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HYDROGEOLOGY BASELINE STUDY OIL SANDS LEASE 13

PREPARED FOR:

SHELL CANADA LIMITED

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<u>1. INTRODUCTION</u>

1.1 GENERAL

Shell Canada Limited is proposing to develop an open pit oil sands mine and bitumen extraction plant within the western part of the Bituminous Sands Lease 13. Related transportation and utility facilities would be established as well. The Lease is located 64 km north of Fort McMurray on the east side of the Athabasca River. The community of Fort MacKay is approximately 12 km southwest of the center of the Lease. The project lands occupy all or parts of Township 95 Ranges 9, 10 and 11, West of the 4th Meridian.

1.2 DEFINITION OF THE REGIONAL AND LOCAL STUDY AREAS

The EIA Study Areas, as defined by Final Terms of Reference, Environmental Impact Assessment (EIA) Report for the proposed Shell Canada Limited, Lease 13 Project, Fort McMurray, Alberta, include the Project Area, as well as, the spatial and temporal areas of individual environmental components outside the Lease 13 boundaries where an effect can be reasonably expected. With respect to this definition, the study area can be divided into:

- Regional Study Area (RSA) is defined by the Athabasca River to the West, a line following McMurray Formation subcrop toward the east to the Firebag River (approximate location Range 6 Township 97 W4M). From this point, it extends southeast to a boundary between Ranges 5 and 6 W4M. The eastern limit is defined by a line separating Ranges 5 and 6 W4M to Township 90. The southern limit is this Township southern boundary which extends west to the Athabasca River (Figure 1). The RSA includes the following other oil sands projects: Lease 13 (Shell), Aurora North (Syncrude), Aurora South (Syncrude), Lease 13 (Mobil), Lease 30 (Gulf), Steepbank Mine (Suncor) and Project Millenium (Suncor).
- 2. Local Study Area (LSA) encompasses Lease 13 extending between Muskeg River and Athabasca River. The north boundary extends 2 km into Syncrude Aurora North Mine (Figure 2) and the South boundary follows a line separating Townships 94 and 95. This area includes open pit mine, tailings disposal areas, overburden and muskeg waste dump/storage areas, overburden drainage, bitumen extraction plant and associated utilities.

The RSA boundaries (Figure 1) were selected based on the following hydrogeological considerations:

1. Athabasca River to the west is a regional drainage feature controlling groundwater circulation in the Quaternary, Cretaceous and possibly upper sections of the upper part of

the Devonian Waterways Formation. Project impacts on groundwater regime will not extend to the west bank of the Athabasca River.

- 2. Northern boundary follows the northern subcrop of the Cretaceous age McMurray Formation to the Firebag River as shown by Green *et al.* (1962). Drawdown cone around mining operations in the Basal Aquifer will likely extend to its northern limit, which lies just south of McClelland Lake. Devonian age Waterways Formation sediments encountered within Lease 13 are usually of low hydraulic conductivity. Thus the cone of depression is not expected to extend for a large distance in these deposits.
- 3. Theoretical extent of the drawdown cone in the Basal Aquifer may reach tens of kilometres. Considering the Basal Aquifer's variable thickness, and possible lack of hydraulic connections between Devonian surface lows, it is not expected that a drawdown exceeding one to two metres will be observed at a distance exceeding 30 km. Thus, eastern and southern RSA boundaries were established within this approximate distance.

The LSA boundaries (Figure 2) were chosen based on the following hydrogeological considerations:

- 1. Overburden (Quaternary sediments and McMurray Formation rejects) drainage, tailings (TFT, MFT, CT) seepage, and potential contamination originating from the extraction plant and mining activities will not extend across Athabasca and Muskeg Rivers.
- 2. Drawdown promoted by overburden drainage will be limited to < 2 km from the mine pit and/or drainage network.

The proposed RSA and LSA were chosen based on interpretation of regional hydrogeological conditions. In our opinion, the coverage selected is conservative and extends beyond expected significant physical and environmental impact zones.

1.3 TERMS OF REFERENCE

Under the Alberta Environmental Protection and Enhancement Act, an Environmental Impact Assessment (EIA) is required for consideration of the Lease 13 Project. The EIA will also serve to provide information for Shell's application to the Alberta Energy and Utilities Board for project approval. Terms of reference for the EIA issued by Alberta Environmental Protection (November 1997) in respect to groundwater include the following activities:

- discuss the groundwater regime of the Local Study Area by summarizing the existing regional databases including flow patterns, groundwater quality and interaction with regional groundwater flows;
- describe the effects of the Project on the existing groundwater resources of the Local Study Area, including water quality, quantity and thermal regime;
- discuss the effects of the Project on the Basal Aquifer;
- discuss the relationship between groundwater and surface water in the Local Study Area;
- describe groundwater monitoring programs and mitigative measures to address impacts on groundwater; and
- describe both the surficial and upper bedrock groundwater regimes in the Local Study Area.

Komex International Ltd. was contracted to provide a hydrogeological assessment as set out in the Terms of Reference. It consists of two major components:

- 1. evaluation of background conditions and preparation of a baseline report; and
- 2. assessment of the potential impacts and interactions associated with the proposed project developments and preparation of an EIA report.

1.4 PROJECT OBJECTIVES

The objectives of the hydrogeological evaluation (baseline and EIA) are to:

- establish background hydrogeological conditions (groundwater circulation and quality) in the study area;
- define present groundwater use in the Local Study Area;
- identify data gaps and recommend measures to eliminate these deficiencies;
- identify potential impacts of project development on groundwater resources;
- define groundwater/surface water interactions;
- evaluate potential impacts of groundwater on project development;
- develop a plan to mitigate any identified impacts of mine projects on the groundwater regime; and
- identify any adverse hydrogeological impacts that cannot be mitigated.

2. REGIONAL BACKGROUND INFORMATION

2.1 TOPOGRAPHY, DRAINAGE AND CLIMATE

2.1.1 TOPOGRAPHY AND DRAINAGE

The regional study area falls within the Saskatchewan Plain division of the Interior Plains physiographic region (Bostock, 1967). Adjacent to the northeast edge of the area is the Athabasca Plain, a subdivision of the Canadian Shield major physiographic region.

To the east of the regional study area is Muskeg Mountain, which rises to approximately 610 metres above seal level (masl). The regional study area itself is an area of subdued topography which slopes gently from Muskeg Mountain towards the Athabasca and Clearwater Rivers (Figures 1 and 2).

Lease 13 is relatively flat, although the ground surface generally slopes to the west toward Athabasca River valley. Ground surface elevations range from approximately 280 to 295 masl. Extensive muskeg deposits occur throughout the Lease. These are locally separated by granular material ridges of glaciofluvial origin.

The Athabasca River flows from south-southeast to north-northwest in a deeply incised valley. Water level in the river fluctuates seasonally. Approximate water elevation may be assumed to be on the order of 232 masl. An approximately 45 m high escarpment is present at the east bank of the river. This topographic feature corresponds to the western boundary of Lease 13. The Muskeg River flows from the northeast to southwest. This low gradient surface drainage feature forms the majority of the eastern boundary of Lease 13. Approximately 8 km south of the Lease 13 southern boundary, the Muskeg River joins the Athabasca River, the major drainage system in the region.

The Athabasca River is adjacent to the western boundary of Lease 13. Mean monthly flows between 1958 and 1994 for "Athabasca River below McMurray" (Environment Canada station #07DA001) are maximum in July (1,420 m³/s) and minimum in February (164 m³/s), data for 1974 - 1994 period, (Environment Canada, 1996). Mean monthly flows for "Muskeg River near Fort MacKay" (Environment Canada station #07DA008) are maximum in May (11.7 m³/s), data for 1974 - 1994 period, and minimum in February (0.3 m³/s, data for 1974 - 1987 period, (Environment Canada, 1996). A detailed description of the hydrological conditions in the study area is provided in Alsands Energy Ltd. (1981a) and Golder Associates Ltd. (1997b).

2.1.2 CLIMATE

The climate of the Fort McMurray area is characterized by long cold winters and short, cool summers. Available meteorological data for the area include:

- 1. long term records available for the Atmospheric Environment Service station at Fort McMurray (Environment Canada, 1994);
- 2. records kept at forestry lookout stations; and
- 3. results of a study of nine stations in the Athabasca oil sands undertaken by the Alberta Oil Sands Environmental Research Program (AOSERP) between 1976 and 1982 (Rudolph *et al.*, 1984).

Rudolph *et al.* (1984) show that, while precipitation is generally higher and temperature lower in the upland areas, the climate in the vicinity of Lease 13 is likely very similar to that in Fort McMurray. The following data are taken from the 30 year climate normals for Fort McMurray for the period 1961 - 1990 (Environment Canada, 1994), and are expected to closely approximate average conditions at Lease 13.

Mean monthly temperature varies between -19.8°C in January and 16.6°C in July. Temperatures recorded over the same period fall between extreme values of -50.6°C and 37.0°C. On average, the temperature stays below freezing for 121 days each year.

Precipitation is moderate, with an annual mean value of 465 mm of which 335 mm falls as rain and the remainder as snow. Precipitation is typically greater in summer than in winter, with mean monthly values of 79.1 mm in July, and 16.0 mm in February. There is typically snow on the ground between October and April. The average depth of snow on the ground at the end of February is 32 cm. The variation of temperature and precipitation with season is shown in Table 1.

Winds are typically moderate, with an annual mean speed of 10 km/h.

Potential evapotranspiration is estimated by Hackbarth and Nastasa (1979) to be 493 mm, slightly greater than the mean annual precipitation. Rudolph et al. (1984) measured pan evaporation daily at their Mildred Lake station in the Athabasca oil sands area. Their results are summarized in Table 2.

The mean daily rates listed in Table 2 may be summed to give a mean pan evaporation value of 824 mm for the period April to October. Negligible pan evaporation is expected to occur between November and March.

2.2 GEOLOGY

Several regional scale studies on the geology of the McMurray area have been carried out (Greiner, 1956; Carrigy, 1959, 1966, 1973a, 1973b; Norris, 1973; and McPherson and Kathol, 1977; Mossop and Shetsen, 1994). These references give detailed descriptions of the regional geology.

The first comprehensive survey of the geology of the Athabasca oil sands area was conducted by Carrigy (1959). The following summary of the geology of this area is based on that work, except where indicated. The table below summarizes the main stratigraphic units which occur within the regional study area. Formations noted in brackets are not present in the local study area. Figure 3a (from Green and Mellon, 1962) illustrates the bedrock geology of the regional study area. The legend is provided in Figure 3b.

A summary of main stratigraphic units, compiled from the above cited literature, is given in Table 3.

2.2.1 PRECAMBRIAN

Precambrian outcrops occur approximately 70 km northeast of Lease 13. Meta-sediments and granite are dominant rock types in this part of the Canadian Shield. The Precambrian rocks are usually considered to be of low hydraulic conductivity and it is expected that they form an impermeable base in the study area.

There is thought to be considerable topography on the Precambrian surface. In the study area two boreholes encountered rocks of Precambrian age at depths ranging between approximately 315 and 325 m below ground surface (W805027 and W751717).

2.2.2 DEVONIAN

Middle Devonian. Formations of the Elk Point Group are the oldest of the Devonian sediments in the regional study area. The deepest Formation in the Group is the La Loche, which consists of coarse grained arkosic sandstones which unconformably overlie the Precambrian basement. The Precambrian surface topography to a large extent controls the thickness of the La Loche Formation which may range between 0 and 40 m (Sproule and Associates, 1974). The shale, siltstone, and dolostone beds of the McLean River Formation (20 - 50 m thick) conformably overlie the La Loche Formation.

The Methy Formation conformably overlies the McLean River Formation, and is predominantly a reefal dolostone in the regional study area. The Methy Formation thins abruptly east of the Athabasca River, suggesting the presence of a reef front along the edge of the Canadian Shield (Hamilton, 1969). Sproule (1974) indicates formation thickness ranges between 0 and 80 m. The Prairie Evaporite Formation forms the upper beds of the Elk Point Group and consists of halite and anhydrite. The greatest thickness (up to 240 m) of Prairie Evaporite in the regional study area occurs close to the Athabasca River. East of the River, the Formation thins rapidly before pinching out. This thinning is attributed to depositional shallowing, and post depositional solution weathering. The Prairie Evaporite is potentially of hydrogeological importance in the area due to the possibility of collapse structures in overlying beds and increasing groundwater salinity being generated by solution weathering of evaporites (McPherson and Kathol, 1977).

The Watt Mountain Formation conformably overlies older sediments. It is represented by an approximately 15 m thick shale bed (Sproule, 1974).

Upper Devonian. The Slave Point Formation in the Athabasca oil sands region is a thin rock unit (less than 15 m thick) consisting of limestone, silty limestone and siltstone. Mossop and Shetsen (1994) indicate that the Slave Point formation is Middle Devonian in age. The Slave Point Formation is bounded top and bottom by paraconformities.

The Waterways Formation comprises the main Upper Devonian rock unit which occurs within the regional study area. Crickmay (1957) subdivided the Waterways Formation into five members. In ascending order, there are: Firebag, Calumet, Christina, Moberly and Mildred. The different members of the Waterways Formation form a series of limestone beds with varying proportions of shale.

2.2.3 LOWER CRETACEOUS

McMurray Formation. The deepest Cretaceous strata in the regional study area are rocks of the McMurray Formation. These strata are separated from the underlying Devonian succession by a major erosional unconformity. The present stream profiles of the lower Athabasca and Clearwater Rivers are now controlled by the pre-Cretaceous erosion surface. Carrigy (1959) suggests that the McMurray Formation may have been deposited in a basin created by solution and removal of evaporite beds within the Devonian sequence. The McMurray Formation has been divided into four stratigraphic units by Carrigy (1959), as described below.

The Pre-McMurray Beds are a coarse grained, cemented quartzose sandstone thought to unconformably underlie the McMurray Formation (Carrigy, 1966), but are not commonly found in the regional study area.

The Lower Member of the McMurray Formation overlies the erosional surface on the Devonian strata, and its lowest beds consist of residual clays formed from weathering of Devonian limestones. These are overlain by coarse sands (the "Basal Aquifer") whose thickness is largely controlled by the topography of the erosional surface on the Devonian sequence. These sands are reported to contain large fragments of uncarbonized wood, well rounded quartz grains,

numerous feldspar cleavage fragments, and small amounts of mica. At the top of this stratigraphic unit is found a black or dark grey carbonaceous shale (the "basal clays"), which contains wood fragments.

The Middle and Upper Members of the McMurray Formation consist mainly of an oilcemented quartz sand, interbedded with lenticular beds of micaceous silts, shales, and in places, clay. The Middle Member, which generally occurs between elevations of 230 and 280 masl is characterized by frequent primary sedimentary structures, particularly current bedding, while the Upper Member is more commonly horizontally bedded. The Middle and Upper Members constitute the ore body being mined in the Athabasca oil sands area.

The Clearwater Formation conformably overlies the McMurray Formation. The deepest beds are composed of glauconitic sandstone and have been termed the Wabiskaw Member. Their distinctive olive green colour makes them useful as an easily identifiable marker bed throughout the area. The Wabiskaw Member grades up into a grey marine shale which makes up the remainder of this Formation. According to Green and Mellon (1962) (Figure 3a), the Clearwater Formation does not occur on Lease 13 but is present in adjacent leases.

Grand Rapids Formation. The Grand Rapids Formation is not found in the area of Lease 13. Where it does occur (further from the Athabasca River), it is described as a "salt and pepper" sand, generally uncemented, and consisting of fragments of quartz, feldspar, glauconite, chert, muscovite and biotite.

2.2.4 QUATERNARY

The surficial geology of the regional study area consists of deposits of Pleistocene and Recent age. These "drift" deposits range from lacustrine clays through a range of glacial and fluvial deposits to aeolian sand. Bayrock (1970) shows the distribution of types of surficial deposits over the regional study area (Figures 4a/b).

McPherson and Kathol (1977) indicate that the thickness of drift varies throughout the regional study area from less than 7.5 m up to 135 m. The thickest drift (typically 70 to 135 m) is identified in upland areas such as the north and west slopes of Muskeg Mountain, and in kame deposits (typically glacio-fluvial sand) in the Fort Hills area. Lease 13 is located in an area, bounded by the Athabasca River, the Fort Hills and Muskeg Mountain, where the drift is generally less than 25 m thick.

2.2.5 STRUCTURE

Two faults affecting the Precambrian surface are discussed by Hackbarth and Nastasa (1979). Of particular significance to the hydrogeology of the region is the Sewetakun Fault, trending from

Tp 81, R 3 to Tp 97, R 11, or approximately south south-west from Bitumount. This fault is discussed further in Section 2.3.

Another structural feature of importance is a post-Cretaceous collapse feature of approximately 60 m depth around Bitumount, known as the Bitumount Basin. This is thought to have been formed due to the solution of water soluble evaporite strata.

2.3 HYDROGEOLOGY

Composition and migration of formation fluids in Western Canada was studied by Hichon (1963, 1964, 1969a, 1969b) and Bachu and Underschultz (1993). The first general description of the regional hydrogeology of the Athabasca oil sands area is given in a report by Sproule and Associates (1974). Between 1975 and 1979 the Alberta Research Council (ARC) conducted a large scale hydrogeological study in the Athabasca oil sands region. A number of observation wells were installed, and existing oil industry exploration wells were utilized for groundwater monitoring by the ARC between 1975 - 1979 (Hackbarth, 1977a).

A detailed evaluation of Athabasca oil sands groundwater monitoring network is given in Piteau Associates Ltd. (1983). Papers of a regional nature include Hackbarth (1971, 1974a, 1974b, 1977a, 1977b, 1978a, 1978b, 1980a and 1980b), Hackbarth and Nastasa (1979), Ozoray (1977 and 1979), Ozoray *et al.* (1979), Schwartz (1979), and Slayback (1979).

A summary of geological, hydrological and hydrogeological studies conducted within Lease 13 area is given in the following Alsands Energy Ltd. documents (1978a, 1978b, 1979a, 1979b, and 1981b). Isotope hydrochemistry in the proposed Alsands project area is discussed in Wallick and Dabrowski (1982).

Operations at the Suncor and Syncrude mines have contributed greatly to the knowledge of hydrogeological conditions in the region. This has been further augmented by many papers published on various aspects of dewatering the Basal Aquifer and overburden (*i.e.*, lean oil sand and Quaternary sediments) (Coward et al., 1977; Coward et al., 1978; Kahil, 1968, 1969; Khan et al., 1982 and Martschuk et al., 1985).

It is generally considered that the following five groundwater-bearing intervals (listed in ascending order) are of regional significance in the Athabasca oil sands area:

- La Loche Formation;
- Methy Formation;
- water sand at the base of the McMurray Formation (Basal Aquifer);
- water-bearing lenses within the oil sands (Intra-orebody aquifers); and
- Quaternary deposits (Surficial aquifers).

These water-bearing zones are discussed in the following sub-sections. Hackbarth and Nastasa (1979) undertook one of the more complete regional hydrogeological studies, and the following is a summary of their work, except where indicated.

2.3.1 DEVONIAN

Devonian strata in the area are divided by Hackbarth and Nastasa (1979) into hydrostratigraphic units D1 and D2. The two units are, however, distinct only west of the Sewetakun Fault. The D1 unit comprises the Middle Devonian Methy and La Loche Formations. The D2 unit includes the Upper Devonian Waterways Formation. The two units are separated west of the Sewetakun Fault by Middle Devonian evaporite beds. East of the Fault, solution of the evaporite has resulted in the hydraulic connection of the two units.

Though control is sparse, the La Loche Formation in the McMurray area is known to vary in thickness from 0 to 40 m and to be permeable at some locations (Sproule and Associates, 1974). The McLean River Formation overlies the La Loche Formation, and is generally impermeable. In that case, it is expected to act as an aquiclude and to isolate La Loche water-bearing strata from shallower aquifers. Information on the Methy Formation is also sparse, but it is known to be porous and permeable at some locations.

The D2 unit in the regional study area (Waterways Formation) is relatively impermeable: it is reported to have a median hydraulic conductivity (K) of around 3×10^{-9} m/s. This unit is expected to act as an effective barrier to upward flow, except in areas where significant fracturing is present (such as the Sewetakun Fault). Hydraulic heads in both D1 and D2 units increase to the east and west away from the Sewetakun Fault (Hackbarth and Nastasa, 1979). This indicates that regional flow in both units is towards the fault. In addition, the hydraulic head in both units in the vicinity of the Sewetakun Fault is similar to the elevation of the Athabasca River (approximately 230 masl), which indicates that these units may discharge into the Athabasca River. The flow rates are not expected to be very high (Hackbarth and Nastasa, 1979).

Available hydrochemical data (Sproule and Associates, 1974) indicate that groundwater in the D1 and D2 units is predominantly of a sodium chloride type. Degree of mineralization varies considerably. Total dissolved solids (TDS) concentrations in the D1 and D2 units east of the Sewetakun Fault decrease rapidly from around 100,000 mg/L close to the Fault to less than 1,000 mg/L within approximately 10 km of the Fault. Higher salinities are found west of the Sewetakun Fault.

Recharge to the Devonian aquifers in the regional study area has been interpreted to occur by infiltration in upland areas east of the Athabasca River basin. Groundwater in the Devonian aquifers in the regional study area is interpreted to flow generally westward, dissolving remaining salts within the Prairie Evaporite. This would have caused, through geologic time, the westerly

migration of the eastern edge of the Devonian salt. The possibility of salt solution causing fracture permeability in the Upper Devonian, and hence possible mixing of Devonian and McMurray waters has also been raised (Sproule and Associates, 1974).

2.3.2 LOWER CRETACEOUS

Cretaceous aquifers in the regional study area include the McMurray Basal Aquifer, minor Intraorebody aquifers within the McMurray Formation, Wabiskaw Member of the Clearwater Formation, and the Grand Rapids Formation.

Throughout much of the regional study area the Basal Aquifer is present between the top of Devonian formations and the base of the McMurray oil-bearing sands. However, its thickness and other hydrogeological properties are controlled by the topography on the Devonian erosional surface, and thus show wide variation throughout the area. The distribution of hydraulic heads in the Basal Aquifer indicates that it may discharge to the Athabasca River. The discharge rate, however, is expected to be relatively insignificant when compared to the flow rate in the River.

Hackbarth and Nastasa (1979), report hydraulic conductivities for the McMurray Formation to range between approximately 10^{-4} to 10^{-9} m/s. Towards the high end, values are assumed to relate to the Basal Aquifer, while towards the low end, values would relate to actual oil sands. The hydraulic properties of the Basal Aquifer are of importance to any mining operation in the area.

The median hydraulic conductivity of the oil sand-bearing formations, calculated from laboratory measurements on re-packed oil sand samples has been reported to be 5×10^{-7} m/s, (Clark, 1960). Water-bearing lenses within the oil sands are generally of limited extent; the majority of the groundwater in the McMurray Formation occurs within the Basal Aquifer.

The Wabiskaw Member is expected to be of only minor significance as an aquifer, and, where present, will be treated together with the Quaternary overburden aquifers. The Grand Rapids Formation is porous, permeable and water-bearing, but as previously noted does not occur within the boundaries of Lease 13. Therefore, it is not discussed further.

Groundwater chemistry is quite variable throughout the McMurray Formation. Both sodium chloride and sodium bicarbonate types are present. Sproule and Associates (1974) report chloride concentrations ranging from less than 100 to approximately 15,000 mg/L, an increase in mineralization west of the Athabasca River, and a change from sodium bicarbonate to sodium chloride waters on moving from east to west of the River. They also note an increase of salinity with depth in many cases, and suggest that this is evidence of possible upwards migration of waters from Devonian strata into the McMurray Formation.

Hackbarth and Nastasa (1979) provide maps of TDS and chloride distribution in the McMurray Formation. These maps indicate chloride concentrations of the order of 1,000 mg/L east of the Athabasca River and an increase to values of approximately 5,000 mg/L on the west side. Sproule and Associates (1974), however, note that there can be sharp local variations in chloride concentrations superimposed on these larger scale trends.

2.3.3 QUATERNARY

Little detailed information is available concerning the stratigraphy and properties of the Quaternary aquifers. This is due to the fact that few of the boreholes in the area have adequate logs of the near surface deposits. It is expected that at least part of the Quaternary strata will be composed of coarser grained material and form locally important unconfined or confined aquifers. Significant Pleistocene buried channels may exist within the surficial deposits. Hackbarth and Nastasa (1979) give a frequency distribution for hydraulic conductivity in the glacial drift with a median value of approximately 10^{-5} m/s.

Hydrochemistry in the Quaternary deposits was reviewed by Sproule and Associates (1974). They concluded that the waters were generally of a calcium magnesium bicarbonate type with a mineralization of less than 1,000 mg/L TDS, but that the chemistry changed quite rapidly with depth to a sodium bicarbonate type with mineralization between 1,000 and 3,000 mg/L TDS. They reported chloride concentrations up to 750 mg/L for this unit.

2.4 HYDROGEOLOGICAL INFORMATION FROM SURROUNDING LEASES

Lease 13 is surrounded by other oil sands leases (Figure 2). To the north are Leases 10, 12 and 34, which are owned by Syncrude and are collectively known as the Aurora Mine North. To the east and northeast are Shell Leases 13 East, 88 and 89. Further east, southeast and northeast are Syncrude Lease 31 (Aurora South) and Mobil Lease 13. To the south is Gulf Lease 30 and approximately 25 km south of Lease 13 are Suncor Steepbank Mine and proposed Millenium Mine.

Available information from recent studies at the Aurora Mine (North and South) includes a hydrogeology baseline study (Golder Associates Ltd., 1996), an environmental impact study (Bovar Environmental, 1996) and supplemental information given in Syncrude Canada Ltd. (1997a and 1997b). Earlier work in this area includes Piteau Engineering Ltd. (1985). Description of hydrogeological conditions in the Steepbank Mine is provided in Klohn-Crippen (1996a and 1996b).

Alsands Energy Ltd. (1981b and 1982) and Golder Associates Ltd. (1996 and 1997a) reports provide summaries of chemical analyses from different aquifers in the Lease 13 and Aurora

Mines. Their findings regarding hydrochemical types and groundwater mineralization are summarized in Table 4.

The Devonian aquifers typically yield highly saline water, with sodium and chloride being the predominant ions. Overall, there is a trend from highly saline sodium chloride type waters in the Devonian formations at depth to fresh calcium bicarbonate type waters near surface. Groundwater in the Basal and Intra-orebody aquifers of the McMurray Formation shows a greater degree of mineralization than that in the Surficial aquifers, with sodium, bicarbonate and chloride ions present in more significant quantities. Groundwater samples collected during Syncrude's (Lease 34) April 1996 aquifer test indicate the presence of sixteen polycyclic aromatic hydrocarbons (PAHs) and alkylated PAHs as well as naphthenic acids (Golder Associates Ltd., 1996).

Groundwater in the Surficial aquifers is typically fresh, with a mineralization of less than 1,000 mg/L TDS. Bicarbonate and calcium are the predominant dissolved ions, with minor amounts of chloride and magnesium. Waters of this type would be considered typical of "young" (*i.e.*, recently recharged) groundwater.

The hydrogeological regime in Aurora Mines (North and South), Steepbank Mine and Lease 13 is broadly consistent with the regional situation described in this section. Overall, the hydrogeological findings at these projects are consistent with (while adding further detail to) the regional picture described by Hackbarth and Nastasa (1979).

2.5 PRESENT GROUNDWATER USE

A search was conducted to find the locations of water wells on record with Alberta Environmental Protection (AEP), in an area defined by Township 94-96 and Range 9-11 W4M. Table 5 summarizes the number of wells on file with AEP within the areas of each of the current leases, the recorded well owner, and the proposed use. Further details of these wells are included in Appendix I.

The water well records obtained show an absence of domestic water wells (*i.e.*, no potential groundwater receptors via water wells). Most wells appear to be of a test or exploration variety. A field-verified survey of water wells in this relatively remote study area was not conducted.

3. SUMMARY OF HYDROGEOLOGICAL EXPLORATION PROGRAMS - LEASE 13

3.1 INITIAL PHASES, 1971 - 1973

During a 1971 exploration program two groundwater samples were collected from Intra-orebody water-bearing zones, and one groundwater sample was collected from the Basal Aquifer. These samples were analyzed for major and minor ions as well as selected general parameters (electric conductivity and pH). No records are available on monitoring well installation and sampling procedures. It is possible that these samples were collected using drill-stem testing equipment.

The first documented hydrogeological exploration at Lease 13 was initiated in May 1972. One water well and five observation wells were drilled as part of this program (Leggette, *et al.*, 1972). During July and August 1972, Leggette, *et al.* (1972) conducted an aquifer test. This test provided the first reliable data on Basal Aquifer hydraulic characteristics and water quality. This information was required for preliminary design of the test pit depressurization system.

The second Basal Aquifer test was initiated in 1973. The main objectives of the program were to obtain more information on hydraulic properties of the Basal Aquifer, observe the effects of long term pumping on the groundwater (potentiometric) surface and to verify the validity of the Leggette *et al.* (1972) proposals regarding the design of a proposed dewatering scheme. The groundwater observation system included the 1972 system (water well and five observation wells) and two additional observation wells drilled in 1973 (de Korompay, 1973).

In 1972 one deep hole penetrating the Methy Aquifer was drilled (W72-1240). Losses of circulation during drilling, relatively high groundwater yield, high piezometric pressure and water salinity caused concern regarding the potential impact of this aquifer on mine design and operations. To map the Methy Aquifer and to determine its hydrogeological regime, three additional deep holes (W73-1404, W73-1481, W73-1489) were drilled and tested in 1973 (de Korompay, 1973).

3.2 TEST PIT DEPRESSURIZATION, 1974 - 1975

In preparation for the Test Pit excavation in early 1974, Shell Canada Limited installed three additional water wells and several observation wells. Depressurization of the Basal Aquifer was initiated in March 1974. Groundwater surface measurements were recorded and a number of water samples for chemical analysis were collected. In the fall of 1974 Hydrology Consultants Ltd. were contracted by Shell to assist in the evaluation, design and supervision of Basal Aquifer depressurization. Following the consultants recommendations, Shell installed five additional wells outside the Test Pit. Data on well construction, performance and effects of

depressurization on groundwater surface are summarized in the "Summary Report on Control of Groundwater for Shell Canada, Lease C-13, Alberta" (Hydrology Consultants Ltd., 1976).

3.3 ALSANDS ENERGY LTD., 1978 - 1982

3.3.1 DEVELOPMENT OF HYDROGEOLOGICAL PROGRAM, 1979

In the summer of 1979, Alsands Energy Ltd. began preparation for a detailed hydrogeological exploration program required for mine plan development.

The first phase, conducted in the fall of 1979, included:

- a review of the existing data;
- identification of potential hydrogeological concerns related to mine development;
- recommendations for the Winter 1980 hydrogeological exploration program; and
- recommendations for on-going studies.

Based on the above information, Alsands Energy Ltd. developed a long range hydrogeological exploration program, which was initiated during the winter of 1980 (Leggette, *et al.*, 1979; EBA Engineering Consultants Ltd., 1979).

3.3.2 GEOTECHNICAL EXPLORATION PROGRAMS, 1978 - 1981

The objective of geotechnical exploration programs conducted in various areas (e.g., Fresh Water Intake, Alternate Water Intake, Temporary Water Intake, Plant Site, Tailings Pond and Mine Site) was to assess foundation conditions, potential seepage and drainage/dewatering requirements. These studies further contributed to the understanding of geological conditions in the Quaternary sediments and Cretaceous formations (*i.e.*, Clearwater, McMurray). During the course of these exploration programs, information on groundwater occurrences, depth to groundwater surface, and hydraulic properties of different sediments were collected. A brief summary of activities is given below.

Fresh Water Intake Areas

The objective of the 1980 Winter geotechnical exploration program conducted by Hardy Associates (1978) Ltd. was to provide baseline information required for a design of the <u>Freshwater Intake</u> in the Isadore's Lake area. Depth of exploration ranged from 4.5 m (80-WI-12) to 87.8 m (80-WI-14). Sixteen holes were drilled around the southern part of the lake. Ten "stand-pipe" and eight pneumatic piezometers were installed in these holes. Groundwater monitoring devices were installed in Quaternary and Cretaceous sediments (upper zone and in the White Sand - Basal Aquifer). Detailed description of this exploration program, including piezometer installation details, is given in Hardy Associates (1978) Ltd. (1980b).

An <u>Alternate Water Intake</u> area located east of the northern part of Ings Island was investigated by EBA Engineering Consultants Ltd. Twenty boreholes were drilled on the river bank and through ice. Depth of exploration ranged from 3.5 to 15.4 m. Fifteen standpipes were installed in the Cretaceous sediments. Detailed description of this exploration program, including standpipe installation details, is given in EBA Engineering (1981b).

<u>Temporary Water Intake</u> area, water supply line and drainage facilities located at approximate northing 6351800N investigated by EBA Engineering (1981c) are located outside of the present project area in the Aurora North Leases.

Plant Site

The objective of the Winter 1980 geotechnical field exploration program conducted by Hardy Associates (1978) Ltd. was to collect sufficient subsurface information for a site preparation and general foundation conditions assessments. Forty-six boreholes were drilled to determine stratigraphy and lithology of geological units intersected. Depth of exploration ranged from 5.1 m (80-P-32, 80-P-39) to 25.05 m (80-P-10). Standpipes were installed in a total of 17 boreholes intersecting various Quaternary and Cretaceous (upper zone) sediments. Detailed description of this exploration program is given in Hardy Associates (1980a).

The second phase of detailed geotechnical investigations was undertaken by EBA Engineering in February 1981. The objective was delineation of subsurface conditions and assessment of their significance to the location of the proposed plant facilities. A total of 104 boreholes were drilled in the plant site area. Depth of exploration ranged from 1.0 m (815166G) to 30.2 m (815122G). Standpipe piezometers were installed in 48 boreholes intersecting Quaternary and Cretaceous sediments (Clearwater Formation locally and McMurray Formation throughout the area). Detailed description of this exploration program is given in EBA Engineering (1981d).

It should be noted that only a few holes were drilled by Hardy Associates and EBA Engineering south of latitude 6351000N (present northern boundary of Lease 13). All other holes are located outside of the present local study area. Information gathered from these investigation advances general knowledge of hydrogeological conditions in the regional study area.

Tailings Pond

In the summer of 1978 and winter of 1980, R.M. Hardy Associates (1978) Ltd. conducted geotechnical investigations in the proposed tailings pond area. In 1978, only 12 holes were drilled due to difficult access conditions. Depth of holes ranged from 9.4 m (78-TP-11) to 25.5 m (78-TP-9). Standpipes were installed in nine holes and groundwater levels recorded. Preliminary site assessment results are described in R.M. Hardy & Associates (1978a and 1978b).

The Winter 1980 program was designed to provide detailed subsoil information to enable preliminary design for the starter and final dykes. A total of 79 boreholes were drilled in the tailings pond area, concentrating along the proposed dyke outline. Depth of exploration ranged from 2 m (80-TP-16, 80-TP-83) to 16.5 m (80-TP-109) intersecting Quaternary and Cretaceous sediments (upper part). Twenty-two standpipes were installed to facilitate groundwater surface elevation measurements. Depth to groundwater surface was also recorded in the majority of holes following completion of drilling. Detailed description of this exploration program is given in Hardy Associates (1980c).

Mine Site

The objective of the 1979 and 1980 exploration programs was an overall geotechnical and geological evaluation of overburden in the 25-year mine area. Approximately 230 boreholes were drilled in the mine area. Depth of investigation ranged from 1.5 m (80-MS-162) to 19.8 m (80-MS-208). Upon completion of each boring, standpipes were inserted into the open holes. The standpipes were left protruding up to 1 m above ground level. These installations were installed to permit monitoring of groundwater levels during drainage of the proposed mine area. Detailed description of these exploration programs is given in Dames & Moore (1979, 1980) and Reimchen Surficial Geology Ltd. (1980).

3.3.3 GROUNDWATER EXPLORATION PROGRAMS

These programs were designed to provide hydrogeological information on bedrock aquifers, namely the Lower Cretaceous - Basal Aquifer and Middle Devonian - Methy Formation. These groundwater-bearing zones are considered to be of regional significance and are important to the project from both environmental and technical perspectives. In the course of these activities some shallow piezometers (Quaternary and Cretaceous - upper part) were also upgraded to ensure that groundwater samples and water level measurements related to a discrete interval. The following is a brief description of three exploration programs.

Piezometer Installation, Winter 1980

During the Winter 1980 program, the following instruments were installed within Lease 13 area:

- nine piezometers in the Basal Aquifer; and
- two observation wells in the Methy Aquifer.

Recognizing the importance of hydrochemistry in the evaluation of hydrogeological conditions, an extensive program of groundwater sampling and laboratory testing was conducted.

Details on piezometer construction, development, recovery tests and groundwater sampling procedures are described in a report by EBA Engineering Consultants (1980a).

Groundwater Monitoring, Summer 1980

This program included upgrading of 33 piezometers installed in the overburden and the redevelopment and upgrading of 33 Basal Aquifer piezometers.

Selected shallow (overburden) piezometers were bailed and water samples were collected for chemical analysis. All piezometers in the Basal and Methy Aquifers were evacuated using compressed air. Groundwater surface recovery was recorded to enable calculation of hydraulic conductivity and groundwater samples were collected for chemical analyses.

Groundwater monitoring was conducted from June to September, 1980 (EBA Engineering Consultants Ltd., 1980b). A summary of hydrogeological exploration programs covering the period ending in 1980 is given in Alsands Energy Ltd. (1981b).

Expansion of Groundwater Monitoring Network, Winter 1981

The program included installation of 10 piezometers in the Basal Aquifer and upgrading of seven piezometers in the Methy Formation. All new piezometers were developed, hydraulic conductivity tests conducted and groundwater samples collected for chemical analyses. Depth to groundwater surface in a number of shallow piezometers was also measured. The objective of this program was to provide additional information required for evaluation of the potential impact of groundwater on mining and the potential affect of mining on groundwater resources in the project area. This includes evaluation of:

- technical aspects of depressurization and dewatering of the Basal Aquifer;
- potential hydraulic connection between Methy Formation and Basal Aquifer; and
- groundwater quality.

Detailed program description and analytical results are given in EBA Engineering Consultants Ltd. (1981a) report. A summary of hydrogeological activities conducted in 1981 is provided in the draft report "Groundwater Hydrology, 1981 Exploration, Alsands Project" (Alsands Energy Ltd., 1982).

3.4 HYDROGEOLOGICAL ASSESSMENT

As part of the mine feasibility assessment, Komex was retained by Fording Coal Ltd. in 1996 to provide a hydrogeological evaluation of potential effects of mine development on the groundwater flow system. The specific objectives of this project were to:

- calculate potential groundwater inflows to the proposed mine blocks;
- perform a preliminary depressurization/dewatering analysis; and
- assess potential impacts from dewatering on streamflow in the Muskeg and Athabasca Rivers.

Program description and assessment results are provided in Komex (1996).

3.5 1997 EXPLORATION PROGRAM

3.5.1 MARCH/APRIL

During this program, Golder Associates Ltd. installed five shallow piezometers (Quaternary interval) along Muskeg River, north of Isadore's Lake and a double (Intra-orebody and Basal Aquifer) piezometer east of Isadore's Lake.

The objective of this program was to enhance the groundwater database for the EIA by collecting the following information:

- geological profile, hydraulic properties, depth to groundwater surface and groundwater quality in the Quaternary deposits present along the Muskeg River; and
- depth, thickness, hydraulic properties, vertical hydraulic gradients and groundwater quality in the Basal Aquifer near Isadore's Lake.

A groundwater sample collected from piezometer MW97-3 completed within Quaternary silty medium grained sand overlying oil sands (3.0 - 5.2 m below ground surface) was submitted for an inorganic and organic laboratory analyses. The results confirmed that this groundwater is typical for this aquifer's ionic composition (HCO₃-Ca-Mg hydrochemical type with a mineralization of TDS = 307 - 416 mg/L).

Organic analysis detected measurable phenol concentration (0.4 μ g/L) and presence of nine PAHs and alkylated PAHs (Golder Associates Ltd., 1997a) in concentrations not exceeding 0.16 μ g/L (per compound).

Program description and interpretation of the hydrogeological data are provided in Golder Associates Ltd. (1997a).

3.5.2 OCTOBER

An inventory of twenty-seven piezometers selected for Winter 1997/98 sampling program was planned. The program objectives are as follows:

- 1. to find and mark piezometers to allow easier location during the winter program;
- 2. to assess each piezometer technical status and suitability for sampling; and
- 3. to check for the presence of H_2S using olfactory method.

Seven Methy Aquifer, fifteen Basal Aquifer and five Quaternary aquifers piezometers were originally selected. The field verified survey confirmed the existence of all Methy installations in

acceptable technical state. Fifteen Basal Aquifer piezometers were located. More than half (eight) were found in good technical state, while seven were damaged to various degrees. It is expected that the majority of the damaged piezometers can be repaired. Only one Quaternary installation was found in good technical state. Two other piezometers were not located in the field. Time restriction did not allow a search for the remaining two piezometers.

Hydrocarbon odour was detected in four of the Basal Aquifer installations. None of the groundwater samples collected from this aquifer had H_2S odour.

4. HYDROGEOLOGY OF THE LOCAL STUDY AREA

Hydrogeological investigations within Lease 13 span a period between 1971 and 1997. Work was done by Shell and a number of consulting companies. Description of program objectives and methodology is usually given in the summary reports (see References in Section 8). Most of these programs were discussed and referenced in the previous section of this report.

With the advent of increasing environmental awareness, groundwater has become recognized as a valued environmental component. Over the past two decades considerable progress has been made in monitoring well design, construction materials, development, sampling techniques, sample preservation and laboratory techniques. These technological and scientific advances have contributed to the higher quality of hydrogeological data collected during more recent programs.

This does not necessarily indicate, however, that data collected in the more distant past are of limited value. On the contrary, exploration programs which followed historically established and proven methodology remain valid and useful in evaluation of local and regional hydrogeological conditions. To support this view, it is noteworthy that the 1980 - 1981 programs confirmed 1971 - 1975 exploration findings, and recent (1995 - 1997) studies in Aurora Mine, Steepbank Mine and Lease 13 are confirming groundwater circulation and quality data collected during the 1971 - 1981 investigations.

A detailed description of hydrogeological programs within Lease 13 including methodology of piezometers installation, development, testing, sampling, and chemical analyses are given in EBA Engineering (1980a, 1980b and 1981b) and Alsands Energy Ltd. (1981b and 1982).

A summary of the early hydrogeological exploration programs and interpretations is given in Alsands Energy Ltd. (1981b). Detailed description of Lease 13 geological conditions is given in Shell Canada Limited (1997). The following description is based on Alsands Energy Ltd. (1981b) updated with 1981 and 1997 exploration results.

According to archival records there are:

- 7 monitoring wells which intercept the Middle Devonian Methy Formation, with 7 chemical analyses of groundwater;
- 35 monitoring wells installed in the Lower Cretaceous Basal Aquifer, with 60 chemical analyses of groundwater;
- 31 monitoring wells installed in the Lower Cretaceous Intra-orebody and near the contact with Quaternary deposits, with 14 chemical analyses of groundwater; and
- 39 monitoring wells installed in Quaternary deposits, with 18 chemical analyses of groundwater.

It should be noted that these wells and analytical data do not include standpipes installed in the course of geotechnical exploration work and chemical analyses which show anomalous groundwater quality results due to drilling fluids and/or cement filtrate influences.

Analytical schedules commonly include main ions (calcium, magnesium, sodium, potassium, bicarbonate, sulphate and chloride), minor ions (iron, manganese and fluoride), general parameters (EC, pH and TDS) and, in selected cases, total metals. The 1997 program included analyses for a number of organic compounds.

The purpose of the groundwater monitoring system was to establish groundwater baseline conditions, collect data required to evaluate potential changes in the groundwater regime as a result of proposed mine development and plant operations, as well as to assess groundwater impact on Project development.

The following is a summary of hydrogeological conditions in the main groundwater-bearing units given in ascending order from the oldest (La Loche Formation) to the youngest (Quaternary sediments). Locations of piezometers (observation wells) in the major groundwater-bearing units are shown on Figures 5 (Methy Formation), 6 (Basal Aquifer), 7 (Intra-orebody) and 8 (Quaternary). The relation between different units along selected lines (Figure 9) is shown on schematic hydrogeological cross-sections in Figures 10, 11 and 12.

4.1 LA LOCHE FORMATION

This formation is located beyond the zone potentially affected by the proposed mining operation, thus no piezometers were installed in this unit.

Drill stem tests (DST) conducted in hole W805021 (now outside of the project area, within Aurora North Leases) and W805027 indicate the presence of groundwater-bearing zones with highly variable thickness and hydraulic properties. The potentiometric surface (converted to equivalent freshwater) stabilizes approximately 25 m below ground surface (W805021) and approximately 12 m above the Methy Aquifer (Alsands Energy Ltd., 1981b). The drill stem tests conducted within high porosity intervals indicate hydraulic conductivity ranging from practically zero to $2x10^{-5}$ m/s. Due to insufficient number of observation wells, groundwater flow direction and velocities cannot be readily defined within this stratigraphic unit.

Only one groundwater sample was collected from this formation (W805021). Groundwater pH was 8.0, mineralization approximately 172,000 mg/L TDS and chloride concentration 102,206 mg/L. This brine represents a sodium-chloride hydrochemical type (Alsands Energy Ltd., 1981b).

4.2 METHY FORMATION

This unit is underlain by a 18 to 48 m thick layer of low hydraulic conductivity McLean River Formation. Observed differences in piezometric elevations between La Loche and Methy Formations indicate that these units are hydraulically separated by intervening McLean River sediments. Location of piezometers completed within the Methy Formation is given on Figure 5. Piezometer completion details, groundwater surface elevations and hydraulic conductivity values are shown in Table 6A.

Groundwater surface elevations in this confined groundwater-bearing zone, as measured in March, 1981 range between 256 masl (W8015039) and 267.8 masl (W731489) (Figure 13). Some of these elevations may represent resultant groundwater surface elevations originating from relatively long sand pack and/or screen interval completions. The hydrographs presented in Alsands Energy Ltd. (1981b) indicate that very small temporal changes (<0.5 m) occur in groundwater surface elevations. This indicates hydraulic isolation of this groundwater-bearing zone.

The Methy Formation includes zones of highly variable hydraulic conductivity. Based on two DST tests, Alsands Energy Ltd. (1981b) reports hydraulic conductivities ranging from unmeasurably small to $3x10^{-6}$ m/s, and from $7x10^{-10}$ to $3x10^{-9}$ m/s based on analysis from two cores. Piezometers completed in this formation indicate hydraulic conductivities ranging from $2x10^{-9}$ m/s to $>1x10^{-4}$ m/s. Zones of high hydraulic conductivity, and associated high yields encountered during piezometer development are most likely limited to reefal build-ups.

Distribution of hydrochemical types and groundwater mineralization, and chloride concentrations within this stratigraphic unit are shown on Figures 14 and 15, respectively. Hydrochemical data are summarized in Tables 8A and 9A.

Groundwater in this unit represents a sodium-chloride hydrochemical type, with mineralization ranging from 9,824 to 78,666 mg/L TDS. This variability is most likely related to either inadequate piezometer development and/or piezometer designs. Sampling during the winter 1997/98 program, more than 15 years following piezometer reconstruction, should clarify the issue of groundwater mineralization.

During the 1980/81 groundwater quality monitoring programs, samples were taken for total metal analyses. The results indicate the presence of high and very high concentrations of some metals (Tables 8A and 9A). These anomalous results are most likely related to high levels of suspended solids and thus are not likely representative of actual concentrations of metals dissolved in groundwater.

For example, during observation well (piezometer) drilling and installation activities, residual drill cutting and materials introduced for construction (sand, bentonite) are usually present. Despite initial development, associated particles may continue to enter the well. When high concentrations of the suspended solids are present and an unfiltered sample is then acidified, the particles become dissolved. Analysis of such a solute loading will represent combined chemistry of water and solids.

In our opinion, analyzing for total metals does not provide replicable results and does not describe natural groundwater chemistry. In the future, analysis for dissolved metals should be conducted.

Hydrogeological cross-sections A-A' and B-B' (Figures 10 and 11) show schematically the relation between Methy Formation and other hydrogeological units in the Lease 13 area. An issue of potential hydraulic connection between Methy and Basal Aquifer, and its impact on proposed mine development, has been raised in the past.

Hydrogeological information available to date indicate that such a hydraulic connection does not exist. The factors leading to this conclusion are as follows:

- piezometric pressures in the Basal Aquifer and Methy Formation are different (Tables 6A and 6B; Figures 10 and 11);
- during long term Basal Aquifer dewatering, associated with the test pit excavation, no drawdown was observed in the Methy Formation (Alsands Energy Ltd., 1981b);
- low seasonal groundwater surface fluctuations in the Methy Formation indicate hydraulic isolation from shallower units (including the Basal Aquifer);
- groundwater chemistry and mineralization is significantly different in both zones (Tables 8A and 8B) and Alsands Energy Ltd. (1981b). Environmental isotopes further confirm isolation of these two groundwater-bearing zones (Wallick and Dabrowski, 1982); and
- the Prairie Evaporite Formation, Watt Mountain Formation and Beaverhill Lake Group, representing in excess of 100 m of low hydraulic conductivity sediments, are acting as an aquiclude, effectively separating the Methy Formation and Basal Aquifer.

In an unlikely event that a hydrogeological "window" between the Methy Formation and Basal Aquifer is opened, in our opinion, saline groundwater inflows can be controlled using a conventional engineering approach. Grouting of groundwater circulation routes may be the best approach in achieving separation between those two aquifers. This should be feasible due to the following factors:

• relatively small differences (10 to 20 m) in piezometric levels exist between the two zones of concern;

- presence of thick sequence (>100 m) of low permeability sediments separating both geological units;
- relatively small storage of saline water within reefal build-ups in Methy Formation; and
- possible lack of hydraulic connection between reefal build-ups.

4.3 BASAL AQUIFER

This confined aquifer is underlain by low hydraulic conductivity basal clay (if present) and Beaverhill Lake Group sediments (Alsands Energy Ltd., 1981b). Locally, groundwater may occur within the upper Devonian fractured zones and/or the weathered uppermost part of this stratigraphic unit. In this instance, it is expected that the upper zone would remains in hydraulic communication with the overlying Basal Aquifer.

The Basal Aquifer is represented by fine to coarse grained sand (0 to 40 m thick) deposited on the erosional surface of Upper Devonian sediments. A number of monitoring wells were installed in this major aquifer (Figure 6). Piezometer completion details, groundwater surface elevations and hydraulic conductivity test results are summarized in Table 6B.

Groundwater surface elevations range from 230.9 to 289.9 masl. Depth to groundwater surface varies from less than 2 m to more than 60 m below ground surface. The vertical hydraulic gradient between the Basal Aquifer and Methy Formation is downward in the mine area and upward in the area adjacent to the Athabasca River. Hydrographs obtained from Basal Aquifer piezometer measurements indicate that very small seasonal changes occur in groundwater surface elevations. In most cases, these fluctuations do not exceed 1 m (Alsands Energy Ltd., 1981b). Small amplitude and lack of a distinct seasonal trend in the groundwater surface elevation fluctuations indicate that direct recharge to the Basal Aquifer occurs far beyond the local study area.

Significant recharge will occur in the areas where McMurray Formation basal sands are subcropping below permeable Quaternary sediments or are outcropping at the ground surface. The presence of tritium in pore water, obtained from oil sands indicates that groundwater in the Basal Aquifer is also recharged through the oil sands. In some areas, (lean oil sands and higher permeability sediments), such recharge may occur within a timeframe of 5 - 10 years (Wallick and Dabrowski, 1982). Where thick layers of high grade oil sands are present, recharge rates will be much slower.

A potentiometric surface contour map for the Basal Aquifer is shown as Figure 16. It shows that in the proposed mine area, groundwater surface elevations range from approximately 275 masl to 289.9 masl.

Although not confirmed, the change in hydraulic gradient west of the proposed mine may reflect a constriction of groundwater flow in the Basal Aquifer. This may be due to relief variations on the Devonian surface which in turn would directly impinge on Basal Aquifer thickness. This may also reflect an overall increase in the hydraulic conductivity of the Basal Aquifer adjacent to Athabasca River. For example, hydraulic connection between the Basal Aquifer and the Athabasca River is inferred to occur in the vicinity of piezometers W805053, W805054, and MW97-42, where groundwater surface elevations (230 - 235 masl) are comparable with elevations in the Athabasca River (230 - 235 masl).

Groundwater flow is generally toward the west with hydraulic gradients ranging between approximately 0.002 (in the proposed mine area) to 0.025 (in the zone of steep hydraulic gradients west of the proposed mine area).

Aquifer tests on Lease 13 performed between 1972 and 1974 were interpreted to give a range of hydraulic conductivity of $2x10^{-5}$ to $3x10^{-4}$ m/s with a geometric mean of $5x10^{-5}$ m/s (Alsands Energy Ltd., 1981b). In addition, 26 single well tests were performed during development of wells in 1981. Sixteen of the wells gave a range of hydraulic conductivity from $1x10^{-5}$ to $>1x10^{-4}$ m/s (Table 6B), which is similar to the range found from the aquifer test referred to above. Ten of the wells gave lower values, in a range of $5x10^{-8}$ to $7x10^{-6}$ m/s (Alsands Energy Ltd., 1981b and 1982). These lower values may be related to some degree of plugging of the piezometer screen with heavy oil, or placement of the screen within oil sands where Basal Aquifer is absent.

Other measurements of hydraulic conductivity based on pumping tests in the Basal Aquifer are also available. Golder Associates Ltd. (1996) refers to the analysis of pumping test on Lease 34 (Aurora Mine North) which was analyzed to give a transmissivity ranging from 21 to 61 m²/d. If a Basal Aquifer thickness of 25 m is assumed (based on isopach maps in Golder Associates Ltd. (1996), then a range in hydraulic conductivity values of 1×10^{-5} to 3×10^{-5} m/s may be calculated.

Based on the results of these aquifer tests, it appears that the Basal Aquifer (clean sand) in the Lease 13 area has a hydraulic conductivity in the range of 1×10^{-5} to $>1 \times 10^{-4}$ m/s. Lower values are associated with oil saturated sands.

Storativity for the Basal Aquifer was calculated from each of four aquifer tests (1972 - 1974) referred to in Alsands Energy Ltd. (1981b). A total of fourteen values were requested. Eleven were within a 0.00001 - 0.0001 range. The two tests conducted in 1974 yielded higher values up to 0.02 which would be considered unusual for a confined aquifer and one was 0.001. Analysis of aquifer tests at OSLO Lease 31 yielded storativity values between 2.2×10^{-5} and 1.3×10^{-4} . Analysis of the 1996 aquifer test at Lease 34 (Aurora Mine North) gave values ranging from 4×10^{-5} to 3×10^{-4} (Golder Associates Ltd., 1996).

Based on these aquifer tests, it would appear that the Basal Aquifer in the Aurora Leases and Lease 13 has a storativity in the range 1×10^{-5} to 4×10^{-4} m/s, typical of a confined aquifer.

In the past programs (1971 - 1981), field measurements of pH, electrical conductivity were not taken. The 1997 results for these parameters are presented in Table 7A. All groundwater analyses representing natural water quality are summarized in Tables 8B and 9B. Samples showing signs of anomalous values due to either drilling fluids and/or cement filtrate influences were excluded from this evaluation.

Distribution of hydrochemical types is shown on Figure 17. Groundwater represents mostly Na-Cl-HCO₃ and Na-HCO₃-Cl hydrochemical types, with mineralization ranging between 1,430 and 7,407 mg/L TDS. An anomalous hydrochemical type was encountered in piezometer W810061, where Na-HCO₃ type water with a relatively low mineralization of 1,430 mg/L TDS was found.

Chloride distribution is shown on Figure 18. Concentrations range from 81 mg/L (W810061) to 2,793 mg/L (W810068). The anomalous hydrochemical type combined with low TDS and chloride concentrations in W810061 suggest the presence of a hydrogeological "window" in the area adjacent to this monitoring well.

Total metal concentrations are generally low. Exceptions are elevated to high iron, manganese, boron and barium concentrations. High concentration of metals recorded in W810069 are most probably associated with high total suspended solids content in the groundwater sample (Table 9C).

4.4 CRETACEOUS - INTRA-OREBODY AND NEAR CONTACT WITH QUATERNARY

Intra-orebody groundwater-bearing zones are represented by generally thin and locally discontinuous layers of silty sands and/or sands with low bitumen content. Such aquifers may be present within the McMurray Formation profile extending from the contact with Quaternary deposits and top of the Basal Aquifer. Groundwater may be under confined conditions, especially in the lower parts of the McMurray Formation. Due to restricted recharge and low storage capacity, the groundwater reserves in the Intra-orebody aquifers are expected to be relatively small.

A relatively small number of observation wells have been installed in this zone (Figure 7). Screened sections (Table 6C) were placed at different elevations, thus development of a representative groundwater surface elevation map was not readily possible. Groundwater surface elevations range from approximately 230 to 300 masl. Seasonal changes in groundwater surface elevations are within 1.5 m range. It is expected that a downward hydraulic gradient dominates within the McMurray Formation.

The bitumen content of the oil sands results in a low hydraulic conductivity, which is often difficult to measure in well tests. Analysis of a Syncrude 1996 pumping test using the Neuman and Witherspoon (1972) method gave an estimate of $2x10^{-10}$ m/s for the vertical hydraulic conductivity of the oil sands (Golder Associates Ltd., 1996). Clark (1960) estimated a range of $3.2x10^{-8}$ to $1x10^{-5}$ m/s based on laboratory studies. Wallick and Dabrowski (1982) estimate a vertical hydraulic conductivity of $4x10^{-8}$ m/s based on a study of tritium concentrations in porewater.

Golder Associates Ltd. (1997a) measured hydraulic conductivity in piezometer MW97-42A within an interval 20.7 - 24.5 m below ground surface. The result, $7x10^{-8}$ m/s, is consistent with results obtained from the literature.

Groundwater quality data are summarized in Table 7B, 8C, and 9C. Six different hydrochemical types of groundwater were encountered within the McMurray Formation (Figure 19). Associated with this variability is a wide range of mineralization 277 - 2,148 mg/L TDS. Chloride concentrations are relatively low and do not exceed 122 mg/L (Table 8C and Figure 20). Total metal concentrations are also relatively low, with the exception of iron and manganese (Tables 8C and 8D).

4.5 QUATERNARY

The Surficial aquifers are represented by relatively thin (less than 20 m) glaciofluvial and alluvial sands and gravels of Quaternary age. These aquifers are usually unconfined. Within the Project area, depth to the phreatic surface varies from 0 to 7 m below ground surface.

A tributary buried valley was identified in the western part of Lease 13, extending north from Isadore's Lake. Groundwater reserves associated with such channels are highly variable depending on the extent and thickness of water-bearing granular deposits.

Depth to the groundwater surface within the Project area was measured periodically to define seasonal groundwater surface fluctuations and direction of groundwater flow. The direction of groundwater flow in surficial sediments is not well defined. However, the aquifers drain toward local topographical depressions and surface drainage systems. A downward vertical hydraulic gradient exists between the Surficial aquifers and the Basal Aquifer.

Hydrographs obtained from Surficial aquifer piezometers indicate a relatively slow response of the groundwater surface to extended periods of rain. In general, seasonal fluctuations in the groundwater surface do not exceed 1.5 m (Table 6D). This is mostly due to the significant storage capacity of the Quaternary sediments. Most surficial piezometers are frozen from December until the end of May. Hydrographs of selected Surficial aquifer piezometers are given in Alsands Energy Ltd., (1981b).

Hydraulic conductivities of Surficial aquifers are highly variable and range from approximately 1×10^{-8} to 1×10^{-3} m/s.

Golder Associates Ltd. (1996) note a range of 10^{-9} to 10^{-3} m/s for the hydraulic conductivity of surficial deposits in the Aurora Mine areas, while Alsands Energy Ltd. (1981b) indicate a range of 10^{-6} to 10^{-3} m/s for Lease 13. The large range is due to the variation in surficial materials from highly permeable sands and gravels to low permeability lacustrine clays. Golder Associates Ltd. (1996) also give a vertical hydraulic conductivity of 5×10^{-10} m/s for lacustrine clay, a vertical hydraulic conductivity range of 6×10^{-11} to 4×10^{-8} m/s for till, and a horizontal hydraulic conductivity range of 6×10^{-7} m/s for till.

A pumping test performed in the main Pleistocene channel in the Aurora Mine South area gave a transmissivity of 3.6×10^{-3} m²/s, which was reported to correspond to a hydraulic conductivity of 1.9×10^{-3} m/s (Golder Associates Ltd., 1996).

Groundwater in Quaternary aquifers represents mostly Ca-Mg-HCO₃ and Ca-Mg-Na-HCO₃ hydrochemical types. Distribution of groundwater hydrochemical types is shown on Figure 21.

The majority of the samples collected from the zone encompassing the Quaternary sediments indicate the presence of fresh water in these aquifers. The data on the chemical composition of the groundwater are summarized in Tables 7C, 8D and 9D. In general, mineralization varies from 239 to 1,729 mg/L TDS, while chloride concentrations are below 135 mg/L (Table 8D).

Local hydrochemical anomalies were found in the Isadore's Lake area, where relatively high mineralization was encountered in holes 80-W1-2 and 80-W1-5. In these holes, mineral content exceed 1,300 mg/L TDS (Table 8D). These holes may be in hydraulic contact with Cretaceous deposits.

Elevated to very high iron, manganese and fluoride concentrations were locally detected (Table 8D). Anomalously high total metal concentrations were found locally (Table 9D). These anomalies are most likely related to high concentrations of total suspended solids.

5. GROUNDWATER AND SURFACE WATER INTERACTIONS

Both the Athabasca and Muskeg Rivers, as well as McClelland and Kearl Lake lie within the theoretical drawdown cone of the proposed mine. The river surface elevations are above the level of the base of the pits, and hence the possibility exists for leakage to occur from the rivers into the Basal Aquifer during dewatering operations. This is of potential concern both from the viewpoint of reduced baseflow to the rivers or lakes, and from the potential cost of pumping extra water from the open pit mines.

Mine pit dewatering will require: 1) draining of Surficial and Intra-orebody aquifers in the area of the active pit; and 2) depressurization of the Basal Aquifer from a piezometric level of approximately 280 masl to an elevation close to the base of the oil sands. The exact depth to which depressurization is required would be determined by operational and mine safety considerations. The possible effects of dewatering on the various surface water bodies are discussed below.

5.1 ATHABASCA RIVER

The Athabasca River is located a minimum of 3 km to the west of the western edge of the proposed mine area. Typical surface elevation of the river is 230 masl. Average low and high water flows are 166 and 990 m³/s, respectively (Water Surveys of Canada, 1991). The potentiometric surface of the Basal Aquifer appears to coincide with the water level in the river (Alsands Energy Ltd., 1981a), possibly indicating hydraulic connection between the two. Drilling in the Isadore's Lake area, at least locally confirmed connection between the Quaternary alluvium and Cretaceous Basal Aquifer. Overall, the river acts as a regional drainage feature for both the Quaternary and the Cretaceous groundwater-bearing zones.

Information on hydraulic heads in the Devonian aquifers is sparse, but regional data presented in Hackbarth and Nastasa (1979) indicate potentiometric surfaces for the Upper and Middle Devonian aquifers slope towards the Athabasca River and reach values similar to River elevation. The above data suggest that the Athabasca River may also act as the discharge zone for Devonian aquifers in the regional study area.

Assuming that the alluvial sediments in the Athabasca River valley and Basal Aquifer are hydraulically connected and that both units are continuous, flow may be induced from the River and alluvial deposits into the Basal Aquifer under proposed mine dewatering conditions. The theoretical rate of seepage, which would occur under this scenario may be determined using the Darcy equation (Darcy, 1856).

where: Q = ki AQ = leakage flux [L³/T]

- k = hydraulic conductivity [L/T]
- A = area of aquifer $[L^2]$
- i = hydraulic gradient [L/L]

The following parameters may be selected:

- average distance between the Athabasca River and the pit, L = 3,000 m;
- maximum drawdown created near open pit closest to the river as a result of dewatering/ depressurization, s = 50 m (static = 260 masl, dynamic = 210 masl);
- river stage elevation = 235 masl;
- hydraulic gradient (i) between the river and pit, = $235 210 \approx 0.01$;

3000

- vertical hydraulic conductivity (k) of 10^{-5} m/s for alluvial sediments is assumed; and
- affected river channel area (A) has width of 500 m and length of 10,000 m.

Based on these assumptions, leakage flux (Q) is estimated to be in the order of 0.5 m^3 /s. This represents less than 1% of the low flow in the Athabasca River assumed to be approximately 166 m³/s.

It should be noted that a different larger leakage flux will occur if plant water supply originates from the Athabasca River. Under this scenario, induced infiltration wells would be placed along the river bank and would draw water from both the river and the alluvial sediments.

5.2 MUSKEG RIVER

The Muskeg River flows through the low lying terrains along the southeastern edge of the proposed mine area. Both swampy and higher topographic areas drain toward the river.

The proposed mine area comes within a minimum of 100 m of the Muskeg River along much of its southeast boundary. Because of this close proximity, dewatering of the Surficial aquifers could have an effect on baseflow to the river. Hydraulic conductivities of surficial deposits along the river vary substantially from 2×10^{-7} to $> 10^{-4}$ m/s (Golder Associates Ltd., 1997a).

Using the formula described in Section 5.1, seepage from the Muskeg River may also be estimated. The following parameters may be selected:

- average distance between the Muskeg River and the pit bottom, L = 300 m;
- maximum drawdown created near open pit closest to the river, s = 100 m;
- hydraulic gradient, i = 100 = 0.333;

300

- average vertical hydraulic conductivity, $k = 5 \times 10^{-6}$ m/s; and
- affected river channel area has with 10 m, and length 5,000 m.

Based on these assumptions, leakage flux (Q) is estimated to be in the order of 0.08 m³/s. This represents nearly 25% of the low flow in the Muskeg River, assumed to be 0.3 m³/s.

Thus, reduction in groundwater discharge will vary considerably along the river bank. It is expected that discharge of water originating from overburden drainage in the project area will more than compensate seepage losses. An overall increase in the river flow is therefore anticipated.

Seepage from the Muskeg River and/or alluvial sediment toward the mine pit, through very low transmissivity oil sands and estuarine deposits is expected to be insignificant.

5.3 KEARL LAKE

Kearl Lake is a shallow water body located more than 12 km from the proposed mine area. It is anticipated that the relatively low to very low transmissivities of the intervening Quaternary and Cretaceous sediments will limit the extent of the drawdown cone development. This, combined with the distance between the lake and the mine, suggests that development of Lease 13 should not have any impact on Kearl Lake.

Presence of a Pleistocene buried channel system was identified by drilling exploration programs in Lease 13 East and Lease 31. It is possible that this system extends toward Kearl Lake. If the Pleistocene channel intersects the full thickness of oil sands and it is hydraulically connected to Kearl Lake, then dewatering of the Basal Aquifer may induce seepage from the lake. Available information is not sufficient to allow a quantitative estimate of the potential losses.

5.4 MCCLELLAND LAKE

McClelland Lake is located approximately 18 km northeast of the proposed mine development. The southern shore of the lake is beyond the subcrop of the Basal Aquifer (Figures 3a and 3b). Thus, it is not expected that Lease 13 development will have any impact on water levels in the lake.

5.5 MUSKEG

Development of a surface drainage system, combined with overburden dewatering operations, will lower the water surface in adjacent muskeg areas. The width of the zone affected will depend on the hydraulic properties of muskeg and underlying strata as well as drawdown development. It is assumed that the impact of drainage is not going to extend more than 1 km from the drainage features. In Section 1.2, the north Local Study Area boundary was conservatively assumed to be at a distance of 2 km from the Lease 13 drainage.

6. SUMMARY AND CONCLUSIONS

The exploration programs conducted at Lease 13 between 1981 - 1997, provided sufficient information to characterize the hydrogeological regime within the Local Study Area. Published and unpublished literature also provides a very detailed description of groundwater conditions within the Regional Study Area.

The Devonian to Quaternary hydrostratigraphy at the Lease 13 broadly conforms to the pattern found regionally. In ascending order, major groundwater-bearing units are as follows:

- Middle Devonian La Loche Formation;
- Middle Devonian Methy Formation;
- Lower Cretaceous Basal Aquifer;
- Lower Cretaceous Intra-orebody; and
- Quaternary (Surficial) sediments.

There are significant differences in the hydrogeological regimes of the La Loche Formation, Methy Formation and Basal Aquifer. Specifically, each aquifer is characterized by a different circulation and hydrochemical regime. Groundwater in Quaternary sediments is usually fresh and represents a HCO₃-Ca-Mg hydrochemical type. Migrating downward, this water is subject to chemical diagenesis resulting in changes in ionic composition and mineralization. Groundwater in the Intra-orebody aquifers forms a transitional zone between Quaternary water-bearing units and Basal Aquifer. The hydraulic and groundwater chemistry properties measured in major groundwater-bearing units are consistent with Regional Study Area data.

La Loche and Methy Aquifers are believed to be isolated from the active groundwater circulation zone within the Local Study Area. Conceptually, recharge to the Basal Aquifer is interpreted to occur by vertical migration of infiltrating precipitation through overlying sediments and via direct recharge in the subcrop/outcrop area northeast of Lease 13. Groundwater flow is generally westerly towards the Athabasca River, which forms a regional groundwater discharge zone. Intra-orebody and Surficial aquifers drain toward local topographical depressions and/or surface drainage systems.

A number of groundwater exploration/monitoring wells have been installed in the Regional Study Area for industrial purposes. There are no records on file with AEP, of domestic groundwater users in either the Regional or Local Study Areas.

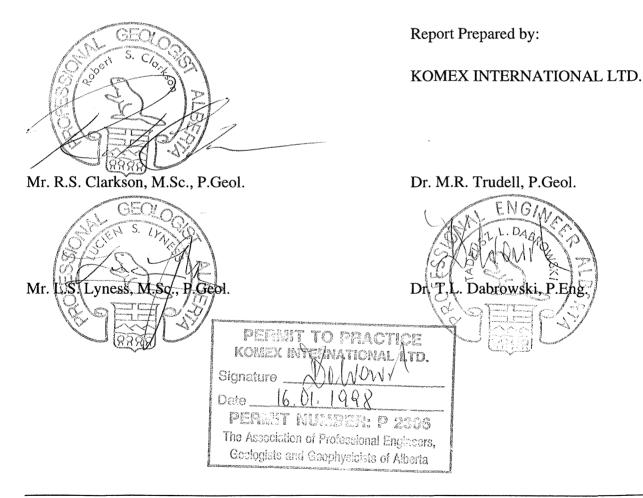
Groundwater control in the Basal and Surficial aquifers is required to assure safe and efficient mining. The Methy Aquifer will be closely monitored during exploration and proposed mining operations. Observations collected to date indicate hydraulic isolation exists between the Basal

Aquifer and the Methy Formation. From these observations it is inferred that the Methy Formation will not be affected by the proposed mining operation.

Mine pit dewatering will require: 1) draining of the Quaternary and Intra-orebody aquifers in the areas adjacent to the open pit; and 2) depressurization of the Basal Aquifer. The potential impacts of these proposed operations on the Athabasca River, Muskeg River, Kearl Lake, McClelland Lake and Muskeg/Wetland have been considered and are estimated to be insignificant outside of the Local Study Area.

Groundwater from the Basal Aquifer in the Regional Study Area was found to contain significant quantities of phenols, naphthenic acids and some polycyclic aromatic hydrocarbons. As discharge of groundwater from the depressurization/dewatering system to the watershed is not anticipated, the presence of these naturally occurring compound are of little significance.

One groundwater sample collected from Quaternary sediments contained measurable concentrations of phenol (0.4 μ g/L) and low concentrations of PAHs and alkylated PAHs (concentrations ranged between 0.02 - 0.16 μ g/L). This single analysis does not allow characterization of organic compounds dissolved in groundwater in Surficial aquifers throughout Lease 13.



7. GLOSSARY OF TERMS

Alluvial DepositsParticles of minerals or rocks which are transported by a river and
deposited along its valley.

- Aquiclude A material of such low permeability that it effectively prevents any movement of water through it or reduces water movement to such a low value relative to the surrounding materials that it can be considered an impervious barrier.
- Aquifer Any water-saturated body of geological material from which enough water can be drawn at a reasonable cost for the purpose required. An aquifer is only a relative term determined largely by economics and is best illustrated by extreme examples. An aquifer in an arid prairie area required to supply water to a single farm may be adequate if it can supply 1 m³/day. This would not be considered an aquifer by any industry looking for cooling water in volumes of 10,000 m³/day. A common usage of the term aquifer is to indicate the water-bearing material in any area from which water is most easily extracted.
- Aquifer Test A method of obtaining quantitative information on the hydraulic characteristics of an aquifer by removing water from the aquifer in a controlled manner and measuring the groundwater surface or piezometric response. Often referred to as a "pump test" or "drawdown test".
- Aquitard A material of intermediate permeability between an aquifer and an aquiclude. An aquitard allows some measure of leakage between the aquifers it separates.

Bitumen Naturally occurring solid or semi-solid hydrocarbons.

Brackish Water Water with total dissolved solids concentration ranging from 1,000 to $10,000 \text{ g/m}^3$.

Brine Water with total dissolved solids concentration exceeding 100,000 g/m³.

Cone of Depression An inverted cone depression in groundwater surface surrounding a pumped well or dewatered/depressurized excavation.

Confined Aquifer A completely saturated aquifer whose upper and lower boundaries are impervious layers. In confined aquifers the pressure of the water is usually higher than that of the atmosphere and the water in wells stands above the top of the aquifer. The water in a confined aquifer is called confined or artesian water.

- *Connate Water* Water entrapped in the interstices of a sedimentary rock at the time the rock was deposited.
- *Depressurization* The lowering of the groundwater piezometric surface over the desired area of a mine or construction site, using a well system.
- *Dewatering* Removal of groundwater from geological formation using well for drainage ditch system.
- *Diagenesis* Process involving physical and chemical changes in groundwater, this includes solution of soluble minerals, cation exchange between groundwater and rock, ions diffusion, etc.
- *Drawdown* Lowering of water level caused by pumping. It is measured for a given quantity of water pumped during a specified period, or after the pumping level has become constant.
- *Drawdown Cone* A conical groundwater surface created in an unconfined aquifer due to pumping, or an imaginary conical surface indicating pressure relief in a confined aquifer due to pumping.
- *Drift Deposits* Any sediment laid down by, or in association with, the activity of glaciers and ice sheets.
- Drill Stem TesterA device used in a borehole to measure hydraulic properties of a tested(DST)interval and/or to collect fluid sample.
- *Evapotranspiration* Combined term for water lost as vapour from soil/water surface (evaporation) and water lost through plants (transpiration).
- *Fresh Water* Water with total dissolved solids concentration below 1,000 g/m³.

Geomorphology The study of the land-forms on Earth's surface and of the processes that formed them.

Glaciofluvial Sediments or land-forms produced by meltwaters originating from glacier/ice sheet.

Groundwater All the water contained in the pores/voids within rocks (unconsolidated and consolidated).

HydraulicA coefficient "k" depends on the physical properties of formation and
fluid. It describes the "ease" with which a fluid will flow through a porous
material. "k" is the rate of flow per unit cross-sectional area under the
influence of a unit gradient, and has the dimension of:

Length³/Length² x Time or Length/Time (e.g., m/s)

but should not be confused with velocity.

Hydraulic Gradient	Is the change in groundwater elevation per unit of distance in a given direction. If not specified, the direction generally is understood to be that of the maximum rate of decrease in head. This coefficient is dimensionless.
Hydrochemical Type	The definition of a chemical composition of groundwater based on cation and anion concentrations.
Hydrogeological Window	The erosional, sedimentional or structural break in geological strata, which allows hydraulic connection between different aquifers.
Hydrogeology	The science that relates to groundwater. Groundwater as used here includes all water in the zone of saturation beneath the earth's surface, except water chemically combined in minerals.
Hydrograph	A graph showing water surface elevations or flow versus time.
Infiltration	The flow or movement of precipitation or surface water through the ground surface into the ground. Infiltration is the main factor in recharge of groundwater reserves.
Leakage	The flow of water from one hydrogeological unit to another. It may be natural or anthropogenic.
Lithology	A term usually applied to describe composition and texture of sediments and rocks.
Meteoric Water	That which occur in or is derived from the atmosphere.
Mineralization of Groundwater	Synonym of total dissolved solid concentration.
Observation Well	A constructed controlled point of access to an aquifer which allows groundwater observations. Small diameter observation wells are often called piezometers.
Olfactory	Concerned with smelling.
Overburden	1. Any loose material which overlies bedrock (often used as a synonym for Quaternary sediments and/or surficial deposits).
	2. Any barren material, consolidated or loose, that overlies an ore body.
Paraconformity	An uncertain or obscure unconformity in which no erosion surface is discernible or in which the contact is a simple bedding plane and in which the beds above and below the break are parallel.

Permeability	A physical property of the porous medium. Has dimensions $Length^2$. When measured in cm^2 , the value of permeability is very small, therefore more practical units are commonly used - darcy (D) or millidarcy (mD).
Physiography	Synonym of geomorphology.
Phreatic Surface	Synonym of unconfined groundwater surface.
Piezometer	See Observation Well.
Piezometric Surface	An imaginary surface that everywhere coincides with the static level of the water in the aquifer. The surface to which the water from a given aquifer will rise under its full head.
Pneumatic Piezometer	A device used to measure hydrostatic and/or pore pressure in a borehole or engineered structure.
Potentiometric	Synonym to piezometric.
Radius of Well	Is the distance from the centre of the well (test pit) to the limit of the
(Test Pit) Influence	drawdown cone.
Recharge	Water added to the saturated zone from any source. This term is commonly combined with other terms to indicate some specific mode of recharge such as recharge well, recharge area, or artificial recharge.
Recovery Test	A method of obtaining quantitative information on the hydraulic characteristics of an aquifer, routinely utilized following a pump test. After pumping has been terminated, the water level will stop dropping and will begin to rise towards its original position. The rise of the water level can be measured as residual drawdowns, i.e., as the difference between the original water level prior to pumping and the actual water level measured at a given time after pumping stopped.
Saline Water	Water with total dissolved solids concentration ranging from 10,000 to $100,000 \text{ g/m}^3$.
Seepage	1. Slow water movement in subsurface.
	2. Flow of water from man made retaining structures.
	3. A spot or zone, where water oozes from the ground, often forming the source of a small spring.
Spring	A place where water flows from rock or soil upon the land or into body of surface water.

StandpipeA device consisting of a perforated/slotted pipe often used in the past to
measure depth to groundwater surface at shallow depths.

Storage Coefficient The storage coefficient and the specific yield are both defined as the volume of water released or stored per unit surface area of the aquifer per unit change in the component of head normal to that surface. Both are designated by the symbol S and are dimensionless.

The storage coefficient refers only to the confined parts of an aquifer and depends on the elasticity of the aquifer material and the fluid. It typically has an order of magnitude of 10^{-4} to 10^{-6} .

The specific yield refers to the unconfined parts of an aquifer. In practice, it may be considered to equal the effective porosity or drainable pore space because in unconfined aquifers the effects of the elasticity of aquifer material and fluid are generally negligible.

It should be kept in mind that small pores do not contribute to the effective pore space because in small pores the retention forces are greater than the weight of the water. For sands the specific yield may be in the order of 0.1 to 0.2.

In American Literature the terms storage coefficient and specific yield are often used synonymously.

Stratigraphy The geological science concerned with the study of sedimentary rocks in terms of time and space.

Subcrop Bedrock unit occurring at the bedrock surface but covered by Quaternary deposits.

Surficial Deposits See Overburden (1).

Transmissivity The product of the average coefficient of hydraulic conductivity (or permeability) and the thickness of the aquifer. Consequently, transmissivity is the rate of flow under a hydraulic gradient equal to unity through a cross-section of unit width over the whole thickness of the aquifer. It is designated by the symbol T. It has the dimension of:

Length³/Time x Length or Length²/Time (e.g., m²/day)

Unconfined Aquifer A permeable bed only partly filled with water and overlying a relatively impervious layer. Its upper boundary is formed by a free water table under atmospheric pressure. Water in a well penetrating an unconfined aquifer does not, in general, rise above the water surface, except when there is vertical flow.

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		Precipitation			Temperature	
Month	Rainfall (mm)	Snowfall (cm)	Total ⁽¹⁾ Precipitation <i>(mm)</i>	Mean Daily Maximum <i>(°C)</i>	Mean Daily Minimum (°C)	Mean Daily Temperature (°C)
January	0.6	27.2	20.4	-14.5	-25.3	-19.8
February	0.8	21.3	16.0	-8.6	-21.3	-14.9
March	0.9	23.2	17.3	-1.1	-14.8	-7.9
April	8.0	15.8	22.6	9.3	-3.8	2.8
May	37.2	3.6	40.7	17.1	3.0	10.1
June	63.9	0.0	63.9	21.5	7.7	14.6
July	79.1	0.0	79.1	23.2	10.0	16.6
August	71.7	+ 0.0	71.8	21.8	8.5	15.2
September	48.1	3.3	51.4	15.1	3.2	9.1
October	20.0	14.1	32.2	8.4	-1.9	3.3
November	2.9	33.1	26.4	-4.5	-13.5	-9.0
December	1.1	30.5	23.0	-12.6	-22.1	-17.3
Annual	335	172	465	6.3	-5.9	0.2

Table 1Variation of Precipitation and Temperature With Season

Note: ⁽¹⁾ Total precipitation is calculated by summing the rainfall, and the amount of water released by melting the snowfall. Note that the amount of water released by melting 1 cm of snowfall varies with the density of the snow from approximately 1.0 mm (wet, warm snow) to approximately 0.7 mm (cold, dry snow).

Table 2Mean Daily Pan Evaporation for the Mildred Lake Station

Month	Mean Daily Pan Evaporation <i>(mm)</i>	Month	Mean Daily Pan Evaporation <i>(mm)</i>
April	4.1	August	3.7
May	4.3	September	4.4
June	4.7	October	0.8
July	5.0		

Table 3Summary of the Main Geological Formations East of the Athabasca River
(Regional Study Area)

Period	Group	Formation	Composition	Thickness (<i>m</i>)	
Quaternary			Till, clay, sand, silt, and gravel	≤ 135	
Lower	Mannville	(Grand Rapids)	Lithic sand and sandstone	≤ 90	
Cretaceous		Clearwater	Shale and siltstone	≤ 130	
		McMurray	Quartzose sand with heavy oil	≤ 105	
Upper Devonian	Beaverhill Lake	Waterways	Limestone, argillaceous limestone, and calcareous shale	≤ 220	
		Slave Point	Limestone, silty limestone, and siltstone	≤ 15	
Middle	Elk Point	Watt Mountain	Shale	≤ 15	
Devonian		Prairie Evaporite	Halite and anhydrite	≤ 240	
		Methy	Reefal dolostone	≤ 85	
		McLean River	Shale, siltstone, and dolostone	18 to 48	
		La Loche	Arkosic sandstone	≤ 40	
Precambrian		~ ~ ~	Granite and metasedimentary rocks		

Table 4Hydrochemical Types in Major Stratigraphic Units

	Golder Asso	ociates Ltd. (1997a)	Alsands Energ	y Ltd. (1981b, 1982)
Stratigraphic Interval	Mineralization (mg/L TDS)	Predominant Hydrochemical Types	Mineralization (mg/L TDS)	Predominant Hydrochemical Types
Surficial Aquifers ⁽¹⁾	290 - 827	Ca-Na-HCO₃ Na-Ca-HCO₃	239 - 1729	$\begin{array}{c} Ca-Mg-HCO_3\\ Ca-Mg-Na-HCO_3\\ Na-Ca-Mg-HCO_3\\ Ca-HCO_3-SO_4\\ Na-HCO_3\\ Na-HCO_3\\ Na-Ca-HCO_3-Cl \end{array}$
Clearwater	348 - 3058	Na-HCO ₃		
Intra-Orebody Aquifers ⁽¹⁾	968 - 1,556	Na-HCO₃-Cl	277 - 2,148	$\begin{array}{c} Ca-Mg-HCO_3\\ Ca-Mg-Na-HCO_3\\ Ca-Na-Mg-HCO_3\\ Na-Ca-Mg-HCO_3\\ Na-Ca-Hg-HCO_3\\ Na-Ca-HCO_3\\ Na-HCO_3\\ \end{array}$
Basal Aquifer	330 - 1970	Na-HCO ₃ -Cl	1,430 - 7,407	Na-HCO ₃ Na-HCO ₃ -Cl Na-Cl-HCO ₃
Upper Devonian ⁽¹⁾	2,034 - 6,014	Na-HCO ₃ -Cl		
Methy	13,050	Na-CI-SO ₄	9,824 - 78,666	Na-Cl
La Loche	16,100	Na-Ca-Cl-SO ₄	172,000	Na-Cl

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Note: ⁽¹⁾ Upper Devonian is not a formation.

Table 5Summary of AEP Well Records for Township 94-96, Range 9-10, W4M

Township	Range W4M	Current Lease Holder	Number of Wells	Proposed Use
94	9	Gulf, Mobil, Home Oil	19	Observation/Industrial
	10	Gulf, Mobil, Home Oil Fort McKay IR 174	6 35	Observation/Industrial Observation/Industrial
	11	Fort McKay IR 174 Talisman	16 1	Observation/Industrial Observation/Industrial
95	9	Shell Canada	10	Observation/Industrial
	10	Shell Canada	15	Observation/Industrial
	11	Shell Canada	1	Observation/Industrial
96	9	None		n n -
	10	Syncrude Crown Land Solvex	4 1 2	Observation/Industrial Observation/Industrial Observation/Industrial
	11	Syncrude	12	Observation/Industrial

Piezometer No.	Ground Elevation	Stick-Up or Steel PVC Pipe	Datum Elevation	Pipe (Steel or PVC) Diameter	Total Depth Of Piezo.	Open Interval	Date	Depth To Water Below Datum	Groundwater Surface Elevation	Hydraulic Conductivity	Lithology
	(masl)	(above ground) (<i>m</i>)	(top of PVC casing) (masl)	(m)	(below ground) (<i>m</i>)	(below ground) (<i>m</i>)	(y-m-d)	(m)	(masl)	(m/s)	
	(111451)	((11/251)	((((y-m-u)	((111451)	(1105)	
W72-1240	288.19	1.00	289.19	0.051	216.0	190.0 - 216.0	81-Mar-17	26.49	262.70	> 1E-04	Methy Formation
W73-1404	285.45	1.00	286.45	0.051	252.3	219.0 - 252.3	81-Mar-14	20.53 *	265.92	3E-08	Methy Formation
W73-1481	293.38	0.10	293.48	0.120	230.0	108.9 - 227.0	81-Mar-17	32.86	260.62	9E-05	See note 5
W73-1489	293.99	1.60	295.59	0.051	213.5	190.0 - 211.0	81-Mar-17	27.74	267.85	> 1E-04	Methy Formation
W75-1717	289.41	1.30	290.71	0.051	297.0	239.0 - 284.0	81-Mar-17	24.11	266.60	2E-08	Methy Formation
W80-5027	298.89	0.77	299.66	0.051	282.0	215.0 - 282.0	81-Mar-17	36.05 *	263.61	2E-09	Methy Formation
W80-5039	287.25	1.15	288.40	0.051	285.0	125.0 - 285.0	81-Mar-09	32.40	256.00	2E-06	See note 5

NOTES: 1. All Devonian piezometers were reconstructed during February and March 1981 program. (EBA Engineering Consultants, 1981a).

2. For pre-1981 completion details and chemical analyses see Alsands Energy Ltd., May 1981, Hydrology, Part 2 - Groundwater Hydrology, Alsands Project, Calgary, Alberta.

3. NA denotes not available.

4. * denotes groundwater surface elevation possibly not stabilized.

5. Hole was in bad condition due to washouts, age, and loss of circulation during drilling. Piezometer pipe broke during installation, effectively leaving an open interval extending throughout Beaverhill Lake Group, Prairie Evaporite Formation, and Methy Formation.

6. Masl denotes metres above sea level.

Table 6B Piezometer Installation Details, Datum / Groundwater Surface Elevations And Hydraulic Conductivities Cretaceous-Basal Aquifer

Piezometer No.	Ground Elevation	Stick-Up or Steel PVC Pipe (above ground)	Datum Elevation (top of PVC casing)	Pipe (Steel or PVC) Diameter	Total Depth Of Piezo. (below ground)	Open Interval (below ground)	Date	Depth To Water Below Datum	Groundwater Surface Elevation	Hydraulic Conductivity	Lithology
	(masl)	(m)	(masl)	(m)	(m)	(m)	(y-m-d)	(m)	(masl)	(m/s)	
W72-1233	289.25	0.60	289.85	0.114	87.5	76.1 - 82.4	80-Jul-05	17.90	271.95	8E-05 ⁽¹⁾ ; 2E-05 ⁽²⁾	Sand
							80-Jul-29	18.55	271.30		
							80-Sep-07	18.01	271.84		
							81-Mar-16	16.55	273.30		
W72-1234	Construction d	etails not available									
W72-1235	288.25	0.20	288.45	0.203	94.8	78.4 - 87.5	80-Jul-04	17.16	271.29	4E-05 ⁽¹⁾ ; 8E-05 ⁽³⁾	Sand
							80-Jul-27	16.35	272.10		
							80-Sep-07	15.76	272.69		
							81-Mar-16	14.42	274.03		
W72-1238	287.25	1.50	288.75	0.168	94.6	76.2 - 85.4	80-Jul-04	17.20	271.55	6E-04 ⁽¹⁾ ; 2E-05 ⁽²⁾	Sand
							80-Jul-29	17.00	271.75		
							80-Sep-07	16.49	272.26		
							81-Mar-16	14.97	273.78		
W72-1239	289.75	0.97	290.72	0.159	96.4	78.1 - 87.4	80-Jul-05	18.65	272.07	8E-05 ⁽¹⁾ ; 2E-05 ⁽²⁾	Sand
	200110						80-Jui-29	18.46	272.26		
							80-Sep-07	17.32	273.40		
							81-Mar-16	16.46	274.26		
W73-1364	284.00	0.69	284.69	0.060	90.0	85.7 - 86.6	80-Jul-06	7.10	277.59	NA	Sand
							80-Jul-29	6.85	277.84		
							80-Sep-07	6.57	278.12		
							81-Mar-16	5.80	278.89		
W73-1365	Construction d	etails not available									
W73-1432	286.50	1.19	287.69	0.060	68.3	64.7 - 66.4	80-Jul-03	16.62	271.07	NA	Sand
		-					80-Jul-29	16.39	271.30		
							80-Sep-07	15.88	271.81		

Table 6B Piezometer Installation Details, Datum / Groundwater Surface Elevations And Hydraulic Conductivities Cretaceous-Basal Aquifer

Piezometer No.	Ground Elevation	Stick-Up or Steel PVC Pipe (above ground)	Datum Elevation (top of PVC casing)	Pipe (Steel or PVC) Diameter	Total Depth Of Piezo. (below ground)	Open Interval (below ground)	Date	Depth To Water Below Datum	Groundwater Surface Elevation	Hydraulic Conductivity	Lithology
	(masl)	(m)	(masl)	(m)	(m)	(m)	(y-m-d)	(m)	(masl)	(m/s)	
W73-1434	292.00	0.50	292.50	0.114	85.4	83.9 - 85.4	80-Jul-07	19.00	273.50	7E-05 ⁽²⁾	Sand
							80-Jul-27	18.75	273.75		
							80-Sep-07	18.21	274.29		
						81-Mar-16	16.87	275.63			
W73-1439	292.50	0.70	293.20	0.060	91.5	90.0 - 91.5	80-Jul-26	16.80	276.40	NA	Sand
							80-Sep-07	16.40	276.80		
							81-Feb-18	15.36	277.84		
W73-1441	295.75	0.81	296.56	0.060	89.1	81.6 - 82.6	80-Jul-07	21.43	275.13	NA	Sand
						80-Jul-26	20.10	276.46			
							80-Sep-03	20.70	275.86		
							81-Feb-18	19.61	276.95		
W73-1478	296.25	0.70	296.95	0.060	84.2	83.2 - 84.2	80-Jul-07	15.45	281.50	NA	Sand
							80-Jul-27	15.39	281.56		
							80-Aug-08	15.20	281.75		
							80-Aug-17	15.07	281.88		
							80-Sep-03	15.00	281.95		
							80-Nov-27	14.78	282.17		
							81-Feb-13	14.53	282.42		
W74-1510	291.00	0.90	291.90	0.060	90.3	82.7 - 83.6	80-Jul-06	21.10	270.80	NA	Sand
							80-Jul-29	20.10	271.80		
							80-Sep-07	20.17	271.73		
							81-Feb-18	18.94	272.96		
W74-1511	289.25	0.05	289.30	0.340	84.8	75.2 - 83.9	80-Jul-06	19.20	270.10	2E-04 ⁽³⁾	Sand
				80-Jul-29	18.62	270.68					
							80-Sep-07	18.05	271.25		
							81-Mar-16	16.35	272.95		

Table 6B Piezometer Installation Details, Datum / Groundwater Surface Elevations And Hydraulic Conductivities Cretaceous-Basal Aquifer

Piezometer No.	Ground Elevation	Stick-Up or Steel PVC Pipe (above ground)	Datum Elevation (top of PVC casing)	Pipe (Steel or PVC) Diameter	Total Depth Of Piezo. (below ground)	Open Interval (below ground)	Date	Depth To Water Below Datum	Groundwater Surface Elevation	Hydraulic Conductivity	Lithology
	(masl)	(m)	(masl)	(m)	(m)	(m)	(y-m-d)	(m)	(masl)	(m/s)	
W74-1512	Construction d	etails not available		· · · · · · · · · · · · · · · · · · ·							*******
W75-1751	288.75	1.25	290.00	0.219	91.8	75.9 - 88.4	80-Jan-18	20.94	269.06	NA	Sand
							80-Feb-14	20.52	269.48		
							80-Mar-13	20.00	270.00		
							80-Apr-10	19.38	270.62		
							80-May-08	19.14	270.86		
							80-Jun-08	18.62	271.38		
							80-Jul-07	19.14	270.86		
							80-Jul-30	18.44	271.56		
							80-Aug-27	18.05	271.95		
							80-Sep-24	17.89	272.11		
							80-Oct-22	17.66	272.34		
							80-Nov-20	17.27	272.73		
W75-1752	Construction d	etails not available									
W75-1753	289.40	0.30	289.70	0.219	88.8	79.2 - 85.6	80-Jul-05	19.20	270.50	2E-05 ⁽³⁾	Sand
							80-Jul-29	17.32	272.38		
							80-Sep-07	18.00	271.70		
							81-Mar-16	15.90	273.80		
W75-1754	289.40	0.34	289.74	0.168	95.2	81.4 - 91.0	80-Jul-05	17.99	271.75	5E-05 ⁽³⁾	Sand
							80-Jui-29	17.64	272.10		
							80-Sep-07	17.11	272.63		
							81-Mar-16	15.56	274.18		
W80-5025	288.40	0.60	289.00	0.051	122.0	NA	80-Mar-11	6.77	282.23	5E-08 ⁽³⁾	Sand
	200.10						80-Aug-09	5.10	283.90		
							80-Aug-18	5.03	283.97		
							80-Sep-05	5.30	283.70		
							80-Sep-08	6.05	282.95		
							80-Nov-12	5.94	283.06		

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Table 6B Piezometer Installation Details, Datum / Groundwater Surface Elevations And Hydraulic Conductivities Cretaceous-Basal Aquifer

Piezometer No.	Ground Elevation	Stick-Up or St eel PVC Pipe (above ground)	Datum Elevation (top of PVC casing)	Pipe (Steel or PVC) Diameter	Total Depth Of Piezo. (below ground)	Open Interval (below ground)	Date	Depth To Water Below Datum	Groundwater Surface Elevation	Hydraulic Conductivity	Lithology
	(masl)	(m)	(masl)	(m)	(m)	(m)	(y-m-d)	(m)	(masl)	(m/s)	
W80-5026	291.60	0.20	291.80	0.051	98.0	80.1 - 86.4	80-Mar-05	16.88	274.92	4E-05 ⁽³⁾	Sand
							80-Jul-08	16.16	275.64		
							80-Jul-26	16.01	275.79		
							80-Aug-04	15.94	275.86		
							80-Aug-17	15.85	275.95		
							80-Sep-03	15.67	276.13		
							80-Nov-11	15.68	276.12		
							81-Feb-15	14.83	276.97		
W80-5043	287.94	0.80	288.74	0.051	100.0	85.0 - 93.5	80-Jul-15	51.62	237.12	1E-05 ⁽³⁾	Sand
							80-Jul-25	51.65	237.09		
							80-Sep-02	51.60	237.14		
							81-Feb-15	51.90	236.84		
W80-5053	293.46	0.90	294.36	0.051	98.0	75.8 - 91.5	80-Mar-20	61.14	233.22	Results not interpretable	Sand
							80-Jul-16	61.80	232.56		
							80-Jul-24	61.25	233.11		
							80-Aug-17	60.92	233.44		
							80-Sep-06	61.11	233.25		
							80-Sep-09	61.65	232.71		
							80-Nov-25	61.50	232.86		
W80-5054	290.74	0.60	291.34	0.051	80.0	70.8 - 75.0	80-Mar-11	55.98	235.36	7E-06 ⁽³⁾	Sand
							80-Jul-24	56.58	234.76		
							80-Aug-18	56.61	234.73		
							80-Sep-06	56.42	234.92		
							80-Sep-09	56.52	234.82		
							80-Nov-26	56.54	234.80		
							81-Feb-15	56.39	234.95		

Table 6B Piezometer Installation Details, Datum / Groundwater Surface Elevations And Hydraulic Conductivities Cretaceous-Basal Aquifer

Piezometer No.	Ground Elevation	Stick-Up or Steel PVC Pipe (above ground)	Datum Elevation (top of PVC casing)	Pipe (Steel or PVC) Diameter	Total Depth Of Piezo. (below ground)	Open Interval (below ground)	Date	Depth To Water Below Datum	Groundwater Surface Elevation	Hydraulic Conductivity	Lithology
	(masl)	(m)	(masl)	(m)	(m)	(m)	(y-m-d)	(m)	(masl)	(m/s)	
W80-5069	291.75	1.00	292.75	0.051	89.0	75.0 - 83.0	80-Mar-20	20.03	272.72	5E-05 ⁽³⁾	Sand
							80-Jul-14	20.05	272.70		
							80-Jul-25	20.01	272.74		
							80-Aug-05	19.91	272.84		
							80-Aug-17	19.86	272.89		
							80-Sep-04	19.86	272.89		
							80-Nov-26	19.81	272.94		
							81-Feb-15	19.82	272.93		
W80-5072	291.16	0.70	291.86	0.051	77.0	61.8 - 64.5	80-Jul-12	5.05	286.81	NA	Sand
							80-Jui-25	4.04	287.82		
							80-Sep-07	1.95	289.91		
							81-Mar-17	1.91	289.95		
W80-5076	299.54	0.60	300.14	0.051	86.0	74.3 - 76.2	80-Mar-07	21.59	278.55	5E-05 ⁽³⁾	Sand
							80-Jul-14	21.36	278.78		
							80-Aug-15	22.30	277.84		
							80-Sep-04	21.24	278.90		
							80-Sep-09	22.26	277.88		
							80-Nov-28	22.09	278.05		
							81-Mar-17	21.07	279.07		
N80-5077	298.62	1.00	299.62	0.051	88.0	74.9 - 81.0	80-Mar-22	21.96	277.66	1E-04 ⁽³⁾	Sand
							80-Jul-14	21.80	277.82		
							80-Jul-25	21.86	277.76		
							80-Aug-14	21.74	277.88		
							80-Sep-03	21.68	277.94		
							80-Sep-08	21.73	277.89		
							80-Nov-27	21.56	278.06		
							81-Mar-17	21.50	278.12		

Table 6B Piezometer Installation Details, Datum / Groundwater Surface Elevations And Hydraulic Conductivities Cretaceous-Basal Aquifer

Piezometer No.	Ground Elevation	Stick-Up or Steel PVC Pipe (above ground)	Datum Elevation (top of PVC casing)	Pipe (Steel or PVC) Diameter	Total Depth Of Piezo. (below ground)	Open Interval (below ground)	Date	Depth To Water Below Datum	Groundwater Surface Elevation	Hydraulic Conductivity	Lithology
	(masl)	(m)	(masl)	(m)	(m)	(<i>m</i>)	(y-m-d)	(m)	(masl)	(m/s)	
W81-0029	297.10	1.00	298.10	0.051	81.7	70.0 - 81.7	81-Mar-07	22.24	275.86	< 1E-07	Sand
W81-0041	299.50	1.25	300.75	0.051	81.7	70.0 - 81.7	81-Mar-09	46.23 *	254.52	< 1E-07	Sand
W81-0043	291.50	1.50	293.00	0.051	75.0	63.5 - 75.0	81-Mar-04	14.08	278.92	1E-06	Sand
W81-0046	293.20	1.25	294.45	0.051	89.6	77.8 - 89.6	81-Mar-07	17.55	276.90	< 1E-07	Sand
W81-0051	286.70	1.31	288.01	0.051	71.5	53.9 - 71.5	81-Mar-08	12.99	275.02	4E-07	Sand
W81-0053	288.00	1.20	289.20	0.051	90.7	78.0 - 90.7	81-Mar-07	53.00	236.20	3E-07	Sand
W81-0061	299.60	1.30	300.90	0.051	89.0	67.5 - 89.0	81-Mar-05	21.43	279.47	6E-05	Sand
W81-0068	289.80	1.40	291.20	0.051	83.0	70.5 - 83.0	81-Mar-09	13.54	277.66	< 1E-07	Sand
W81-0069	287.90	1.50	289.40	0.051	102.0	81.6 - 102.0	81-Mar-10	11.90	277.50	1E-05	Sand
W81-0072	300.10	1.30	301.40	0.051	82.9	72.0 - 82.9	81-Mar-08	22.74	278.66	2E-07	Sand
MW97-42	280.75	0.61	281.36	0.051	89.0	77.0 - 89.0	97-Apr-03	50.50	230.86	> 1E-04	Sand

NOTES:

1. Hydraulic conductivity measurements were conducted by Leggette, Brashears, and Graham Consulting Groundwater Geologists on August 23-27, 1972.

2. Hydraulic conductivity measurements were conducted by Shell Canada Ltd. on September 21 - October 11, 1973.

3. Hydraulic conductivity measurements were conducted by EBA Engineering Consultants Ltd. following instrument development using compressed air. Therefore, the results should be considered as approximate.

4. NA denotes not available.

5. * denotes groundwater surface elevation possibly not stabilized.

6. Hydrographs for piezometers 1478 and 1751 for periods 1974-1976 and 1975-1979 (respectively) are shown in Alsands, 1981 - Hydrology, Part 2 - Groundwater Hydrology, Alsands Project, Calgary, Alberta, May 1981.

7. Piezometer installation details for MW97- series were taken from Golder Associates 1997 report.

8. Where the basal sand is absent, piezometers may be completed in the oil sand (>7% bitumen).

9. Masi denotes metres above sea level.

Table 6C

Piezometer Installation Details, Datum / Groundwater Surface Elevations And Hydraulic Conductivities

Cretaceous - Intra Orebody and Near Contact with Quaternary Deposits
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	Elevation	Stick-Up or Steel PVC Pipe	Datum Elevation	Pipe (Steel or PVC) Diameter	Total Depth Of Piezo.	Open Interval	Date	Depth To Water Below Datum	Groundwater Surface Elevation	Hydraulic Conductivity	Lithology
	((above ground)	(top of PVC casing)	()	(below ground)	(below ground)	(()	(magl)	(()	*
	(masl)	(m)	(masl)	(m)	(m)	(m)	(y-m-d)	<u>(</u> m)	(masl)	(m/s)	
Alsands Wat	ter Intake Are	<u>ea</u>									
80-WI-1A	284.64	1.0	249.64	0.025	6.7	NA	80-Mar-24	4.40	245.24	NA	Silty Clay/Oil Sand
							80-Mar-25	4.38	245.26		
							80-Aug-10	4.54	245.10		
							80-Sep-08	4.52	245.12		
Alsands Nor	th of Isadore	e's Lake									
815002G	244.4	NA	NA	NA	11.7	11.1 - 11.7	81-Mar-11	1.5	232.9	NA	Oil Sand
815003G	240.9	NA	NA	NA	9.0	8.4 - 9.0	81-Feb-10	6.3	234.6	NA	Clay Shale, Oil Sand
							81-Mar-11	1.5	239.4		
815004G	236.3	NA	NA	NA	8.5	7.9 - 8.5	81-Feb-10	2.4	233.9	NA	Clay Shale, Oil Sand
							81-Mar-11	2.7	233.6		
											2 10
815005G	237.3	NA	NA	NA	13.1	12.5 - 13.1	81-Mar-11	1.2	236.1	NA	Oil Sand
815006G	238.2	NA	NA	NA	9.5	8.8 - 9.5	81-Mar-11	7.4	230.8	NA	Clay Shale, Oil Sand
815007G	249.1	NA	NA	NA	12.6	12.0 - 12.6	81-Mar-11	1.6	247.5	NA	Clay Shale, Oil Sand
0130070	245.1	NA .	117		12.0	12.0	or marri	1.0	241.0		oray onale, on oand
815008G	248.9	NA	NA	NA	6.1	5.5 - 6.1	81-Mar-12	5.8	243.1	NA	Oil Sand
815009G	250.0	NA	NA	NA	5.9	5.3 - 5.9	81-Feb-12	7.6	242.4	NA	Oil Sand
							81-Mar-12	0.4	249.6		
815010G	260.0	NA	NA	NA	14.2	13.6 - 14.2	81-Mar-11	10.4	249.6	NA	Clay Shale, Oil Sand
					_						
815011G	245.4	NA	NA	NA	5.5	4.9 - 5.5	81-Mar-11	0.8	244.6	NA	Oil Sand, Clay Shale
815012G	246.3	NA	NA	NA	7.2	6.6 - 7.2	81-Feb-09	7.1	239.2	NA	Oil Sand
							81-Mar-11	0.3	246.0		
815013G	239.8	NA	NA	NA	14.5	13.9 - 14.5	81-Mar-11	2.2	237.6	NA	Clay Shale, Oil Sand

Table 6C Piezometer Installation Details, Datum / Groundwater Surface Elevations And Hydraulic Conductivities

Piezometer No.	Ground Elevation	Stick-Up or Steel PVC Pipe	Datum Elevation	Pipe (Steel or PVC) Diameter	Total Depth Of Piezo.	Open Interval	Date	Depth To Water Below Datum	Groundwater Surface Elevation	Hydraulic Conductivity	Lithology
	(masl)	(above ground) (<i>m</i>)	(top of PVC casing) (masl)	(m)	(below ground) (<i>m</i>)	(below ground) (m)	(y-m-d)	(m)	(masl)	(m/s)	
815014G	238.9	NA	NA	NA	12.6	12.0 - 12.6		11.8	227.1	NA	Clay Shale
815017G	242.3	NA	NA	NA	4.6	4.0 - 4.6	81-Mar-11	1.6	240.7	NA	Clay Shale, Oil Sand
0100174	242.0				4.0	4.0 - 4.0	01-141-11	1.0	240.7		Clay Shale, Oil Sand
815018G	246.2	NA	NA	NA	5.9	5.3 - 5.9	81-Mar-11	2.1	244.1	NA	Oil Sand
Alsands Pla	nt Site										
80-P-01	299.4	1.72	301.12	0.075	12.14	NA	80-Feb-17	3.02	298.10	NA	Oil Sand
							80-Mar-08	3.47	297.65		
							80-Mar-23	3.72	297.40		
							80-Sep-04	3.42	297.70		
							80-Sep-08	3.42	297.70		
							81-Feb-19	3.81	297.31		
80-P-18	299.43	0.43	299.86	0.075	10.57	NA	80-Sep-04	1.12	298.74	NA	Clay Shale/Oil Sand
							80-Sep-08		298.66		
							81-Feb-20	0.30	299.56		
80-P-1 9	297.74	0.84	298.58	0.075	14.34	NA	80-Mar-08	2.13	296.45	NA	Oil Sand
							80-Mar-23	2.58	296.00		
							80-Sep-04	0.93	297.65		
							80-Sep-08	0.90	297.68		
							81-Feb-19	0.95	297.63		
80-P-20	296.57	1.11	297.68	0.075	12.02	NA	80-Mar-08	1.64	296.04	NA	Oil Sand
							80-Sep-04	2.46	295.22		
							80-Sep-08	2.86	294.82		
							81-Feb-19	2.59	295.09		
<u>Alsands Tai</u>	lings Pond A	rea									
80-TP-5	300.76	0.14	300.90	0.075	8.11	NA	80-Mar-23	1.54	299.36	NA	Clay Shale/Oil Sand
							80-Jul-13	1.12	299.78		
							80-Jul-29	0.60	300.30		
							80-Sep-06	1.30	299.60		
							80-Sep-08	1.31	299.59		
							80-Nov-27	1.12	299.78		

Cretaceous - Intra Orebody and Near Contact with Quaternary Deposits

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Table 6C

Piezometer Installation Details, Datum / Groundwater Surface Elevations And Hydraulic Conductivities

Piezometer No.	Ground Elevation	Stick-Up or Steel PVC Pipe (above ground)	Datum Elevation (top of PVC casing)	Pipe (Steel or PVC) Diameter	Total Depth Of Piezo. (below ground)	Open Interval (below ground)	Date	Depth To Water Below Datum	Groundwater Surface Elevation	Hydraulic Conductivity	Lithology
	(masl)	(m)	(masl)	(m)	(m)	(m)	(y-m-d)	(m)	(masl)	(m/s)	
80-TP-13	294.17	1.20	295.37	0.075	8.12	NA	80-Mar-23	1.37	294.00	NA	Clay Shale/Oil Sand
							80-Jul-28	2.00	293.37		
							80-Sep-06	1.93	293.44		
80-TP-42	284.02	0.70	284.72	0.075	11.54	NA	80-Mar-23	1.30	283.42	NA	Clay Shale/Oil Sand
							80-Jul-29	1.00	283.72		
							80-Sep-06	0.88	283.84		
							81-Feb-20	0.78	283.94		
80-TP-48	283.55	0.80	284.35	0.075	9.33	NA	80-Mar-09	1.30	283.05	NA	Oil Sand
							80-Jul-12	0.91	283.44		
							80-Jul-29	1.00	283.35		
							80-Aug-11	1.00	283.35		
							80-Aug-16	0.96	283.39		
							80-Sep-06	0.98	283.37		
							80-Nov-26	0.88	283.47		
80-TP-58	296.49	0.80	297.29	0.075	7.86	NA	80-Mar-09	2.20	295.09	NA	Clay Shale/Oil Sand
							80-Jul-29	1.20	296.09		
							80-Sep-06	0.98	296.31		
							81-Feb-20	1.04	296.25		
80-TP-66	288.05	0.40	288.45	0.075	9.08	NA	80-Mar-24	4.50	283.95	NA	Clay Shale
							80-Jul-29	2.23	286.22		
							80-Sep-06	2.11	286.34		
							81-Feb-20	2.04	286.41		
MW97-42A	NA	0.61	NA	0.051	24.5	20.7 - 24.5	81-Apr-03	14.14	267.3	7 X 10 ⁻⁸	Sand

Cretaceous - Intra Orebody and Near Contact with Quaternary Deposits

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Table 6C

Piezometer Installation Details, Datum / Groundwater Surface Elevations And Hydraulic Conductivities

Piezometer No.	Ground Elevation	Stick-Up or Steel PVC Pipe (above ground)	Datum Elevation (top of PVC casing)	Pipe (Steel or PVC) Diameter	Total Depth Of Piezo. (below ground)	Open Interval (below ground)	Date	Depth To Water Below Datum	Groundwater Surface Elevation	Hydraulic Conductivity	Lithology
	(masl)	(m)	(masl)	(m)	(m)	(m)	(y-m-d)	(m)	(masl)	(m/s)	
Mine Site A	rea										
W71-1119	Construction d	etails not available									
W71-1182	Construction d	etails not available									
W72-1213	Construction d	etails not available									
815185G	299.9	NA	NA	NA	4.6	NA	81-Mar-06	2.0	NA	NA	Oil Sand
815186G	299.2	NA	NA	NA	.4.7	3.7 - 4.7	81-Mar-07	1.8	NA	NA	Oil Sand
815188G	297.9	NA	NA	NA	5.0	NA	81-Mar-07	2.3	NA	NA	Oil Sand
815189G	296.9	NA	NA	NA	5.0	4.2 - 5.0	81-Mar-07	3.1	NA	NA	Clay Shale, Oil Sand

Cretaceous - Intra Orebody and Near Contact with Quaternary Deposits

NOTES: 1. 80- and 81- series piezometer installation details for Water Intake, North of Isadore's Lake, Plant Site, Tailings Pond and Mine Site areas were taken from Hardy Associates (1978) Ltd. and EBA Engineering Consultants Ltd. reports prepared for Alsads in 1980 and 1981.

2. NA denotes not available.

3. Selected hydrographs are shown in Alsads, 1981 - Hydrology, Part 2 - Groundwater Hydrology, Alsads Project, Calgary, Alberta, May, 1981.

4. Piezometer installation details for MW-series were taken from Golder Associates, 1997 report.

5. "Standpipes" installed during the geotechnical exploration programs, unless upgraded, are not included in this table.

6. Masl denotes metres above sea level.

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Piezometer No.	Ground Elevation (masl)	Stick-Up or Steel PVC Pipe (above ground) (m)	Datum Elevation (top of PVC casing) (masl)	Pvc Pipe Diameter (<i>m</i>)	Total Depth Of Piezo. (below ground) (m)	Depth Interval Of Sand (below ground) (m)	Date (y-m-d)	Depth To Water Below Datum (<i>m</i>)	Groundwater Surface Elevation (masl)	Hydraulic Conductivity (m/s)	Lithology
Alsands Wate	r Intake Area		-								
80-WI-2	239.22	0.50	239.72	0.025	9.0	NA	80-Mar-24 80-Aug-10 80-Sep-08	0.57 1.13 1.50	239.15 238.59 238.22	NA	Silty Clay
80-WI-4B	233.06	0.50	233.56	0.025	5.5	NA	80-Aug-10 80-Sep-08	0.52 0.45	233.04 233.11	NA	Silty Clay
80-WI-5	237.32	1.10	238.42	0.025	10.55	NA	80-Mar-24 80-Mar-25 80-Aug-10 80-Sep-08	3.30 3.82 4.72 3.68	235.12 234.60 233.70 234.74	NA	Silty Clay
80-WI-6A	250.37	NA	NA	NA	NA	NA	80-Mar-25	1.12	249.25	NA	NA
80-WI-7	234.92	NA	NA	NA	5.2	NA	80-Mar-25	0	234.92	NA	Sand/clay
80-WI- 9	234.69	NA	NA	NA	6.5	NA	80-Mar-24 80-Mar-25	3.60 3.69	231.09 231.00	NA	Sand
80-WI-13	233.09	NA	NA	NA	6.0	NA	80-Mar-24 80-Mar-25	1.30 1.32	231.79 231.77	NA	Sand
80-WI-14B	233.20	NA	NA	NA	5.2	NA	80-Mar-24	0.3	232.90	NA	Sand
80-WI-15B	232.90	NA	NA	NA	2.6	NA	80-Mar-25	0.1	232.80	NA	Peat

Piezometer No.	Ground Elevation (masl)	Stick-Up or Steel PVC Pipe (above ground) (m)	Datum Elevation (top of PVC casing) (masl)	Pvc Pipe Diameter (m)	Total Depth Of Piezo. (below ground) (m)	Depth Interval Of Sand (below ground) (m)	Date (y-m-d)	Depth To Water Below Datum (m)	Groundwater Surface Elevation (masl)	Hydraulic Conductivity (m/s)	Lithology
Alsands Plant	t Site Area										ayaan ahaa ahaa ahaa ahaa daa dada dada ahaa ahaa dada d
80-P-04	299.24	1.05	300.29	0.075	2.85	NA	80-Mar-08	2.70	297.59	NA	Sand
							80-Sep-04	2.23	298.06		
							80-Sep-08	2.26	298.03		
							81-Feb-19	2.85	297.44		
Alsands Tailir	ngs Pond Are	<u>a</u>									
80-TP-80	283.87	1.09	284.96	0.075	2.17	NA	80-Mar-10	1.45	283.51	NA	Peat
							80-Jul-15	1.24	283.72		
							80-Jul-29	1.00	283.96		
							80-Aug-11	0.93	284.03		
							80-Aug-16	0.93	284.03		
							80-Sep-06	0.94	284.02		
							80-Nov-29	0.87	284.09		
80-TP-84	288.01	1.00	289.01	0.075	2.80	NA	80-Mar-13	1.50	287.51	NA	Sand
							80-Jul-10	1.90	287.11		
							80-Jul-29	1.20	287.81		
							80-Aug-17	1.39	287.62		
							80-Sep-06	1.37	287.64		
							80-Sep-09	1.41	287.60		
							80-Nov-25	1.40	287.61		
80-TP-120	284.38	0.74	285.12	0.075	4.29	NA	80-Jul-29	2.55	282.57	NA	Gravel
							80-Sep-06	2.10	283.02		
							80-Sep-08	2.09	283.03		
MW97-6	283.32	0.76	284.08	0.051	2.20	0.60 - 1.70	97-Mar-29	Dry	<282.48	NA	Sandy Silt

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Piezometer No.	Ground Elevation (masl)	Stick-Up or Steel PVC Pipe (above ground) (m)	Datum Elevation (top of PVC casing) (masl)	Pvc Pipe Diameter (<i>m</i>)	Total Depth Of Piezo. (below ground) (m)	Depth Interval Of Sand (below ground) (m)	Date (y-m-d)	Depth To Water Below Datum (<i>m</i>)	Groundwater Surface Elevation (masl)	Hydraulic Conductivity (m/s)	Lithology
Mine Site Are	<u>a</u>										
80-MS-33	282.17	0.60	282.77	0.025	2.75	NA	80-Jul-27 80-Aug-01 80-Aug-03 80-Aug-19 80-Sep-05 80-Nov-11	0.78 0.70 0.59 0.55 0.53 0.38	281.99 282.07 282.18 282.22 282.24 282.39	NA	Sand, Clay, Peat
80-MS-35	286.71	0.29	287.00	0.025	3.05	NA	81-Mar-03 80-Aug-01 80-Sep-05 81-Feb-13	0.48 0.90 0.60 1.55	282.29 286.10 286.40 285.45	NA	Silty Sand
80-MS-37	293.81	1.00	294.81	0.025	11.87	NA	80-Aug-01 80-Sep-05 80-Sep-07 81-Mar-03	1.86 1.32 1.34 3.10	292.95 293.49 293.47 291.71	NA	Sand, Clay
80-MS-101	283.65	0.50	284.15	0.025	2.80	NA	80-Aug-08 80-Sep-03 80-Sep-07	1.45 1.45 1.51	282.70 282.70 282.64	NA	Sand
80-MS-103	280.12	1.33	281.45	0.025	2.10	NA	80-Jul-27 80-Aug-08 80-Aug-14 80-Sep-03 80-Sep-07 80-Nov-27	1.65 1.60 1.57 1.53 1.52 1.45	279.80 279.85 279.88 279.92 279.93 280.00	NA	Sand, Peat

4

Piezometer No.	Ground Elevation	Stick-Up or Steel PVC Pipe (above ground)	Datum Elevation (top of PVC casing)	Pvc Pipe Diameter	Total Depth Of Piezo. (below ground)	Depth Interval Of Sand (below ground)	Date	Depth To Water Below Datum	Groundwater Surface Elevation	Hydraulic Conductivity	Lithology
	(masl)	(m)	(masl)	(m)	(m)	(m)	(y-m-d)	(m)	(masl)	(m/s)	
80-MS-104	289.52	0.50	290.02	0.025	2.65	NA	80-Aug-01	0.68	289.34	NA	Sand
							80-Sep-03	0.64	289.38		
							80-Sep-07	0.73	289.29		
80-MS-106	287.45	0.91	288.36	0.025	3.45	NA	80-Aug-01	2.02	286.34	NA	Sand
							80-Sep-03	1.51	286.85		
							80-Sep-07	1.53	286.83		
80-MS-108	289.95	0.50	290.45	0.025	1.05	NA	80-Aug-08	0.59	289.86	NA	Sand, Peat
							80-Sep-03	0.60	289.85		
							80-Sep-07	0.61	289.84		
80-MS-112	291.89	1.60	293.49	0.025	4.13	NA	80-Aug-08	1.63	291.86	NA	Sand, Peat
							80-Sep-03	1.67	291.82		
							80-Sep-07	1.69	291.80		
80-MS-116	293.71	1.15	294.86	0.025	2.93	NA	80-Aug-06	1.20	293.66	NA	Sand, Clay
							80-Sep-05	1.21	293.65		
							81-Mar-03	0.85	294.01		
80-MS-223	282.77	0.60	283.37	0.025	4.74	NA	80-Aug-01	1.20	282.17	NA	Sand, Clay
							80-Sep-05	0.53	282.84		
							80-Sep-07	0.53	282.84		
							81-Mar-03	4.55	278.82		
80-MS-224	288.44	1.95	290.39	0.025	3.10	NA	80-Aug-07	1.95	288.44	NA	Sand
							80-Sep-05	1.90	288.49		
							80-Sep-07	1.85	288.54		
							81-Mar-03	1.80	288.59		

Piezometer No.	Ground Elevation	Stick-Up or Steel PVC Pipe (above ground)	Datum Elevation (top of PVC casing)	Pvc Pipe Diameter	Total Depth Of Piezo. (below ground)	Depth Interval Of Sand (below ground)	Date	Depth To Water Below Datum	Groundwater Surface Elevation	Hydraulic Conductivity	Lithology
	(masl)	(m)	(masl)	(m)	(m)	(m)	(y-m-d)	(m)	(masl)	(m/s)	
80-MS-227	299.62	0.80	300.42	0.025	1.89	NA	80-Jul-30	0.86	299.56	NA	Sand
							80-Sep-05	0.79	299.63		
							80-Sep-08	0.80	299.62		
80-MS-249	293.16	0.56	293.72	0.025	2.70	NA	80-Jul-31	1.20	292.52	NA	NA
							80-Sep-05	1.17	292.55		
							81-Feb-13	0.67	293.05		
80-MS-253	284.12	0.80	284.92	0.025	3.75	NA	80-Aug-07	3.54	281.38	NA	NA
							80-Sep-05	3.40	281.52		
							80-Sep-07	3.42	281.50		
							81-Mar-04	2.46	282.46		
80-MS-260	298.45	0.95	299.40	0.025	2.82	NA	80-Apr-16	2.62	296.78	NA	NA
							80-Apr-23	2.61	296.79		
							80-Apr-27	2.14	297.26		
							80-May-05	1.91	297.49		
							80-May-22	1.91	297.49		
							80-May-27	1.49	297.91		
							80-Jun-06	1.58	297.82		
							80-Jun-17	1.81	297.59		
							80-Jun-25	1.74	297.66		
							80-Jul-02	2.09	297.31		
							80-Jul-06	1.83	297.57		
							80-Jul-26	1.67	297.73		
							80-Jul-30	1.40	298.00		
							80-Aug-08	2.09	297.31		
							80-Aug-15	1.98	297.42		
							80-Sep-05	1.93	297.47		

Piezometer No.	Ground Elevation (masl)	Stick-Up or Steel PVC Pipe (above ground) (m)	Datum Elevation (top of PVC casing) (masl)	Pvc Pipe Diameter (m)	Total Depth Of Piezo. (below ground) (m)	Depth Interval Of Sand (below ground) (m)	Date (y-m-d)	Depth To Water Below Datum (m)	Groundwater Surface Elevation (masl)	Hydraulic Conductivity (m/s)	Lithology
80-MS-264	291.16	0.90	292.06	0.025	4.20	NA	80-Aug-08	0.92	291.14	NA	NA
							80-Sep-05	0.97	291.09		
							80-Sep-07	0.95	291.11		
							81-Mar-17	0.90	291.16		
80-MS-273	292.31	1.56	293.87	0.075	4.62	NA	80-Apr-12	2.96	290.91	NA	Clayey Silt
							80-Apr-17	3.01	290.86		
							80-Apr-22	2.87	291.00		
							80-Apr-27	2.53	291.34		
							80-May-05	2.17	291.70		
							80-May-21	2.18	291.69		
							80-May-28	2.37	291.50		
							80-Jun-05	2.45	291.42		
							80-Jun-16	2.10	291.77		
							80-Jun-23	2.15	291.72		
							80-Jul-02	2.37	291.50		
							80-Jul-07	2.03	291.84		
							80-Jul-15	2.26	291.61		
							80-Jul-21	1.98	291.89		
							80-Jul-25	1.84	292.03		
							80-Jul-31	1.80	292.07		
							80-Aug-05	1.65	292.22		
							80-Aug-15	1.53	292.34		
							80-Aug-16	1.61	292.26		
							80-Aug-27	1.65	292.22		
							80-Sep-04	1.64	292.23		
							80-Sep-05 80-Sep-22	1.62	292.25 292.36		
							80-Sep-22 80-Oct-03	1.51 2.21	292.30		
							80-Nov-26		@ 292.14		

Table 6D Piezometer Installation Details, Datum / Groundwater Surface Elevations And Hydraulic Conductivities Quaternary Deposits

Piezometer No.	Ground Elevation	Stick-Up or Steel PVC Pipe (above ground)	Datum Elevation (top of PVC casing)	Pvc Pipe Diameter	Total Depth Of Piezo. (below ground)	Depth Interval Of Sand (below ground)	Date	Depth To Water Below Datum	Groundwater Surface Elevation	Hydraulic Conductivity	Lithology
	(masl)	(m)	(masl)	(m)	(m)	(m)	(y-m-d)	(m)	(masl)	(m/s)	
80-MS-280	292.21	0.44	292.65	0.025	4.19	NA	80-Jul-31 80-Sep-05	1.65 1.58	291.00 291.07	NA	Silty Sand
80-MS-286	295.50	0.90	296.40	0.025	2.90	NA	80-Jul-31 80-Sep-05 80-Sep-08	0.90 0.86 0.88	295.50 295.54 295.52	NA	Sand
MW97-1	284.77	0.73	285.50	0.051	4.60	2.00 - 3.80	97-Apr-03	3.18	282.32	4 x 10 ⁻⁷	Silty Gravel
MW97-2	283.14	0.73	283.87	0.051	3.80	1.10 - 2.90	97-Apr-03	1.17	282.70	>10 ⁻⁴	Fine to Medium Grained Sand
MW97-3	287.30	0.70	288.00	0.051	5.20	3.10 - 5.20	97-Apr-03	3.48	284.52	9 x 10 ⁻⁷	Silty, Medium Grained Sand
MW97-4	282.25	0.61	282.86	0.051	3.40	2.30 - 3.40	97-Apr-03	1.14	281.72	2 x 10 ⁻⁷	Medium Grained, Silty Sand
MW97-5	284.95	0.85	285.80	0.051	3.70	1.50 - 3.70	97-Apr-03	3.51	282.29	2 x 10 ⁻⁶	Silty Gravel

NOTES:

1. 80- series piezometer installation details for Water Intake, Plant Site, and Tailings Pond Areas were taken from Hardy Associates (1978) Ltd. and EBA Engineering Consultants Ltd. reports prepared for Alsands in 1980 and 1981.

2. Piezometer installation details for Mine Site Area were taken from Robinson Dames & Moore reports prepared for Alsands in 1980.

3. NA denotes not available.

4. Selected hydrographs are shown in Alsands, 1981 - Hydrology, Part 2 - Groundwater Hydrology, Alsands Project, Calgary, Alberta, May 1981.

5. Piezometer installation details for MW97-series were taken from Golder Associates, 1997 report.

6. "Standpipes" installed during the geotechnical exploration programs, unless upgraded, are not included in this table.

7. Masi denotes metres above sea level.

Table 7A

Groundwater Quality: Field Measured Parameters

Monitoring Station	Date of Sampling	Temperature	EC	рН	Remarks
	(y-m-d)	(°C)	(µS/cm)	(units)	
MW97-42	97-Apr-04	6.9	3740	7.12	

Cretaceous - Basal Aquifer

Table 7B

Groundwater Quality: Field Measured Parameters

Cretaceous - Intra Orebody and Near Contact with Quarternary Deposits

Monitoring Station	Date of Sampling	Temperature	EC	рН	Remarks
	(y-m-d)	(°C)	(µS/cm)	(units)	
MW97-42A	97-Apr-04	4.5	1326	6.92	

Table 7C

Groundwater Quality: Field Measured Parameters *Quaternary Deposits*

Monitoring Station	Date of Sampling	Temperature	EC	рН	Remarks
	(y-m-d)	(°C)	(µS/cm)	(units)	
Alsands Tailings Pond	d Area		ge generaties namen als klass dage werde generaties of his his his		
MW97-6	97-Apr-04	NA	NA	NA	Dry
Aine Site Area					
MW97-1	97-Apr-04	2.1	741	7.14	
MW97-2	97-Apr-04	1.1	377	7.14	
MW97-3	97-Apr-04	0.9	518	6.80	
MW97-4	97-Apr-04	1.3	867	6.96	
MW97-5	97-Apr-04	2.3	1285	7.70	

NOTES:

1.

Table 8AWater Quality: Indicator Concentrations

Monitoring Station	Date of Sampling	рН	Sulphate	Chloride	Total Dissolved Solids	Iron	Manganese	Fluoride	Hydrochemical Type
	(y-m-d)	(units)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	
W72-1240	81-Mar-14	7.3	3,734	22,340	42,468	0.45	0.11	NA	CI-Na
W73-1404	81-Mar-13	See note 3	3						
W73-1481	81-Mar-13	7.4	3,640	21,223	40,724	59.5	1.64	NA	CI-Na
W73-1489	81-Mar-08	7.6	2,726	5,920	13,948	10.9	0.43	NA	CI-Na
	81-Mar-15	7.4	2,551	5,735	13,462	0.12	0.06	NA	CI-Na
W75-1717	81-Mar-16	7.6	3,177	9,606	20,638	200	2.15	NA	CI-Na
W80-5027	81-Mar-01	7.6	1,160	4,915	9,824	0.10	< 0.01	NA	CI-Na
W80-5039	81-Mar-06	7.3	4,737	43,563	78,666	3.30	0.38	NA	CI-Na

Devonian - Methy Formation

NOTES: 1. All piezometers completed in the Methy Formation Carbonates were reconstructed in February and March 1981. (EBA Consultants Ltd. 1981a).

2. The hydrochemical data for these piezometers, prior to reconstruction, are given in Alsands Energy Ltd. -Hydrogeology, Part 2 - Groundwater hydrogeology, Alsands Project, May 1981, Calgary, Alberta.

3. Groundwater sample collected from piezometer 1404 on March 13, 1981 had pH = 11.1, indicating contamination with cement filtrate.

4. Iron and manganese represent total concentrations. High concentration of suspended solids is expected to contribute to elevated and high levels of these metals.

Table 8BGroundwater Quality: Indicator Concentrations

Monitoring Station	Date of Sampling	рН	Sulphate	Chloride	Total Dissolved Solids	Iron	Manganese	Fluoride	Hydrochemica Type
	(y-m-d)	(units)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	
W71 1110	1971	8.1	34	949	4,046	NA	NA	NA	HCO₃-CI-Na
W71-1119	1971	7.9	60	949 1,170	3,992	NA	NA	NA	CI-HCO ₃ -Na
W72-1233	80-Aug-06	8.6	39	1,050	3,280	0.1	0.4	NA	CI-HCO ₃ -Na
W72-1235	72-Aug-26	7.5	46	1,056	3,764	Trace	NA	NA	Cl-HCO ₃ -Na
	73-Sep-30	7.5	55	1,173	3,929	NA	NA	NA	CI-HCO₃-Na
	73-Oct-05	7.4	35	1,173	3,881	NA	NA	NA	Cl-HCO₃-Na
	73-Oct-11	7.4	16	1,173	3,938	NA	NA	NA	Cl-HCO₃-Na
	80-Jul-04	8.3	24	1,139	3,699	0.6	0.1	1.6	Cl-HCO₃-Na
	80-Jul-27	8.1	22	1,095	3,745	2.5	0.2	1.6	CI-HCO₃-Na
W72-1238	80-Jul-04	8.2	64	1,061	3,894	0.1	0.1	1.8	CI-HCO₃-Na
W73-1365	74-Oct-23	7.6	27	1,050	3,734	NA	NA	NA	CI-HCO₃-Na
	75-Jan-28	7.9	60	1,028	3,695	0.2	NA	NA	Cl-HCO₃-Na
	75-Jan-29	7.9	60	1,028	3,682	0.2	NA	NA	Cl-HCO₃-Na
	75-Jan-30	7.9	63	1,028	3,686	< 0.1	NA	NA	CI-HCO₃-Na
W73-1432	80-Jul-03	8.4	21	1,435	4,586	1.4	0.9	1.0	Cl-HCO₃-Na
	80-Jul-25	8.4	6	1,363	4,459	NA	NA	NA	Cl-HCO₃-Na
W73-1434	80-Jul-07	8.2	29	1,033	3,613	0.9	0.1	1.7	CI-НСОз-Na
	80-Jul-24	8.1	16	1,072	3,693	NA	NA	NA	Cl-HCO₃-Na
W73-1439	74-Oct-27	8.0	12	1,011	3,711	NA	NA	NA	CI-HCO₃-Na
	74-Oct-07	8.0	16	1,044	3,770	NA	NA	NA	CI-HCO₃-Na
	80-Jul-27	8.1	10	1,050	3,653	< 0.1	< 0.1	1.8	Cl-HCO₃-Na
W74-1510	80-Jul-07	8.2	33	1,083	3,706	0.7	0.6	1.9	Cl-HCO₃-Na
W74-1511	74-Oct-24	7.7	32	1,106	3,877	NA	NA	NA	CI-HCO₃-Na
	80-Jul-06	8.2	27	1,056	3,684	0.2	0.1	1.6	Cl-HCO₃-Na
W74-1512	74-Oct-27	8.0	21	1,296	3,639	NA	NA	NA	CI-HCO₃-Na
	74-Oct-27	8.0	13	1,167	3,672	NA	NA	NA	CI-HCO 3 -Na
W75-1750	75-Jan-26	8.2	16	1,061	3,511	NA	NA	NA	CI-HCO₃-Na
W75-1751	75-Feb-01	8.1	39	1,050	3,590	NA	NA	NA	CI-HCO ₃ -Na
	76-Jul-16	7.5	36.7	1,010	3,658	NA	NA	1.5	CI-HCO ₃ -Na
W75-1752	75-Jan-29	8.3	58	1,050	3,492	NA	NA	NA	CI-HCO ₃ -Na
W75-1753	75-Feb-02	8.1	52	1,072	3,693	NA	NA	NA	CI-HCO₃-Na
	80-Jul-06	8.2	30	1,117	3,617	0.1	0.1	1.8	CI-HCO ₃ -Na
W75-1754	80-Jul-05	8.1	45	1,061	3,715	0.1	0.1	1.8	CI-HCO 3 -Na

Cretaceous - Basal Aquifer

Table 8B

Groundwater Quality: Indicator Concentrations

Monitoring Station	Date of	рН	Sulphate	Chloride	Total Dissolved	Iron	Manganese	Fluoride	Hydrochemical Type
Station	Sampling				Solids				туре
	(y-m-d)	(units)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	
W80-5025	80-Mar-10	8.0	28	729	2,943	1.3	0.1	2.0	HCO₃-CI-Na
W80-5026	80-Mar-05	8.5	90	1,089	4,069	9.0	0.5	2.3	CI-HCO 3 -Na
	80-Jul-08	8.3	29	1,111	3907	0.2	0.1	1.6	CI-HCO ₃ -Na
W80-5043	80-Mar-20	8.0	8	639	3650	0.6	0.1	1.3	HCO₃-CI-Na
	80-Jul-15	8.4	16	693	4003	0.1	0.1	1.0	HCO3-CI-Na
	80-Jul-25	8.3	3	693	3973	0.1	0.1	1.2	HCO₃-CI-Na
W80-5053	80-Mar-20	8.0	11	517	2294	3.5	0.4	1.4	HCO₃-CI-Na
	80-Jul-16	8.3	12	335	2503	1.6	0.3	1.4	HCO3-CI-Na
	80-Jul-24	8.1	52	346	2599	0.8	0.3	1.5	HCO₃-CI-Na
W80-5054	80-Mar-11	7.9	22	385	2378	0.8	0.1	1.5	HCO₃-CI-Na
	80-Jul-24	8.2	5	424	2507	0.1	0.1	1.5	HCO₃-CI-Na
W80-5069	80-Mar-20	8.0	7	729	3393	0.7	0.1	1.3	HCO₃-CI-Na
	80-Jul-14	8.3	12	726	3425	0.3	0.1	NA	HCO₃-CI-Na
W80-5076	80-Mar-06	8.3	17	246	2080	5.5	0.3	1.2	HCO₃-CI-Na
	80-Jul-14	8.4	12	257	2021	0.8	0.2	NA	HCO₃-CI-Na
W80-5077	80-Mar-22	8.5	74	614	3255	3.0	0.2	1.3	HCO₃-CI-Na
	80-Jul-14	8.5	13	681	3164	0.3	0.1	1.2	HCO₃-CI-Na
W81-0043	81-Mar-04	8.2	7	1385	4516	0.07	0.08	NA	CI-HCO₃-Na
W81-0051	81-Mar-08	8.2	14	1229	4360	0.13	0.03	NA	CI-HCO₃-Na
W81-0053	81-Mar-07	8.1	6	648	3857	0.68	0.05	NA	HCO3-CI-Na
W81-0061	81-Mar-03	7.9	4	113	1407	0.16	0.14	NA	HCO₃-Na
	81-Jul-23	7.9	3	81	1430	NA	NA	NA	HCO₃-Na
W81-0068	81-Mar-18	7.9	12	2793	7407	30.3	1.06	NA	CI-HCO₃-Na
W81-0069	81-Mar-10	8.2	22	1206	3966	0.05	0.02	NA	CI-HCO₃-Na
W81-0072	81-Mar-08	8.2	8	2039	5942	2.77	0.18	NA	CI-HCO₃-Na
MW97-42	97-Apr-06	7.4	85.7	122	815	2.85	0.42	NA	CI-HCO₃-Na-Ca
	97-Apr-10	7.3	24.0	548	2380	NA	NA	NA	HCO3-CI-Na

Cretaceous - Basal Aquifer

NOTES:

1.

Iron and manganese represent total concentrations. High concentration of suspended solids is expected to contribute to elevated and high levels of these metals.

Table 8C

Groundwater Quality: Indicator Concentrations

Monitoring Date Sulphate Chloride Total pН Iron Manganese Fluoride Hydrochemical Station of Dissolved Туре Sampling Solids (TDS) (y-m-d) (units) (mg/L) Alsands Plant Site Area HCO3-Ca-Mg-Na 80-P-1 80-Jul-20 7.1 10 14 NA 542 NA NA **Alsands Tailings Pond Area** 80-TP-5 80-Jul-16 7 7.0 6 429 NA NA NA HCO3-Ca-Mg 80-TP-13 80-Jul-16 7.1 4 7 739 Trace NA NA HCO3-Ca-Mg 80-Aug-05 7.1 3 7 734 20.0 3.4 0.2 HCO3-Ca-Mg 80-TP-42 80-Aug-12 7.6 18 6 562 NA NA NA HCO3-Ca-Mg 80-TP-48 80-Aug-12 7.1 24 8 277 NA NA NA HCO3-Ca-Na-Mg 80-TP-58 80-Aug-07 6.6 7 7 385 NA NA NA HCO3-Ca-Mg-Na 80-TP-66 80-Jul-16 7.7 5 6 1,451 NA NA NA HCO3-Ca-Mg-Na 80-Aug-07 6 9 1,279 9.4 1.7 HCO3-Na-Ca-Mg 7.3 0.4 MW97-42 1997 7.4 81.3 122 799 3.32 0.5 NA HCO3-Na-Ca Mine Site Area W71-1119 1971 8.0 12 42 1,002 NA NA NA HCO3-Na HCO3-Na 1971 63 67 2,148 NA NA NA 8.3 W71-1182 8 7 846 NA NA HCO3-Na-Ca-Mg 1971 7.6 Trace 7 W72-1213 2 971 NA HCO3-Na-Ca 1971 8.0 Trace NA

Cretaceous - Intra Orebody and Near Contact with Quarternary Deposits

NOTES:

1.

Iron and manganese represent total concentrations. High concentration of suspended solids is expected to contribute to elevated and high levels of these metals.

Table 8D

Groundwater Quality: Indicator Concentrations *Quaternary Deposits*

Monitoring Station	Date of Sampling	рН	Sulphate	Chloride	Total Dissolved Solids (TDS)	Iron	Manganese	Fluoride	Hydrochemical Type
	(y-m-d)	(units)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	
Alsands Water	Intake Area	yy ang ang kang kang kang kang kang kang k				91041404992444444499944494494494494494	*****		
80-WI-2	80-Sep-15	7.5	42	134	1,328	3.9	4.0	NA	HCO₃-CI-Na-Ca
80-WI-4B	80-Sep-15	7.2	34	34	677	14.4	0.5	NA	HCO₃-Ca-Na-Mg
80-WI-5	80-Sep-15	7.7	119	34	1,729	0.2	0.6	NA	HCO₃-Na
Alsands Plant No hydrochem		available I	for this area						
Alsands Tailir	igs Pond Ar	ea							
80-TP-80	80-Aug-16	7.0	2	8	302	Trace	NA	NA	HCO₃-Ca-Mg
80-TP-84	80-Jul-21	6.9	24	6	321	Trace	NA	NA	HCO₃-Ca-Mg
80-TP-120	80-Jul-16	7.3	10	5	478	NA	NA	NA	HCO ₃-Ca-Mg
Mine Site Area	<u>a</u>								
80-MS-35	80-Aug-04	6.7	6	13	593	2.2	0.9	0.2	HCO₃-Ca-Mg-Na
80-MS-37	80-Aug-01	7.6	20	20	749	NA	NA	NA	HCO₃-Na-Ca-Mg
80-MS-104	80-Aug-01	6.9	44	23	367	NA	NA	NA	HCO₃-CI-SO₄-Ca-Na
80-MS-227	80-Jul-28	7.2	72	6	500	Trace	NA	NA	HCO₃-SO₄-Ca
80-MS-273	80-Jul-22	7.0	5	11	291	4.2	0.2	< 0.1	HCO₃-Na-Ca-Mg
80-MS-286	80-Jul-31	6.8	26	8	414	NA	NA	NA	HCO₃-Ca-Mg
MW97-1	97-Apr-04	7.3	48.8	2.4	464	23.2	2.08	NA	HCO₃-Ca-Mg
MW97-2	97-Apr-04	7.4	28.5	2.4	239	6.3	0.215	NA	HCO₃-Ca-Mg
MW97-3	97-Apr-04 97-Apr-10	6.8 6.9	13.3 7.1	1.6 0.9	307 416	8.98 NA	1.14 NA	NA NA	HCO ₃-Ca-Mg HCO ₃-Ca-Mg
MW97-4	97-Apr-04	7.2	13.3	24.5	539	8.23	0.516	NA	HCO₃-Ca-Mg
MW97-5	97-Apr-04	7.9	300	5	846	0.634	0.507	NA	HCO ₃-SO ₄-Na-Ca-Mg

NOTES:

1.

2.

Iron and manganese represent total concentrations. High concentration of suspended solids is expected to contribute to elevated and high levels of these metals.

Deeper piezometers, eg. 80-WI-5, 80-MS-37 may be completed partially in Quaternary and partially in Cretaceous sediments. This may result in higher TDS of groundwater.

Table 9A

Groundwater Quality: Selected Metals Concentrations (Total)

Devonian - Methy Formation

Monitoring Station	Date of	Aluminum	Boron	Barium	Cadmium	Chromium	Copper	Lead	Tin	Zinc	Silver	Mercury	Selenium	Arsenic	Uranium
	Sampling														
	(y-m-d)	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	μg/L	mg/L	mg/L	mg/L
W72-1240	81-Mar-14	1.35	2.80	0.05	<0.1	0.11	<0.05	<0.2	NA	0.22	<0.2	<0.01	<0.001	<0.001	0.05
W73-1404	81-Mar-13	See Note 3													
W73-1481	81-Mar-13	31.3	2.50	0.22	<0.1	0.12	0.01	0.08	NA	0.76	<0.2	<0.01	<0.001	0.022	0.10
W73-1489	81-Mar-08	0.95	0.82	0.018	<0.02	0.02	0.016	0.02	NA	0.42	0.04	<0.01	<0.001	<0.001	NA
	81-Mar-15	0.40	0.44	0.01	<0.01	0.01	0.01	<0.03	NA	0.11	<0.03	<0.01	<0.001	<0.001	NA
W75-1717	81-Mar-16	95.5	1.58	0.36	0.04	0.29	0.36	0.16	NA	2.81	0.06	<0.01	<0.001	0.080	NA
W80-5027	81-Mar-01	0.34	0.02	0.13	<0.02	<0.02	0.15	<0.04	NA	0.22	<0.04	<0.01	<0.001	<0.001	NA
W80-5039	81-Mar-06	18.7	36.8	3.4	<0.2	<0.2	<0.1	<0.4	NA	<0.4	<0.4	<0.01	<0.001	<0.001	0.05

NOTES:

1. All piezometers completed in the Methy Formation Carbonates were reconstructed in February and March 1981.

(EBA Consultants Ltd. 1981a).

2. The hydrochemical data for these piezometers, prior to reconstruction, are given in Alsands Energy Ltd. -Hydrogeology, Part 2 - Groundwater hydrogeology, Alsands Project, May 1981, Calgary, Alberta.

3. Groundwater sample collected from piezometer 1404 on March 13, 1981 had pH = 11.1, indicating contamination with cement filtrate.

Table 9B

Groundwater Quality: Selected Metals Concentrations (Total)

Cretaceous - Basal Aquifer

Monitoring	Date	Aluminum	Boron	Barium	Cadmium	Chromium	Copper	Lead	Tin	Zinc	Silver	Mercury	Selenium	Arsenic	Uranium
Station	of Sampling														
	(y-m-d)	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	μg/L	mg/L	mg/L	mg/L
													an an that a start second second		
W72-1238	80-Jul-04	<0.05	1.44	0.165	<0.01	<0.01	<0.005	<0.02	0.5	<0.02	<0.02	NA	NA	NA	NA
W73-1434	80-Jul-07	< 0.05	1.45	0.145	<0.01	<0.01	<0.005	<0.02	<0.1	<0.02	<0.02	0.05	<0.001	0.008	NA
W75-1753	80-Jul-06	<0.05	1.51	0.186	<0.01	<0.01	<0.005	<0.02	<0.1	<0.02	<0.02	NA	NA	NA	NA
W75-1754	80-Jul-05	<0.05	1.46	0.044	<0.01	<0.01	<0.005	<0.02	<0.1	<0.02	<0.02	NA	NA	NA	NA
W80-5026	80-Jul-18	0.06	1.48	0.236	<0.01	0.02	0.019	<0.02	<0.1	<0.02	<0.02	NA	NA	NA	NA
W80-5043	80-Jul-15	<0.05	3.34	0.305	<0.01	<0.01	0.009	0.07	0.2	<0.02	<0.02	<0.05	<0.001	<0.001	NA
W80-5053	80-Jul-16	<0.05	3.48	0.164	<0.01	<0.01	<0.005	0.02	0.2	0.5	<0.02	<0.05	<0.001	<0.001	NA
W80-5077	80-Jul-14	0.16	2.27	0.249	<0.01	<0.01	0.005	0.02	NA	0.3	<0.02	<0.05	<0.001	<0.001	NA
W81-0043	81-Feb-04	0.17	1.33	0.25	<0.01	<0.01	0.006	<0.02	NA	0.09	<0.02	<0.01	<0.001	<0.001	<0.02
W81-0051	81-Mar-08	0.15	2.24	0.33	<0.01	<0.01	<0.005	<0.02	NA	0.08	<0.02	<0.01	<0.001	<0.001	<0.02
W81-0053	81-Mar-07	0.38	3.00	0.40	<0.01	<0.01	<0.005	<0.02	NA	0.20	<0.02	<0.01	<0.001	<0.001	0.38
W81-0061	81-Mar-05	0.25	1.81	0.54	<0.01	<0.01	<0.005	<0.02	NA	0.07	<0.02	<0.01	<0.001	<0.001	<0.02
W81-0068	81-Mar-09	13.9	2.23	37.9	<0.01	<0.01	0.06	0.16	NA	0.68	<0.02	<0.01	<0.001	0.009	<0.02
W81-0069	81-Mar-10	0.10	1.40	0.31	<0.01	<0.01	<0.005	<0.02	NA	0.33	<0.02	<0.01	<0.001	<0.001	0.10
W81-0072	81-Mar-08	1.22	2.02	1.49	<0.01	<0.01	0.005	<0.02	NA	0.24	<0.02	<0.01	<0.001	<0.001	<0.02

NOTES:

Table 9C

Groundwater Quality: Selected Metals Concentrations (Total)

Cretaceous - Intra Orebody and Near Contact with Quaternary Deposits

Monitoring Station	Date of	Aluminum	Boron	Barium	Cadmium	Chromium	Copper	Lead	Tin	Zinc	Silver	Mercury	Selenium	Arsenic
	Sampling (v-m-d)	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	μg/L	mg/L	mg/L
Alsands Pla												<u>,,,,</u>		
Alsalius Fla	III SILE AIEA													
80-P-1	80-Aug-20	0.05	0.06	0.088	<0.01	<0.01	0.131	<0.02	<0.1	0.23	<0.02	NA	NA	NA
80-P-9	80-Aug-20	0.13	0.05	0.087	<0.01	<0.01	0.051	0.02	<0.1	0.16	<0.02	NA	NA	NA
Alsands Tail	lings Pond A	rea												
80-TP-5	80-Aug-18	0.26	0.02	0.249	<0.01	<0.01	0.106	<0.02	<0.1	0.12	<0.02	<0.05	0.001	0.003
80-TP-13	80-Aug-18	0.10	0.12	0.394	<0.01	<0.01	0.2	<0.02	0.1	0.19	<0.02	NA	NA	NA
80-TP-42	80-Aug-12	0.46	0.05	0.166	<0.01	<0.01	0.3	0.25	NA	0.12	[°] <0.02	<0.05	0.006	<0.001
80-TP-48	80-Aug-12	0.64	0.05	0.136	<0.01	<0.01	0.281	0.14	NA	0.21	<0.02	<0.05	0.006	<0.001
80-TP-66	80-Aug-07	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	<0.05	<0.001	0.002

NOTES: 1. NA denotes not available or not analysed.

ý

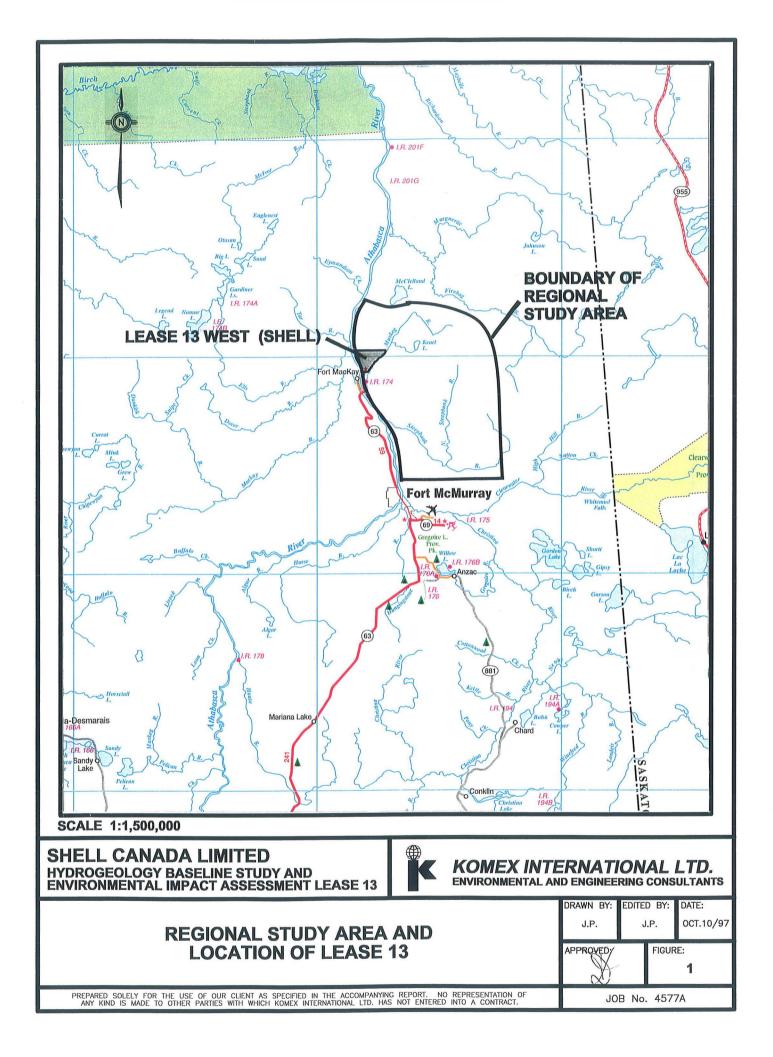
Table 9D

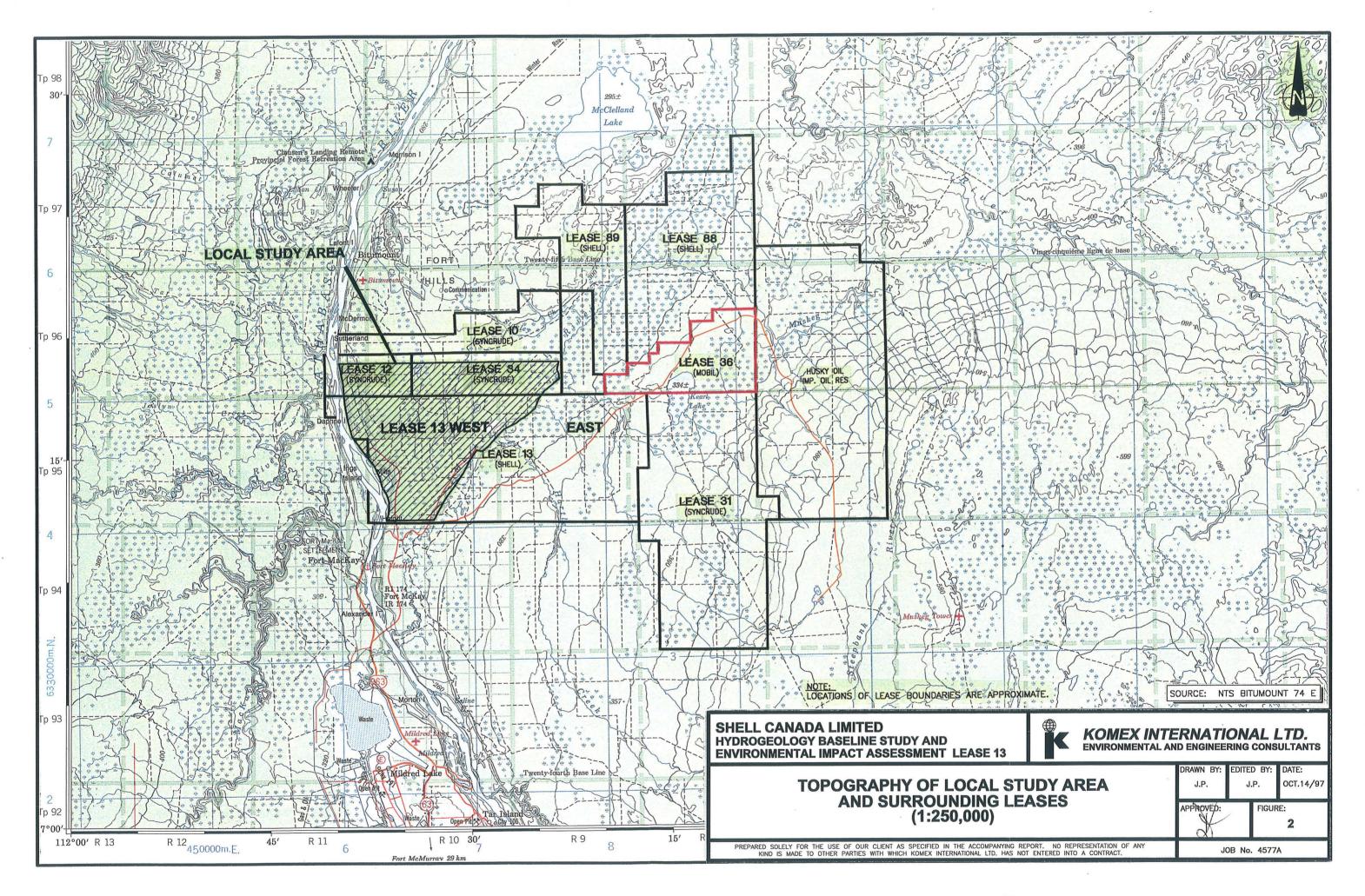
Groundwater Quality: Selected Metals Concentrations (Total)

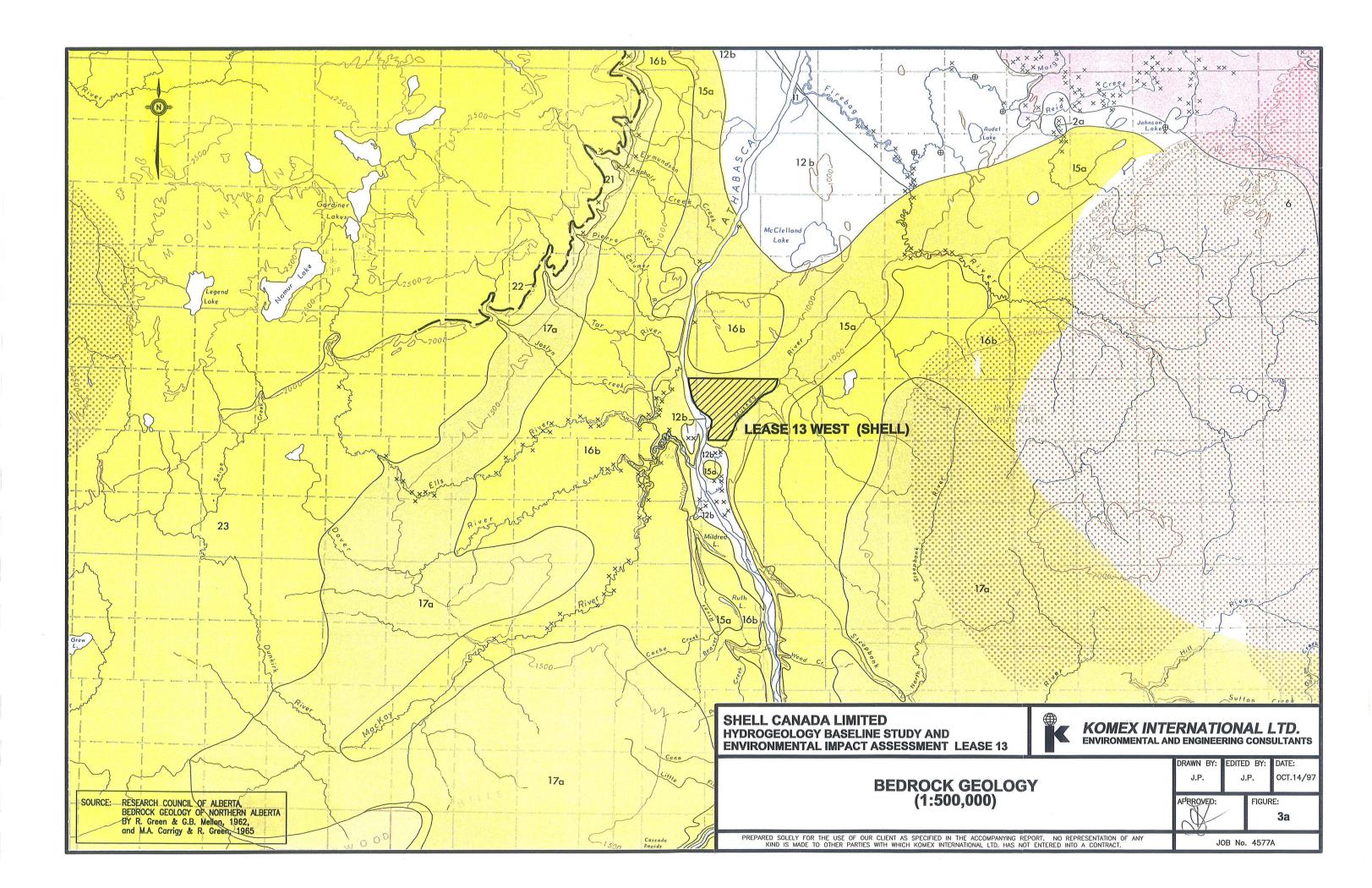
Quaternary Deposits

Monitoring Station	Date of	Aluminum	Boron	Barium	Cadmium	Chromium	Copper	Lead	Tin	Zinc	Silver	Mercury	Selenium	Arsenic
outon	Sampling													
	(y-m-d)	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	μg/L	mg/L	mg/L
Alsands Tailing	s Pond Area													
80-TP-80	80-Aug-06	0.17	0.02	0.071	<0.01	<0.01	0.156	<0.02	<0.1	0.18	<0.02	<0.05	<0.001	0.002
80-TP-84	80-Aug-21	6.3	0.04	0.276	<0.01	<0.01	0.678	0.04	<0.1	0.60	<0.02	<0.05	<0.001	<0.001
80-TP-120	80-Aug-16	0.42	0.02	0.161	<0.01	<0.01	0.139	<0.02	<0.1	0.18	<0.02	<0.05	<0.001	0.002
Mine Site Area														
80-MS-37	80-Sep-23	0.27	0.51	0.229	<0.01	<0.01	0.194	<0.02	NA	0.14	<0.02	<0.05	0.003	<0.001
80-MS-104	80-Aug-01	132	0.77	4.08	0.19	0.34	0.770	0.81	NA	1.13	<0.02	<0.05	0.023	0.001
80-MS-227	80-Jul-28	1.0	0.04	0.412	<0.01	<0.01	0.172	<0.02	<0.1	0.30	<0.02	NA	NA	NA
80-MS-286	80-Jul-31	0.27	0.51	0.276	<0.01	<0.01	0.194	<0.02	NA	0.14	<0.02	NA	NA	NA

NOTES: 1. NA denotes not available or not analysed.







LEGEND

CRETACEOUS

23

LABICHE FORMATION: dark grey shale and silty shale, ironstone partings and concretions; thin fish scale-bearing silty beds in lower part; marine

PELICAN FORMATION: fine-grained quartzose sandstone, silty and glauconitic in lower part; marine

JOLI FOU FORMATION: dark grey fossiliferous shale, silty interbeds in upper part; marine

17a

16b

20

19

GRAND RAPIDS FORMATION: fine-grained quartzose and feldspathic sandstone, laminated siltstone and silty shale; thin coaly beds; deltaic to marine

CLEARWATER FORMATION: dark grey fossiliferous silty shale, laminated siltstone, fine-grained cherty sandstone; glauconitic sandstone (WABIS-KAW MEMBER) near base; marine

15a

McMURRAY FORMATION: crossbedded quartzose sandstone and siltstone; oilimpregnated with grey silty shale interbeds in upper part; deltaic

DEVONIAN

12b

WATERWAYS FORMATION: grey and greenish-grey shale and argillaceous limestone units alternating with grey and greyish-brown fine-grained and clastic limestone units; marine

11

CARIBOU MEMBER, SLAVE POINT FORMATION: grey and brown fine- to medium-grained limestone and dolomitic limestone; minor shale, gypsum; marine

6

MIDDLE DEVONIAN (undivided) includes METHY FORMATION: brown and buff massive porous dolomite, brown to grey thin-bedded dolomite, dolomitic limestone, minor anhydrite and gypsum; McLEAN RIVER FORMATION and leached PRAIRIE EVAPORITE FORMATION: gypsum, anhydrite, grey-green silty and dolomitic shale, minor dolomite; marine to evaporitic

SOURCE: RESEARCH COUNCIL OF ALBERTA, BEDROCK GEOLOGY OF NORTHERN ALBERTA, BY R. Green & G.B. Mellon, 1962, and M.A. Carrigy & R. Green, 1965

PRECAMBRIAN



sedimentary rocks

Geological boundary
Outcrop location
Loose slab, probably from nearby unexposed bedro
Spring
Thick drift
Sinkhole area
Surface contour (contour interval 500 feet)
Highway
Road
Township boundary
Indian reservation
Railway
Park boundary

SHELL CANADA LIMITED HYDROGEOLOGY BASELINE STUDY AND **ENVIRONMENTAL IMPACT ASSESSMENT LEASE**

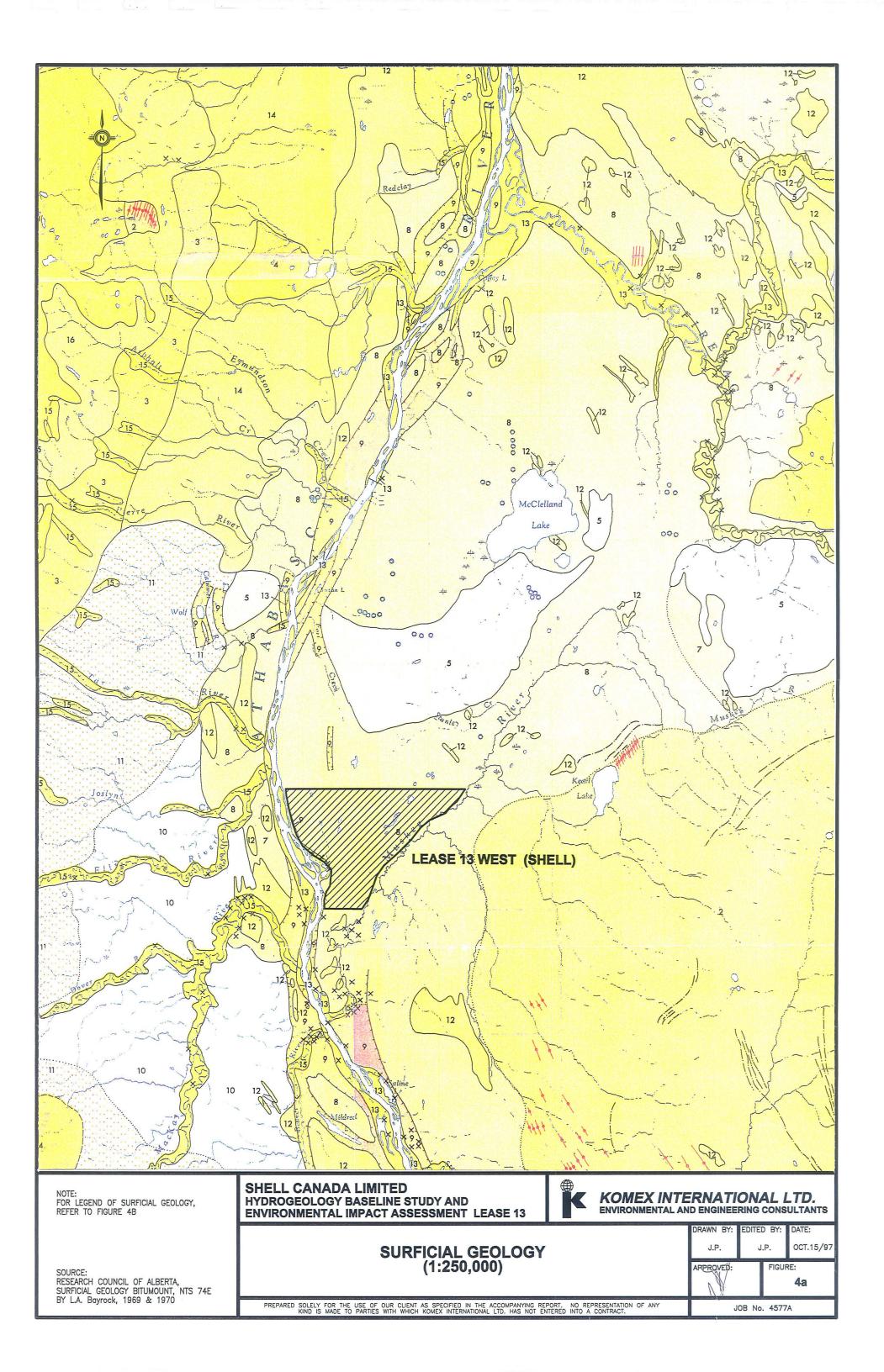
LEGEND FOR BEDROC

PREPARED SOLELY FOR THE USE OF OUR CLIENT AS SPECIFIED IN THE ACCOMP. KIND IS MADE TO OTHER PARTIES WITH WHICH KOMEX INTERNATIONAL LTD

UNDIVIDED GRANITIC PLUTONIC ROCKS: including biotite granite, porphyroblastic and porphyritic granites; some granite gneiss and meta-

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K GEOLOGY		DRAWN BY: J.P.	EDITED BY: J.P.		DATE: OCT.14/97	
		APRROVED:	APIRROVED:		FIGURE: 3b	
ANYING REP D. HAS NOT	ORT. NO REPF ENTERED INTO	RESENTATION OF ANY A CONTRACT.	JOB No. 4577A			



RECENT

EROSIONAL FEATURES



Slump: mixed glacial and bedrock materials; unstable slope

Gully, creek valley: thin colluvial cover on valley slopes; thin alluvial materials along streams

ALLUVIAL DEPOSITS



Alluvial fan: bedded silt, sand and clay; variable thickness, overlying glacial deposits

Stream alluvium: mainly sand along Athabasca River; silt, clay and sand along other streams

AEOLIAN DEPOSITS



Aeolian sand, dunes: medium-grained quartzitic sand in sheet and dune form; thick in dunes, 2 to 10 feet in sheet sand

PLEISTOCENE

GLACIOLACUSTRINE DEPOSITS



10

Mixed: bedded silt, clay and sand with pebbles and till-like layers; overlying till

Silt and clay: bedded silt and clay with minor sand; overlying till

GLACIOFLUVIAL DEPOSITS



8

Meltwater channel sediment: medium- to coarse-grained sand, overlying thin gravel and lag gravel containing many large boulders; in part, early Athabasca River sediments

Outwash sand: medium- to coarse-grained sand with pebbles and small gravel lenses; generally thin; surface level to gently undulating



Outwash sand and gravel: sand and gravel to gravel forming outwash plains; generally thick; surface level to gently undulating; some discontinuous terraces



Outwash sand and gravel overridden by glacier: fluted and drumlinized outwash of sand and gravel to gravel, with many large boulders; generally thick to very thick; topography undulating to rolling



Ice-contact deposits: sand and gravel to gravel, numerous very large boulders; rolling topography, individual hills reach heights of several hundred feet; includes kame moraine, eskers, moulin kames, crevasse fillings, and other related ice-contact glaciofluvial deposits; form end moraines of glacier advances

GLACIAL DEPOSITS



Hummocky moraine: till composed of mixed sand, silt and clay with gravel; generally thick; topography undulating to gently rolling



2

Colluviated ground moraine: till composed of sand, silt and clay, mantling colluviated steep slopes; partly bedded near surface; stable slope; generally thin

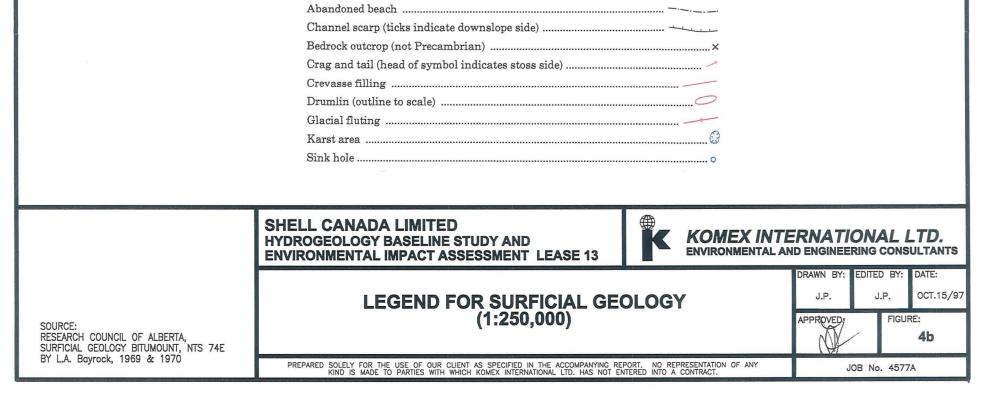
Ground moraine: till composed of sand, silt and clay with gravel, variable in thickness; topography level to undulating

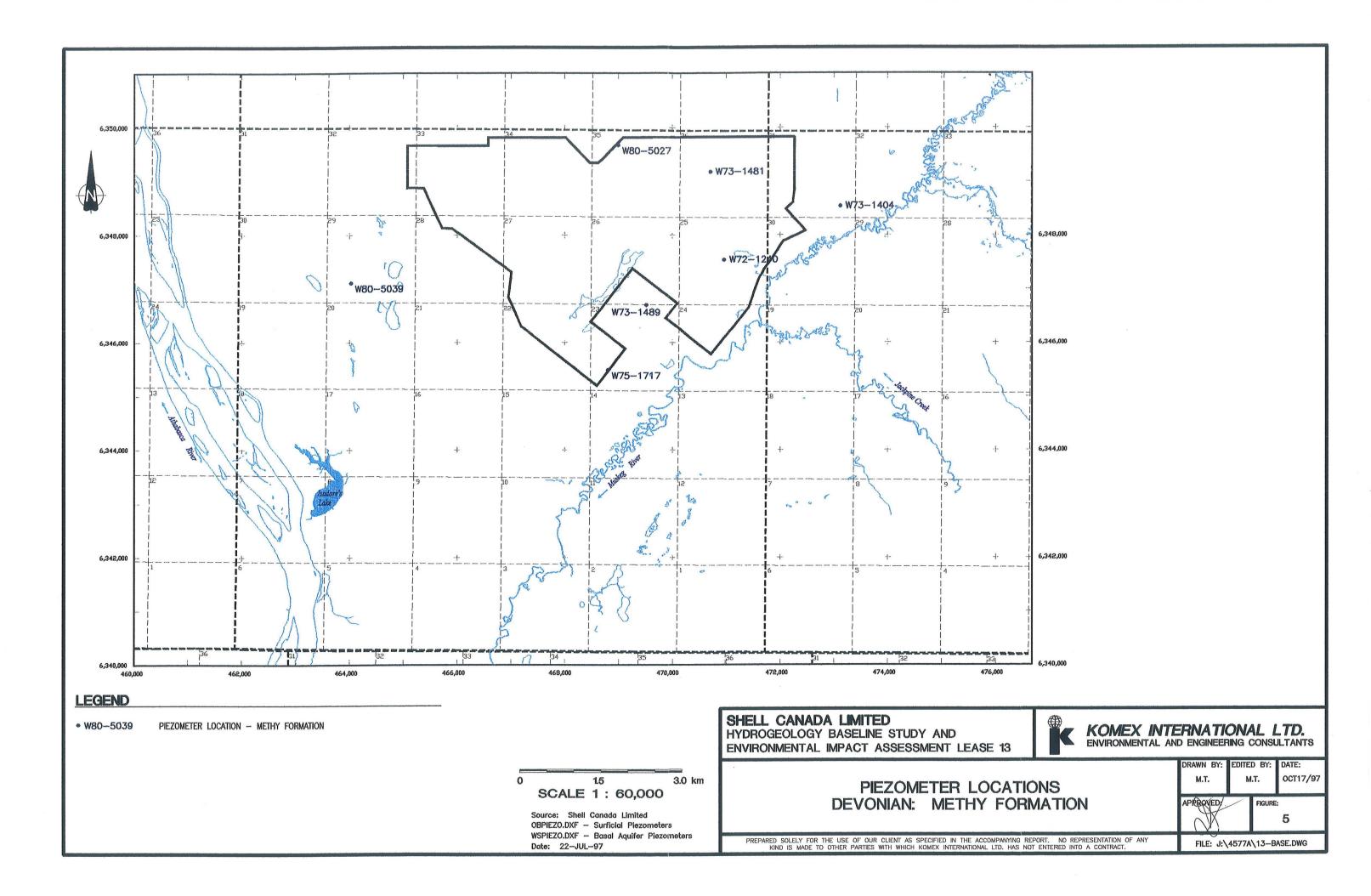
PRECAMBRIAN

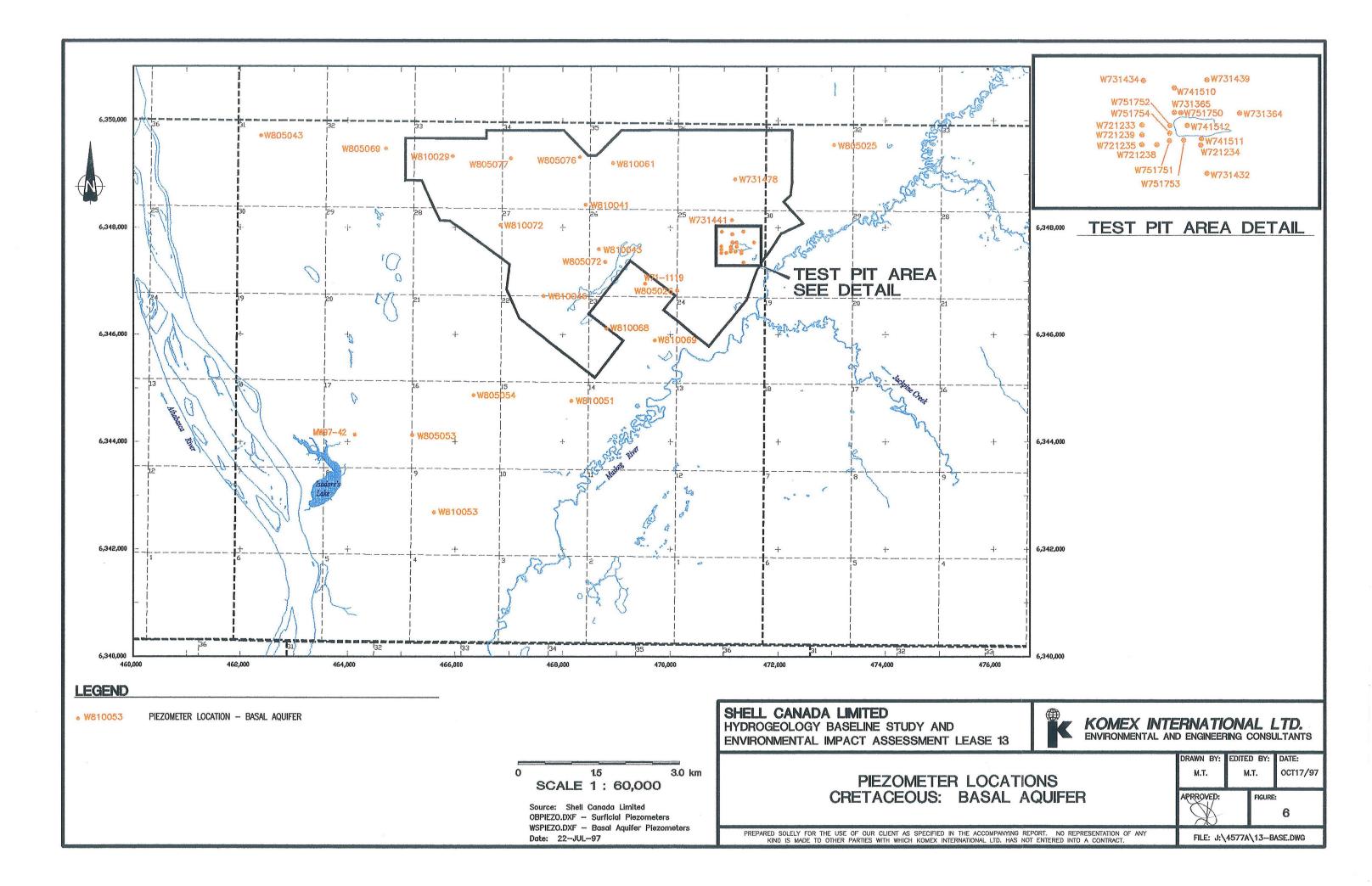


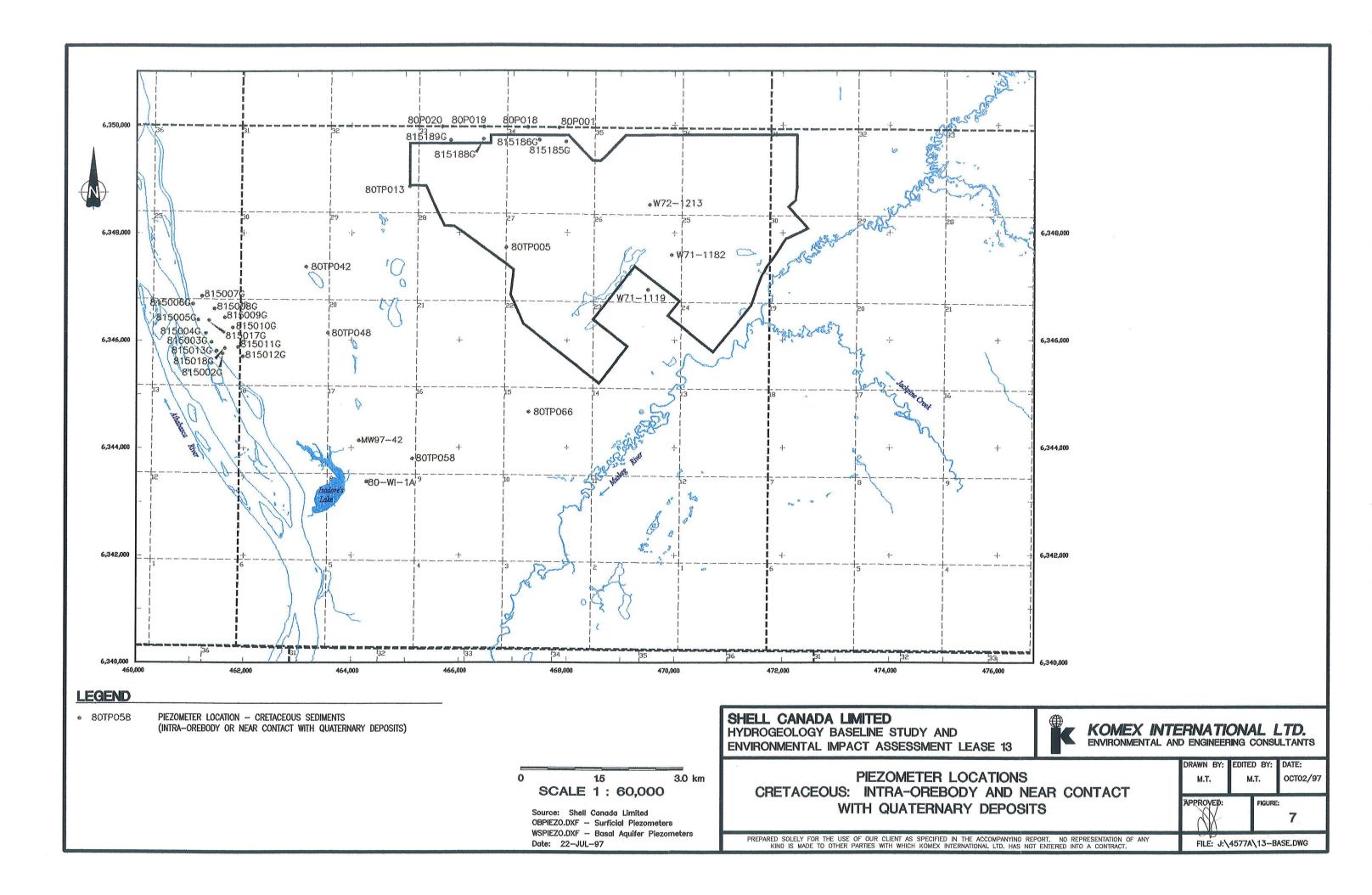
Granite, gneiss and metasedimentary rocks: outcrops form hills and knolls; generally bare with glacial deposits on the lee side of outcrops[†]

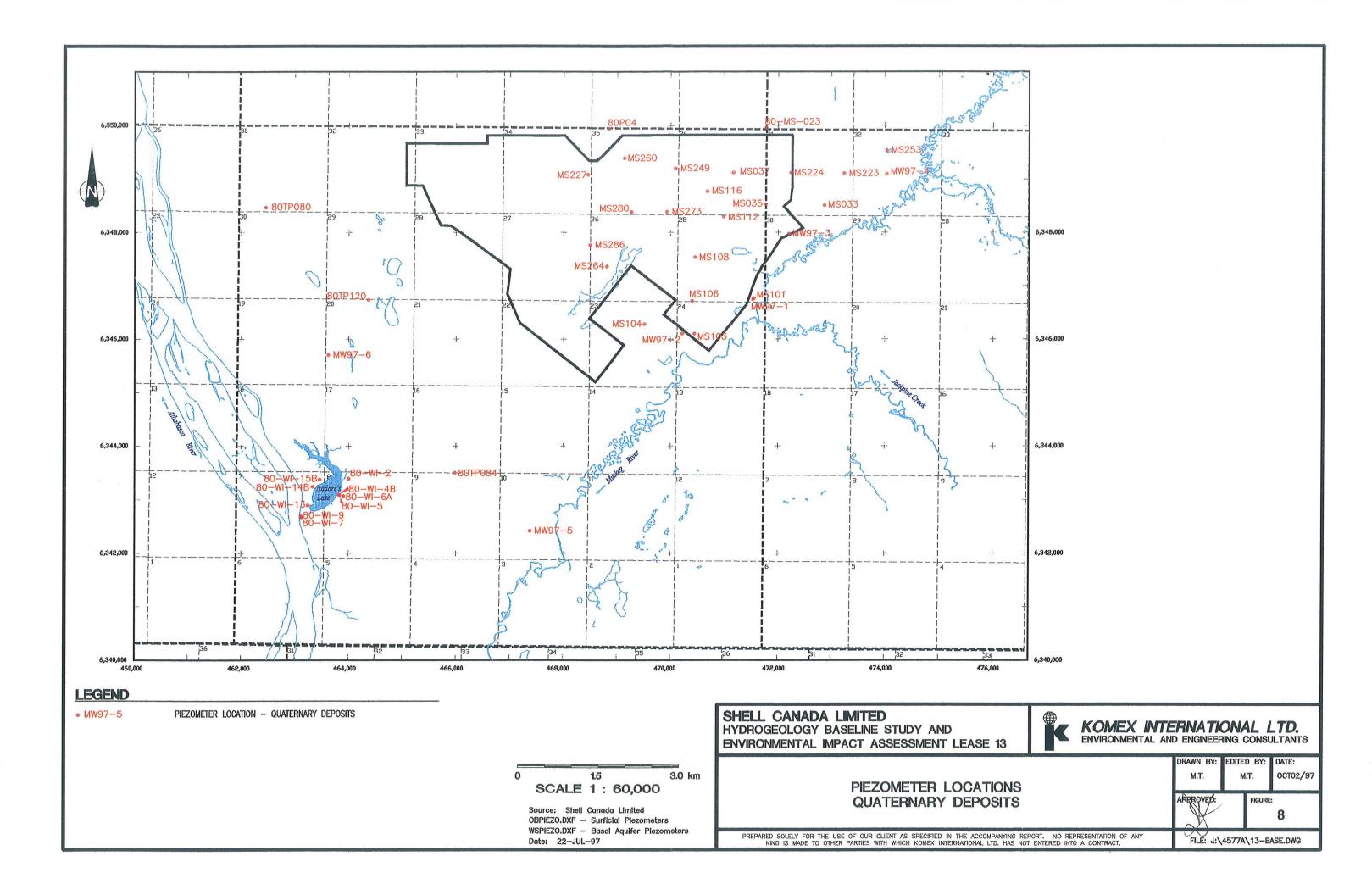
Geological boundary; defined, approximate, assumed

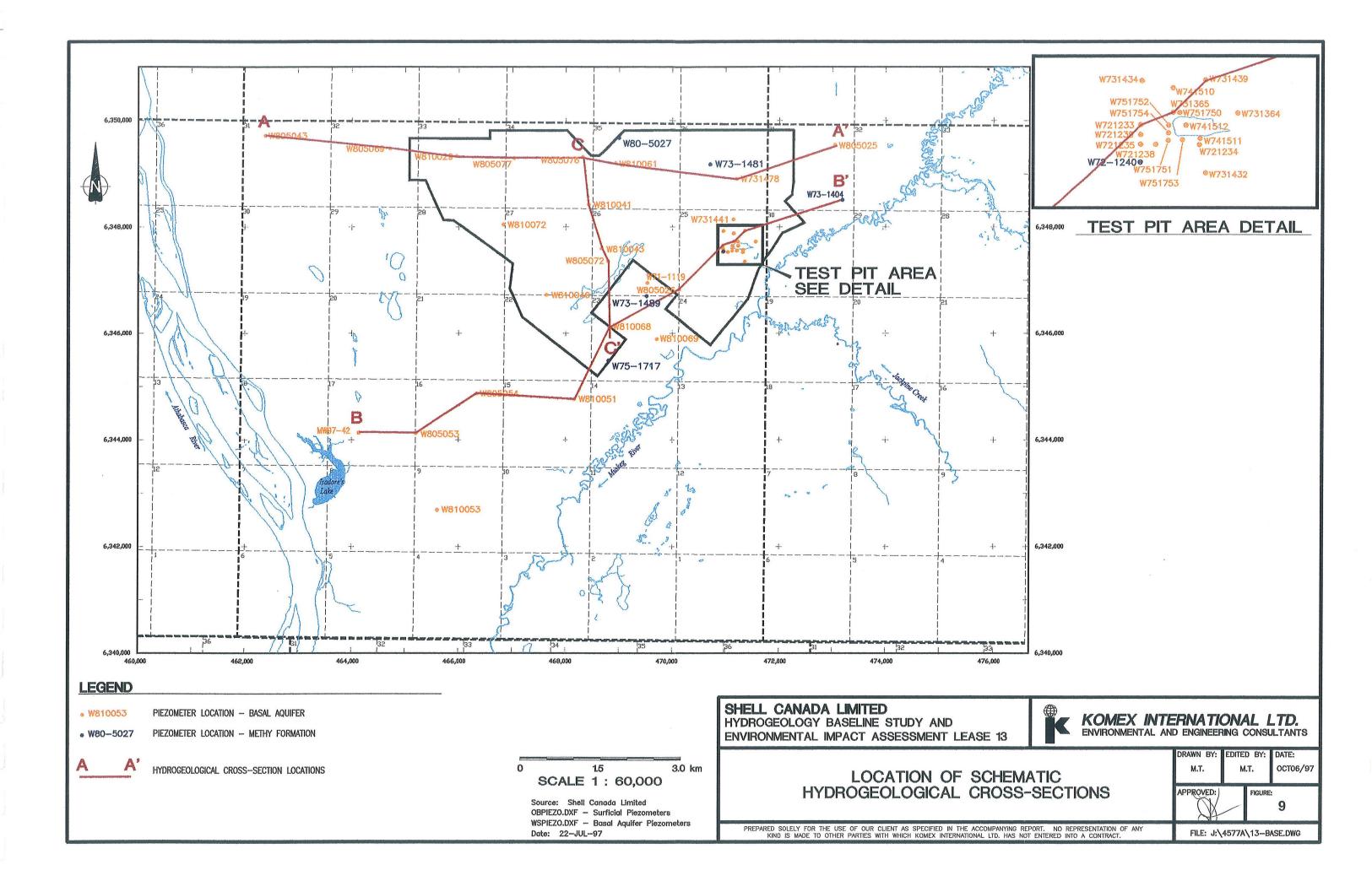


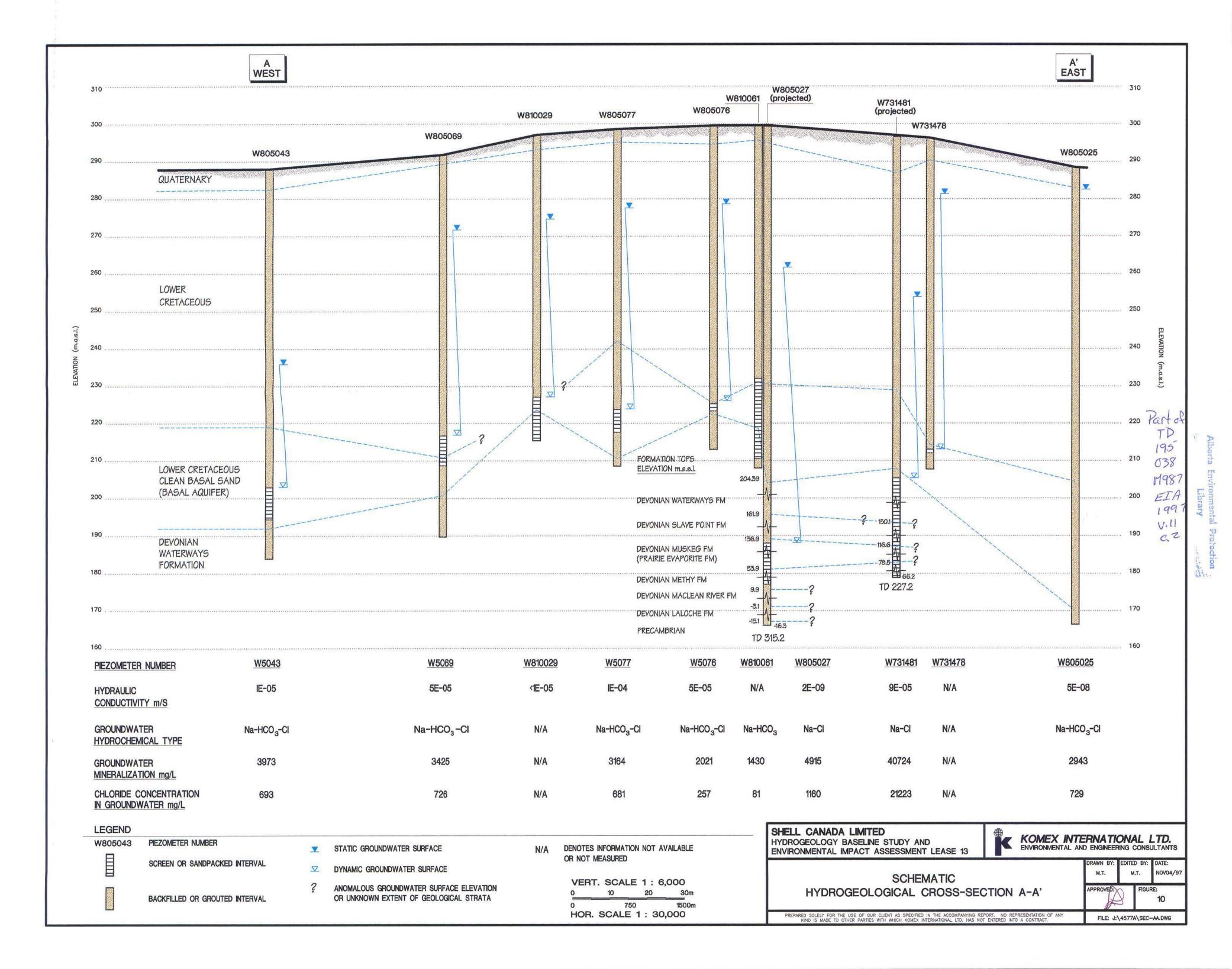


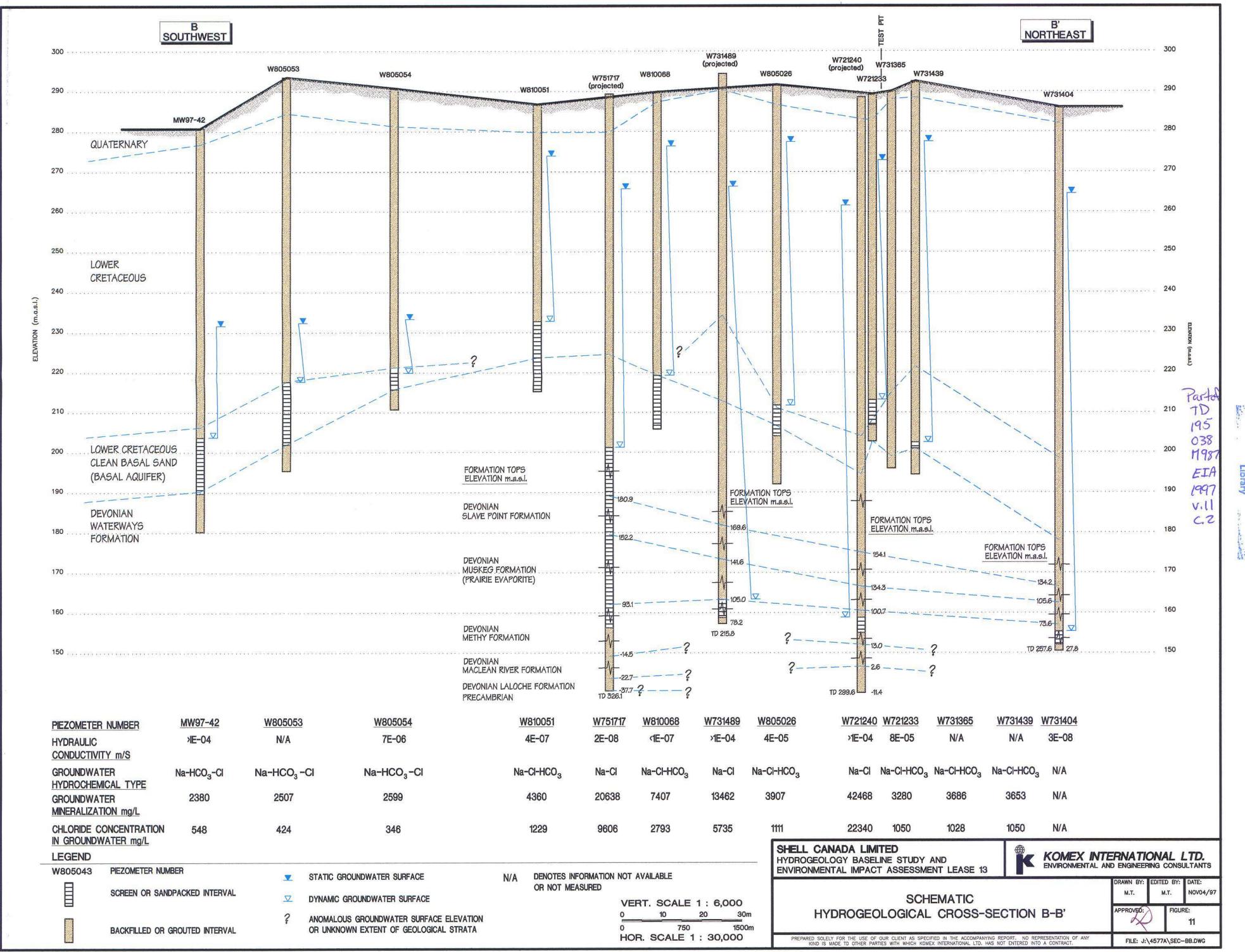




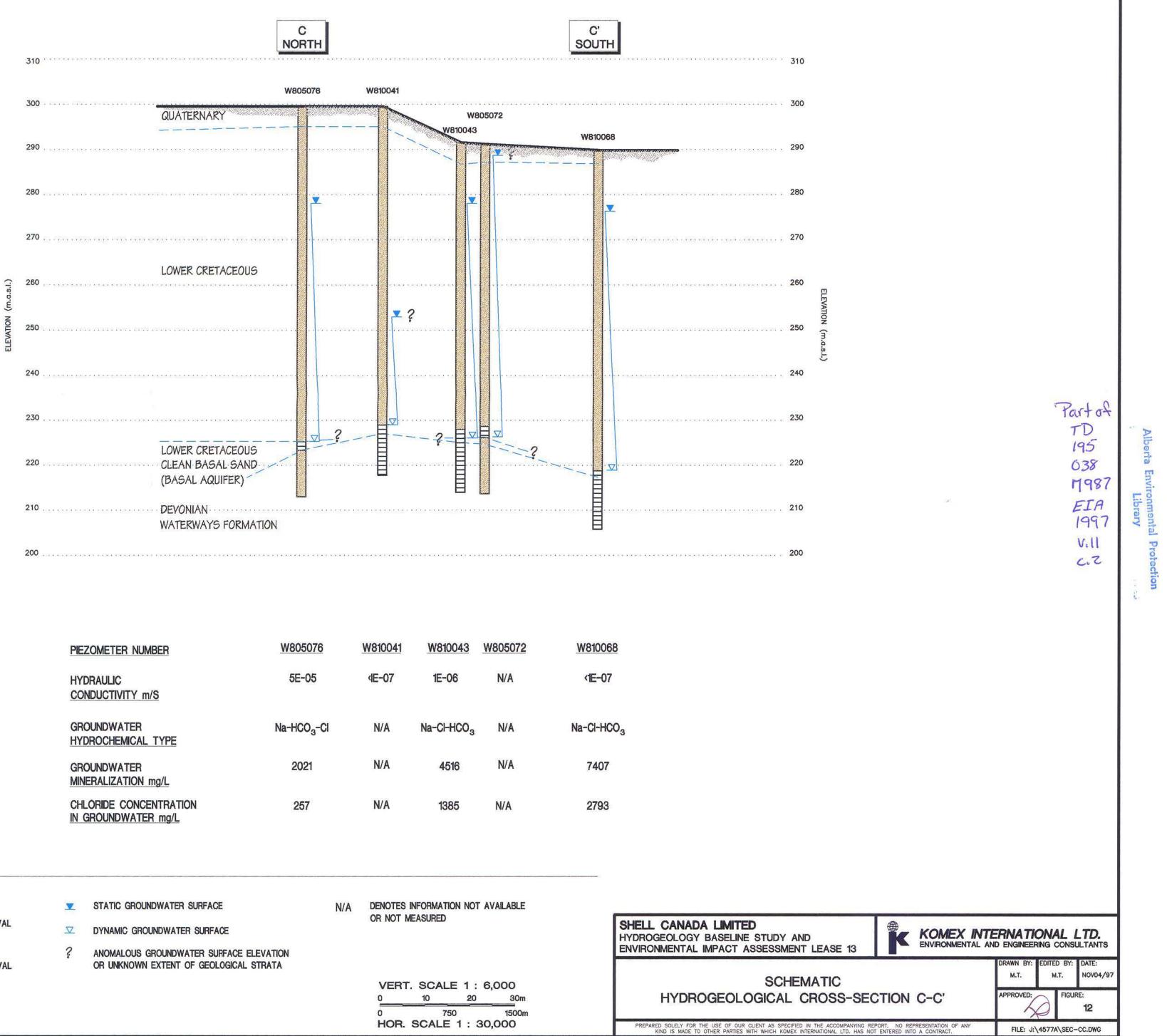








Library

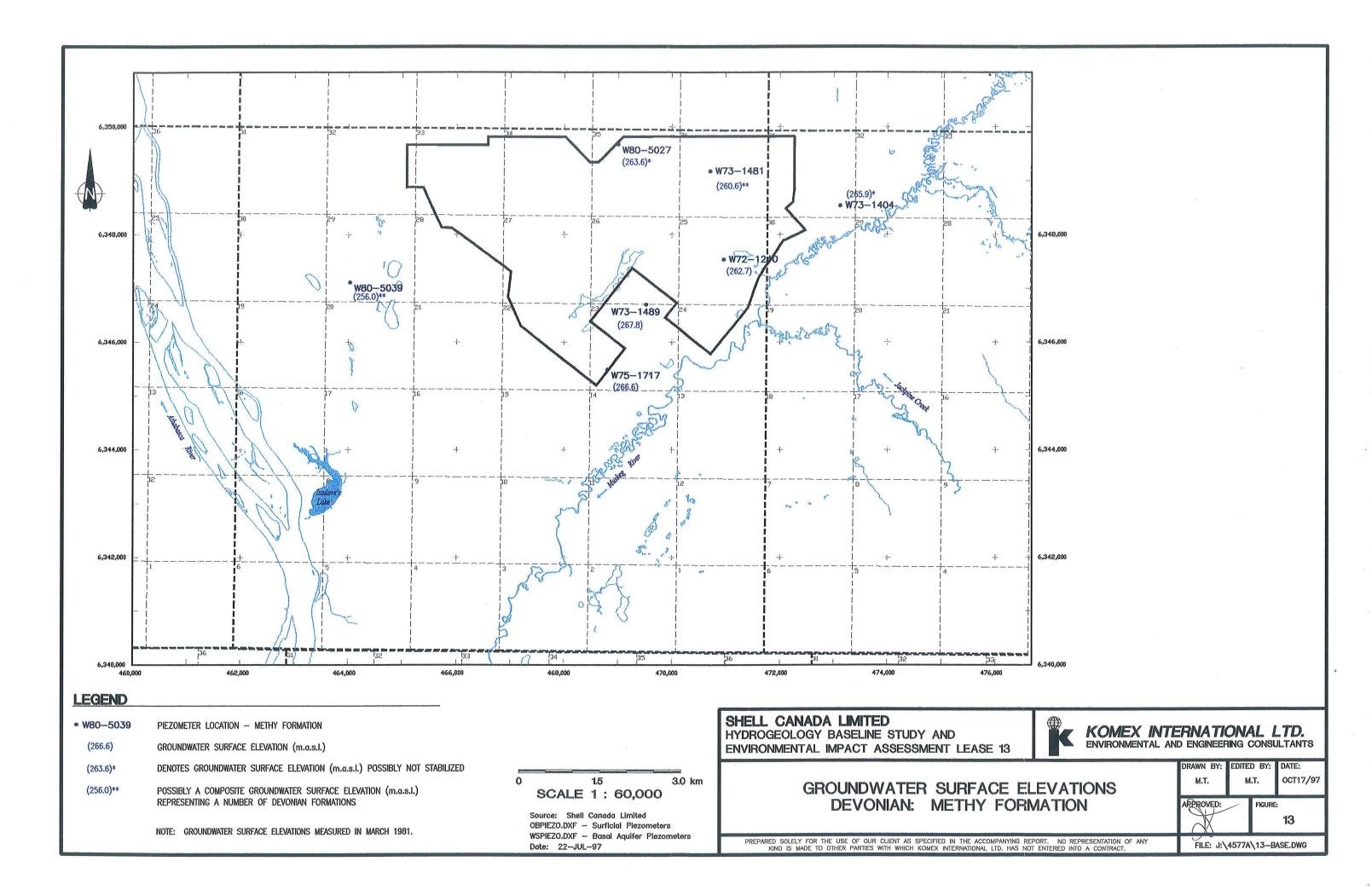


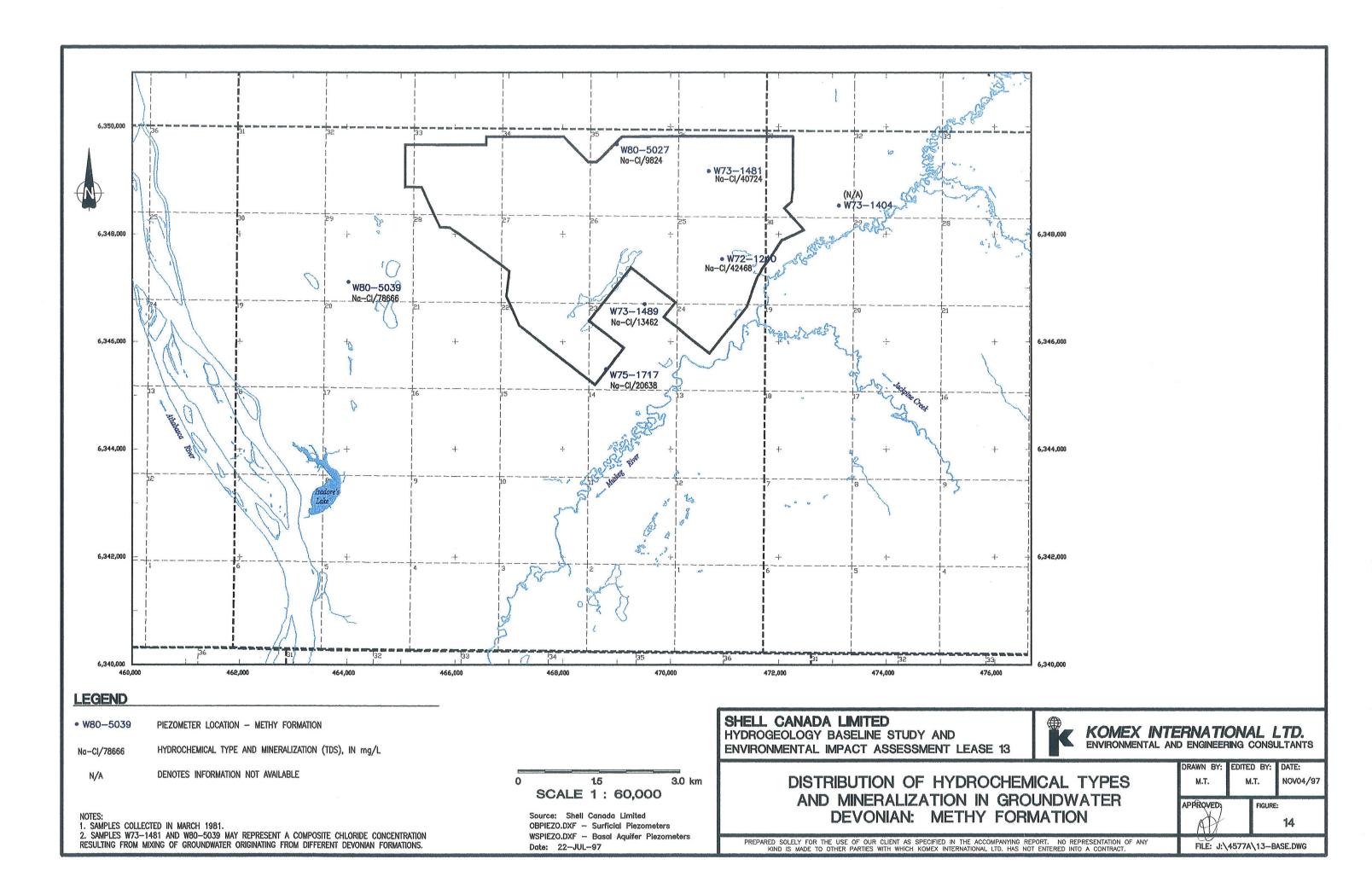
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HYDRAULIC CONDUCTIVITY m/S	5E-05	< E−07	1E-06	N/A
GROUNDWATER HYDROCHEMICAL TYPE	Na-HCO ₃ -Cl	N/A	Na-CI-HCO3	N/A
GROUNDWATER MINERALIZATION mg/L	2021	N/A	4516	N/A
CHLORIDE CONCENTRATION	257	N/A	1385	N/A

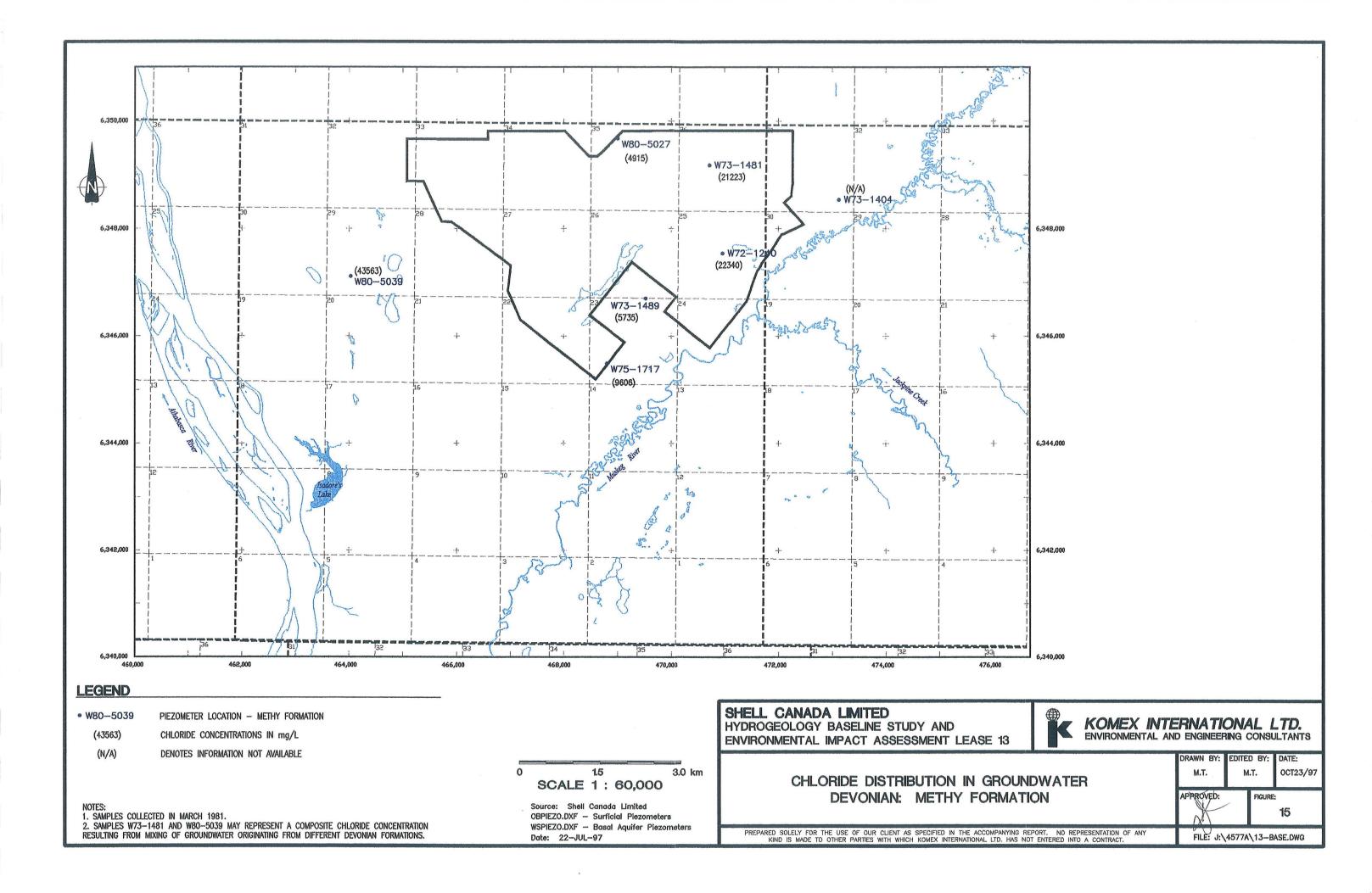
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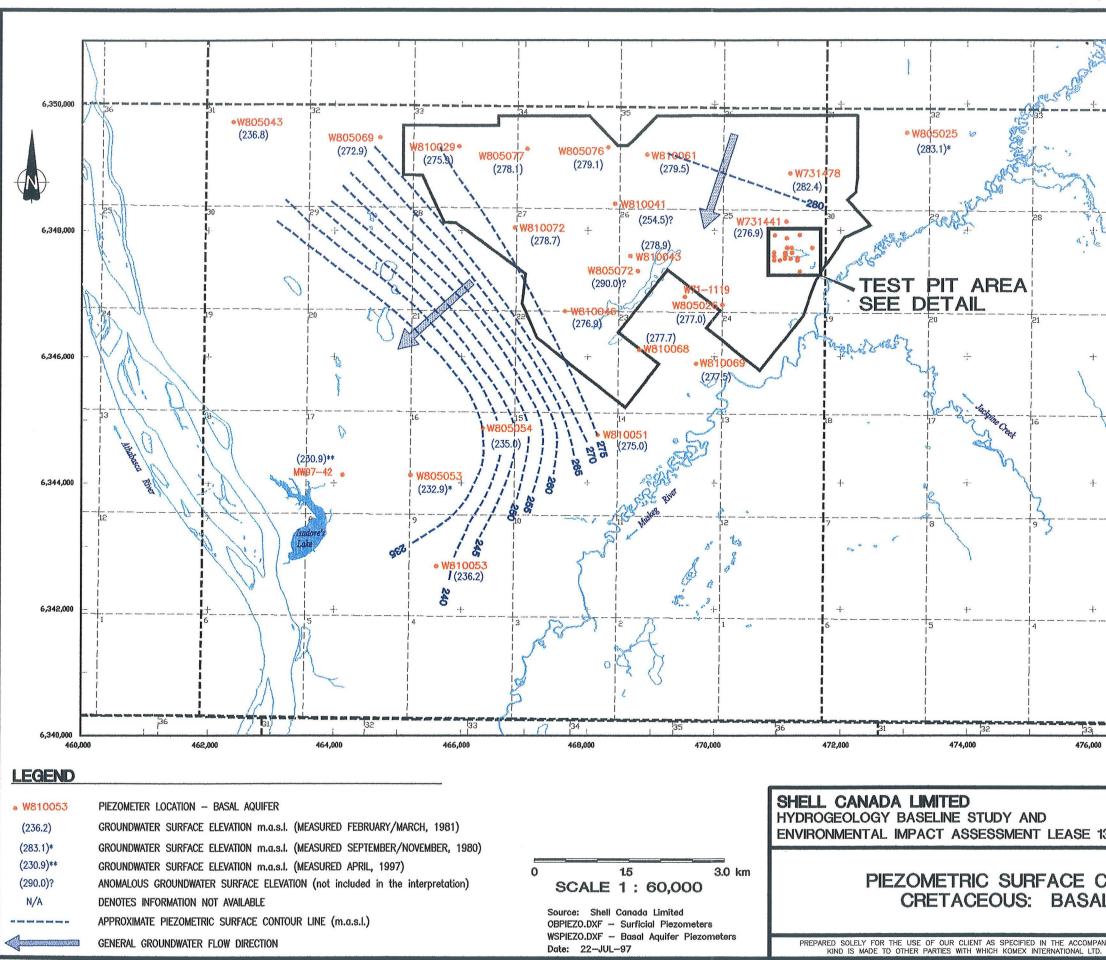
PIEZOMETER NUMBER W805043

SCREEN OR SANDPACKED INTERVAL

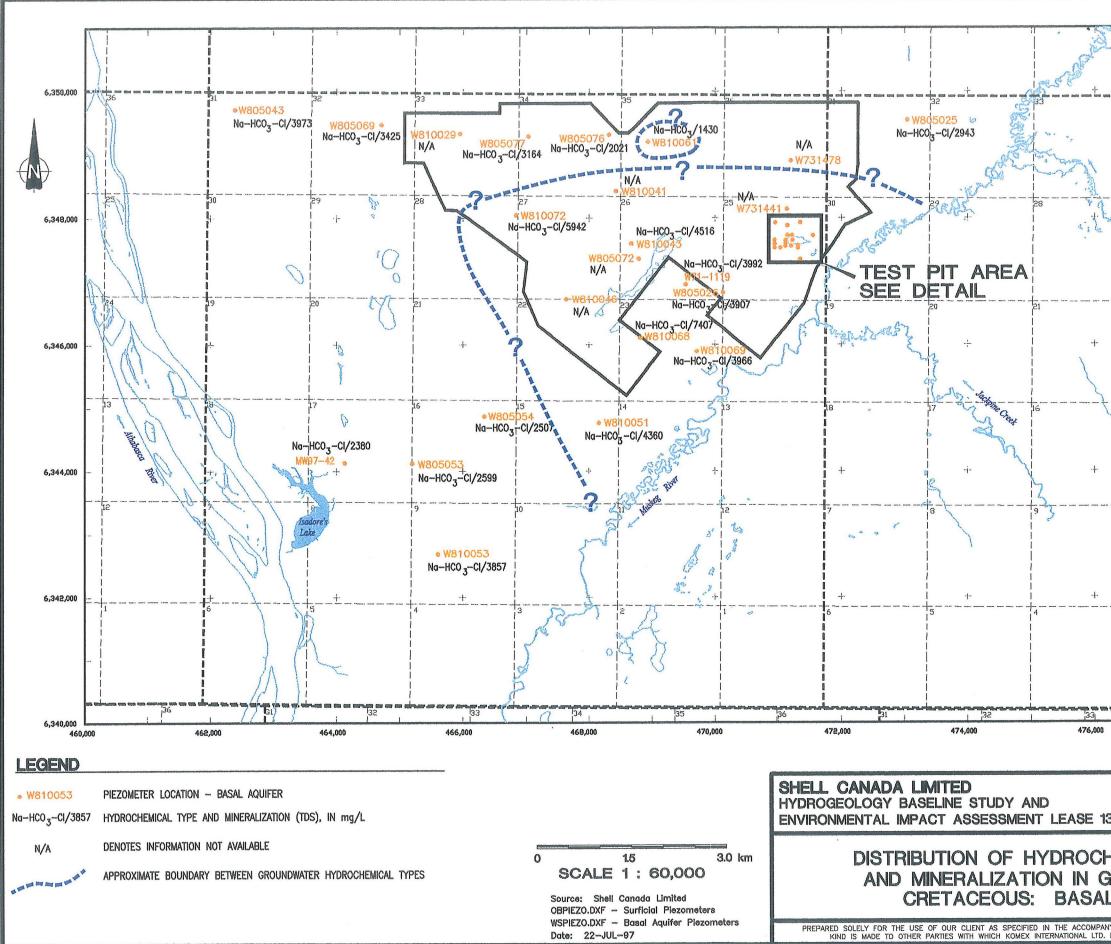




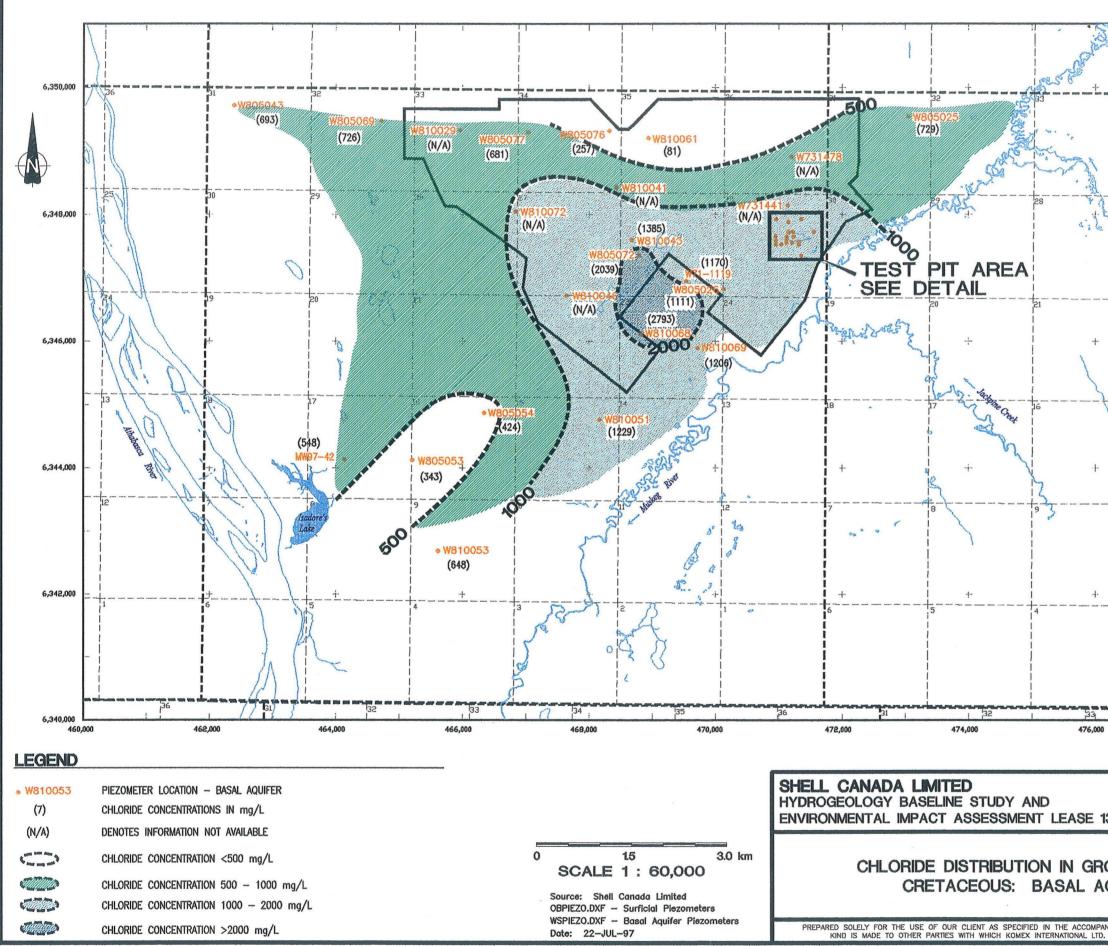




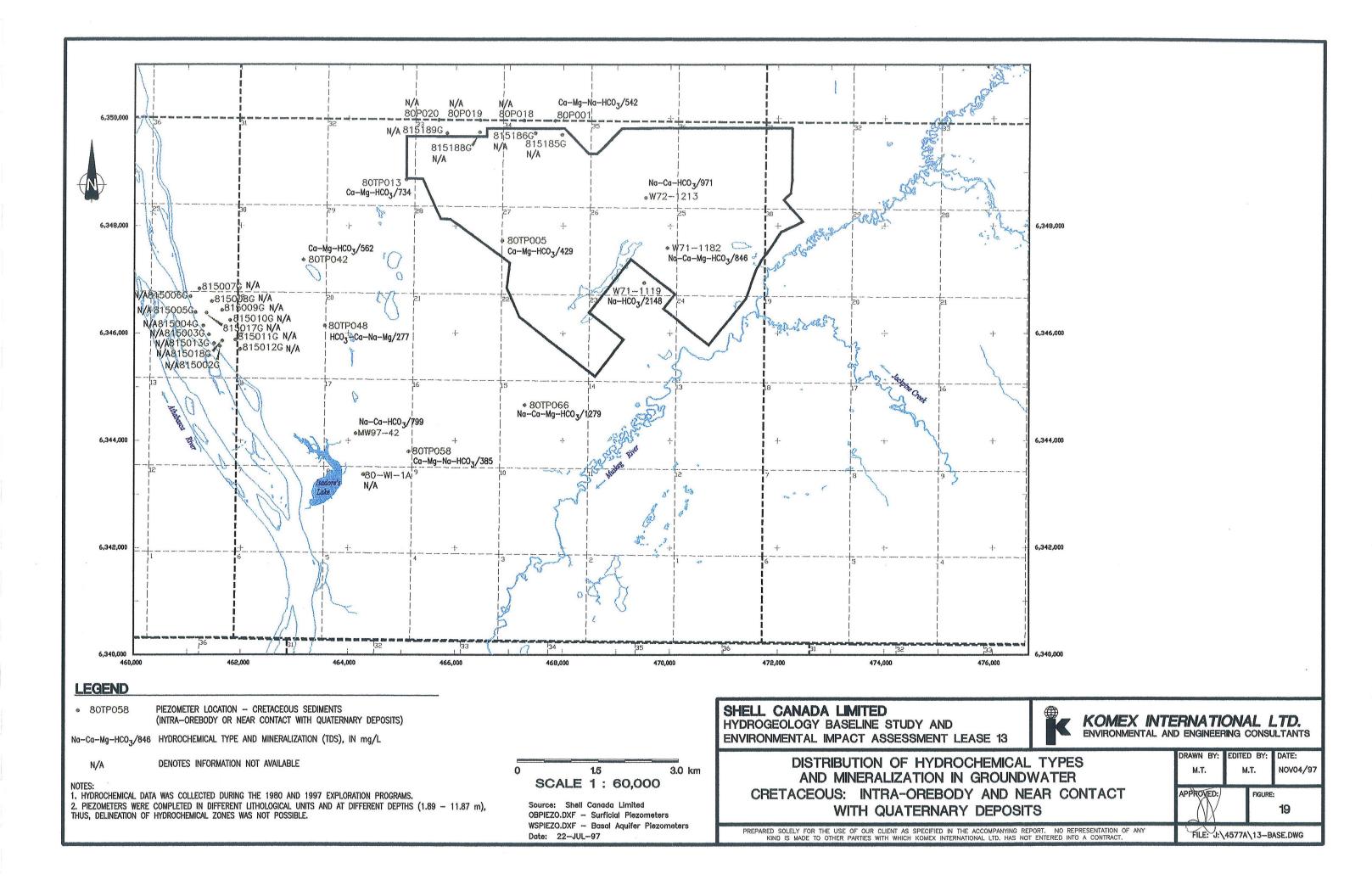
	(275.6)₩731434 @ (N/A)₩751755 (274.2) ₩751755 (273.3) ₩721233 @ (274.3) ₩721239 @ (274.0) ₩721235 @ (273.8)₩7212 (272.7)*₩7 (273.8)₩	[®] W741510 (27 ² W731365 (N/A [●] ●W751750 [●] W741512 [●] [®] W741 38 [●] [®] W741 [₩] [®] W7412 [®] [®] W7412 [№]) ®W731364 (278.9)		
Start a	6,348,000 TEST	PIT AREA	DETAIL		
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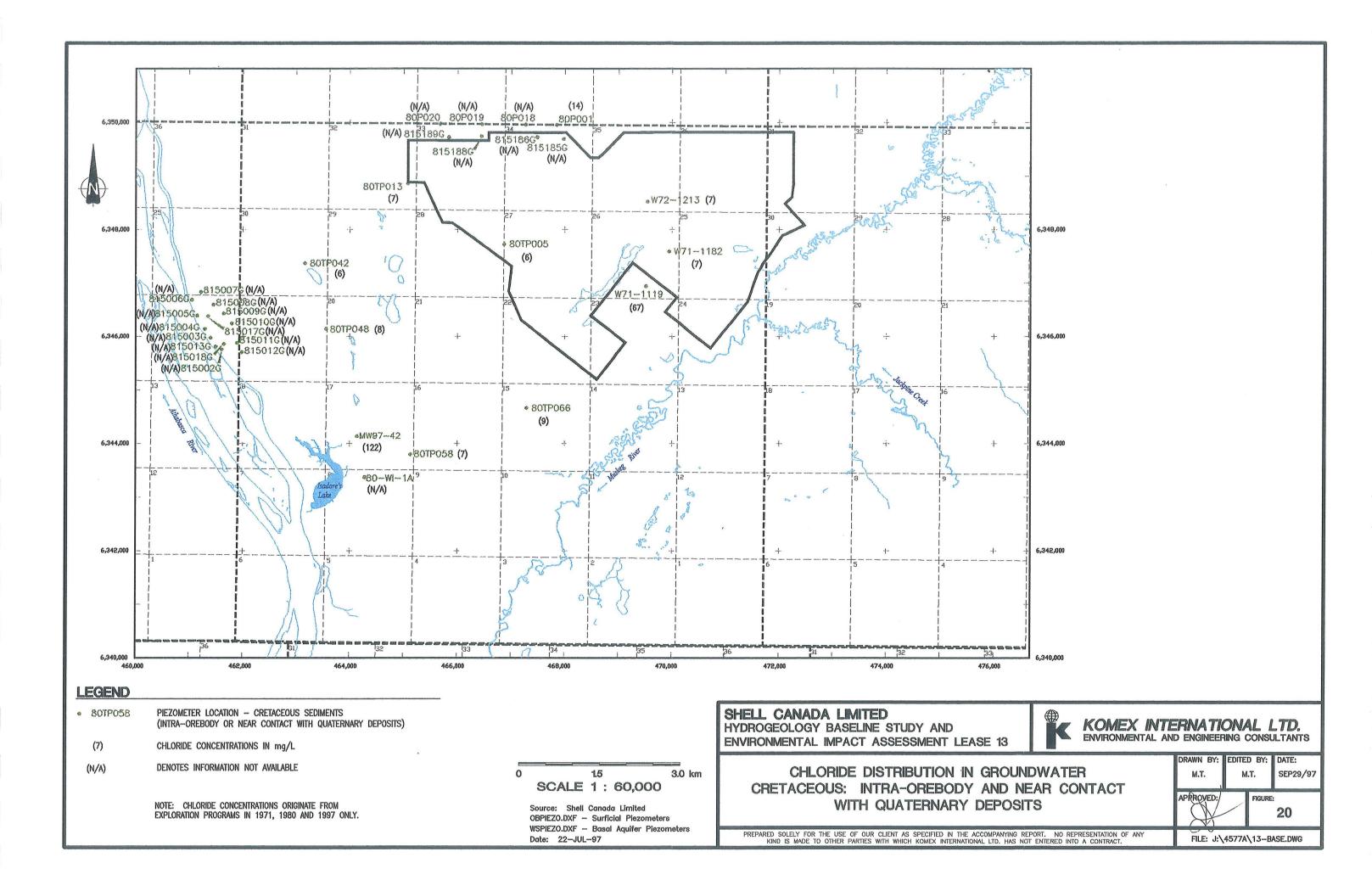


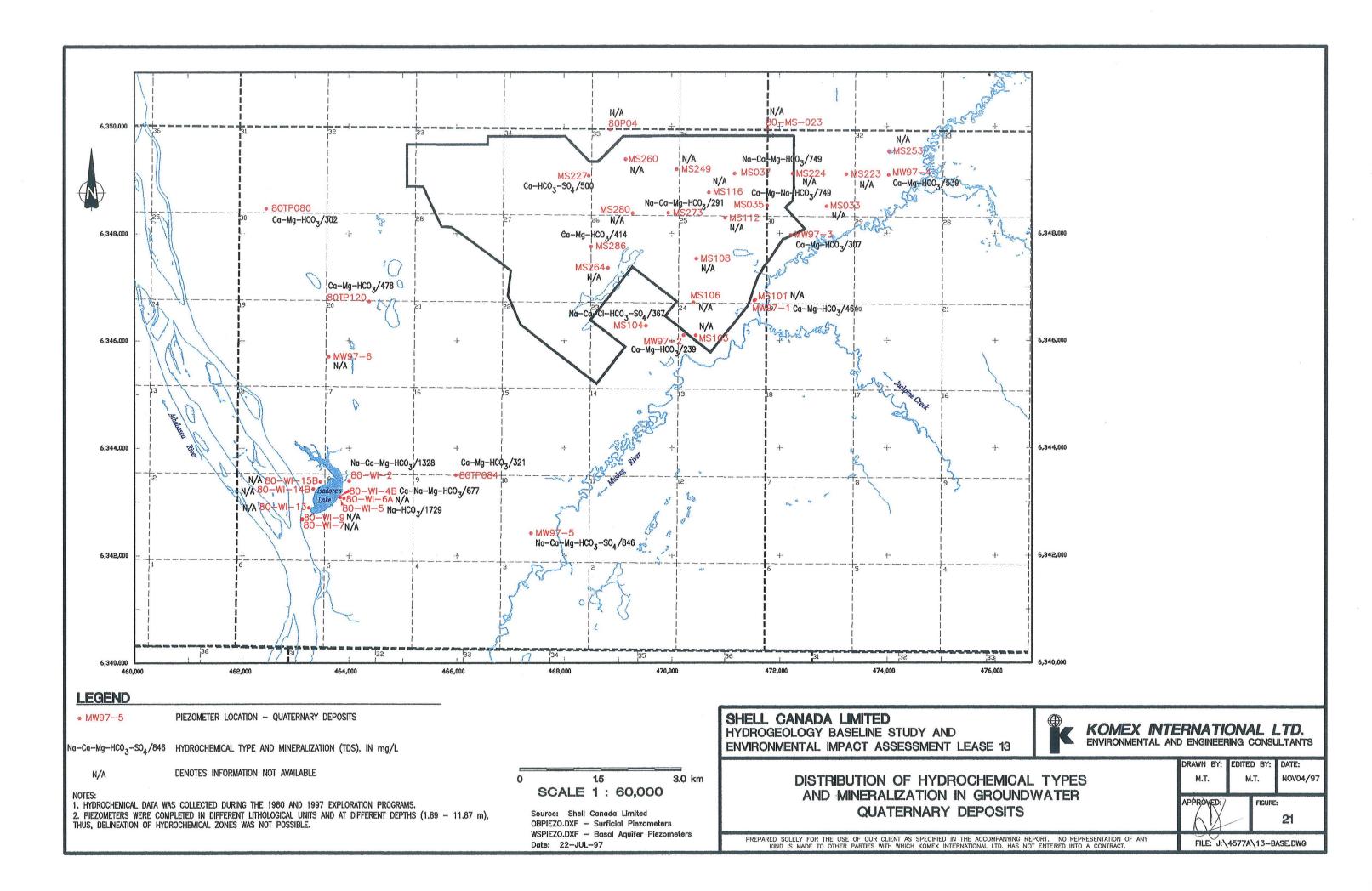
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	Na-CI-HC03/3492 W751752	● W751750 W741512 Na-C W741511 N W721234 N/A ● W731432	0 ₃ /3706 CI-HCO ₃ /3511 7 <mark>31364</mark> N/A XI-HCO ₃ /3672 Ia-CI-HCO ₃ /3877
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NYING REP	PORT. NO REPRESENTATION OF ANY T ENTERED INTO A CONTRACT.	FILE: J:\4577A	13-BASE.DWG



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	((1050) W751752	W741510 (10 731365 W751750 W741512 W741512 W7212	(1061) ************************************	34 (N/A)
		(1010), W75175.	7 @W73 3	1432 (1363))
inter i	6,348,000	TEST PIT	AREA	DET	<u>'AIL</u>
 		NOTE: CHLORIDE CONCENTR EXPLORATION PROGRAMS (19			
	6,346,000				
	6,344,000	· · · · ·			
	6 0 4 0 M				
+	6,342,000				
	6,340,000				
13	K	ENVIRONMENTAL AN	ERNATIC D ENGINEERI	DNAL L NG CONSU	.TD. Iltants
oun Quif	DUNDWATER DUNDWATER ARRROVED: FIGURE:				
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NYING RE	PORT. NO I	REPRESENTATION OF ANY NTO A CONTRACT,	FILE: J:\4	1577A\13-B	ASE.DWG







APPENDIX I

AEP WELL RECORDS FOR TOWNSHIPS 94-96, RANGES 9-10, W4M

(ARCHIVAL DATA FROM THE GROUNDWATER INFORMATION CENTRE -ALBERTA ENVIRONMENTAL PROTECTION)

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ALBERTA ENVIRONMENTAL PROTECTION

COMPUTER GENERATED WATER WELL DRILLER'S REPORT FORM WELLID. 233856 THIS DATA MAY NOT BE FULLY CHECKED; THE PROVINCE DISCLAIMS ALL RESPONSIBILITY FOR ITS ACCURACY: Page 1 of 1

CONTRACTOR:		WELL OWNER:	WEL	L LOCAT	ION:	rcs. (00
NAME UNINOWN DRILL	DP	NAMPA SHELLAPW-J	- OR LS	SEC	TWP	RGE	W. MEH
			10	24	095	09	W4
ADDRESS:		ADDRESS		UN VERIFIC	ATTON M	l	
			LOCATI	UN IN QUAL	TER	- TOMOR	•
LICENCE NO.1 JOI	RNEYMAN NO .:	POSTAL CODE					
PORMATION LOG DI		ULLING METHOD: UNKNOWN	WELL ELE	BLOCI v. 1053.51	Foot No	LAN: w obtain: Sl	RVEY-TRA
Ground Les	TT TT	PE OF WORE: NEW WELL		TION TE	T:		
		OWING WELLNO RATE:	TEST DA		Water 1		t TIMPs to Water ng Rocovery
		s present: No OIL present: No Te of anandonment:	Time in Min:Sec	Level Durin	Pamping	Level Dari	ag Rocovery
f	MA	TREIAL USED:					
	<i>FK</i>	OPOSED USE: OBSERVATION	J				<u> </u>
		WELL COMPLETION DATA:	 				
		VELL FINISUL SCREEN & OPEN HOLE					
	—— т	OTAL HOLE DEPTH: 103 Feet]		
·	c	ASING TYPE UNKNOWN					
1		IZE OD1 8.63 Ineb WALL TILICKNESS 0.264 Inch				·····	NINILLILL
		OTTOM AT: 52 Feet					
		FORATED CASING/LINER: VPE:		<u> </u>			
		12E OD: loch					
	W	VALL THICKNESS: Inch					
	-	OP AT: Ø Feet BOTTOM AT: Feet					
	P	ERFORATED FROM: Feet TO: Feet Feet TO: Feet					
		Feet TO: Feet			ł		
	S	IZE OF PERFORATIONS: Lich X Lich					
	B	IOW PERFORATED:					
		L TYPE:					
		NTERVAL TOP: 0 Feet TO: Feet					
		PHYSICAL LOG TAKEN; AINED ON FILE:					
	803	JEIENia					
	1	ATERIAL STAINLESS STEEL					·······
		12E ID (CLEAR): Incb SLOT STZE Incb NTERVAL TOP: 52 Post TO: 73 Post					
	¹	Foct TO: 73 Feet					
	r	NETALLATION METHOD: ATTACHED TO RISER	├				
		OP FITTINGS, RISER PIPE	WATER I	EMOVAL S	ATEDURI	NG TEST:	Gal/Min
		OTTOM FITTINGS: TAIL PIPE	TEST DU			o Wre	Minutoe
		r type: SAND rain size: amount:	DEPTH O	F PUMP/DB			Feel Feel
	V		NON-PUN	PINGOTAJ RAWDOWN	TC) WATE		VEE
		ITLESS ADAPTER TYPE	RECOMM	ENDED PU	MPING RA		Gal/Min
	D	ROP PIPE TYPE: LENGTH: Feet DIAMETER: Incb	TYPE OF	ENDED PU PUMP INST			Fact
ATE WORK STARTE		DIFITIONAL FUMP INFORMATION: COMMENTS:	MODEL			EL.P.,	
ATE WORK COMPLA		(Maximum of 9 lines printed)					
ATB DATA RECEIVI		•					
DDITIONAL TEST AND/O							
HEMISTRIES TAKENN TELL OWNER'S ANTICIP		OCUMENTS HELD: 9 IMENTS PER DAY:					
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Shell A	0W2-2		11J 483 MUNE	∃≮₽-ЭJ∠∠	
Lab. No	983	CHEMICAL WA	TER ANALYSIS REQUEST	http://www.weekanon.com/doi/10/00/00/00/00/00/00/00/00/00/00/00/00/	
	Sept. 21184	ALCOUNT AND AND	IRU MINDENG VERNESI		s analysis will
Project Code No		P	LEASE PRINT FIRMLY	dau	tribute to a resource a bank and be ilable to the public.
History					
Location of Sample		/			
4.1	<u>OSOW</u>	N		·	
	(NAM	E)	(STREET)	(CITY	, TOWN, VILLAGE)
•••		- 1	(POSTAL CODE)		TELEPHONE)
NB" L	ocation <u>LSD</u> 10	% Section	. Township	1 0	Meridia
Source of Sample:			•••••••••••••••••••••••••••••••••••••••		*******
	•	GOUT, WELL TAP, ETC.)	feet, Depth to Water Le		
					nøter5,184
			(DRILLED, DUG, SCREEN, SETT	LING ETC.)	·····
Submitted by:	Yeh-1110 m	Chae-		Phone	427-6231
• • •		(ADD RESS) (POSTAL CODE)	*****	
Results to: A	bove D or				
Date of Sample:	Sent. 17	1904	Sampler's Comments:	Icon Pre	cipitation
	,				
Reason for Sample:		 1	Interpretation Contact Local Her		
	LIVESTOCK COM	SUMPTION L For	Interpretation Contact Local Vet	erinarian	
	IRRIGATION	For	Interpretation Contact Irrigation	Specialist	
			TER ANALYSIS REPORT		
		CHEFICAL WA	ILK ANALIJIJ KLYVKI		
Analysis			1 ~ 3		
Date Completed	0 x 2/89	<u> </u>	EC		m Slemens/cm
он <u>8-1</u>	•••••		SAR7		
	Sample Results	Canadian Drinking Watar		Sample Results	Cenadian Drinking Watar
	mg/L (ppm)	Standerds mg/L (ppm)		mg/L (ppm)	Standards mg/L (ppm)
alcium	101	<u>N.E.</u> Ca	Iran	26-8	
-	17		Fluoride		1.5. F
Aagnesium	323	•		2-4	
lardness, Total	6-9	<u> </u>	Sulphate	2.7	<u>500</u> so ₄ 250 ci
iodium	3./	N.E. K	Chloride		
otassium	14		Nitrate-Nitrogen P	<0.07	10.0
erbonate	368	<u>N.E.</u>	Nitrite-Nitrogen		<u>10.0</u> N
licarbonate		N.E. HCO3	Nitrite-Nitrogen		1.0 N
Alkalinity, Total	325	<u>500</u> CaCO ₃			
	******		Ammonium-	0-42	0.5 N
	***************		Nitrogen		*****
	***************	*****	Tasat Rivertur d	979	ስ ብሰብ
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WATER ANALYSIS

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OBSERVATION WELL NUMBER SHELL PW-2 Lsd 10 Sec 24 Twp 95 R 9 W4th Alberta Research Council

Sample source SHELL PW-2 @ 12 hours pumping @ 275 igpm SCL

Date sampled

August 10, 1972

Time 11.45 pm

	Mg/L	Meq/L	Percent Cations or Anions
Calcium (Ca ⁺⁺)	106	5.29	67.3
Magnesium (Mg ⁺⁺)	17	1-40	17.8
Sodium (Na ⁺)	,		
Potassium (K ⁺) Na + K	· 27	1.17	14.9
Carbonate (CO_3)	· 0	0	D
Bicarbonate (HCO3)	439	7.20	91.6
Sulfate $(50\frac{1}{4})$	2	0.04	0.5
Chloride (Cl [°])	22	D.62	7.9
Nitrate (NO_3^{m})			
Sílica (SiO ₂)			
Hydroxide (OH ⁻)			
Calcium (Acidified)			
Magnesium (Acidified)			
Total dissolved solids	613 calc	ulated	
Total Anions (epm)	Total C	ations (ep	n)
Other Co	onstituents		
Lab:	Field:		
Conductivity	Tempera	ture (C)	
рН 7.4	рH		
Fluoride (F ⁻)	Carbona	te (CO_3^m)	
	Bicarbo	mate (HCO_3))
	Hydroxi	de (OH [°])	
	Conduct	ivity	

Major Constituents

97%

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WATER ANALYSIS

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OBSERVATION WELL NUMBER SHELL PW-2 Lsd 10 Sec 24 Twp 95 R 9 W4th Alberta Research Council

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Sample source SHELL PW-2 @ 146 hours @ 275 igpm SCL

Date sampled

August 16, 1972

Time 1.30 pm

	Mg/L	Meq/L	Percent Cations or Anions
Calcium (Ca ⁺⁺)	105	5.24	65.3
Magnesium (Mg ⁺⁺)	20	1.64	20.4
Sodium (Na [†])			•
Potassium (K ⁺) Na + K	26	1.15	14.3
Carbonate (CO [*])	0	Ő	0
Bicarbonate (HCO3)	451	7.39	82.0
Sulfate (50_4^*)	1	0.02	0,2
Chloride (Cl [*])	- 22	0.62	7.7
Nitrate (NO ^m 3)			
Silica (SiO ₂)			
Hydroxide (OH [°])			
Calcium (Acidified)			
Magnesium (Acidified)			
Total dissolved solids	625 calcu	lated	
Total Anions (epm)	Total C	ations (epi	n)
0	ther Constituents		
Lab:	Field:		
Conductivity	Tempera	ture (C)	
рН 7.3	pH		
Fluoride (F [*])	Carbona	te $(C0_{3}^{-})$	
	Bicarbo	nate (HCO_3^2))
	Hydroxi	de (OH [°])	
	Conduct	ivity	
		100 ·	166

Major Constituents

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WATER ANALYSIS

SUEFF LN- E-1' 233856

OBSERVATION WELL NUMBER SHELL PW-2 Lsd 10 Sec 24 Twp 95 R 9 W4th Alberta Research Council

Sample source Bailed Date sampled July 17, 1976

		Mg/L	Meq/L	Percent Cations or Anions
Calcium (Ca ⁺⁺)	and a second	102.0	5.09	71
Magnesium (Mg ⁺⁺)		16.4	1.35	19
Sodium (Na ⁺) .		15.0	0.65	9
Potassium (K ⁺)		2.5	0.06	3
Carbonate (C0 ₃)		0.0	0.00	0
Bicarbonate (HCO ₃)		388.0	6.36	96
Sulfate (50_4^2)		4.3	0.09	1
Chloride (Cl ⁻)		6.0	0.17	3
Nitrate (NO ₃)	ت. ت	1.2	0.02	0
Silica _. (SiO ₂)		14.4		
Hydroxide (OH ⁻)				
Calcium (Acidified)		101.2		
Magnesium (Acidified)		17.6		
fotal dissolved solids		384		
Total Anions (epm)	6.64	Total C	ations (epm) 7.16
	Other Cons	tituents		
Lab:	F	ield:		
Conductivity	600	Tempera	ture (C)	5.0
На	7.6	рH		6.5
Fluoride (F ⁻)	0.2 Mg/L	Carbona	tc (C0 [°] ₃)	
		Bicarbo	nate (BCO_)	478 Ma/L

Major Constituents

Conductivity	600	Temperature (C)	5.0
рН	7.6	Нą	6.5
Fluoride (F ⁻)	0.2 Mg/L	Carbonate (CO ₃)	
	:	Bicarbonate (HCO_3)	478 Mg/L
		Hydroxide (OH [^])	
		Conductivity	

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ANALYSIS MULTIELEMENT OBSERVATION WELL NUMBER SHELL PW-2 J.sd 10 Sec 24 Twp 95 R W4th 9 Alberta Research Council

414 / 2276417641

Date sampled: July 17, 1976

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Value

Element

Value
VATUE

Ag	<.002	Mn	- 775
Au	<.003	Мо	<.006
Al	<.002	Na	14.5
As	<.038	Ni	<.010
B	.194	P	0.66
Ba	<.200	Pb	<.088
Ве	.002	Se	<.060
Ca	126.5	Si	10.5
Cd	<.002	Sn	<.045
Со	<.010	Sr	.303
Cr	<.006	Te	<.065
Cu	.025	Ti	<.0009
Eu	<.015	υ	<.020
Fe	33.8	V	.013
K	66.0	W	<.078
Mg	19.4	Zn	.077

NOTES:

- 1. All values in milligrams per liter
- 2. Sample bailed from well
- 3. Analysis done by Multielement Radio Frequency Induction Coupled Plasma Emission Spectrometer at Earringer Research Ltd., Rexdale, Ontario.

96%

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110.010 w 4 w SHELL PW-2-E-7. 233856

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SHELL PW-2-E-78 233856

WATER ANALYSIS

OBSERVATION WELL NUMBER SHELL PW-2 Lsd 10 Scc 24 Twp 95 R 9 W4th Alberta Research Council

Sample source Bailed Date sampled July 8, 1977

		Ng,'L	Neq/L	Percent Cations or Aniona
Calcium (Ca ⁺⁺)		105.0	5.24	75.9
Magnesium (Mg ⁺⁺)		16.5	1.36	19.7
Sodium (Na [†])		6.3	0.27	4_ D
Potassium (K ⁺)		1.3	0.03	0.5
Carbonate (C0 ⁷ 3)		0.0	0.00	0.0
Bicarbonate (HCO ₃)		434.0	7.11	96.7
Sulfate (SO_4^{e})		8.0	0.17	2.3
Chloride (Cl [°])	. .	2.0	0.06	0.8
Nitrate $(NO_{\overline{3}}^{\overline{3}})$		1.3	0.02	0.3
Silica _. (SiO ₂)		17.1		
Hydroxide (OH [°])				
Calcium (Acidified)		95.0		
Magnesium (Acidified)		16.1		
Total dissolved solids		444.0		
Total Anions (epm)	7.36	Total C	stions (epm)	6.91
	Other Cons	tituents		
Lab: .	ŕ	icld:		
Conductivity	670	Tempera	ture (C)	5.0
рH	6.8	рH		6.8
Fluoridc (F [*])	0.3 ppm	Carbona	te (C0 [±] 3)	
		Bicarbo	nate (HCO_{3}^{-})	512.0 ppm
		Hydroxi	de (OH [°])	
		Conduct	ivity	

Major Constituents

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ALBERIA RESEARCH COUNCIL WAIER ANALYSIS REPORT 233856

Mer 4 Tp	95 Rge	9 Sec 24 Lad 10	
		D	MY
(. ab no.	78 248	Date sempled 08 (17 78
Index no.	DH 648	Date submitted 17 i	37 78
Well depth(ft)	108.0	Date analysed(major) 8	678
Water level(+t)	-	Date enalysed(minor)	
Top open interval(ft)		Sampled by HACKE	JARTH
Bottom open Interval(ft)	Sample Source	WELL
Altitude(ft)		Owners name SHELL	PN=2
Bedrock elevation(ft)		Hardness(as CaCD3)	338,2
TDS(mg/1)	426.0	Alkalinity(as CaCO3)	332,0
Field Cand(micromhos/	'cm)	Cond(m(cromhos/cm025C)	570
Fleid pH	6.7	Lab pH	6,9

MAJOR CONSTITUENTS

		20	f total anion
	mg/1	neq/1	or cation
Calcium(Ca)	167.0	5,34	76.1
Magnesium(Mg)	17.3	1.42	20.3
Sod(um(Na)	5,0	0.22	3.1
Potassjum(K)	1.3	0.03	0.5
Carbonate(C03)	0.0	0.00	0.0
Bicarbonate(HC03)	415.0	6,80	99.5
Sulphate(S04)	0.0	8.00	0.0
Chlor(de(Cl)	0.0	0.00	0,0
Nitrate(NO3)	5*9	0.03	0,5
Hydrox (de (OH)	,		
Siliça(SiD2)	17.2	Total anions(epm)	6.834
Calcium(Acid)	91.0	Total cations(epm)	7.014
Hagneslum(Acid)	16.1	Ion balance error(%)	1.
Calculated TDS	353.9	TDS balance error(%)	+17,

MINOR CONSTITUENTS

Aluminum	0.04	ppm
Copper	9	ppb
lodine	Ø	ppm
Iron	27,1	ppm
Lead	0,3	ppb
Manganese	0.62	maq
Mercury	0.04	dqa

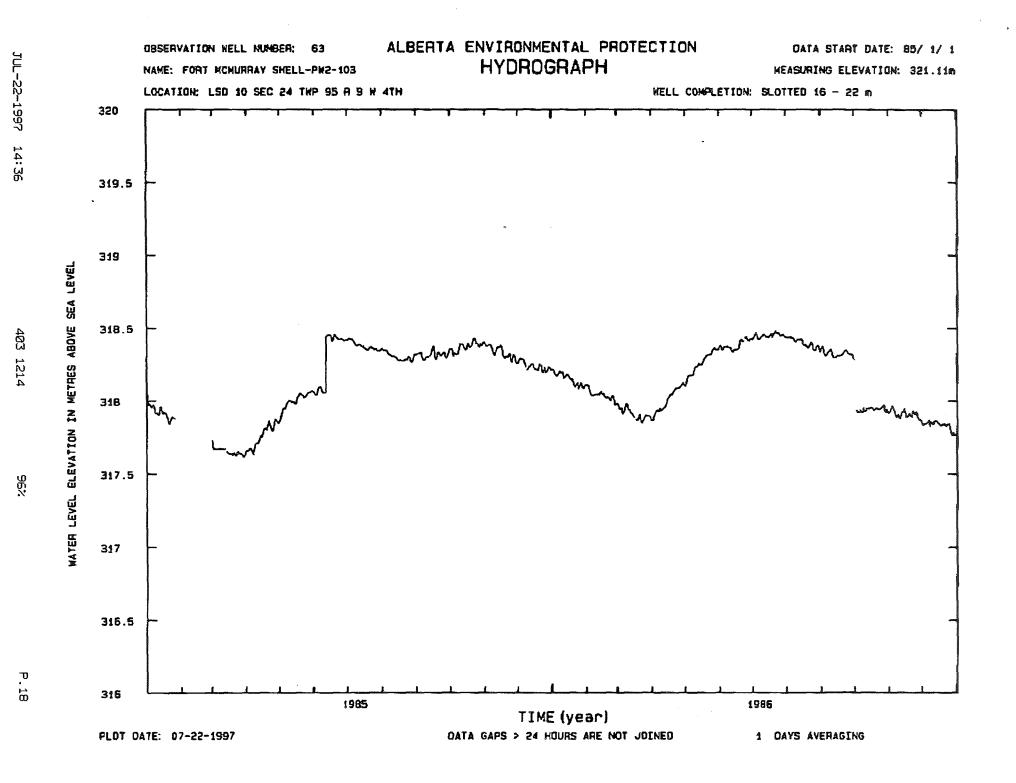
OTHER MEASUREMENTS						
Field Temp(C)	4.00	Fluoride(F)	0,30			
Fleid Bicarbonate(HC03	3) 507 ppm					

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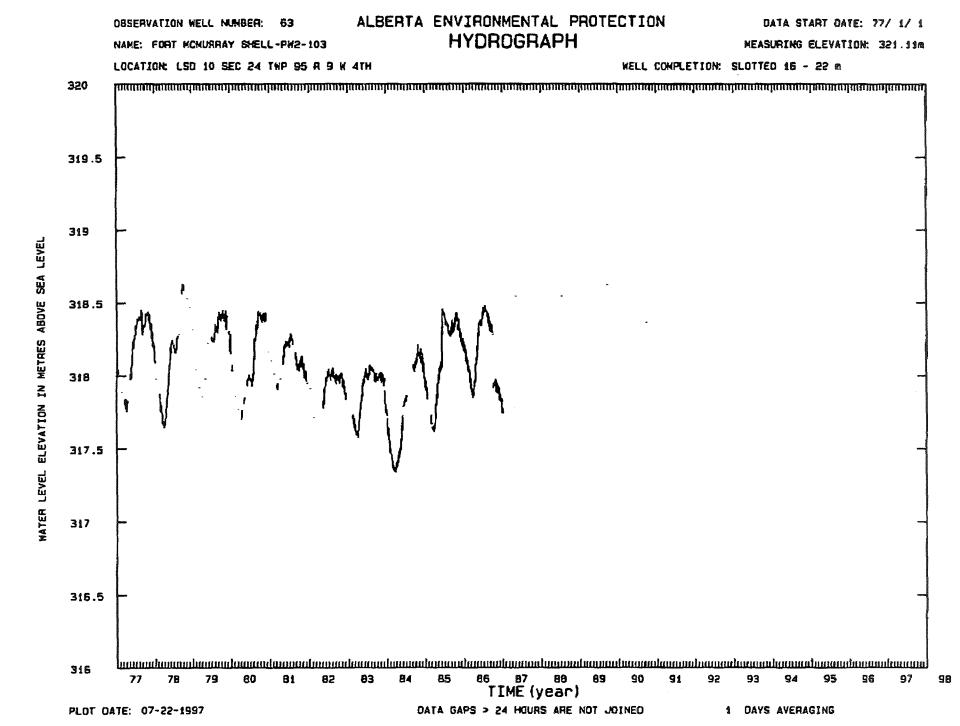
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ALBERTA ENVIRONMENTAL PROTECTION

COMPUTER GENERATED WATER WELL DRILLER'S REPORT FORM WI THIS DATA MAY NOT BE FULLY CHECKED; THE PROVINCE DISCLAIMS ALL RESPONSIBILITY FOR ITS ACCURACY: 233859 WELL I.D. Page 1 of 1

			-	Construction of the second				
CONTRACTOR:		WELL OWNER:		WELL	LOCATE	DN:	IC#:	02
NAME: UNKNOWN DRILLER		NAME: SHELL#PW-4	[V. OR LSD	SEC	9WT	PIGE	W. MER
		ADDRESS:		10	25	095	10	W4
ADDRESS:		Abbreas.			VERIFICA		HOD: FIEL	ـــــــــــــــــــــــــــــــــــــ
				LOCATION	IN QUART	ER;		-
LICENCE NO.: JOURNEYMAN I	IQ.:	POSTAL CODE:			BLOCK		* ***	
FORMATION LOG DESCRIPTIO	N: DRIL	LING METHOD: UNKNOWN		ELL ELEV:			'LAN: ow obtain: l	est/mated
Depth (Feet): Lithology: Ground to:		OF WORK: NEW WELL			TON TES	T:		
	and	NING WELL: No RATE:		TEST DAT Elapsed (Dogth to	Water	Dent	IT THME: h to Water
		HESENT: NO OIL PRESENT: NO OF ABANDONMENT:		Time In Min:Sec	avel During) Pumping	Level Du	ring Recovery
	MATE	POSED USE: OBSERVATION		I				
	ļ							
		WELL COMPLETION DATA:						
		LL FINISH: SCREEN & OPEN HOLE TAL HOLE DEPTH: 301 Feet						
			-					
		SING TYPE: UNKNOWN						
		E OD: 8.63 Inch WALL THICKNESS: 0.264 Inc TTOM AT: 235 Feet						
		DRATED CASINGALINER:	-					
	איד	E:						
		E OD; Inch						
		LL THICKNESS: Inch P AT: 0 Feet BOTTOM AT: Feet						
		RFORATED FROM: Feet TO: Feet						
		Feet TO: Feet Feet TO: Faet	-					
	₅₁₇	E OF PERFORATIONS: Inch X Inch						
		W PERFORATED:	-					
	SEAL	TYPE: CEMENT/GROUT						
		ERVAL TOP: 0 Feet TO: 215 Feet						· · · · · · · · · · · · · · · · · · ·
		HYSICAL LOG TAKEN: NED ON FILE:						
	SCRE	EN:					A	·····
	1	TERIAL: UNKNOWN						
		E ID (CLEAR): 6.13 inch SLOT SIZE: 0.020 inch ERVAL TOP; 249 Feet TO: 270 Feet						
		280 Feet TO: 290 Feet						
		TALLATION METHOD: ATTACHED TO CASING						
		P FITTINGS: TTOM FITTINGS:			MOVAL RA			Gal/Mi
	PACK		1	TEST DUR			ours	Minutes Fee
	GR/	AIN SIZE: AMOUNT:	1	NATER LE	VEL AT EN	OF TEST		Fex
				TOTAL DR	AWDOWN:			Fee
		LEGS ADAPTER TYPE: DP PIPE TYPE: LENGTH: Faat	1	RECOMME	NDED PUN	IP INTAKE	E: AT:	Gal/Min Feet
	ADI	DIAMETER: Inch DITIONAL PUMP INFORMATION:		MODEL:	UMP INSTA		H.P.:	
DATE WORK STARTED: DATE WORK COMPLETED:		COMMENTS:						
	uary 2, 197	(Maximum of 8 lines printed) 5						
CHEMISTRIES TAKEN: N HELD: 7		CUMENTS HELD: 8						
WELL OWNER'S ANTICIPATED WATER I	EQUIREMEN	TS PER DAY:						
ATE FORM PRINTED: July 21, 1997	/ 14:	25:26 DATE DATA KEYED: March 3, 1994		DATA	GWICDA	TAIGIC4		MM

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SHELL PW-4-E-77 233859

WATER ANALYSIS

OBSERVATION WELL NUMBER SHELL PW-4 Lsd 10 Sec 25 Twp 95 R 10 W4th Alberta Research Council

Sampl	e source	SF
Date	sampled	Fe

SHELL PW-4 (SCL)

February 2, 1975

Major Constituents

Time

	Mg/L	Meq/L	Percent Cations or Anions
Calcium (Ca ⁺⁺)	19	0.95	
Magnesium (Mg ⁺⁺)	25	2.06	
Sodium (Na ⁺) Na + K Potassium (K ⁺)	1130	49.17	
Carbonate (CO_3)	C	0	
Bicarbonate (HCO3)	1327	21.75	
Sulfate (SO ²)	- 39	0.81	
Chloride (Cl [^])	1050	29.62	
Nitrate (NO_3)			
Silica (SiO ₂)			
Hydroxide (OH ⁻)			
Calcium (Acidified)			
Magnesium (Acidified)			
Total dissolved solids	3590 calcu	lated	

Total Anions (epm)

Total Cations (epm)

96%

Other Constituents

Lab:		Field:
Conduc	tivity	Temperature (C)
рН	8.18	рН
Fluori	.de (F [~])	Carbonate (CO ³)
Iron	. 0	Bicarbonate (HCO_3)
H ₂ S	0	Hydroxide (OH [^])
		Conductivity

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OBSERVATION WELL NUMBER SHELL FW-4

Lsd 10 Sec 25 Twp 95 R 10 W4th

Alberta Research Council

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MULTIELEMENT

Date sampled: July 16, 1976

Element	Value	Element	Value
Ag	<.002	Mn	. 100
Au .	<.003	Мо	<.006
Al	0.22	Na	1028
As	<.038	Ni	<.010
B	1.67	Р	<.110
Ba	<.200	Pb	<.088
Ве	<.001	Se	<.060
Ca	58.2	Si	2.76
Cd	<.002	Sn	<.045
Co	<.010	Sr	1.45
Cr	<.006	Te	<.065
Cu	.019	Ti	<.0009
Eu	<.015	ប	<.020
Fe	0.79	v	0.009
ĸ	99	W	<.078
Mg	28.9	Zn	0.077

NOTES:

- 1. All values in milligrams per liter
- 2. Sample bailed from well
- 3. Analysis done by Multielement Radio Frequency Induction Coupled Plasma Emission Spectrometer at Earringer Research Ltd., Rexdale, Ontario.

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96%

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SIIELL PW-4-E-77 233859

WATER ANALYSIS

OBSERVATION WELL NUMBER SHELL PW-4 Lsd 10 Sec 25 Twp 95 R 10 W4th Alberta Research Council

Sample source Bailed Date sampled July 16, 1976

Mg/L	Meq/L	Percent Cations or Anions
58.0	2.89	5
31.0	2.55	5
1113.0	48.41	89
15.8	0.40	ł
0.0	0.00	O
1388.0	22.75	44
36.7	0.76	2
- 1010.0 -	28.48	55
1.0	0.02	Ο.
4.0		
60.5		
33.0		
7910	. <i>.</i>	
Total C	ations (epm) 54.26
stituents		
Field:		
Tempera	iture (C)	6.0
рН		7.2
Carbona	te (C0 ₃)	
Bicarbo	mate (HCO_3)	1449 Hg/L
	1113.0 15.8 0.0 1388.0 36.7 1010.0 1.0 4.0 60.5 33.0 7910 Total C stituents Field: Tempera pH Carbona	<pre>1113.0 48.41 15.8 0.40 0.0 0.00 1388.0 22.75 36.7 0.76 1010.0 - 28.48 1.0 0.02 4.0 60.5 33.0 7910 Total Cations (epm stituents Field: Temperature (C)</pre>

Major Constituents

96%

Conductivity

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233859 SHELL PW-4-E-78

WATER ANALYSIS

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OBSERVATION WELL NUMBER SHELL PW-4 Lsd 10 Sec 25 Twp 95 R 10 W4th Alberta Research Council

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Major Constituents

Sample so	urce	Baile	bd	
Date somp	led	July	8,	1977

	Ng/L	Meq/L	Percent Cations or Anions
Calcium (Ca ⁺⁴)	51.0	2.54	4.8
Magnesium (Mg ⁺⁺)	29.0	2.39	4-5
Sodium (Na ⁺)	1088.0	47.32	89.8
Potassium (K ⁺)	16.3	0.42	0.8
Carbonate (CO ₃)	D.0	0,00	0.0
Bicarbonate (HCO ₃)	1430.0	23.44	44.1
Sulfate (SO_4^{\bullet})	27.B	0.58	1.1
Chloride (Cl ⁻)	1032.0	29.10	54.B
Nitrate (NO [°] ₃)	0.2	0.00	0.0
Silica.(SiO ₂)	4.6		
Hydroxide (OH ⁻)			
Calcium (Acidified)	4B.0		
Magnesium (Acidified)	27.0		
Total dissolved solids	2928.0		
Total Anions (epm) 53.12	Total	Cations (ep:	n) 52.67

Other Constituents

F	ielč:	
5500	Temperature (C)	7.0
7.4	рН	7.5
2.3 ppm	Carbonate (CO [#])	
	Bicarbonate (HCG ₃)	1449.0 ppm
	Hydroxide (OH ⁻)	
	5500 7.4	7.4 pH 2.3 ppm Carbonate $(CO_{\overline{3}}^{\bullet})$ Bicarbonate $(HCC_{\overline{3}})$

Conductivity

96%

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NU.DII W14

233859

ALBERTA RESEARCH COUNCIL WATER ANALYSIS REPORT

Mer 4 lo	95 Rge	10 Sec 25 Lsd 10	
			DMY
Loo no.	78 247	Date sampled 2	8 07 78
Index no.	DH 647	Date submitted	7 07 78
well depth(ft)	.310.0	Date analysed(major)	8 8 7 8
water level(ft)	301	Date analysed(minor)	
Top open intervalift)	Sempled by HA	CKBARTH
Bottom open interval		Sample Source	WELL
Altitude(ft)		Owners name SHE	LL PW.4
Bedrock elevation(1t)	Hardness(as CaCO3)	214,3
TDS(mg/1)	2850,0	Alkelinity(as CaCO3)	1103.2
Field Cond(micromhos	/cm)	Cond(micromhos/cm@25C)	
Field pH	7 • 5	Lab pH	7,5

MAJOR CONSTITUENTS

		X 0f	rotal anion
	mg/1	meq/1	or eation
Calcium(Ca) .	43.0	2,15	4,3
Magnes um (Mg)	26.0	2.14	4.2
Sodium(Na)	1050.0	45,67	90.7
Potassium(K)	16.3	0.42	0.8
Carbonate(C03)	0.0	0.00	0,0
Bicarbonate(HCO3)	1379.0	22 . 60	42.9
Sulphate(504)	28.5	0.59	1.1
Chloride(C1)	1045.0	29,47	55,9
Nitrate(NO3)	0.8	0,01	0,0
Hydroxide(0H)	-		,
Silica(Si02)	4,6	Total anions(epm)	52,679
Calcium (Acid)	27.0	Total cations(epm)	50,375
Magnesium (Acid)	20.0	Ion balance error(%)	2.
Calculated TDS	2892.3	TDS belance error(%)	1.

MINOR CONSTITUENTS

Aluminum	0.04	ppm
Capper	2:25	9pm
lodine	0.03	ppm
Iron	, б	ppm
Lead	0.3	dqq
Manganese	4.05	ppm
Mercury	N,36	ppb

OTHER MEASUREMENTS					
Field	Temp(C)	6.00	Fluoride(F)	1.80 ppm	
Field	Bicarbonate(HCOS)	1400 ppm			

JUL-22-1997 14:44

403 1214

LIVESTOCK CONSUMPTION For Interpretation Contact Local Veterinerien IRRIGATION For Interpretation Contact Irrigation Specialist CHEMICAL WATER ANALYSIS REPORT Analysis Date Completed pH2_2 Canadian Drinking Weter Sample Results mg/L (ppm) Calcium	Lab. No.	175	@1128##@A# BA##@@@			
Project Code No.		***************************************	CHEMICAL WATER	ANALYSIS REQUEST	·····	
Project Code No.	Date Rec'd	6pt.21184	an a a an a an b a an a a a a a a a a a	, με μαραίζεων τι αυταιώσει το του του του του του του του πο		
History Location of Semple: D S D W/V INAME: ISTREET: COTV. YOW, VILLAGE: NB* Location & S.D. //D. X Section 25 Township	C	<i>yy</i>	PLEAS	E PRINT		
Location of Sample: D 5 D W M INAME! INA	Project Loue No		-17	IMLT	849	llable to the public.
D S D W // (name) (ST NEET) (CTY, TO WA, VILLAGE) (NAME) (ST NEET) (CTY, TO WA, VILLAGE) NB* Location (SS P. 10, X Section, 2.5) Township, 7.5) Range, 1.0, W W Source of Semple: (ST NEAR, OUEDUT, WELL TAP, FC.) NS* Well D Depth melers, test, Ospit 10 Water Level W Submitted by: Vel & Depth melers, test, Ospit 10 Water Level Phone, 4227-6231 Regults to: Above (or	History					
(POSTAL CODE) TTELEPHONE) NB* Location & S.D. / D. X. Section	Location of Sample:		/			
(POSTAL CODE) TTELEPHONE) NB* Location & S.D. / D. X. Section		0500	ŴN	()) ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;		
NB* Location 452.1.0. X Section .2.5		(NAMI				
Source of Sample: (ETREAM, DUDDUT, WELL TAP, ETC.) NB* Well Depth Well Completion (DMILLED, DUG, SCREEN, SETTLING ETC.) Submitted by: YEA-Mean YEA-Mean Child Q IADD RESS) (POETAL CODE) Results to: Above © or Date of Sample: MUMAN CONSUMPTION LIVESTOCK CONSUMPTION For Interpretation Contact Local Health Unit LIVESTOCK CONSUMPTION For Interpretation Contact Local Veterinarian IRRIGATION For Interpretation Contact Unigation Specialist Considian Date Completed Out 2/FH EC 3.8H m Sigmens/cm Magnesium Liston Considian Magnesium ME: Cenadian Magnesium Liston Considian Magnesium Liston Sample Standards Standards		***************************************	***************************************	(POSTAL CODE)	······	TELEPHONE)
NB* Well Dopth metere, test, Depth to Water Level metere, metere, Submitted by:	NB° Lo	cation <u>45</u> <i>D</i> 10	% Section	vnship <u>95</u> Aang	e	
NB* Well Dopth metere, test, Depth to Water Level metere, metere, Submitted by:	Source of Samolo					
Well Completion (DRILLED, DUG, SCREEN, SETTLING ETC.) Submitted by: YEA-Mara (ha.2) IADD RESS) (POOTAL CODE) Results to: Above E or Date of Semple: Lapt 15 194.4 Semple: Lapt 15 194.4 Date of Semple: Lapt 15 194.4 Resson for Sample: HUMAN CONSUMPTION LIVESTOCK CONSUMPTION For Interpretation Contact Local Health Unit IRRIGATION For Interpretation Contact Local Health Unit Resson for Sample: CHEMICAL WATER ANALYSIS REPORT Analysis Date Completed O.S. 2/F.4 EC 3	Surve of Sample.	(STREAM, DU	GOUT, WELL, TAP, ETC.)		*****	•••••••••••••••••••••••••••••••••••••••
Submitted by: YeA-Maen. (An.2) Phone. 4227-0231 Results to: Above I or IADDRESS) (POETAL CODE) Results to: Above I or Sampler's Comments: Results to: Above I or Ind Y Sampler's Comments: Results to: Above I or Ind Y Sampler's Comments: Results to: Ind Y Sampler's Comments: Results Ind Y Results MUMAN CONSUMPTION For Interpretation Contact Local Health Unit LIVESTOCK CONSUMPTION For Interpretation Contact Infigution Specialist ChEMICAL WATER ANALYSIS REPORT Analysis Date Completed Oct 2/PH Canadian Date Completed Oct 2/PH Canadian Date Completed Oct 2/PH Canadian Date Completed Oct 2/PH Canadian Date Completed Oct 2/PH Canadian Bandeare Marki	NB° We	II 🖸 Depth	meters,	feet, Depth to Water Le	vel	nətərs,fee
Submitted by: YeA-Maen. (An.2) Phone. 4227-0231 Results to: Above I or IADDRESS) (POETAL CODE) Results to: Above I or Sampler's Comments: Results to: Above I or Ind Y Sampler's Comments: Results to: Above I or Ind Y Sampler's Comments: Results to: Ind Y Sampler's Comments: Results Ind Y Results MUMAN CONSUMPTION For Interpretation Contact Local Health Unit LIVESTOCK CONSUMPTION For Interpretation Contact Infigution Specialist ChEMICAL WATER ANALYSIS REPORT Analysis Date Completed Oct 2/PH Canadian Date Completed Oct 2/PH Canadian Date Completed Oct 2/PH Canadian Date Completed Oct 2/PH Canadian Date Completed Oct 2/PH Canadian Bandeare Marki	We	Il Completion			*****	
IADDRESS: (POETAL CODE) (POETAL CODE) Date of Sample: Japt 1.5. 19.6.4 Sample: Japt 1.5. 19.6.4 Sample: Lippt 1.5. 19.6.4 Sample: Lippt 1.5. 19.6.4 Sample: HUMAN CONSUMPTION For Interpretation Contact Local Veter/Insrian INTERPRETATION For Interpretation Contact Local Veter/Insrian IRRIGATION CHEMICAL WATER ANALYSIS REPORT Analysis Date Completed Quit 2/F# Canadian Marking Water Sample Bandrade Gatelum All ST Canadian Origing Sample Results on Sample		$\sqrt{a} = AA$	(DR	ILLED, DUG, SCREEN, SETT	LING ETC.)	427- 1221
Date of Sample: J.S. J.M.L.Y. Sampler's Comments: Resson for Sample: HUMAN CONSUMPTION For Interpretation Contact Local Health Unit LIVESTOCK CONSUMPTION For Interpretation Contact Local Veterinerian IRRIGATION For Interpretation Contact Local Veterinerian Resson for Sample: HUMAN CONSUMPTION For Interpretation Contact Irrigation Specialist CHEMICAL WATER ANALYSIS REPORT Analysis Date Completed Oct 2/PH EC 3.8H m Sismens/cm PH 2-2 SAR JST Semple Drinking Water Standards Resulta Sample Canadian Drinking Water Standards Mater Standards Standards Resulta Canadian Drinking Water Standards Semple Resulta Drinking Water Standards Resulta Canadian Drinking Water Standards Standards Mater Standards Standards Resulta Sample Sample Sample Standards Standards Standards Resulta NE: Ce Iron GLOST O.3 Fe Magnesium Sample SSO SO		/				
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Date of Sample: J.S. J.M.L.Y. Sampler's Comments: Resson for Sample: HUMAN CONSUMPTION For Interpretation Contact Local Health Unit LIVESTOCK CONSUMPTION For Interpretation Contact Local Veterinerian IRRIGATION For Interpretation Contact Local Veterinerian Resson for Sample: HUMAN CONSUMPTION For Interpretation Contact Irrigation Specialist CHEMICAL WATER ANALYSIS REPORT Analysis Date Completed Oct 2/PH EC 3.8H m Sismens/cm PH 2-2 SAR JST Semple Drinking Water Standards Resulta Sample Canadian Drinking Water Standards Mater Standards Standards Resulta Canadian Drinking Water Standards Semple Resulta Drinking Water Standards Resulta Canadian Drinking Water Standards Standards Mater Standards Standards Resulta Sample Sample Sample Standards Standards Standards Resulta NE: Ce Iron GLOST O.3 Fe Magnesium Sample SSO SO	Results to: Ah	ove D or		****	*******	
Reason for Sample: HUMAN CONSUMPTION For Interpretation Contact Local Health Unit LIVESTOCK CONSUMPTION For Interpretation Contact Local Veterinarian IRRIGATION For Interpretation Contact Local Veterinarian CHEMICAL WATER ANALYSIS REPORT Analysis Date Completed Oct 2/FH Canadian Sample Reaction Contact Irrigation Specialist Chemical WATER ANALYSIS REPORT Analysis Date Completed Oct 2/FH Canadian Diriking Magende Canadian Magende Canadian Marking Magenesium A.S. Calcium A.S. Magenesium A.S. Magenesium A.S. Net Social for Magenesium A.S. Net Social	Date of Semaler	ent. 15. 1	984	Sampler's Comments		
LIVESTOCK CONSUMPTION For Interpretation Contact Local VeterInerian IRRIGATION For Interpretation Contact Irrigation Specialist CHEMICAL WATER ANALYSIS REPORT Anelysis Date Completed OCT 2/PH Canadian Diriking Magnesium Anelysis Sample Canadian Diriking Water Sample Canadian Diriking Magnesium Sample	Date of Campiepr.	7.7.				**************
IRRIGATION For Interpretation Contact Irrigation Specialist CHEMICAL WATER ANALYSIS REPORT Anetysis Date Completed O.X 3/PH EC 3.PH m Siemens/cm Sample Canadian Diriking Water Sample Canadian Diriking Sample Canadian	Reason for Sample:	HUMAN CONSUM	MPTION For Intern	retation Contect Local Hea	ilth Unit	
CHEMICAL WATER ANALYSIS REPORT Analysis OFT 2/64 Some service Date Completed OFT 2/64 EC 3.84 m Siemens/cm Date Completed OFT 2/64 EC 3.84 m Siemens/cm Date Completed OFT 2/64 EC 3.84 m Siemens/cm Date Completed Semple Semple Canadian Date Completed Semple Canadian Semple Canadian Semple Canadian Magnesium A.E. Cenadian OFT Cea Iron Cenadian Magnesium Cenadian A.E. Ceadian Standards Iron Ceadian Magnesium Ceadian Ceadian Sodium Ceadian		LIVESTOCK CON	SUMPTION D For Inters	retation Contact Local Vet	erinarian	
CHEMICAL WATER ANALYSIS REPORT Analysis OFT 2/64 Some service Date Completed OFT 2/64 EC 3.84 m Siemens/cm Date Completed OFT 2/64 EC 3.84 m Siemens/cm Date Completed OFT 2/64 EC 3.84 m Siemens/cm Date Completed Semple Semple Canadian Date Completed Semple Canadian Semple Canadian Semple Canadian Magnesium A.E. Cenadian OFT Cea Iron Cenadian Magnesium Cenadian A.E. Ceadian Standards Iron Ceadian Magnesium Ceadian Ceadian Sodium Ceadian		IBRIGATION				
Analysis Oct. 2/84 EC 3.84 m Siemens/cm pH 9-9 SAR 157/ SAR Canadian pH 9-9 SAR 157/ SAR Drinking Weter Sample Canadian Sample Canadian Drinking Magnesium 1 N.E.* Ce Iron 150/000 Semple Standards Magnesium 1 N.E.* Ce Iron 1.6.057 0.3 Fe Magnesium 1 N.E.* Ce Iron 1.6.057 0.3 Fe Magnesium 1 5 500 CeCo3 Sulphate 2.7/ 500 So4 Sodium 277 300 Na Chloride 2.6.07 10.0 N Potassium 2.7 N.E. K Nitrite-Nitrogen 10.0 N Bicarbonate 1.85 500 CaCO3 Nitrite-Nitrogen 1.0 N Alkelinity, Total 5555 500 CaCO3 Nitrite-Nitrogen 1.0 N						
Date Completed Q. # 2/F# EC 3.84 m Siemens/cm pH 2-2 SAR						
Date Completed Q. # 2/F# EC 3.84 m Siemens/cm pH 2-2 SAR			CHEMICAL WATER	ANALYSIS REPORT		
Sample Results Canadian Drinking Water Sample Results Canadian Drinking Water Sample Results Canadian Drinking Water Calcium ////////////////////////////////////	Asstrain		CHEMICAL WATER	ANALYSIS REPORT		
Sample Results Canadian Drinking Water Sample Results Canadian Drinking Water Sample Results Canadian Drinking Water Calcium ////////////////////////////////////	Analysis	0.72/			4	m Siemens/cm
Sample Results Drinking Water Sample Standards Drinking Water rmg/L (ppm) Standards rmg/L (ppm) Presults Drinking Water Calcium ////////////////////////////////////	Date Completed	Q.\$ 2/		EC	4	m Siemens/cm
Results mg/L (ppm) Water Standards mg/L (ppm) Water Standards mg/L (ppm) Water mg/L (ppm) Calcium	Date Completed	Q.\$ 2/		EC	4	m Siemens/cm
(ppm) mg/L (ppm) (ppm) mg/L (ppm) Calcium	Date Completed	_	S 4 Canadian	EC		Cenedian
Magnessium $D-6$ 150MgFluoride 1.5 FHardness, Total S^{-1} 500 $CaCO_3$ Sulphate $2-2'$ 500 SO_4 Sodium 277 300 NaChloride $F62$ 250 ClPotassium 2.7 N.E.KNitrate-Nitrogen PlusCarbonate 1.6 NBicarbonate 1.86 N.E. CO_3 Nitrite-Nitrogen $<6-07$ 10.0 NBicarbonate 2.95 N.E. HCO_3 Nitrite-Nitrogen $<6-07$ 10.0 NAlkelinity, Total $S-555$ 500 $CaCO_3$ Nitrite-Nitrogen $1.2-6$ 0.5 NTotal Dissolved 2026 1000 Total Dissolved 2026 1000	Date Completed	 Sample Results	Canadian Drinking Water	EC	Semple Results	Cenadian Drinking Water
Magnessium $D-6$ 150MgFluoride 1.5 FHardness, Total S^{-1} 500 $CaCO_3$ Sulphate $2-2'$ 500 SO_4 Sodium 277 300 NaChloride $F62$ 250 ClPotassium 2.7 N.E.KNitrate-Nitrogen PlusCarbonate 1.6 NBicarbonate 1.86 N.E. CO_3 Nitrite-Nitrogen $<6-07$ 10.0 NBicarbonate 2.95 N.E. HCO_3 Nitrite-Nitrogen $<6-07$ 10.0 NAlkelinity, Total $S-555$ 500 $CaCO_3$ Nitrite-Nitrogen $1.2-6$ 0.5 NTotal Dissolved 2026 1000 Total Dissolved 2026 1000	Date Completed	 Sample Results mg/L	Canadian Drinking Water Standards	EC	Semple Rezults mg/L	Cenadian Drinking Water Standerde
Hardness, Total S 500 $CaCO_3$ Sulphate $Z = 1^{-1}$ 500 SO_4 Sodium 277 300 NaChloride E/EP 250 ClPotassium $Z.7$ N.E.KNitrate-Nitrogen PlusCarbonate 186 N.E. CO_3 Nitrite-Nitrogen $\sqrt{e-er7}$ 10.0 NBicarbonate 298 N.E. HCO_3 Nitrite-Nitrogen $\sqrt{e-er7}$ 10.0 NAlkelinity, Total 5755 500 $CaCO_3$ Nitrite-Nitrogen 1.0 NTotal Dissolved 226 0.5 NTotal Dissolved 2026 1000	Date Completed pH <u>Я-</u> .Я	 Sample Results mg/L (ppm)	Canadian Drinking Water Standards mg/L (ppm)	ec	Semple Rezults mg/L (ppm)	Cenadian Drinking Water Standerds mg/L (ppm)
Sodium 777 300 Na Chloride 762 250 Cl Potassium 27 N.E. K Nitrate-Nitrogen Plus Nitrate-Nitrogen Plus Carbonate 186 N.E. CO3 Nitrite-Nitrogen 260.07 10.0 N Bicarbonate 278 N.E. HCO3 Nitrite-Nitrogen 100 N Alkelinity, Total 555 500 CaCO3 Nitrite-Nitrogen 1.0 N Mitrate-Nitrogen 1.0 N 500 CaCO3 Nitrite-Nitrogen 1.0 N Mitrate-Nitrogen 500 CaCO3 Nitrite-Nitrogen 1.0 N Mitrate-Nitrogen 500 CaCO3 100 100 1000	Date Completed pH <u>9-9</u>	Sample Results mg/L (ppm)	Canadian Drinking Water Standards mg/L (ppm) N.E.* Ca	EC	Semple Rezults mg/L (ppm) 0-05	Cenadian Drinking Water Standerds mg/L (ppm) 0.3
Potassium 2.7 N.E. K Nitrate-Nitrogen Plus Carbonate 186 N.E. CO ₃ Nitrite-Nitrogen <0.07 10.0 N Bicarbonate 2.98 N.E. HCO ₃ Nitrite-Nitrogen <0.07 10.0 N Alkelinity, Total 5.55 500 CaCO ₃ Nitrite-Nitrogen 1.0 N Alkelinity, Total 5.55 500 CaCO ₃ Nitrite-Nitrogen 1.0 N Mitrogen 1.0 N 1.0 N 1.0 N Total Dissolved $2.92.6$ 1000 5000 5000 5000 5000 5000 1000 1000	Date Completed pH <u>9-9</u> Calcium Magnesium	Sample Results mg/L (ppm) 	Canadian Drinking Water Standarda mg/L (ppm) 	EC 3.8 SAR 157 Iron Fluoride	Semple Rezults mg/L (ppm) 0-05	Cenedian Drinking Water Standerds mg/L (ppm) 0.3
Carbonate 186 N.E. CO_3 Nitrite-Nitrogen CO_7 10.0 N Bicarbonate 298 N.E. HCO_3 Nitrite-Nitrogen 1.0 N Alkelinity, Total 5555 500 $CaCO_3$ Nitrite-Nitrogen 1.0 N Alkelinity, Total 5555 500 $CaCO_3$ Nitrite-Nitrogen 1.0 N (T. Alk.) $Mmonium$ -Nitrogen $1.2-6$ 0.5 N Total Dissolved 2026 1000 5000 5000 1000	Date Completed pH <u>??</u> Calcium Magnesium Hardness, Total	Sample Results mg/L (ppm) / 	Canadian Drinking Water Standards mg/L (ppm) <u>N.E.</u> Ca 	EC	Semple Rezults mg/L (ppm) 0_05 ⁻ <u>2-4</u>	Cenadian Drinking Water Standerde mg/L (ppm) 0.3Fe F
Bicarbonate <u>295</u> <u>N.E.</u> HCO ₃ Nitrite-Nitrogen <u>1.0</u> N Alkelinity, Total <u>5555</u> <u>500</u> CaCO ₃ Ammonium- Nitrogen <u>1.0</u> N <u>1.0</u> N <u>1.0</u> N <u>1.0</u> N <u>1.0</u> N <u>1.0</u> N <u>1.0</u> N	Date Completed pH <u>9-9</u> Calcium Magnesium	Sample Results mg/L (ppm) 	Canadian Drinking Water Standards mg/L (ppm) 	EC	Semple Rezults mg/L (ppm) 0_05 ⁻ <u>2-4</u>	Cenadian Drinking Water Standerde mg/L (ppm) 0.3Fe F
Alkelinity, Total	Date Completed pH <u>??</u> Calcium Magnesium Hardness, Total	Sample Results mg/L (ppm) 	Canadian Drinking Water Standards mg/L (ppm) 	EC	Semple Rezults mg/L (ppm) 0-05 ⁻ 2-4 <u>2-4</u> <u>862</u>	Cenadian Drinking Water Standerde mg/L (ppm) 0.3Fe F
Alkelinity, Total	Date Completed pH <u>9-9</u> Calcium Magnesium Hardness, Total Sodium	Sample Results mg/L (ppm) 	Canadian Drinking Water Standards mg/L (ppm) 	EC 3.8 SAR	Semple Rezults mg/L (ppm) 0-05 ⁻ 2-4 <u>2-4</u> <u>862</u>	Cenedian Drinking Water Standerds mg/L (ppm) 0.3Fe F
(T. Alk.) Ammonium- Nitrogen Total Dissolved Splids (TDS)	Date Completed pH	Sample Results mg/L (ppm) / 	Canadian Drinking Water Standarda mg/L (ppm) 	EC	Semple Rezults mg/L (ppm) 0-05 ⁻ 2-4 <u>2-4</u> <u>862</u>	Cenadian Drinking Water Standerde mg/L (ppm)
Nitrogen Total Dissolved 2026 1000	Date Completed pH <u>??</u> Calcium Magnesium Hardness, Total Sodium Potassium Carbonate	Sample Results mg/L (ppm) / D-6 S ⁻ 777 27 /86 298	Canadian Drinking Water Standards mg/L (ppm) <u>N.E.*</u> Ca 	EC	Semple Rezults mg/L (ppm) 0-05 ⁻ 2-4 <u>2-4</u> <u>869</u>	Cenadian Drinking Water Standerde mg/L (ppm)
Total Dissolved 2026 1000	Date Completed pH	Sample Results mg/L (ppm) / D-6 5 777 27 27 27 186 298	Canadian Drinking Water Standards mg/L (ppm) N.E.* Ca 150 Mg 500 CaCO ₃ 300 Na N.E. K N.E. CO ₃ M.E. K N.E. HCO ₃ 500 CaCO ₃	EC	Semple Rezults mg/L (ppm) 0-05 ⁻ 	Cenadian Drinking Water Standerde mg/L (ppm)
Splide (TDS)	Date Completed pH	Sample Results mg/L (ppm) / D-6 5 777 27 27 27 186 298	Canadian Drinking Water Standards mg/L (ppm) N.E.* Ca 150 Mg 500 CaCO ₃ 300 Na N.E. K N.E. CO ₃ M.E. K N.E. HCO ₃ 500 CaCO ₃	EC	Semple Rezults mg/L (ppm) 0-05 ⁻ 	Cenadian Drinking Water Standerde mg/L (ppm)
Splide (TDS)	Date Completed pH	Sample Results mg/L (ppm) / 0-6 5 ⁻ 777 27 27 186 298 5-55	Салаdian Drinking Water Standards mg/L (ppm) 	EC	Semple Rezults mg/L (ppm) 0-05 ⁻ 2-4 845 845 845 845 845 845 845 845 845 84	Canadian Drinking Water Standards mg/L (ppm)
	Date Completed pH	Sample Results mg/L (ppm) / 0-6 5 ⁻ 777 27 27 186 298 5-55	Салаdian Drinking Water Standards mg/L (ppm) 	EC 3.8 SAR 157 SAR 157 Fluoride Sulphste Chloride Nitrate-Nitrogen Nitrite-Nitrogen Nitrite-Nitrogen Nitrite-Nitrogen	Semple Rezults mg/L (ppm) 0-05 ⁻ 2-4 862 Nus <0-07	Canadian Drinking Water Standards mg/L (ppm)
	Date Completed pH	Sample Results mg/L (ppm) D6 27 27 27 27 27 27 28 5-55	Canadian Drinking Water Standards mg/L (ppm) N.E.* Ca 150 Mg 500 CaCO ₃ 300 Na N.E. K N.E. K N.E. HCO ₃ 500 CaCO ₃	EC 3.8 SAR	Semple Rezults mg/L (ppm) 0-05 ⁻ 2-4 862 Nus <0-07	Canadian Drinking Water Standards mg/L (ppm)

mistory					
Location of Samp	le:				
	050	ωN	(STREET)		
	(NAME	5)	(STREET)	CITY	, TOWN, VILLAGE)
	******	*********	(POSTAL CODE)		(TELEPHONE)
NR*	Location LSD 10	% Section 25	Township	Range 10 W	4 Maridian
				0	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
Source of Sample	STREAM, DU	OUT, WELL, TAP, ETC.)			••••••••••••
NRT		metera	feet, Depth to Wa	tor Lovelr	natars
	•				
			(DRILLED, DUG, SCREEN,		
Submitted by:	<u> Уер-Шроп</u>	Chae		Phone	427-6231
			(Postal Coe		
Results to:	About PLas	AUDA	-55) (POSIAL COL		
NESUITS TO:				E. LA.d	n. L! 1.
Date of Sample:	20.207	· · · · · · · · · · · · · · · · · · ·	Sampler's Comme	nts: JAR & DXACK	ALCIAS
Reason for Sample			For Interpretation Contact Loca	al Health Unit	
-	LIVESTOCK CON		For Interpretation Contact Loca	I Veterinarian	
	IRRIGATION		For Interpretation Contect Irrig		
Concernation and the second	IBRIGATION	ا السبوية	or interpretation contact intg		
			ATER ANALYSIS REPO	DT	
		UNCHICAL N	MILK MAMLIJIJ KLEV		
Analysis					
Date Completed	Øst 2/8	4	EC	.11	m Slømens/cm
pH 8-15	•		SAR ZZ		
pri			JAR	······	
	Sampla	Çanadibri Drinkîng		Sample	Cenadian Drinking
	Results mg/L	Water Standards		Results mg/L	Water Standarda
	(ppm)	mg/L (ppm)		(ppm)	mg/L (ppm)
Calcium	5-8	N.E.* Ca	Iron	0-15	<u>0.3</u> Fe
Magnesium	30	<u>150</u> Mg	Fluoride		<u>1.5</u> F
Hardness, Total	270		0 ₃ Sulphate	34	
Sodium	1042	300 Na	Chloride	995	250 CI
	16	<u>N.E.</u> K			
Potassium			Nitrate-Nitrog	1007	
Carbonate	0	<u>N.E.</u> CO ₃	_	en	<u>10.0</u> N
Bicarbonate	1414	<u>N.E</u> HCC	Nitrite-Nitroge	n	1.0 N
Alkalinity, Totel (T. Alk.)	1159	<u>500</u> CeC	0 ₃		
	****	*** * *** * ** **********	Ammonium-	2-66	0.5 N
		*****	Nitrogen	*****************	N
	****************	*** ***********	•	1877	4000
			Total Dissolva Solida (TDS)	d <u>7872</u>	1000
			· · · · · · · · · · · · · · · · · · ·		
Laboratory Commo		particles			
<i>m.</i> Q	visible	pariettes			•••••••••••••••••••••••••••••••••••••••
					••••••••••••••••
NB Land Locatic samples.	on and Well Depths must	be given for all groun	dwater P	1	
NE*Not Establish	ned.			GRAVELAND NCH HEAD	

WHITE - Submittee: YELLOW - File; PINK - Municipal Engineering; BLUE - Hydrogeology Branch

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NAME: FORT NCHURRAY SHELL-PN4-301

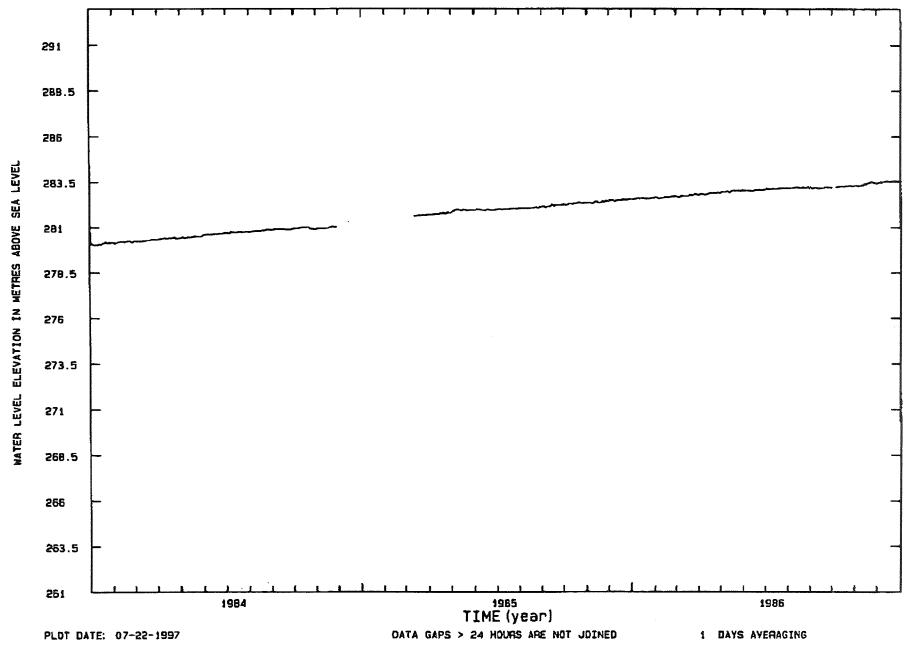
LOCATION: LSO 10 SEC 25 TWP 95 R 10 W 4TH

ALBERTA ENVIRONMENTAL PROTECTION HYDROGRAPH

DATA START DATE: 84/ 1/ 1

MEASURING ELEVATION: 291.08m

WELL COMPLETION: SCREEN 74.9-82.3; 85.4-88.4 m



914032474811

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13:23

87722797

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96X

OBSERVATION WELL NUMBER: 65

DATA START DATE: 77/ 1/ 1

Р.18

96%

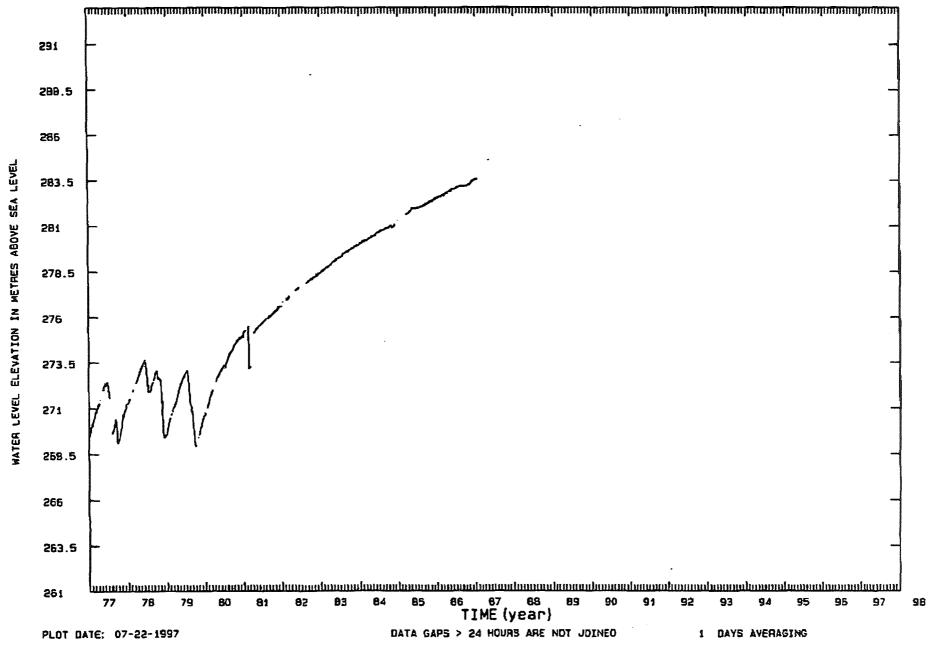
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JUL-22-1997

MEASURING ELEVATION: 291.08m





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722/70

ALBERTA ENVIRONMENTAL PROTECTION COMPUTER GENERATED WATER WELL DRILLER'S REPORT FORM with the province disclaims all responsibility for its accuracy: WELL I.D.

233860 Page 1 of

CONTRA	CTOR:		WELL OWNE	:R:			WELL	LOCATH	ON:	IC#:	03
NAME: UN	iknown Dailler		NAME: SHELL#1	085-7			VA OR LSI	SEC	TWP	RGE	W. MER
			ADDRESS:				10	25	095	10	W4
ADDRESS:							LOCATIO	N VERIFICA	TION METH	HOD: FIELD)
							LOCKILL		EH:		
LICENCE N	·	<u>.</u>	POSTAL CODE:	and the second			LOT:	BLOCK	: F	LAN:	
FORMAT Depth (Feel)	ION LOG DESCRIPTION: Lithology:	DRIL	LING METHOD:	UNKNO	JWN		WELL ELEV:	953.	Feet H	ow obtain: E	STIMATED
Ground to:		TYPE	OF WORK: N	EW WELL			PRODUC	-	T:	~~~~~	T TIME:
310	Unknown	FLOW	VING WELL: No	RATE	E:		TEST DA	Depth to	Water	Deoth	to Water
380	Greenish Gray Calcareous Shale		RESENT: NO OF ABANDONMENT:		RESENT:	No	Time in Min:Sec	Level Durini	g Pumping	Level Duri	Ing Recovery
403	Argiliaceous Umestone	MATER	RIAL USED:								
445	Gray Soft Shale		POSED USE: 0								
475	Umestone	"	NELL COMPLETI	ON DATA:							
480	Grey Saft Shele			EN HOLE							
500	Silly Limestone		AL HOLE DEPTH:	983 Fee	76						
510	Dolomite	CAS	SING TYPE: UNKNO	SMN							
565	See Comments	SIZE	≘00: 5.50 Inch	WALL TH	ICKNES6;	Inch					
675	See Comments	BOT	TTOM AT: 367	Feet							
690	See Commants]	RATED CASINGAUN	EA:							
	Gray Soft Shele	TYP		ich							
595	Dolomite	-	L THICKNESS:	Ind	ħ					ļ	
615	Limestone	1		est EOTTOM	AT:	Feet					
840	Unknown	PER	FORATED FROM:		TO:	Feet					
543	Lost Circutation				t TO: t TO:	Feet					
983		617	E OF PERFORATION	c.	Inch X	Inch					
····	· · · · · · · · · · · · · · · · · · ·	1	E OF PERFORATED:	5:	Inch A	Inch					<u></u>
		SEAL 1									
		INTI	ERVAL TOP: 0	Feat TO:	:	Feet					
		1	HYSICAL LOG TAKEI NED ON FILE:	€;							
		SCIPIEE	en:								
· · · · · · · · · · · · · · · · · · ·		MAT	TERIAL:								
		1	E ID (CLEAR):	Inch SLO		Inch					
			ERVAL TOP:	Feet TO: Feet TO:		Feet Foet					
		INS	TALLATION METHO) ;							
		TOF	FITTINGS:				WATER R	EMOVAL RA		G TEST:	Gal/Mi
		-	TOM FITTINGS:				TEST DUI			fours	Minutes
		PACK		AMOUNT:			DEPTHO	F PUMP/DR	ILL STEM:	r .	Fee
		GHA	NN SIZE:	AMOUNT:			NON-PUN	PING(GTAT			FE
		PITI	ESS ADAPTER TYP	 E:				ENDED PUI	MPING RAT		Gai/Min
		DRC	OP PIPE TYPE:	L	ENGTH:	Feet Inch	RECOMM	ENDED PUI PUMP INST.	MP INTAKE	AT:	Feet
DATE 100		ADD	DITIONAL PUMP INFO	DRMATION:	CEE E	ILE FOR DET	MODEL:	ID. LAICE C. LAI	10 000 L C	H.P.;	10
	ORK STARTED: ORK COMPLETED:		A A		PLUG	ILE FOR DETI GED BACK T	0 750'	a. WELL W		7 10 903 AU	1.1
DATE DA	TA RECEIVED: August 1	7, 1972	•	of 9 lines prir	n(90)						
-	IL TEST AND/OR PUMP DATA: IES TAKEN: N MELD: 5	nor	CUMENTS HELD: 8								
•	IES TAREN: NY RELD: D IER'S ANTICIPATED WATER REQU										
					-						
ite form	PRINTED: July 21, 1997	14:	25:15 DATE DAT	a keyed:	August 6	S, 1996	DATA	IGWICDA	TAIGIC4	Ľ	00

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WATER ANALYSIS OBSERVATION WELL NUMBER SHELL OBS-7 Lsd 10 Sec 25 Twp 95 R 10 W4th Alberta Research Council

Sample source	SHELL OBS-7 (SCL)
Date sampled	August 17, 1972

,

	Mg/L	Meq/L	Percent Cations or Anions
Calcium (Ca ^{**})	1032	51.50	13.7
Magnesium (Mg ⁺⁺)	271	22.29	6.0
Sodium (Na ⁺)	•		
Potassium (K ⁺) Na + K	6960	302.63	80.4
Carbonate (CO ^T ₃)	0	- 0	٥
Bicarbonate $(HCO_{\overline{3}})$	390	6.39	1.7
Sulfate (SO_4^-)	2944	61.32	16.3
Chloride (Cl ⁻)	10947	308.71	82.0
Nitrate (NO_3^*)			
Silica (SiO ₂)	· .		
Hydroxide (OH [*])			
Calcium (Acidified)			
Magnesium (Acidified)			
Total dissolved solids	22544 cal	culated	
Total Anions (epm)	Total	Cations (epi	m)

Major Constituents

Other Constituents

Lab:		Field:
Conductivity		Temperature (C)
рН	7.1	На
Fluoride (F ⁻)		Carbonate (CO_3)
H ₂ S	None	Bicarbonate (HCO_3)
		Hydroxide (OH [°])
		Conductivity

97%

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WATER ANALYSIS

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OBSERVATION WELL NUMBER SHELL OBS-7 Lsd 10 Sec 25 Twp 95 R 10 W4th Alberta Research Council

Bailed Sample source July 16, 1976 Date sampled

.,,			
	Mg/L	Meq/L	Percent Cations or Anions
Calcium (Ca ^{*+})	5.5	0.27	4
Magnesium (Mg ^{**})	2.3	0.19	3
Sodium (Na ⁺)	158.0	6.87	92
Potassium (K ⁺)	5.0	0.13	· 2
Carbonate (CO ₃)	7.2	0.24	3
Bicarbonate (HCO3)	142.0	2.33	32
Sulfate (SO ₄)	13.6	0.28	4
Chloride (Cl [°])	160.0	4.51	- 61
Nitrate (NO_3)	0.3	0.00	0
Silica (SiO ₂)	0.1		
Hydroxide (OH ⁻)			
Calcium (Acidified)	5.4		
Magnesium (Acidified)	2.5		

Major Constituents

Total Anions (epm)

Total dissolved solids

Total Cations (epm) 7.37

7.46

Other Constituents

Lab:		-		
Conductivity	730	Temperature (C)	6.0	
рН	8.4	рН	9.0	
Fluoride (F ⁻)	0.6 Hg/L	Carbonate $(C0_3)$	53	Hg∕L
	•	Bicarbonate (HCO_{3})	68	Mg/L

380

Conductivity

Hydroxide (OH^{*})

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97%

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MULTIELEMENT ANALYSIS **OBSERVATION WELL NUMBER** SHELL OBS-7 Lsd 10 Sec 25 Twp 95 R 10 W4ch Alberta Research Council

Date sampled:

10.10

July 16, 1976

Element	Value	Element	Value
Ag	<.002	Mn	<.001
Au	<.003	Mo	<.006
A1	<.002	Na	144
As	<.038	-Ni	<.010
B	-334	P	<.110
Ba	<.200	РЪ	<.088
Be	001	Se	<.060
Ca	7.30	Si	. 40
Cd	<.002	Sn	<.045
Со	<.010	Sr	.130
Cr	<.006	Te	<.065
Cu	.008	Ti	<.0009
Eu	<.015	U	<.020
Fe	.033	V	<.0008
K	<.150	W	<.078
Mg	2.38	Zn	<.002

NOTES:

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- 1. All values in milligrams per liter
- Sample bailed from well 2.
- Analysis done by Multielement Radio Frequency 3. Induction Coupled Plasma Emission Spectrometer at Carringer Research Ltd., Rexdale, Ontario.

96%

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WATER ANALYSIS

OBSERVATION WELL NUMBER SHELL 085-7 Lsd 10 Sec 25 Twp 95 R 10 W4th Alberta Research Council

Sample source Bolled Date sampled July 8, 1977

• .	Mg/L	Meq/L	Percent Cations or Anions
Calcium (Ca ⁺⁺)	8.8	3,44	2.5
Magnesium (Mg ⁺⁺)	B.6	Q. 71	· 4.0
Sodium (Na ⁺)	378.0	15.44	92.0
Potassium (K ⁺)	10.8	- 0.28	1.5
Carbonate ($CO_3^{\overline{5}}$)	7.2	9.24	1.3
Bicarbonate (HCO ₃)	224.0	3.67	20.1
Sulfate (SO ₁)	28.1	0.59	3.2
Chloride (Cl ⁻)	488.0	13.76	75 . 3
Nitrate (NO_{3}^{-})	0.7	2.01	0.1
Silica (SiO ₂)	0.4		
Hydroxide (OH ⁻)			
Calcium (Acidified)	8.3		
Magnesium (Acidified)	8.5		
Total dissolved solids	1036.0		
Total Anions (epm) 18.2	7 Total (Cations (epr	n) 17.87

Major Constituents

Other Constituents

ab:			Field:		
	Conductivity	2000	Temperature (C)	7.0	
	рН	8.5	рH		
	Fluoride (F [*])	1.2 ppm	Carbonate (CO_3^{*})	24.0	ppm
	:		Bicarbonate $(HCO_{\overline{3}})$	195.0	ppm
			Hydroxide (OH ⁻)		
			Conductivity		

Lab

97%

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ALBERTA RESEARCH COUNCIL WATER ANALYSIS REPORT

Mer 4	1p 95	Rge	10	Sec	25	Lsd	10			
								D	Μ	٧
Lab no.	78	246		Date	samp	led		68	07	78
Index no.	DH	646		Date	subm	Itted		17	07	78
well depth(ft)	31	87.2		Date	anal	ysed(r	nalor)	8	8	78
Noter level(ft)				Date	onal	ysed(n	ninor)			
Top open interval	(11)			Samp	led b	y		HACH	BAP	S1H
Bottom open inter				Samp	le So	urce			W F	ELL
Altitude(ft)				Owner	rs 118	n e		SHELL	,083	S∞7
Bedrock elevation	(fe)			Herdr	ness(as Ça(:03)		119	-
TDS(mg/1)		42.0		Alka	linit	y(as (C033)		275	-
Field Condimicrom	hos/cm)			Cond	(mlar	omhosi	'cm025	C)	36	130
Field pH		8:4		Lab p	эΗ				7	.8

MAJOR CONSTITUENTS

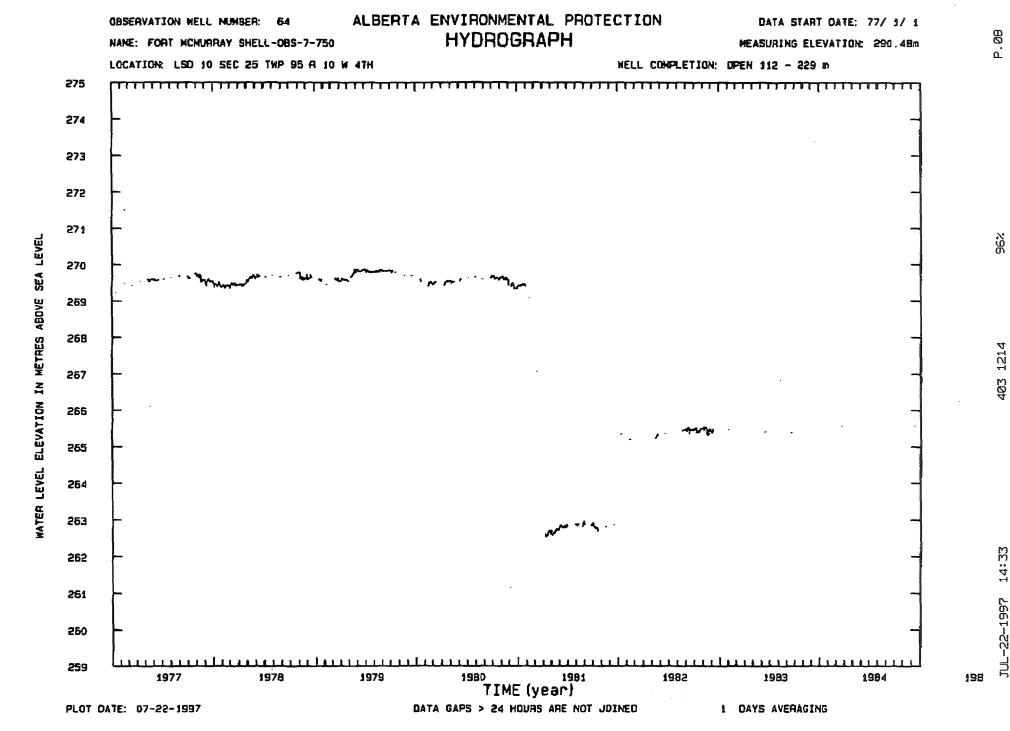
		2 01	fictal anion
	mp/1	neo/1	or cation
Calcium(Ca)	15.0	0,75	2.5
Magnesium(Mg)	20.0	1,65	5,5
Sodium(Na)	619.0	26,92	90.5
Potassium(K)	17.1	0,44	1.5
Carbonate(C03)	0,0	0.00	0,0
Bicerbonate(HCDJ)	344.8	5,64	17.7
Sulphate(S04)	36.3	0,76	2.4
Chloride(C))	905.0	25,52	79,9
Nitnate(NO3)	1.7	0.03	0,1
Hydroxide(0H)			
Silica(SiD2)	1.2	Total anions(epm)	31,943
Calcium (Acid)	14.4	Total cations(epm)	29,757
Magnesium(Acid)	18.7	lon balance error(%)	4.
Calculated TD5	1784.4	TDS belance error(%)	2.

MINOR CONSTITUENTS

Aluminum	0.04	ppm
Cooper	Ø	DDD
Iodine	И.03	DDM
Iron	B	ppm
Lead	0	opb
Monganese	6,03	₽p M
Mercury	0.52	opb

		OTHER ME	EASUR	REMENTS	
Field	Temp(C)	6.00		Fluoride(F)	1,00 ppm
Field	Carbonate(CO3)	14	ppm		
Field	Bicarbonate(HC03)	307	ppm		

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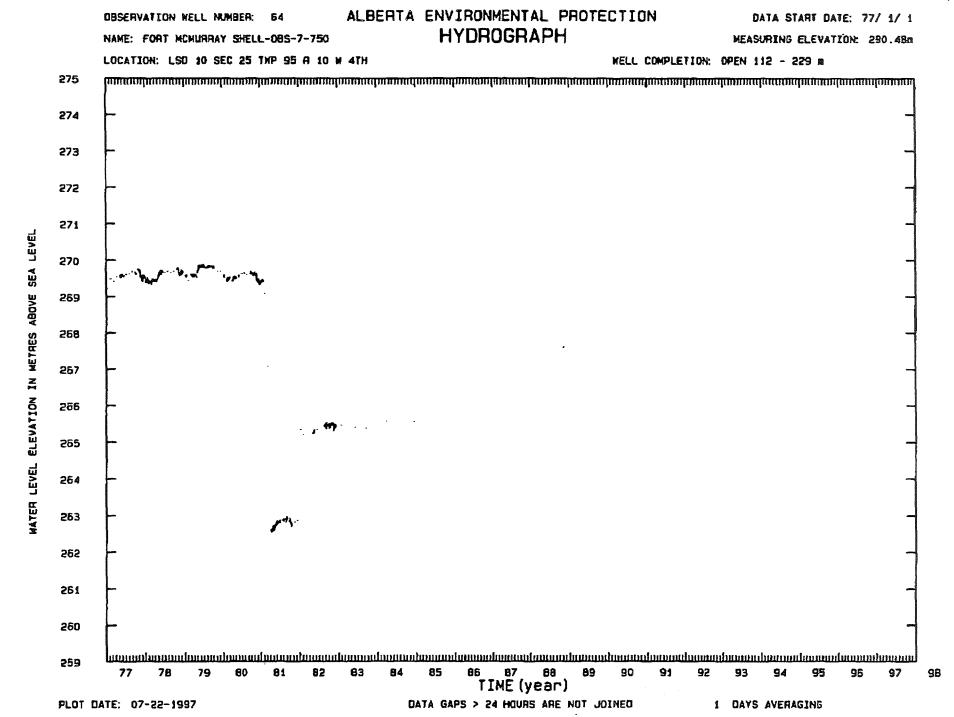
ND.876

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ALBERTA ENVIRONMENTAL PROTECTION

COMPUTER GENERATED WATER WELL DRILLER'S REPORT FORM WELL 1.D. 233959 THIS DATA MAY NOT BE FULLY CHECKED; THE PROVINCE DISCLAIMS ALL RESPONSIBILITY FOR ITS ACCURACY: Page 1 of 2

CONTRA	CTOR:		WELL OV	WNER:			WELL	LOCATIC	DN:	IC#:	02
							V. OR LSD	SEC	TWP	RGE	W MER
NAME: UN	KNOWN DRILLER		NAME: PETI	-QPINA*	\$1J-2		01	10	096	11	W4
ADDRESS:			ADDRESS:					I VERIFICAT	ION METH	10D: FIELD	, ,
LICENCE N	O.: JOURNEYMAN NO.:		POSTAL COD	I:		****	LOT:	BLOCK:		LAN:	
FORMAT	ON LOG DESCRIPTION:	DRIL	LING METHO	D:	UNKNOWN		WELL ELEV:	942.	Feet H	w obtain: E	STIMATED
Ground to:		TYPE	OF WORK:	NEY	WELL		PRODUCT	TON TES E: March			T TIME:11:0
100	Qverburdan	FLOW	WING WELL:	No	RATE:		Eloneod .	Danth In	Water	Danti	to Water
	Unknawn	GASP	RESENT: NO)	OIL PRESENT:	No	Time in Min:Sec	Level During	Pumping	Level Duri	ing Recovery Feeti
112	Tarsand		OF ABANDONMI FIAL USED:	ENT:			3:00	172.	42		
171			POSED USE:	OBS	ERVATION		5:00	172.	82		
178	Clay		NELL COMPL	FTION	I DATA.	an a	7:00	173.	02		
193	Tarsand		-				10:00	173.	44		
207	Gray Clay		LL FINISH: TAL HOLE DEPT		EN & OPEN HOLE		12:00	173.	67		
227	Tersand		IAL HULE DEPT	n; JU2	rdei		15:00	173.			
239	Gray Clay	CA	SING TYPE: UN	KNÓW	'N		20:00	174.			~~~~~
	Tarsand		E OD:		WALL THICKNESS:	Inch	25:00	174.			
259	Chay		TTOM AT:		Feet		30:00 35:00				
275		PERFC	RATED CASING	JUNEA:			40:00	174.			
278	Tersand	TYF	PE:				60:00	175.			<u></u>
282	Olay	SIZ	E OD:	inch			60:00	175.			
308	Water Bearing Sand	WA	LL THICKNESS:		Inch		70:00	175,	73		
374	Unknawn		PAT: 0	Feel	BOTTOM AT:	Feet	80:00	176.	07		
	Water Bearing Sand	PEF	PFORATED FROM	V :	Feet TO: Feet TO:	Feet Feet	90:00	176.	23		
322	ปกไตาอิพา				Feet TO:	Feet	104:00	176.	34		
329					inch X	inch	110:00	178.	57		
837	Gray Clay		E OF PERFORAT		inch X	Inch	120:00	176.	74		
344	Water Bearing Sand	SEAL					135:00	176.			
352	Gray Clay		ERVAL TOP:	0	Feet TO:	Feet	150:00	177.			
359	Green Clay	1	HYSICAL LOG T	-			185:00	177.			
			NED ON FILE:				180:00 240:00	177. 178.			
		SCRE	en:				270:00	178.			
		MA	TERIAL: UI	VKNOV	VN		300.00	178,			
		SIZ	E ID (CLEAR):	1	nch SLOT SIZE:	inch	330:00	179,			
		INT	ERVAL TOP:		Fest TO:	Feet	360:00	179,	22		
					Feet TO:	Foot	395:00	179.	50		
			TALLATION MET	HOD:			420:00	179.	79		
		-	P FITTINGS:					EMOVAL RA			33 Gal/Min
		4	TTOM FITTINGS				TEST DUP	iation: Method: /	24 H PUMP	lours	0 Minutes
			TYPE: NATUR				DEPTH O	PUMP/DRI	LL STEM:	r. 11	Fee: 93.1 Fee:
		GH.	AIN SIZE:	,	MOUNT:		NON-PUM	PINGISTAT	IC) WATER	ILEVEL:	165.0 FEE
								AWDOWN:			18 Fee
			LESS ADAPTER OP PIPE TYPE:	TYPE:	LENGTH:	Fest	AECOMM	ENDED PUN ENDED PUN	AP INTAKE		Gal/Min Feet
				INFORM	OIAMETER: ATION:	Inch	MODEL:	UMP INST.	ALLED:	H.P.;	
DATE WC	ORK STARTED: January				OMMENTS:						
DATE WC	ORK COMPLETED: February				lines printed)						
	TA RECEIVED:		(.		· ····································						
	L TEST AND/OR PUMP DATA:										
CHEMISTR	IES TAKEN: N HELD: 3	DO	CUMENTS HELD); 14							
WELL OWN	IER'S ANTICIPATED WATER REQU	IREMEN	TS PER DAY:								
TE FORM	PRINTED: July 21, 1997	74.	:25:37 DATE	DATA	EVED: March 4	, 1994	DATA	GWICDA	TA\GIC4	. /	MM

ALBERTA ENVIRONMENTAL PROTECTION

COMPUTER GENERATED WATER WELL DRILLER'S REPORT FORM WELL I.D. 233959 THIS DATA MAY NOT BE FULLY CHECKED; THE PROVINCE DISCLAIMS ALL RESPONSIBILITY FOR ITS ACCURACY: P398 2 of 2

CONTRACTOR:		WELL OWNER	R:			WELL	LOCATIO	DN:	IC#:		
NAME: UNKNOWN DRILLER		NAME: PETROFINA#79-2					SEC	TWP	RGE	W. M	R
		ADDRESS:				01	01	096	11	W	4
ADDRESS:		NUMEUS,				LOCATION	N VERIFICAT	LION METI ER:	1		لـــ
UCENCE NO.: JOURNEYMAN NO.;		POSTAL CODE:		LOT:	BLOCK	: F	LAN:				
FORMATION LOG DESCRIPTION: Depth (Feet): Linalogy:	DRILL	ING METHOD:				WELL ELEV:			w obtain:		
Ground to:	TYPE	of work:				PRODUCT	TION TES TE: March		STA	RT TIME:	1:1
	GAS PF	ING WELL: RESENT:	1	RATE: OIL PRESENT:		Elopsed Time in Min;Sec	Depth to Level During (Feel	Water Pumping	Dapi Level Du		
		DF ABANDONMENT: IAL UGED:				480:00	780.				
		OSED USE:				540:00	180.	32			
	N		OND	ATA:		BOD:OD	180 .	57			
						660:00	180.				
		L FINISH: AL HOLE DEPTH:		Fest		720:00	181.				
] ''''					840:00	781.				
	CAS	ING TYPE;				860:00	781.				
		OD: Inch	WA	LL THICKNESS:	Inch	1080:00	182.				
	801	TOM AT:	Fee	ət		1200:00	182.				******
	PERFO	RATED CASINGUNE	ea:			1320.00	183.	13			,
	түрі	E:				<u>├</u>				····	
	SIZE	OD: Inc	ch								
	WAL	L THICKNESS:		Inch		Ì					
	TOP		iet BO	TTOM AT:	Feat						
	PER	FORATED FROM:		Feet TO: Feet TO:	Feat Feat						
				Fest TO:	Feet						
			-		1						
		OF PERFORATIONS	5:	Inch X	Inch						
	SEALT	V PERFORATED:									
	1	FIVAL TOP:	For	et TO:	Feet						
	GEOPH	IVSICAL LOG TAKEN IED ON FILE:									
	SCREE										
		ERIAL:									_
		ID (CLEAR):	inch	BLOT SIZE:	Inch					- · · · · · · · · · · · · · · · · · · ·	
		RVAL TOP:	For	et TO:	Fest	·					
			Fee	at TO:	Feet	<u>├</u> }				·	
	INST	ALLATION METHOD	Ŀ			<u> </u>			•		
	TOP	FITTINGS:				WATER RI	EMOVAL RA	TE DURIN	G TEGT:	33 Ga	Mi
	вот	TOM FITTINGS:				TEST DUP	METHOD:	24 +	lours	0 Min	
	PACKT	YPE:				DEPTH OF	PUMP/DRI	LL STEM:			Fee
	GRA	IN SIZE:	AMC)UNT:		NON-PUM	VEL AT ENI				Fee
	PITI	ESS ADAPTER TYPE			<u>-</u> ,		AWDOWN:	PINGRAT	۴۰	18 Gal/	Fee
		P PIPE TYPE:		LENGTH: DIAMETER:	Feet Inch	RECOMM	ENDED PUN	AP INTAKE	AT:	Fee	
	ADD	ITIONAL PUMP INFO	RMAT		+, 1¥** *	MODEL:			H.P.;		
DATE WORK STARTED:				AMENTS:							
DATE WORK COMPLETED: DATE DATA RECEIVED:		(Maximum c	of 8 lini	ee printed)							
ADDRONAL WROW ALIDIAN CLUB CAR											
ADDITIONAL TEST AND/OR FUMP DATA:	~~~	LINELTO LIME A.									
ADDITIONAL TEST AND/OR PUMP DATA: CHEMISTRIES TAKEN: HELD: WELL OWNER'S ANTICIPATED WATER REQUI		UMENTS HELD:									

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RESEARCH COUNCIL OF ALBERTA WATER ANALYSIS REPORT

Mer 4 To	96 Rge 11	Sec 1 Lad 1	S 11 11
	T 1	Dete sampled	D M V 30 3 74
Lab no.	T 1	Date submitted	2 4 7 4
Field temp	4.0	Date analysed(major	
Field pH	486	Date analysed(minor	
Field Cond(micromhos/	:m) 4000		KBARTH
Field Bizarbonate(HCO)		Sample Source PUMP	TEST 3.5 HR
Well deoth(ft)	330.0	TDS(pom)	2506.0
Koter level(ft)	165.0	Hardness(as CaCO3)	142.6
Top open interval	318.0	Alkalinity(as CaCO3	
Bottom open interval	330,0	Cond(micromhos/cm#2	
Altitude		Lab pH	7.7
Bedrock elevation			
Queers name PETROF!	INA 73-2		
•	MAJOR CONSTI	ITUENTS	
			of total anion
	PDM .	epm	or cation
Calcium(Ca)	30.8	1.54	3.3
Magnes(um(Mg)	16.0	1.32	2.5
Spdlum(Na)	981.0	42,66	91.9
Potassium(K) Carbonate(CO3)	36.0	0,00	2.0 0.0
Bicarbonate(HCO3)	0.0 2130,8	34.92	74 <u>4</u>
Sulphate(SO4)	7.0	0.15	6.3
Chlaride(C1)	420.0	11.85	25.2
Ntrate(ND3)	0.5	0.01	0.0
Phosphate(P205)	- • •		
5111co(S102)			
		Total anions(epm)	46.919
		Total cations(apm)	46.431
		Anions:Cations(com)	
		TDS balance	1,318
	MINOR CONSTI	ITUENTS	
	nqq		<u>ê ê m</u>
Aluminium(Al)	0,150	Iron Total(Fo)	0.340
Antimony(Sb)		Lithium(Li)	
Arsenic (As)		Lead(Pb)	0.00520
Barlum(Ba)		Manganese(Mn)	0.150
Boron(B) Bromide(Br)		Mercury(Hg) Nitrogen(N)	0.00008
Chromium hex.(Cr)		Selenium(Se)	
Cobalt(Co)		Stront(um(Sr)	
Copper(Cu)	0.00290	Tin(Sn)	
Fluoride(F)	1.300	Vanadium(V)	
Hydroxide (OH)		Zinc(Zn)	
lodide(I)	0.080		

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96%

IC.02 P.06

RESEARCH COUNCIL OF ALBERTA WATER ANALYSIS REPORT

Mer 4 Tp	96 Rge 11	Sec 1 Lod 1	DMY
	5	Date sampled	31 3 74
Lab no.	i c	Date submitted	2 4 74
Field temp	3.8	Date analysed(major	
Field pH	090	Date analysed(minor	
Field Cond(micromhos/c	m) 4030		KBARTH
Field Blearbonate(HC03		Sample Source PUMP	TEST 22 HR
Well depth(ft)	330.0	TDS(ppm)	2424.0
Water level(ft)	165.0	Hardness(as CaCO3)	128,9
Top open interval	318.0	Alkalinitv(as CaCO3	
Bottom open interval	330.0	Cond(micromhos/cme2	
Altitude		Leb pH	8.0
Bedrock elevation			
Owners name PETROFI	INA 73-2		
	MAJOR CONSTI		
			of total anion
	DDM	epm	or cation
Calcium(Ca)	26.3	1.31	3.0
Magnesium(Mg)	15.4	1.27	85° 0 5°8
Sodium(Na)	931.0 36.0	40.48 0.92	2.1
Potassium(K) Carbonate(CO3)	0.0	0.00	0.0
Bicarbonate(HCO3)	2111.3	34.60	75.6
Sulphate(\$04)	10,0	0.21	Ø,5
Chloride(Cl)	388.0	10.94	23.9
Nitrate(NO3)	0,7	0.01	0.0
Phosphate(P205)	- • •		
S111ca(S102)			
		Total anions(epm)	45.762
		Total cations(com)	43.983
		Anions:Cations(com)	
		TDS balance	0.068
	MINOR CONSTI	TUENTS	
	DDM		p p m
Aluminium (Al)	0.120	Iron Total(Fe)	0.150
Antimony (Sb)		Lithium(Li)	
Arsenic (As)		Lead(Pb)	0.00620
Barium(Be)		Manganese(Mn)	0.150
Boron(B)		Morcury(Hg)	0.00010
Bromide(Br)		N(trogen(N) Relandum(Se)	
Chromium hex.(Cr) Cobait(Co)		Selenium(So) Strontium(Sp)	
Copper(Cu)	0.00650	Tin(Sn)	
Fluoride(F)	1,200	Vanad(um(V)	
Hydroxide(OH)	a 11 64 4 84		
Iodide(I)	0,080		
······································			

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96%
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: 	2.7	$\gamma_{i,Z}$	20	-) •	a .)		0	0	7414		aj e
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			(330	.3	141	.01	U	U	18.7	33.1	
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	1.9	41.2	1.0		- 6	40.5		0			26.4 49.	
4-9 4	9-3	2-4			.4	22.1		0	0			
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.04		38.8	30	2.2	190	5	• 8	1.10	48	0 •	0	9.6
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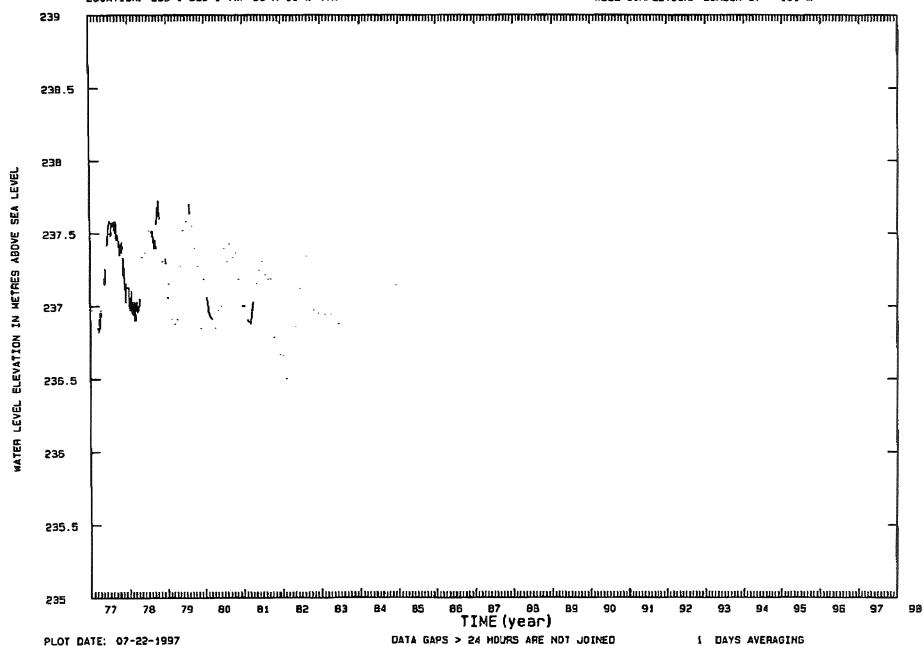


NAME: FORT MCMURRAY FINA-73-2-330

DATA START DATE: 77/ 1/ 1

NEASURING ELEVATION: 287.83m

WELL COMPLETION: SCREEN 97 - 101 m

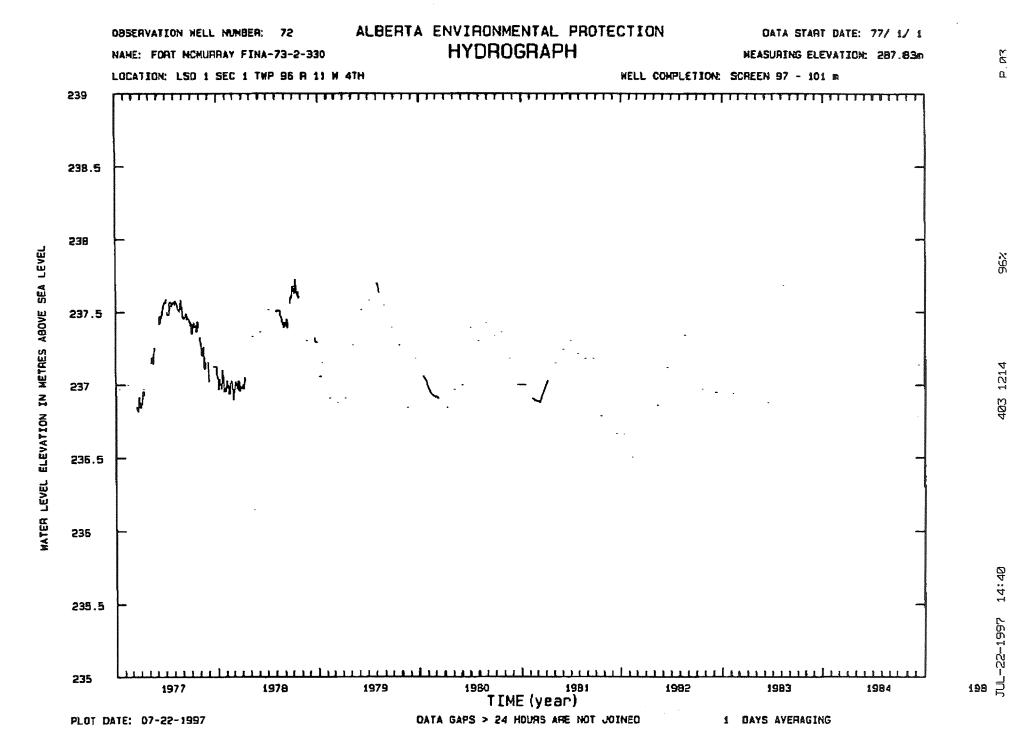


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96%

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