1	Characterization of cryobiological responses in TF-1 cells using interrupted freezing
2	procedures
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## 1 Abstract

2 Cryopreservation currently is the only method for long-term preservation of cellular viability and 3 function for uses in cellular therapies. Characterizing the cryobiological response of a cell type is 4 essential in the approach to designing and optimizing cryopreservation protocols. For cells used 5 in therapies, there is significant interest in designing cryopreservation protocols that do not rely 6 on dimethyl sulfoxide (Me2SO) as a cryoprotectant, since this cryoprotectant has been shown to 7 have adverse effects on hematopoietic stem cell (HSC) transplant patients. This study 8 characterized the cryobiological responses of the human erythroleukemic stem cell line TF-1, as 9 a model for HSC. We measured the osmotic parameters of TF-1 cells, including the osmotically 10 inactive fraction, temperature-dependent membrane hydraulic conductivity and the membrane 11 permeability to 1M Me2SO. A two-step freezing procedure (interrupted rapid cooling with hold 12 time) and a graded freezing procedure (interrupted slow cooling without hold time) were used to 13 characterize TF-1 cell recovery during various phases of the cooling process. One outcome of 14 these experiments was high recovery of TF-1 cells cryopreserved in the absence of traditional 15 cryoprotectants. The results of this study of the cryobiology of TF-1 cells will be critical for 16 future understanding of the cryobiology of HSC, and to the design of cryopreservation protocols 17 with specific design criteria for applications in cellular therapies.

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keywords: TF-1, osmotic properties, hydraulic conductivity, osmotically-inactive fraction,
solute permeability, cryopreservation, hematopoietic stem cells, dimethyl sulfoxide

### 1 Introduction

2 Cryobiology plays a key role in the long-term storage of native and engineered cells and 3 tissues for research and applications in many disciplines. Cryopreservation, which involves 4 storing cells and tissues at low subzero temperatures, is currently the only feasible method for the 5 long-term maintenance of biological structure and function. Success in cellular therapies often 6 depends critically on the number of functional cells transplanted, thus reviving interest in 7 maximizing cell survival and function during collection, processing, and preservation. As new 8 sources of cells are being explored, it is becoming clear that effective tools are required to 9 understand the cryobiology of these cells.

10 The survival of cells and tissues after freezing and thawing depends on the ability of the 11 cells to withstand a variety of stresses imposed by the cryopreservation protocol. As 12 extracellular ice forms during cryopreservation, there is a resulting increase in extracellular 13 solute concentration, which imposes osmotic stresses on the cell [41]. The osmotic response of 14 the cell is largely dependent on the movement of water across the plasma membrane [40]. The 15 movement of water across the membrane is the result of movement of water molecules by 16 diffusion through the membrane or through water channels (aquaporins). The osmotic 17 parameters governing the movement of water and cryoprotectants across the membrane are 18 specific to each cell type; thus the osmotic responses to anisotonic conditions are different for 19 different cell types. If a permeating cryoprotectant is present then both the net water and 20 cryoprotectant movements depend on the osmotic parameters of the cell membrane. Therefore, 21 measuring the osmotic parameters of the cell membrane is important to further understand the 22 cryobiology of a cell.

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Electronic particle counters have been used to measure cell volumes as a function of time

for cells exposed to anisotonic solutions [48]. In kinetic studies, sequential measurements of cell
volumes allow determination of cell permeability characteristics by fitting the experimental data
with theoretical models. Using this method, osmotic parameters have been determined for a
variety of cell types including: human lymphocytes [21]; bovine chondrocytes [47]; pancreatic
islet cells [31,61]; human corneal endothelial, stromal, and epithelial cells [9]; several African
mammalian spermatozoa [17]; and HSC [16,22,60].

7 In addition to characterizing cellular osmotic responses, exploring how freezing results in 8 cell damage, is also critical. Mazur *et al.*'s "two-factor hypothesis" of freezing injury [33,37] 9 proposes that there are two independent mechanisms of damage during freezing: injury during 10 slow cooling, where cell injury is caused by exposure to high solute concentrations as water in 11 the extracellular solution is converted to ice; and injury during rapid cooling, where cell injury is 12 related to the presence of intracellular ice [38,41]. Maximum survival is normally obtained by 13 selecting a cooling rate that is sufficiently high to avoid the injury from exposure to the 14 concentrated solutes, yet low enough that the cells can osmotically dehydrate to avoid 15 intracellular ice formation. This approach almost always requires a cryoprotectant, such as 16 Me<sub>2</sub>SO. Like other permeating cryoprotectants, Me<sub>2</sub>SO protects the cell primarily against slow 17 cool injury by reducing the amount of ice formed at any temperature, hence reducing the 18 concentrations of other solutes and injury related to exposure [67]. There are, however, 19 drawbacks to using cryoprotectants in cryopreservation of clinical samples, which include 20 cellular osmotic stress during addition and removal, toxicity to cells during processing and 21 preservation, and transplant-related toxicity for the patient. A better understanding of the 22 nature and kinetics of cellular responses to temperature-induced conditions would allow novel 23 approaches to the cryopreservation of new cell types.

1 In most practical cryopreservation procedures, cells are typically cooled to a low 2 temperature (e.g. -80°C); the process being empirically optimized for cell type by varying 3 cooling rate and cryoprotectant type and concentration to minimize cryoinjury. However, it has 4 long been known that there are critical subzero temperature ranges where interrupting the 5 cooling process improves cell recovery [35]. There are two procedures specifically designed to 6 explore cryoinjury by separating damage which occurs during the initial cooling to this critical 7 temperature range, during time spent in this temperature range itself, and during subsequent 8 cooling to storage temperatures. These two procedures are two-step freezing (interrupted rapid 9 cooling with hold time) [14] and graded freezing (interrupted slow cooling without hold time) 10 [44].

11 The two-step freezing procedure, used by Farrant et al. is a logical method to examine the 12 effects of interrupted rapid cooling on cell recovery over a broad range of subzero temperatures 13 and conditions. Using this procedure [14], human lymphocytes were cooled rapidly to various 14 subzero temperatures and held for various periods of time before being either (a) thawed directly 15 from that holding temperature or (b) rapidly cooled to -196°C (liquid nitrogen) before thawing 16 (see schematic - Figure 1a). This two-step freezing procedure is uniquely different from 17 previous procedures using interrupted cooling as it also includes a separate analysis of damage 18 which occurs during the initial cooling to the hold temperature. In further studies, McGann and 19 Farrant reported that subzero temperature and the length of hold time at that temperature were 20 important factors affecting cell survival [45]. McGann also used two-step freezing to explore the 21 differing actions of penetrating and non-penetrating cryoprotectants and for the cryopreservation 22 of Chinese hamster fibroblasts with 20 % HES; with cell recovery comparable to 10 % Me<sub>2</sub>SO 23 [43]. It should be noted that the two-step procedure [14] is a modification of previously reported

1 procedures [2,54,57], which did not include the direct thawing step from the hold temperature.

2 A variation of the two-step freezing procedure, the graded freezing procedure, was used by 3 McGann to investigate progressive cell injury during slow cooling [44]. In this procedure, 4 samples were cooled at a low linear rate to various subzero temperatures before being either (a) 5 thawed directly or (b) rapidly cooled to -196°C (liquid nitrogen) before thawing. The difference 6 between the two-step and graded freezing procedures is that two-step freezing uses interrupted 7 rapid cooling with a hold step at an intermediate temperature, while graded freezing uses 8 interrupted slow cooling to an intermediate temperature, without a hold step (see schematic 9 - Figure 1b). Both approaches allow separation of damage which occurs during the initial 10 cooling phase from that which occurs during subsequent cooling to the storage temperature.

11 Although HSCs are routinely cryopreserved for clinical use using dimethyl sulphoxide 12 (Me<sub>2</sub>SO), this cryoprotectant is associated with morbidity and mortality in some HSC transplant 13 patients [7,8,11,56,68] and contributes to osmotic stresses for stem cells [60]. As with other cells 14 used in therapies, it would be beneficial to eliminate Me<sub>2</sub>SO from the cryopreservation protocol. 15 TF-1 cells have been used as a model cell type for hematopoietic stem cells (HSC). These cells 16 express the CD34+ antigen and are able to differentiate into the various hematopoietic lineages 17 [28,29,36], and as such have been used in various studies [4,5,30,36]. This study explores the 18 cryobiology of TF-1 cells, a model for HSCs, by examining cryoinjury during interrupted rapid 19 cooling and interrupted slow cooling procedures. Specifically, this study will use two-step 20 freezing and graded freezing procedures to characterize the cryobiological responses of TF-1 21 cells.

22 Experimental materials and methods

23 TF-1 cell culture

1 TF-1 cells ((Lot #2056376) ATCC, Manassas, Virginia) were cultured at 37 °C in 5 % 2 CO<sub>2</sub> in Modified RPMI 1640 Medium (ATCC) with 10 % fetal bovine serum (ATCC), and 3 supplemented with 2 ng/mL recombinant human GM-CSF (Stemcell Technologies, Vancouver, 4 Canada). Prior to experiments, cells were washed twice with serum-free RPMI media and 5 incubated in serum-free RPMI overnight to accumulate the cells in the  $G_1/G_0$  phase of the cell 6 cycle [30], resulting in a more uniform cell size distribution. Cells were then centrifuged and re-suspended in serum-free RPMI (4 x  $10^6$  cells/mL) prior to experiments. Serum-free media 7 8 was chosen for experiments in order to compare experimental results with and without different 9 types of cryoprotectants.

10 *Cell volume measurements* 

A Coulter Electronic Particle Counter (ZB1, Coulter Inc., Hialeah, Florida), fitted with a
pulse-height analyzer (The Great Canadian Computer Company, Spruce Grove, AB, Canada)
was used to monitor cell volume as a function of time as cells passed through the 100 μm
aperture [18-20,48]. This system has been previously used to monitor changes in cell volume for
a variety of cells in suspension [3,9,21,31,61], including HSC [16,59].

16 TF-1 cells (150-200 µL) were injected into well-mixed hypertonic experimental solutions (10 mL) at experimental temperatures that were maintained using a circulating water bath and a 17 18 custom insulated jacket. Pulse heights, proportional to the cell volumes, were digitized and the 19 time recorded as each cell traversed the aperture of the Coulter counter [48]. The upper and lower volume limits were  $1750 \pm 1 \ \mu m^3$  and  $218 \pm 6 \ \mu m^3$ , respectively. 20 There was 21 approximately 2 % coincidence correction for the cell density used in the experiments [6]. 22 Various concentrations of phosphate-buffered saline ((PBS) GIBCO Invitrogen Corp., Carlsbad, 23 California) were prepared by diluting 10X PBS (GIBCO) with distilled water to final

osmolalities of 291 ± 6 (1X), 583 ± 25 (2X), 861 ± 22 (3X), 1150 ± 17 (4X) and 1434 ±
20 mOsm/kg (5X) respectively (mean ± sd of 16 replicates). Volume measurements to
determine the permeability of Me<sub>2</sub>SO used Me<sub>2</sub>SO (Sigma, Missisauga, Canada) in 1X PBS for a
final concentration of 1 M Me<sub>2</sub>SO. Osmolalities were measured using a freezing-point
depression Osmometer (Precision Systems Inc., Natick, Massachusetts), calibrated using 100,
300 and 500 mOsm/kg osmometry standards (Precision Systems Inc.).

7 For PBS solutions, the experimental temperatures were  $4.8 \pm 0.1$ ,  $12.9 \pm 0.3$ ,  $23.3 \pm 0.2$ , 8 and  $37.4 \pm 0.1$  °C (2-5X PBS data pooled mean  $\pm$  sem; n=36) and  $4.6 \pm 0.2$ ,  $8.0 \pm 0.2$ ,  $11.0 \pm 0.2$ , 9  $16.3 \pm 0.2$ ,  $19.4 \pm 0.3$ , and  $28.8 \pm 0.2$  °C (3X PBS data mean  $\pm$  sem; n=9). The temperatures 10 were measured immediately following data acquisition while still in the insulated jacket using a 11 Digi-Sense thermocouple thermometer (Cole Parmer, Anjou, Canada). For Me<sub>2</sub>SO experimental 12 solutions, 3 temperatures were investigated:  $4.9 \pm 0.3$ ,  $10.7 \pm 0.4$ , and  $23.4 \pm 0.5$  °C. For each 13 experiment, 3 replicate measurements were performed for each solution at each temperature. 14 The experiments were repeated a minimum of 3 times using cells from different passages. Latex 15 beads (15 µm diameter; Beckman Coulter, Miami, Florida) were used as calibrators to convert 16 pulse heights to actual volumes in 1X PBS and in the experimental solutions.

17 *Cell permeability parameters* 

## 18 <u>Osmotically-inactive fraction</u>

19 Cellular osmotic parameters relevant to cryopreservation are the osmotically-inactive 20 fraction, hydraulic conductivity, and solute permeability for permeating cryoprotectants and 21 activation energies. The osmotically-inactive fraction (*b*) of the cell is the fraction of the cell 22 volume not involved in the osmotic activities. The Boyle van't Hoff relationship [34] has been 23 used to express equilibrium cell volume in solutions of impermeant solutes:

$$\frac{V}{V_o} = \frac{\pi^o}{\pi} (1-b) + b \tag{1}$$

1 where *V* is the equilibrium cell volume ( $\mu$ m<sup>3</sup>), *V<sub>o</sub>* is the isotonic cell volume ( $\mu$ m<sup>3</sup>),  $\pi^o$  is the 2 isotonic osmolality (osmoles/kg water),  $\pi$  is the experimental osmolality (osmoles/kg water), 3 and *b* is the osmotically-inactive fraction of the cell volume, a parameter found by fitting Eq. 1 to 4 data.

#### 5 <u>Hydraulic conductivity</u>

Jacobs and Stewart [24,25] used the following equation to describe the rate of water
movement across the plasma membrane :

$$\frac{dV}{dt} = L_p ART (\pi_i - \pi_e)\rho$$
<sup>(2)</sup>

where V is the volume of the cell ( $\mu m^3$ ), t is the time (min),  $L_p$  is the hydraulic conductivity 8  $(\mu m^3/\mu m^2/min/atm)$ , A is the cell surface area  $(\mu m^2)$ , R is the universal gas constant 9 ( $\mu m^3 \cdot atm/mol/K$ ), T is the absolute temperature (K),  $\pi_e$  is the extracellular osmolality 10 (osmoles/kg of water),  $\pi_i$  is the intracellular osmolality (osmoles/kg of water), and  $\rho$  is the 11 density of water (assumed to be constant at  $1.0 \times 10^{-15} \text{ kg/}\mu\text{m}^3$ ). Experimental measurements of 12 13 cell volume as a function of time in the presence of an impermeant solute were fit to Eq. 2, with 14 the following initial conditions: i) the intracellular solution was at isotonic concentration and the 15 extracellular solution was at the experimental concentration; ii) the cell volume was calculated 16 from the Boyle-van't Hoff equation (Eq. 1). The differential equation Eq. 2 was integrated 17 using Euler's method with sufficiently small discretization in EXCEL (e.g. time increment approximately 8 x 10<sup>-4</sup> min). Experimental data were fit to the differential equation solutions 18 using the least squares method (EXCEL Solver) to estimate a best fit value for  $L_p$ . 19 The

assumptions used in these calculations are: i) intracellular and extracellular solutions are dilute,
 so the values of osmolality and concentration are the same; ii) the density of water is 1 g/mL; and
 iii) the cell surface area was calculated from the spherical cell volume.

4 <u>Solute permeability</u>

Jacobs and Stewart coupled Eq. 2 with the following equation to describe the volumechanges and solute movement across a membrane as a function of time:

$$7 \qquad \qquad \frac{dS}{dt} = P_s A \left( C_s^e - C_s^i \right) \rho \tag{3}$$

where S is the number of solute molecules (mole),  $P_s$  is the solute permeability ( $\mu m^3/\mu m^2/min$ ), 8 9  $C_s$  is the solute concentration (molal), the superscript *e* denotes extracellular, and the superscript 10 *i* denotes intracellular. In the presence of a permeant solute, experimental data were fit to Eqs. 2 11 and 3 using the following conditions: i) the initial conditions were that the intracellular solution 12 was at isotonic concentration, containing no permeant solute; and ii) the experimental conditions 13 were that the extracellular solution consisted of the permeant solute at the experimental 14 concentration and an impermeant solute at the isotonic concentration. The differential equation 15 Eq. 3 was integrated using Euler's method with sufficiently small discretization in EXCEL, and 16 the experimental data were fit using the least squares method (EXCEL Solver) to estimate either 17  $P_s$  or both  $P_s$  and  $L_p$ .

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### 19 <u>Temperature dependencies of permeability parameters</u>

Also relevant to cryopreservation are the temperature dependencies of  $L_p$  and  $P_s$  which are normally described with Arrhenius relationships [53]:

$$L_p = L_p^o \exp\left(-\frac{E_a^{Lp}}{R}\left(\frac{1}{T} - \frac{1}{T_o}\right)\right)$$
(4)

$$P_s = P_s^o \exp\left(-\frac{E_a^{P_s}}{R}\left(\frac{1}{T} - \frac{1}{T_o}\right)\right)$$
(5)

1 where  $L_p^o$  and  $P_s^o$  are the reference water and solute permeabilities, respectively, at the 2 temperature  $T_o$ ,  $E_a$  are the Arrhenius activation energies (kcal/mol), R is the universal gas 3 constant (kcal/mol/K), and T is the absolute temperature (K). The Arrhenius activation energies 4 for  $L_p$  or  $P_s$ , described by Eqs. 4 and 5 respectively, were determined by fits using linear 5 regression of the natural logarithm of  $L_p$  or  $P_s$  as a function of the inverse absolute temperature.

#### 6 Statistical analysis

7 Statistical comparisons used a standard two-way analysis of variance (ANOVA) (p=0.05 level of significance) for estimates of  $L_p$  and b respectively between the 4 groups of experimental 8 9 temperatures and PBS concentrations, including evaluation of interactions between these 10 parameters. A one-way ANOVA (p=0.05) was used to further evaluate statistical differences between temperatures for L<sub>p</sub>. Due to small sample size, a Kruskal-Wallis non-parametric 11 12 statistical test (p=0.05) was used to compare estimates of  $P_s$  when solved for separately from  $L_p$ , with estimates of  $P_s$  when solved for simultaneously with  $L_p$ . For all mean values reported, the 13 14 standard error of the mean was also calculated and included in the result (i.e. mean  $\pm$  sem).

15 *Two-step freezing procedure (interrupted rapid cooling with hold step)* 

Samples of 0.2 mL TF-1 cell suspension in serum-free RPMI were transferred to glass
tubes (6x50 mm; Fisher, Edmonton, Canada) and allowed to equilibrate at room temperature for
5 min. Control samples were either warmed in a 37 °C water bath or plunged directly into liquid
nitrogen. Experimental samples were individually transferred into a stirred methanol bath

1 (Kinetics Thermal Systems, New York, USA) preset at -3, -6, -9, -12, -15, -20, -30, or -40 °C 2 and allowed to equilibrate for 2 min at that temperature prior to ice nucleation with cold forceps. 3 After nucleation, samples were held at the experimental temperature for 3 min before either 4 thawing in a 37 °C water bath or plunging into liquid nitrogen. Plunge samples were stored in 5 liquid nitrogen for a minimum of 1 hour prior to thawing in a 37 °C water bath. Sample 6 temperatures were monitored throughout the experiments using a Type T thermocouple. 7 Experiments were also performed using different hold times. Samples were cooled to various 8 experimental hold temperatures (-5, -7, -9, -12, -25 °C), nucleated with cold forceps, and held for 9 0.5, 0.7, 1, 2, 3, 5, 7 or 10 min. Duplicate samples were used for each experimental 10 measurement and each experiment was repeated in triplicate with cells from different passages. 11 Samples cooled to hold temperatures of -20, -25, and -30°C spontaneously nucleated prior to 12 reaching the hold temperature; however time zero for all experimental samples was calculated as 13 time after nucleation.

### 14 Graded freezing procedure (interrupted slow cooling without hold step) no cryoprotectant

15 Samples of 0.2 mL cell suspension in serum-free RPMI were transferred to glass tubes 16 and cooled in a 0 °C wet ice bath for 5 min. Control samples were removed and either warmed 17 in a 37 °C water bath or plunged into liquid nitrogen. Experimental samples were transferred 18 into a methanol bath (FTS Systems, Inc., Stone Ridge, New York) preset at -3 °C and allowed to 19 equilibrate for 5 min prior to ice nucleation in each tube with cold forceps. The bath was then 20 cooled at 0.9 °C/min, and the temperature monitored using a Type T thermocouple (Omega, 21 Laval, Canada). At each experimental temperature (-3, -6, -9, -12, -15, -20, -30, and -40 °C), one 22 set of duplicate samples was thawed directly in a 37 °C water bath and another set was plunged 23 into liquid nitrogen. Plunge samples were kept in liquid nitrogen for a minimum of one hour prior to being thawed in a 37 °C water bath. Duplicate samples were used for each experimental
 temperature. Other experiments used cooling rates of 0.2 and 0.5 °C/min. Each experiment was
 repeated in triplicate with cells from different passages.

4 *Graded freezing procedure with* Me<sub>2</sub>SO

5 Samples of 0.2 mL cell suspension in 10 % Me<sub>2</sub>SO in serum-free RPMI at room 6 temperature were transferred to glass tubes and placed in a 0 °C ice bath for 5 min. Control 7 samples were removed and either warmed in a 37 °C water bath or plunged into liquid nitrogen. 8 Experimental samples were transferred into a methanol bath preset at -3 °C and allowed to 9 equilibrate for 5 min prior to ice nucleation with cold forceps. Although this temperature is 10 slightly above the predicted freezing point of this solution, the presence of ice crystals was 11 verified by visual examination at the end of the hold time. After 5 min, the bath was cooled at 12 0.9 °C/min. At each experimental temperature (-3, -6, -9, -12, -15, -20, -30, and -40 °C), one set of duplicate samples was thawed directly in a 37 °C water bath and another set was plunged into 13 14 liquid nitrogen. Plunge samples were kept in liquid nitrogen for a minimum of one hour prior to 15 being thawed in a 37 °C water bath. Duplicate samples were used for each experimental 16 temperature. Each experiment was repeated in triplicate with cells from different passages.

17 Assessment of cell recovery

Membrane integrity is widely used as an indicator of cryoinjury to cells, and there is evidence that the plasma membrane is a primary site of freezing-thawing injury [1,39]. Although not a rigorous test of cell function, the membrane integrity assay indicates the upper limit for cell viability. In these studies, the membrane integrity assay was performed by incubating cells with SYTO® 13 (Molecular Probes, Eugene, Oregon) and ethidium bromide (EB) (Sigma, Mississauga, Canada) [64]. SYTO® 13 (SYTO) permeates the cell membrane of all cells, complexes with DNA, and fluoresces green under UV exposure. Ethidium bromide penetrates
 cells with damaged plasma membranes and also complexes with DNA fluorescing red under UV
 conditions.

4 The SYTO/EB stain was prepared daily from 1X phosphate-buffered saline (PBS) and 5 stock solutions, which were stored at 4 °C (EB) and at -20 °C (SYTO). Final concentrations 6 were 0.25 mM EB and 0.125 mM SYTO. Twenty µL of stain was added to 200 µL of cell 7 suspension, mixed, and incubated for 2 min at room temperature. Fluorescent images were 8 captured using a Leitz Dialux 22 fluorescence (440-480nm) microscope (Leitz, Wetzlar, 9 Germany) fitted with a PIXERA Viewfinder Pro digital camera (Pixera Corporation, Los Gatos, 10 CA, USA). A viability assessment program (The Great Canadian Computer Company, Spruce 11 Grove, Canada) was used to quantify cell membrane integrity from digital images [26].

12 Results

13 *Isotonic cell volume* 

14 Synchronizing TF-1 cells in the  $G_0/G_1$  phases of the cell cycle resulted in a narrow log 15 normal distribution [6,12], with a mean isotonic volume 916 ± 15 µm<sup>3</sup> (mean ± sem) from 16 replicate samples. The width of the distribution was 916 ± 35 (± sd of the distribution),

17 Osmotic parameters (b,  $L_p$ ,  $E_a^{Lp}$ )

Figure 2 shows representative plots of mean cell volume as a function of time after exposure of TF-1 cells to 3X PBS at 4 different temperatures. Values for the osmotically-inactive fraction (*b*) and the hydraulic conductivity ( $L_p$ ) were calculated by simultaneously fitting  $L_p$  and *b* to the data using Eq. 2, from cell volume measurements in different experimental solutions (2X-5X) and different temperatures ( $4.8 \pm 0.1$ ,  $12.9 \pm 0.3$ ,  $23.3 \pm 0.2$ , and  $37.4 \pm 0.1$  °C), to examine the concentration and temperature dependence of  $L_p$  and *b*.

1 Values of the osmotically-inactive fraction calculated for all the experimental conditions 2 in Table 1 show that the osmotically-inactive fraction for TF-1 cells was not dependent on 3 concentration (p>0.05), but was dependent on temperature (p<0.05). Further analysis showed 4 that among temperatures, some were statistically significant, indicating possible slight 5 From an Arrhenius plot, the activation energy describing the temperature dependence. temperature dependence for the osmotically-inactive fraction  $(E_a^{\ b})$  in TF-1 cells was 0.80 ± 6 0.14 kcal/mol, which is very low. Furthermore, a two-way ANOVA analysis revealed that there 7 8 was no statistically significant interaction effect between osmolality and temperature on b9 (p>0.05). Original data for all temperatures and osmolalities were pooled and the overall mean 10 value for the fitted osmotically-inactive fraction was  $0.355 \pm 0.005$ .

11 A Boyle van't Hoff plot of equilibrium cell volume as a function of inverse osmolality 12 for the pooled temperature data is shown in Figure 3. The y-intercept of the linear regression 13 estimates the osmotically-inactive fraction to be  $0.368 \pm 0.004$  (calculated with the LINEST 14 function in EXCEL). There was no statistical difference between the osmotically-inactive 15 fractions calculated by these two approaches (Mann-Whitney U test; p>0.05). The osmotically-16 inactive fraction calculated from the Boyle van't Hoff plot was chosen for use in further analysis 17 for several reasons, including: it is the standard in cryobiology; and it is easier to interpret as it 18 only uses equilibrium data, as opposed to kinetic data; which is evident in the smaller error.

Table 2 shows the calculated hydraulic conductivity for TF-1 cells at different temperatures and extracellular osmolalities. Two-way ANOVA statistical tests indicated that  $L_p$ changed significantly with temperature (p<0.001), but did not change significantly with extracellular osmolality (p>0.05). This test also revealed statistically significant interaction between the effects of osmolality and temperature on  $L_p$  (p<0.05), indicating evidence that the 1 effect of temperature is dependent on concentration in predicting  $L_p$ . Due to this interaction 2 effect, statistical significance should be interpreted with caution. Values at different osmolalities were pooled for each experimental temperature. In order to calculate the activation energy of  $L_p$ , 3 4 Eq. 4 was linearized by taking the natural logarithm of each side of the equation and the data 5 were plotted as  $\ln L_p$  as a function of inverse absolute temperature. The pooled mean values in Table 2 were fitted to this equation using linear regression, giving an activation energy for  $L_p$  of 6  $14.2 \pm 1.1$  kcal/mol. An Arrhenius plot of the experimental data and the fitted line is shown in 7 8 Figure 4. The data for 3X PBS and pooled data for 2-5X PBS are plotted separately as 9 experimental techniques were slightly different (i.e. n=9 and n=36, respectively).

### 10 *Me*<sub>2</sub>SO permeability properties

11 Figure 5 shows the typical volume responses when TF-1 cells are exposed to a solution 12 containing 1 M Me<sub>2</sub>SO at 3 different temperatures. Using EXCEL Solver, P<sub>s</sub> was calculated using two different approaches: 1) using values for  $L_p$  that were calculated from  $E_a^{Lp}$ , and fitting 13 14 data to Eqs. 1, 2 and 3 to get values for  $P_{s;}$ , and 2) fitting data to Eqs. 1, 2 and 3 to get values for  $P_s$  and  $L_p$ . The values for  $P_s$  and  $L_p$  in Table 3 show that for pair-wise comparison of the two 15 16 parameter estimation methods at each temperature give the values within experimental error (p>0.05), with the exception of  $L_p$  at 23.4 °C (p<0.001). A Kruskal-Wallis statistical test 17 indicated that temperature is a significant predictor of both  $P_s$  and  $L_p$ , regardless of the 18 19 calculation approach used to determine these parameters (p < 0.001). The mean values in Table 3 20 were fitted to the linearized Arrhenius equation, Eq. 4, (using linear regression), giving an 21 activation energy for  $P_s$  of 13.8  $\pm$  0.1 kcal/mol and 16.3  $\pm$  1.1 kcal/mol, respectively for the two 22 different methods of calculation. For the second method, the activation energy for  $L_p$  was also 23 calculated (17.5  $\pm$  0.9 kcal/mol).

2 Figure 6 shows experimental results for TF-1 cells, suspended in serum-free RPMI without 3 cryoprotectant, cooled rapidly to various experimental temperatures and held for 3 min, prior to 4 direct thaw or plunge into liquid nitrogen. Data were normalized with control TF-1 samples (i.e. 5 TF-1 samples at room temperature;  $94.4 \pm 0.2$  %). Samples cooled to hold temperatures of 6 -20 °C and below, spontaneously nucleated prior to reaching the hold temperature. The direct 7 thaw samples showed little loss of membrane integrity at hold temperatures down to -9 °C, but 8 membrane integrity declined sharply between -9 and -20 °C, indicating that damage incurred 9 during cooling to, or at the hold temperature. For samples plunged into liquid nitrogen, some 10 protection against injury was conferred by holding for 3 min at -3 to -15 °C. Maximum 11 membrane integrity after plunge and thaw was  $62.2 \pm 2.1$  % and  $61.8 \pm 6.7$  % at hold temperatures -12 °C and -15 °C, respectively. Membrane integrity for TF-1 cells that were 12 13 plunged directly from room temperature was  $6.7 \pm 1.3$  % and demonstrates that the absence of 14 ice nucleation at high subzero temperatures and holding before plunging results in lower 15 membrane integrity after thawing.

## 16 *Effect of hold times in two-step freezing*

Figure 7 shows the membrane integrity of TF-1 cells as a function of hold time at -5 or -25 °C. Data were normalized with control TF-1 samples (i.e. TF-1 samples at room temperature;  $91.6 \pm 2.7$  % and  $91.3 \pm 2.2$  %, respectively).For direct thaw samples at -5 °C, membrane integrity remained high for up to at least 10 min. Cells plunged into liquid nitrogen from -5 °C showed maximum membrane integrity with a 2 min hold time (65.4 ± 0.5 %). Comparable results for membrane integrity were obtained for hold temperatures between -7 °C and -9 °C (data not shown). Cell damage was evident during cooling to a hold temperature of

1 -25 °C, which limited the membrane integrity of cells plunged into liquid nitrogen. Samples 2 cooled to -25 °C spontaneously nucleated prior to reaching the hold temperature. Figure 8 shows 3 contour plots of membrane integrity for TF-1 cells subjected to two-step freezing over a range of 4 hold temperatures and hold times. Figure 8a shows that cells directly thawed after being held for 5 various times at the hold temperatures show progressive decrease in membrane integrity as the 6 hold temperature was reduced below -9 °C and to a lesser extent, as hold time was increased. 7 Figure 8b shows that cells held for 1-3 min at temperatures between -5 °C and -7 °C prior to 8 plunging into liquid nitrogen, resulted in the highest percentage of membrane integrity (60 %). 9 A hold time of greater than 5 min resulted in a marked decrease in cell survival. This data 10 indicates that there is a zone of subzero hold temperatures (-5 °C to -12 °C) which, when held for 11 1-6 min, confers protection against cryoinjury associated with plunging to liquid nitrogen 12 temperatures.

### 13 Graded freezing without cryoprotectant

14 Membrane integrity as a function of experimental temperature for TF-1 cells cooled at 15 0.9 °C/min, prior to direct thaw or plunge into liquid nitrogen is shown in Figure 9. Data were 16 normalized with control TF-1 samples (i.e. TF-1 samples at 0 °C; membrane integrity 92.5  $\pm$ 17 2.9 %). Samples cooled to hold temperatures of -20 °C and below, spontaneously nucleated 18 prior to reaching the hold temperature. Similar results were found for cooling rates of 19 0.2 °C/min and 0.5 °C/min (data not shown). Data from all 3 cooling rates demonstrated a 20 progressive decline in membrane integrity for cells thawed directly from the experimental 21 temperature, with a 50% loss at -12 °C, indicating injury related to exposure to the concentrated 22 extracellular solution. Cells plunged into liquid nitrogen from the experimental temperature 23 incurred additional injury. The zone of subzero experimental temperatures between -3 °C and

-9 °C confers some protection against injury during plunge into liquid nitrogen (membrane
integrity 30.1 ± 0.7 % at -9 °C). Membrane integrity for TF-1 cells that were plunged directly
from 0 °C was 11.8 ± 2.7 %.

4

#### 5 Graded freezing with Me<sub>2</sub>SO

6 Figure 10 shows the recovery of TF-1 cells cooled at 0.9 °C/min in 10 % Me<sub>2</sub>SO to various 7 subzero temperatures ranging from -3 to -40 °C, and either thawed directly or plunged into liquid 8 nitrogen. Data were normalized with control TF-1 samples (i.e. TF-1 samples at 0 °C; 9 membrane integrity 91.4  $\pm$  3.2 %). Maximum membrane integrity after plunge and thaw was 10  $71.5 \pm 4.1$  % at a plunge temperature of -15 °C. Note, for comparison, that the membrane 11 integrity of TF-1 cells following a conventional HSC cryopreservation protocol (cooling 12 0.9 °C/min to -40 °C and then plunging into liquid nitrogen ) was  $63.0 \pm 6.4$  %. Membrane integrity for TF-1 cells in 10 % Me<sub>2</sub>SO that were plunged directly from 0 °C was  $30.9 \pm 3.1$  %. 13 14 It also demonstrates that when comparing the results to having no Me<sub>2</sub>SO present, Me<sub>2</sub>SO 15 confers protection even without ice nucleation at high subzero temperatures.

16

# 17 Discussion

18 Cell recovery following cooling to low temperatures depends in part on cellular osmotic 19 responses which are described by a set of osmotic parameters. The average size of TF-1 cells 20  $(916 \pm 15 \ \mu\text{m}^3)$  was higher than that previously reported for both human bone marrow CD34<sup>+</sup> 21 cells of 345  $\mu\text{m}^3$  [16] and umbilical cord blood CD34<sup>+</sup> cells of 274 ± 13  $\mu\text{m}^3$  [22].

In the range of osmolalities studied, TF-1 cells follow the Boyle van't Hoff relationshipyielding an osmotically-inactive fraction of 0.37. A previously reported value for human bone

marrow hematopoietic CD34<sup>+</sup> cells was 0.205 [16], and for human umbilical cord blood CD34<sup>+</sup>
cells was 0.32 [60] and 0.27 ± 0.01 [22]. The value of osmotically-inactive fraction reported
here is also within the range for a variety of mammalian cell types (0.2-0.41)
[9,16,17,21,31,46,52].

5 Permeability parameters were calculated from cell volume measurements between 4 and 37 °C, showing that osmotically-inactive fraction was largely independent of temperature but 6 7 that hydraulic conductivity was strongly temperature-dependent. The value for  $L_p$  was 0.339  $\mu$ m/min/atm at 20 °C. The value reported here for  $L_p$  is higher than the  $L_p$  previously 8 reported for human cord blood CD34<sup>+</sup> cells of 0.168 ± 0.03 µm/atm/min at 20 °C [22,60], 9 indicating that the rate of water movement in TF-1 cells is larger than that in other HSC. The  $L_p$ 10 11 value is also within the range reported for many nucleated mammalian cells, such as rat 12 megakaryocytoporietic cells, Chinese hamster lung fibroblast cells, bovine immature oocytes, 13 chondrocytes, corneal endothelial, epithelial and stromal cells [52].

The Arrhenius activation energy of  $L_p$  of 14.2 kcal/mol reported here, is within the range of some other mammalian cells (9-16 kcal/mol) [9,21,31,51]. Based on  $L_p$  values reported by Hunt et al. at 2 temperatures [22], we calculated the  $E_a^{Lp}$  in cord blood CD34<sup>+</sup> cells to be 18.8 kcal/mol. It has been reported that an  $E_a^{Lp}$  of <6 kcal/mol may be indicative of channelmediated water transport [13], and an  $E_a^{Lp} > 10$  kcal/mol may indicate transport water across the plasma membrane primarily by solubility-diffusion [13].

The conventional method for cryopreserving HSC, utilizes Me<sub>2</sub>SO as a cryoprotectant
[65]. The calculated permeability of Me<sub>2</sub>SO in TF-1 cells, 14.3 μm/min at 22 °C, is higher than
reported for human cord blood CD34<sup>+</sup> cells (9.4 μm/min (22 °C) [60]; 4.4 μm/min (20 °C) [22]),
but within the range of reported values found for a variety of mammalian cell types [51],

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including human corneal endothelial, keratocyte and epithelial cells [10], hamster islet cells [3], human granulocytes [58], canine red blood cells [32], and neonatal porcine islet cells [15].

- 3 In the absence of cryoprotectants, this study showed that using two-step freezing 4 (interrupted rapid cooling with hold time), TF-1 cells sustained less injury at lower subzero hold 5 temperatures than using graded freezing (interrupted slow cooling without hold time). However, 6 using two-step freezing, there was also damage associated with cooling down to and exposure at 7 the hold temperatures. Cells thawed directly from the hold temperatures showed a decline in 8 membrane integrity with decreasing temperature, reaching 50% at -17 °C, indicating that a major 9 portion of cells were damaged prior to being plunged into liquid nitrogen. This damage is 10 associated with cooling down to the hold temperature and exposure at the hold temperature, with 11 intracellular ice formation as a likely cause. These results also demonstrate that for hold 12 temperatures below -15 °C, no additional damage is incurred by cooling to liquid nitrogen 13 temperatures, implying that the cells remaining intact at the end of the hold step have lost a 14 sufficient amount of intracellular water and that there is no additional damage due to intracellular 15 ice formation during the plunge. The highest recovery (membrane integrity) for samples thawed 16 from liquid nitrogen were  $62.2 \pm 2.1$  % at a hold temperature of  $-12^{\circ}$ C and  $61.8 \pm 6.7$  % at a hold 17 temperature of -15 °C, both with a hold time of 3 min. Avoidance of intracellular ice formation 18 during the plunge step requires osmotic dehydration during the hold step. The hydraulic 19 conductivity and its activation energy are different for different cell types, so the optimal hold 20 temperature and time will be cell-type dependent.
- Using the graded freezing procedure, this study demonstrated the progressive damage incurred by slow cooling TF-1 cells to subzero experimental temperatures, indicating the deleterious effect of exposure to concentrated extracellular solutions. There was a marked

1 difference between the membrane integrity for cells directly thawed and those plunged into 2 liquid nitrogen, which has also been shown for other cell types [49,50,63,65,66]. The maximum 3 recovery for plunge samples using graded freezing without Me<sub>2</sub>SO was 27.8  $\pm$  0.8 %, while 4 results from the literature for other HSCs were 32 % for nucleated white cells and 17 % for 5 CD34<sup>+</sup> cells [65].

6 Table 4 compares maximum recovery of TF-1 cells cooled in liquid nitrogen (plunge 7 thaw) using different freezing protocols. The maximum two-step freezing recovery (membrane 8 integrity  $62.2 \pm 2.1$  %) was higher than recovery using graded freezing profiles without Me<sub>2</sub>SO 9 (membrane integrity  $30.1 \pm 0.7$  %). Furthermore, the two-step freezing membrane integrity 10 (without cryoprotectant) were comparable with membrane integrity of TF-1 cells cooled using a 11 conventional cryopreservation protocol (cooling at 0.9 °C/min in 10 % Me<sub>2</sub>SO to -40 °C and 12 plunging into liquid nitrogen) of  $63.0 \pm 6.4$  %. Although there is no true standard 13 cryopreservation method for HSCs, there is an overall conventional approach of slow cooling in 14 5-10 % Me<sub>2</sub>SO solution. Based on the HSC cryopreservation literature, this approach leads to 15 recoveries of  $79 \pm 5$  % (membrane integrity; 1 °C/min with plunge at -50 °C using 10 % Me<sub>2</sub>SO) [23],  $67.4 \pm 2.0 \%$  (1 °C/min with plunge at -60 °C using 10 % Me<sub>2</sub>SO) [62], and  $85.8 \pm$ 16 17 6.8 % (4 °C/min with plunge at -44 °C using 5 % Me<sub>2</sub>SO) [65]. While the exact cooling 18 protocols and Me<sub>2</sub>SO solutions may differ to varying degrees from the present study, the 19 influence of Me<sub>2</sub>SO on increasing cell survival at lower temperatures during slow cooling is a 20 commonality. The trends using graded freezing with Me<sub>2</sub>SO, are comparable to those seen using 21 graded freezing with nucleated white blood cells, [65], CD34+ UCB stem cells [65], and chinese 22 hamster fibroblasts [42]. The maximum recovery obtained using graded freezing with Me<sub>2</sub>SO 23 was 71.5  $\pm$  4.1 %; however, this was using a relative high plunge temperature of -15 °C (Table 1 4).

The data in this study are also comparable to previously published results by Karlsson et al. [27] using slow cooling and Me<sub>2</sub>SO with mouse oocytes. They showed low cell recovery at high plunge temperatures, which increased at lower plunge temperatures. They also suggested that the observed cell damage at high subzero plunge temperatures was the result of intracellular ice formation, based on predictions of a mechanistic model [27], which would also explain the plunge results in this study.

8 The use of Me<sub>2</sub>SO as a cryoprotectant has been identified as a problem for HSC 9 transplant patients due to its clinical toxicity [7,11,56,68]. The experimental results reported 10 here for TF-1 cells without cryoprotectants indicate that higher cell recovery is possible by 11 manipulating the cooling profile. This data indicates that there is a zone of subzero hold 12 temperatures (-5 to -12 °C) and hold times (1-6 min), that confers cryoprotection comparable to 13 the conventional 10 % Me<sub>2</sub>SO solution with slow cooling down to-40 °C in TF-1 cells. The 14 pattern of recovery as a function of hold time and temperature was similar to that previously 15 shown for fibroblasts [45].

By comparing the post-thaw recovery of TF-1 cells, following slow cooling, with water permeability results, it is evident that cells with a relatively low hydraulic conductivity are damaged during slow cooling without a cryoprotectant (membrane integrity 27.8  $\pm$  0.8 %). However, human red blood cells (RBC), which have a much higher  $L_p$  (12 µm/min/atm at 22-24 °C) [51], sustain even greater injury during slow cooling (hemolysis >95 %) [55].

Practical cryopreservation procedures have largely been limited to the use of constant
 cooling rates. Interrupted freezing procedures, such as two-step and graded freezing, provide
 useful insight into the mechanisms of damage occurring at various temperatures throughout the

1 cooling profile [44]. These procedures allow manipulation of different variables of the 2 cryopreservation protocol, including cooling profiles, plunge temperatures, cryoprotectants, and 3 storage temperatures. In this study, both procedures allowed additional characterization of the 4 cryobiology of cells, and the ability to cryopreserve TF-1 cells (a model for HSC) without the 5 need for Me<sub>2</sub>SO and to improve recoveries when using Me<sub>2</sub>SO. Ultimately, this approach will 6 enable to systematic exploration of alternatives to constant cooling rates.

### 7 Acknowledgement

8 We would like to thank Ruth Nelson and Nelly Wu for their technical assistance. This 9 research was funded by the Canadian Institutes for Health Research (CIHR; MOP 85068, 86492 10 and CPG 75237) and the Natural Sciences and Engineering Research Council (NSERC) of 11 Canada. J.A.W. Elliott holds a Canada Research Chair in Interfacial Thermodynamics.

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Figure 1. Schematics of (a) two-step freezing, including initial rapid non-linear cooling to hold
 temperature, hold time, and either directly thawing or plunging and then thawing following
 storage time, and of (b) graded freezing, including initial slow linear cooling to experimental
 temperatures and either direct thawing or plunging and then thawing.

5 Figure 2. Representative cell volume kinetics of TF-1 cells exposed to 3X PBS at 4 different 6 temperatures. The symbols show the experimental volume measurements averaged over 7 300 msec time intervals and the solid lines represent Eqs. 1 and 2 fitted to the data using the least 8 squares method, yielding a value of  $L_p$  and b at each temperature.

9 Figure 3. The Boyle van't Hoff plot for TF-1 cells. The symbols represent the experimental
10 relative equilibrium cell volumes in hypertonic solutions and the solid line represents the linear
11 regression fit of Eq. 1 to the data. The y-intercept gives the osmotically-inactive fraction, *b*.

Figure 4. Arrhenius plot of the natural logarithm for  $L_p$  (µm/min/atm) of TF-1 cells (± sem) as a function of inverse temperature (K<sup>-1</sup>) (± sem). The open diamond symbols represent all experiments done in 2-5X PBS, with different concentration data pooled (n = 36). The closed symbols represent all experiments done in 3X PBS (n = 9). The solid line represents the linear regression of the data for calculation of the activation energy ( $E_a$ ) from the slope (R<sup>2</sup>=0.93).

Figure 5. Representative plots of cell volume kinetics of TF-1 cells exposed to 1M DMSO at (a) 4°C, (b) 10°C, and (c) 22°C. The symbols show the experimental volume measurements averaged over 300 msec time intervals and the solid lines represent Eqs. 1, 2, and 3 fitted to the data using the least squares method, yielding a value of  $P_s$  at each temperature.

Figure 6. Two-step freezing. Membrane integrity for TF-1 cells (± sem; normalized) in serumfree RPMI media cooled to various subzero plunge temperatures from room temperature, held 3
minutes, and then either thawed directly (dashed) or plunged into liquid nitrogen (solid) before

1 being thawed.

Figure 7. The membrane integrity of TF-1 cells (± sem; normalized) in serum-free RPMI media
as a function of hold time for cells cooled rapidly to -5 °C (black) or -25 °C (grey), held for a
period of time before either thawed directly (dashed) or plunged into liquid nitrogen (solid)
before being thawed.

Figure 8. Contours of membrane integrity of TF-1 cells (normalized) in serum-free RPMI media
after being cooled rapidly to various subzero hold temperatures and held for a duration ranging
from 0.5 to 10 minutes before being either (a) thawed directly or (b) plunged into liquid nitrogen
prior to thawing.

Figure 9. Graded freezing without cryoprotectant. Membrane integrity of TF-1 cells (± sem;
normalized) in serum-free RPMI media after being cooled at 0.9 °C/min to various subzero
experimental temperatures and either thawed directly (dashed) or plunged into liquid nitrogen
(solid) prior to thawing.

Figure 10. Graded freezing with Me<sub>2</sub>SO. Membrane integrity of TF-1 cells (± sem; normalized)
in 10 % Me<sub>2</sub>SO in RPMI media after being cooled at 0.9 °C/min to various subzero experimental
temperatures and either thawed directly (dashed) or plunged into liquid nitrogen (solid) prior to
thawing.

	Temperature			
Osmolality (osm/kg)	4.8 ± 0.1 °C	12.9 ± 0.3 °C	23.3 ± 0.2 °C	37.4 ± 0.1 °C
583 ± 7	0.399 ± 0.006	0.336 ± 0.021	0.334 ± 0.008	0.294 ± 0.022
861 ± 6	0.347 ± 0.024	0.374 ± 0.014	0.338 ± 0.006	0.339 ± 0.016
1150 ± 4	0.387 ± 0.027	0.385 ± 0.019	0.355 ± 0.007	0.344 ± 0.019
1434 ± 5	0.368 ± 0.009	0.400 ± 0.012	0.371 ± 0.008	0.312 ± 0.012
pooled mean	0.375 ± 0.010 <sup>a</sup>	0.374 ± 0.010 <sup>a</sup>	0.349 ± 0.004 <sup>a,b</sup>	0.325 ± 0.009 <sup>b</sup>

TABLE 1. Osmotically-inactive volume, b, values for TF-1 cells (mean  $\pm$  sem; n = 9)

Different superscripts indicate statistical difference (p<0.05)

	Temperature			
Osmolality (osm/kg)	4.8 ± 0.1 °C	12.9 ± 0.3 °C	23.3 ± 0.2 °C	37.4 ± 0.1 °C
583 ± 7	0.075 ± 0.003	0.119 ± 0.005	0.355 ± 0.012	1.348 ± 0.093
861 ± 6	0.070 ± 0.003	0.123 ± 0.005	0.395 ± 0.013	1.413 ± 0.074
1150 ± 4	0.075 ± 0.004	0.119 ± 0.004	0.407 ± 0.010	1.447 ± 0.106
1434 ± 5	0.074 ± 0.004	0.112 ± 0.002	0.386 ± 0.013	1.512 ± 0.061
pooled mean	0.074 ± 0.002 <sup>a</sup>	0.118 ± 0.002 <sup>ª</sup>	0.386 ± 0.006 <sup>b</sup>	1.425 ± 0.044 <sup>c</sup>

TABLE 2. Hydraulic conductivity,  $L_p$ , values for TF-1 cells (mean  $\pm$  sem; n = 9)

Different superscripts indicate statistical difference (p<0.05)
1M Me <sub>2</sub> SO	Using calculated $L_p$ from $E_a^{Lp}$		Solving for simultaneously	$L_p$ and $P_s$
Temperature	$L_p$	$P_s$	$L_p$	$P_s$
(°C)	(µm/min/atm)	(µm/min)	(µm/min/atm)	(µm/min)
$4.9 \pm 0.3$	0.09	$3.36 \pm 0.40$	$0.08 \pm 0.00$	$2.92 \pm 0.22$
$10.7 \pm 0.4$	0.15	$5.67 \pm 0.51$	$0.17 \pm 0.01$	$6.00 \pm 0.76$
$23.4 \pm 0.5$	0.45	$15.95 \pm 1.08$	$0.61 \pm 0.02^*$	$18.8 \pm 1.66$
E <sub>a</sub> (kcal/mol)	14.2	$13.8 \pm 0.1$	$17.5 \pm 0.9$	$16.3 \pm 1.1$

TABLE 3. Me<sub>2</sub>SO Permeability properties for TF-1 cells (mean  $\pm$  sem; n = 9)

\* Signifies statistically significant difference from the  $P_s$  value estimated using the method of calculating  $L_p$  from  $E_a^{Lp}$  (p<0.001)

Protocol	Maximum recovery after storing in liquid nitrogen
Conventional Freezing protocol <sup>1</sup>	63 ± 6.4 %
Graded Freezing (without 10% Me <sub>2</sub> SO) <sup>2</sup>	30.1 ± 0.7 %
Two-step Freezing (without $Me_2SO$ ) <sup>3</sup>	62.2 ± 2.1 %
Graded Freezing (with 10% Me <sub>2</sub> SO) <sup>4</sup>	71.5 ± 4.1 %

TABLE 4. Maximum recovery of TF-1 cells (plunge thaw), as assessed by membrane integrity (mean  $\pm$  sem; normalized).

<sup>1</sup>0.9 °C/min to -40 °C and plunge <sup>2</sup>0.9 °C/min to -9 °C and plunge <sup>3</sup>non-linear cooling with 3 minute hold at -12 °C followed by plunge <sup>4</sup>0.9 °C/min to -15 °C and plunge



Ross-Rodriguez\_Fig 1a























**Ross-Rodriguez\_figure 8** 



