 3). With increasing pressure of the CO₂ environment from 57 and 200 bar, the isotherms became very steep at a_w level of 0.73 and 0.70, respectively. This behavior was attributed to the effect of HPCD treatment on the interactions between protein, salt and water present in the beef jerky. In addition, the net isosteric heat of sorption of water was found to be higher in the low moisture content range in the CO₂ environment compared to the air environment, which indicated that more energy was needed to vaporise water from the food matrix. Therefore, CO₂ performed like a "glue" between water molecules and food matrix, making water less available in the CO_2 environment at low moisture content range. Because water plays an important role (i.e. formation of carbonic acid) for microbial inactivation by HPCD, it is more challenging to inactivate microorganisms in low aw foods by HPCD. The findings contribute to better understanding of the changes in HPCD environment and the microbial inactivation mechanisms in low aw products so that new strategies can be developed to enhance the efficacy of the HPCD treatment.

In terms of the physicochemical properties, response surface methodology was used to investigate the effects of HPCD treatment parameters (pressure, temperature, processing time, and depressurization rate) on the a_w, color profile (*L*, *a*, *b*), fat content, and Warner-Bratzler shear force of beef jerky (Chapter 4). The results demonstrated that pressure, temperature and depressurization rate had significant influence on the response variables evaluated. Specifically, a_w was affected by temperature, surface color was influenced by pressure, quadratic pressure and depressurization rate; no input variable had a significant effect on fat content, and Warner-Bratzler shear force was affected by quadratic depressurization rate and temperature. Within the range of levels investigated, the optimum HPCD treatment condition to minimize the changes in the physicochemical properties was determined as *P*=92.9 bar, *T*=59.1°C, *t*=35.9 min and *DR*=56.3 bar/min.

This thesis research was part of a larger project, focusing on the HPCD treatment as a technique to enhance the microbial safety of low water activity food products while minimizing quality changes. Based on the findings of this thesis research, HPCD treatment shows potential to be a processing aid for beef jerky products while minimizing changes in its quality attributes.

5.2 Recommendations for future work

Despite the great potential demonstrated, there are remaining questions that need to be answered and more research is needed before HPCD can be used in large scale food industries.

In future studies, other analysis techniques can be applied for better understanding of the phenomenon at the molecular level. For instance, the use of pulsed nuclear magnetic resonance to probe water relations in foods is a feasible approach to study water molecular mobility in food systems. The challenge is to apply such techniques under high pressure CO_2 environment to demonstrate the impact of CO_2 on the interactions of water with other food components as well as microorganisms. In this research, attempts were made to measure the relative humidity *in situ*

under high pressure CO_2 condition, unfortunately, the sensor was not operational when placed in a 100% CO_2 environment. Therefore, the samples have to be removed from the high pressure chamber for a_w and moisture content determinations; however, water solubilized into the supercritical CO_2 phase precipitates back on the sample during depressurization, Since there is no available device currently to determine the relative humidity under high pressure CO_2 condition, it is worthwhile to develop a theoretical model and new sensor to measure relative humidity under HPCD condition. Such approaches will contribute to unraveling the microbial inactivation mechanisms under low moisture conditions. The microbial inactivation efficiency under the optimum condition generated in the present study needs to be determined.

Regarding the quality aspects, it would be valuable to investigate the effect of HPCD saturated with water on the quality parameters of beef jerky since water-saturated HPCD showed a higher inactivation efficiency in a parallel study by Schultze (2019). In addition, it is worthwhile to investigate in the future, the effects of HPCD treatment on the sensory properties of beef jerky to relate the physicochemical properties evaluated in this study by instrumental techniques to sensory attributes. Potential changes in flavor were not assessed and this needs to be evaluated using a sensory panel since flavor is the top priority attribute for customers to choose a food product. Beef jerky is just one example out of a large number of low water activity foods. Therefore, more research could be conducted on other low moisture foods, for example, nuts, flour, and dry fruit with similar approaches to assess the impact of HPCD treatment on their quality attributes.

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