

Characterizing Asymmetry across the Whole Sit to Stand Movement in Healthy Participants

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1 **Abstract**

2
3 Sit-to-stand transfer (STS) is a common yet critical prerequisite for many daily tasks. Literature
4 conducted on healthy STS often assume the body to behave symmetrically across the left and
5 right side; yet only a few studies have been conducted to investigate this supposition. These
6 studies have focused on a single numerical indicator such as peak joint moment (JM) values to
7 describe symmetry; however, STS is a dynamic and time dependent movement. This study
8 addresses the validity of peak value analyses through the introduction of a time based peak-offset
9 measure and proposes two time-dependent techniques to further characterize asymmetry and
10 assesses their feasibility in ten (10) healthy male participants. JM and joint power (JP) over the
11 whole STS movement was determined using motion capture and inverse dynamics. Using a
12 paired one-tailed t-test differences were found in the time at which the left and right side reached
13 peak values in all lower extremity joints with exception of the hip JM ($p < 0.05$). Using a measure
14 of JM and JP straight-difference it was determined that the ankle joint displayed the largest
15 number of JM and JP development strategies of all the lower extremity joints. Finally, through
16 numerical integration of the JM and JP data with respect to time, it was found that the longer one
17 side spends dominating the movement, the larger the excess angular impulse and work that can
18 be expected from that side. The results suggest that when analyzing STS movements, one must
19 be aware of the potential asymmetry present even in healthy movements. Furthermore, a simple
20 peak JM or JP analysis may not fully describe the extent of these asymmetries.

Introduction

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Sit-to-stand (STS) movements are a functional prerequisite for many daily tasks and consequently an independent lifestyle (Burnett *et al.*, 2011; Fotoohabadi *et al.*, 2012). Therefore, understanding the biomechanics to accomplish STS is necessary for rehabilitation and therapeutic programs focused on patients with lower extremity impairment.

Clinically, STS symmetry can be used as an assessment tool for lower extremity function. STS symmetry has been used to evaluate knee function following arthroplasty focusing on peak vertical ground reaction forces (VGRF) (Boonstra *et al.*, 2008, 2010; Christiansen *et al.*, 2011) as well as assess movements in the elderly, hemiparetic and amputee populations among others (Agrawal *et al.*, 2011; Fotoohabadi *et al.*, 2012; Gao *et al.*, 2011; O’Meara & Smith, 2005; Roy *et al.*, 2007). Although asymmetry is an indication of impairment, perfect symmetry is not necessarily exhibited in healthy populations (Lundin *et al.*, 1995).

When quantifying healthy STS movements, several studies assume bilateral symmetry, where joint moments (JMs) are assumed contralaterally equivalent across the left and right sides (Kuo *et al.*, 2009; Roberts & McCollum, 1996; Sibella *et al.*, 2003; Yoshioka *et al.*, 2009). Yet, lower limb kinetic asymmetry has been widely demonstrated in healthy populations performing tasks such as gait (Seeley *et al.*, 2008, 2010), or during the propulsive phase of gait in elderly subjects (Sadeghi *et al.*, 2004). Furthermore, strength asymmetry has been demonstrated in healthy populations; exhibiting stronger quadriceps and weaker hamstrings in their dominant sides during knee flexion and extension (Lanshammar & Ribom, 2011).

46 Limited research has been conducted on healthy STS symmetry. Asymmetry was shown in the
47 sagittal JMs of the hips in elderly (n=7, mean [SD] age: 22.9 [1.0]) and young (n=7, mean [SD]
48 age: 74.3 [4.1]) participants with further asymmetry at the knees of the young group (Lundin et
49 al., 1995). Burnett *et al.* evaluated peak VGRFs in relation to leg dominance and found no
50 significant difference between sides (Burnett et al., 2011). However, these two studies were
51 limited to the evaluation of peak JMs and VGRFs, respectively, focusing on a single point in the
52 STS movement to evaluate symmetry.

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54 To address this limitation, while studying a single above knee amputee, Gao *et al.* assessed STS
55 asymmetry using principle-component-analysis. This technique accounted for whole cycle
56 movements in all three body planes; a unique approach for STS based research. However, able
57 bodied research rarely addresses movements across the whole STS cycle (Gao et al., 2011). It is
58 important to recognize STS is a dynamic movement in which biomechanical requirements follow
59 a time dependent cycle. Peak values are achieved at a single instant during that cycle and thus
60 may not be a comprehensive measure of asymmetry.

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62 This study addresses the validity of peak value analyses through the introduction of a time based,
63 peak-offset measure. Furthermore two novel methods for evaluating STS symmetry, while
64 incorporating whole cycle data are proposed and their feasibility analyzed.

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Methods

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Ten healthy male participants were recruited internally through the institution’s engineering faculty (Table 1). Males were selected to remove possible biomechanical gender differences present in non-STS related motion analysis (Moisio *et al.*, 2003). Potential participants reporting prior or current conditioning and/or injuries that may affect their STS movements were excluded from the study. Ethics approval was obtained through the institution’s ethics board and informed consent was obtained prior to participation.

Insert Table 1

Reflective markers (1.5 cm diameter) were positioned on participants according to the Helen Hayes protocol (Kadaba *et al.*, 1990). Additional markers were adhered between the clavicles, centered on the sternum and affixed to the C7, to capture torso position. An 8 camera, Eagle Digital motion capture system (Motion Analysis Corp., Santa Rosa, CA, USA), sampling at 120Hz, and two force plates (Advanced Mechanical Technology Inc., Newton, MA, USA), sampling at 2400Hz captured marker motions and GRFs, respectively.

A backless, armless, 48cm tall chair was positioned such that participants could place one foot approximately centered on each force place (Lundin *et al.*, 1995). Participants were instructed to sit comfortably toward the front of the chair, and symmetry of the initial posture was visually verified prior to each trial. To remove inertial effects of upper limb movements, subjects folded their arms across their chest. When prompted, participants rose at a self-selected pace. The procedure included 10 trials for each participant.

92 Marker motion data was smoothed using a 4Hz, fourth-order, Butterworth filter, and imported
93 into Visual 3D software (C-Motion Inc., Germantown, MD, USA) for inverse dynamic
94 calculations. Each participant's body-segment properties were input according to height and
95 mass dependant 50th percentile anthropometric data (Winter, 1990; Zatsiorsky, 2002). Lower
96 extremity JMs, joint angles and joint angular velocities were extracted for this analysis. JM
97 values were normalized to participant body mass and height. Joint power (JP) was determined
98 through the multiplication of the normalized JM and joint angular velocity data.

99

100 To determine total JMs and JPs, the Euclidian Norm was used by treating orthogonal JMs about
101 each joint using Eq. (1). This procedure was repeated for JP data.

102

103 *Insert Equation 1*

104

105 STS was defined as occurring during the time interval between mass transfer (torso anterior
106 rotation characterized by hip flexion) and the point at which joint motion ceased (Miyoshi, *et al.*,
107 2005). Initiation time was determined when the hip joint angle fell outside +/- 3 standard
108 deviations of the initial static position (based on averaging the first 20 data points); completion
109 was determined when the hip joint angle fell within +/- 3 standard deviations of the final static
110 position (based on averaging the final 10 data points). Cycle time was normalized to a pseudo
111 time scale of % STS completion. JM and JP curves were averaged for each participant's 10 trials
112 on the left and right side independently.

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Peak Offset

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116 The peak JM (or JP) value was defined as the maximum absolute value occurring during the STS
117 cycle. The times, in units of % STS completion, at which peak values occurred on the left and
118 right side for each joint were collected independently (Fig. 1). The time at which each joint's
119 peak value occurred was arranged into two groups, first side to peak and last side to peak. A
120 paired, one-tailed t-test was conducted to test for a significant difference in the means of these
121 groups ($P < 0.05$).

122

123 *Insert Figure 1*

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Straight-Difference

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126 To characterize side dominance, straight difference (SDIF) plots were created by subtracting the
127 averaged right side JM (JP) data from the averaged left for each joint of each participant.

128 Positive (negative) SDIFs value indicated left (right) side dominance (Fig. 1).

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130 SDIF plots were categorized according to the number of slope reversals present. A slope reversal
131 was defined as a shift in a plot's slope from positive to negative (or negative to positive) with
132 amplitude in excess of 25% the absolute global maximum of the plot. Therefore, this procedure
133 neglects minor fluctuations in the SDIF data. Corresponding to each joint, participants were
134 categorized based on the number of slope reversals present.

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Angular Impulse, Work and Time

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138 Percent angular impulse (PAI) and percent work (PW) enabled characterization of the
139 relationship between length of time a side dominated JM (or JP) development, and excess
140 impulse (or work) that resulted from that side. Positive PAI (PW) was derived through exclusive

141 summation of the positive regions of the SDIF JM (JP) plot multiplied by the 2% time interval
142 between each JM (JP) data point. This numerical integration was then repeated for the negative
143 components. Therefore, the positive (negative) integral component represents the total excess
144 PAI or PW contributed from the left (right) side (Fig. 2). The percentage of the cycle a JM (JP)
145 SDIF plot remained positive (negative) was recorded and defined as the positive %time (negative
146 %time) (Fig. 2).

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148 *Insert Figure 2*

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Results

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Peak Offset

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154 Peak offset values ranged from 0% through 40% completion of STS. On average the ankle
155 produced the largest JM and JP offset values of the three joints (3.6% \pm 5.15% time and 12.0%
156 \pm 14.3% time respectively). The knee had the smallest average peak offset for both JM and JP
157 values (0.80% \pm 1.03% time and 1.00% \pm 1.05% time respectively). Significant difference was
158 found in the peak times of both JM and JP values of all joint with exception of hip JM values
159 (P<0.05) (Table 2).

160

161 *Insert Table 2*

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Straight-Difference

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165 Figure 3 plots the slope reversal of each participant according to joint. Table 3 highlights the
166 number of slope reversals demonstrated by each participant and groups based on the number of
167 reversals demonstrated. The ankle demonstrated the most slope reversal groups of all the three

168 joints; participants demonstrated 0, 1, 2 or 3 JM, and 2, 3, 4, 5 or 6 JP slope reversals. As a
169 result participant ankles can be divided into 4 JM and 5 JP groups. JM data at the knee and hip
170 both show 3 groupings representative of 1, 2 or 3 and 1, 2 or 4 reversals respectively. JP at the
171 knee and hip can be divided into 3 groups and 4 groups, respectively.

172

173 *Insert Figure 3*

174 *Insert Table 3*

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Angular Impulse, Work and Time

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178 Fig. 5 plots for the length of time a side dominates and the excess PAI and PW contributed from
179 that side. In total, the participant group produced 10 positive PAI (PW) values and 10
180 corresponding positive %time values at each joint (similarly 10 negative PAI (PW) and %time
181 values). It is evident that the longer a side spent dominating the STS cycle, the greater the excess
182 PAI (or PW) contribution from that side. This relationship is presented in all but the left hip and
183 knee PW data where the largest excess PW contributions occur when the left side dominates
184 approximately 45 to 75% of the STS cycle.

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186 *Insert Figure 4*

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Discussion

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189 The literature typically addresses healthy STS asymmetry through a single numerical indicator,
190 such as peak JMs or GRFs (Burnett, *et al.*, 2011; Boonstra, *et al.*, 2010; Christistiansen, *et al.*,
191 2011; Argawal, *et al.*, 2011; Lundin, *et al.*, 1995). Although peak values quantify the maximum
192 requirements of the task, they neglect how and when the body arrives at this condition.

193

194 Significant peak offsets were found in the ankle and knee JM and for all three joints for JP
195 ($p < 0.05$). Therefore, comparing peak values may only evaluate maximum conditions and does
196 not necessarily compare values from the same point in time. Consequently peak analyses may
197 not sufficiently characterize asymmetry as a whole. The ankle produced the largest average JM
198 and JP peak offset of all joints, suggesting that ankle symmetry should be evaluated using a time
199 dependent measure. However, smaller peak offset values were found at the knee. Therefore,
200 determining clinically relevant offset values would enable further understanding of the validity a
201 peak analysis holds at each joint.

202
203 The proposed straight-difference method enables characterization of STS strategies based on
204 slope reversals. These reversals are an indication of asymmetry in the rate of JM (or JP)
205 development across the body. Either one joint is reducing, or the contralateral side is increasing,
206 its excess contribution. Therefore the different numbers of reversals during a STS movement
207 illustrates different strategies for which the body shares JM (or JP) requirements between sides.
208 The ankle was determined to have the largest number of strategies, for both JM and JP (4 and 5
209 respectively) which is believed to result from the high mobility of the joint and its role in balance
210 and stability (Hylton, *et al.*, 2005; Hoch, *et al.*, 2005). No apparent relationship was present
211 between participants across joints. For instance participants 1 and 5 both demonstrated a 3
212 reversal ankle JM strategy. Yet at the knee and hip participant 1 showed 2 and 4 reversals
213 respectively where participant 5 demonstrated 3 and 2 reversals respectively. The lack of
214 commonality suggests that reversal strategies of one joint may not be predictable by viewing the
215 other two. As seen in Figure 3, a vast array of STS strategies were present in the able bodied
216 group. These numerous strategies to perform a relatively simple movement further reiterate the

217 complexity of predicting asymmetry during this task. Several variables beyond those examined
218 in this study may affect asymmetry such as individual inequalities in limb proportions, small
219 variations in foot placement and strength dominance among others.

220

221 The PAI, PW and time plots illustrated an intuitive relationship: the amount of excess angular
222 impulse (work) of one side increased with the time that side spent dominating JM (JP)
223 development (excluding left-dominant knee and hip PW data). This suggests that the time a side
224 dominates may be a more appropriate measure of asymmetry than a simple peak analysis. It is
225 possible one side will achieve a higher peak than the other, yet spend minimal time dominating.
226 By employing a peak analysis dominance of the movement would be mislabelled. These PAI,
227 PW and time measures have the potential to robustly label side dominance as they account for
228 asymmetry over the duration of the STS movement. However, further investigation with a larger
229 sample size is warranted to explicitly quantify the nature of these relationships.

230

231 Limitations of this study lie in the instructed posture of the participants and the sample size.
232 Participant rose from a standard chair height with arms folded across their chest. By no means do
233 these variables account for every configuration present in day-to-day movements, and
234 consequently may affect the symmetry of STS movements. Furthermore a sample size of 10 was
235 used to evaluate the feasibility of the proposed symmetry measures. Collected data often
236 presented relatively high standard deviations. Although this may weaken statistical power, it
237 further reiterates the variation in symmetry of healthy populations; this is especially evident in
238 Figure 3. Asymmetry in STS presents itself unpredictably and is not necessarily captured through
239 peak values alone.

240
241 In conclusion, the able-bodied sample group (n=10) demonstrated an array of STS strategies.
242 Peak JM and JP values were found to occur at different times during the movement therefore
243 questioning the validity of peak analyses. Two proposed methods, evaluating slope reversals in
244 SDIF plots, and analyzing the relationship between PAI, PW and time, allowed for
245 characterization of asymmetry over the duration of the STS movement; perhaps a more
246 comprehensive measure. Further understanding these asymmetries present in STS may be
247 particularly relevant in studying affected populations. As STS symmetry is being incorporated in
248 measurements of lower extremity function (Agrawal *et al.*, 2011; Boonstra *et al.*, 2008, 2010;
249 Christiansen *et al.*, 2011; Fotoohabadi *et al.*, 2012; Gao *et al.*, 2011; O’Meara & Smith, 2005;
250 Roy *et al.*, 2007), it is pertinent to understand STS is a time dependant movement an evaluation
251 of peak values alone holds inherent limitations.

252

253 **Conflict of Interest Statement**

254 The authors have no financial or personal conflicts of interest to declare.

255

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259

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Table 1 Participant Summary

Where BMI signifies body mass index, Min and Max represent the minimum and maximum values present in the sample group, and SD the standard deviation among participants.

	Age	Height	Mass	BMI
	(yrs)	(m)	(Kg)	(kg/m ²)
Min	20	1.90	49	18.22
Max	35	1.64	79	25.56
Mean	25.4	1.77	70.5	22.55
SD	4.2	0.09	8.7	2.44

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Equation (1) The Euclidian Norm for Joint Moments

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The total resultant moment for each joint was defined as the Euclidian Norm vector summation of the anteroposterior (ap),
273 medial-later (ml) and superior-inferior (si) direction moment components for each leg.

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275

$$JM_{total} = \sqrt{JM_{ap}^2 + JM_{ml}^2 + JM_{si}^2}$$

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Figure 1 Graphical Representation JM

279 Graphical representation knee JM plot and resulting SDIF plot for an individual participant's knee. Where JM and
280 SDIF represent joint moment and straight difference respectively, units are given in Newton meters per kilogram
281 (Nm/Kg) normalized to body mass (BM) and body height (BH)

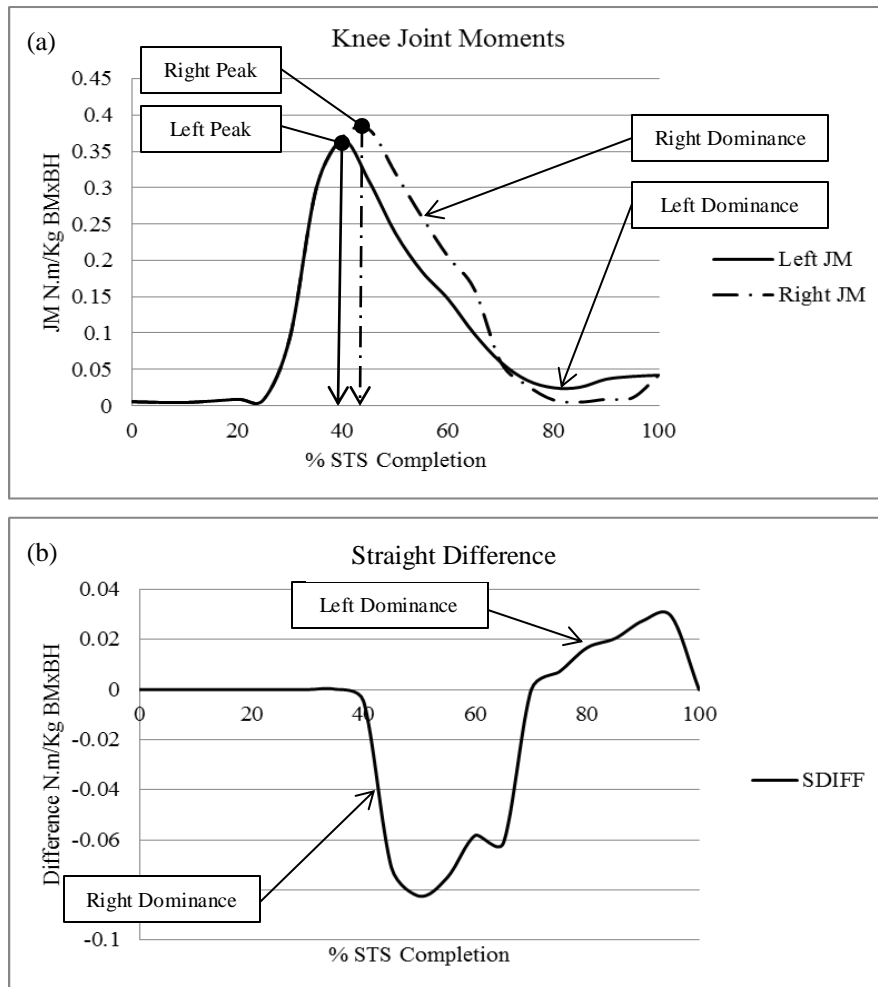
282 (a) Procedure to identify the time at which each side's peak occurred with peak offset corresponding to the interval
283 between the left and right side %STS Completion values. This procedure was conducted for both JM and JP curves
284 at each joint for each participant.

285 (b) Procedure to identify SDIF (left JM – Right JM) from the JM data. This procedure was conducted for both JM
286 and JP curves at each joint for each participant.

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Figure 2 Graphical Representation of Percent Angular Impulse Procedure

291 Top: identification of areas of excess JM contribution. Bottom: integration of the SDIFF curve to identify the excess
292 PAI values. Negative PAI is representative of right side excess and positive values indicate areas of left side excess.

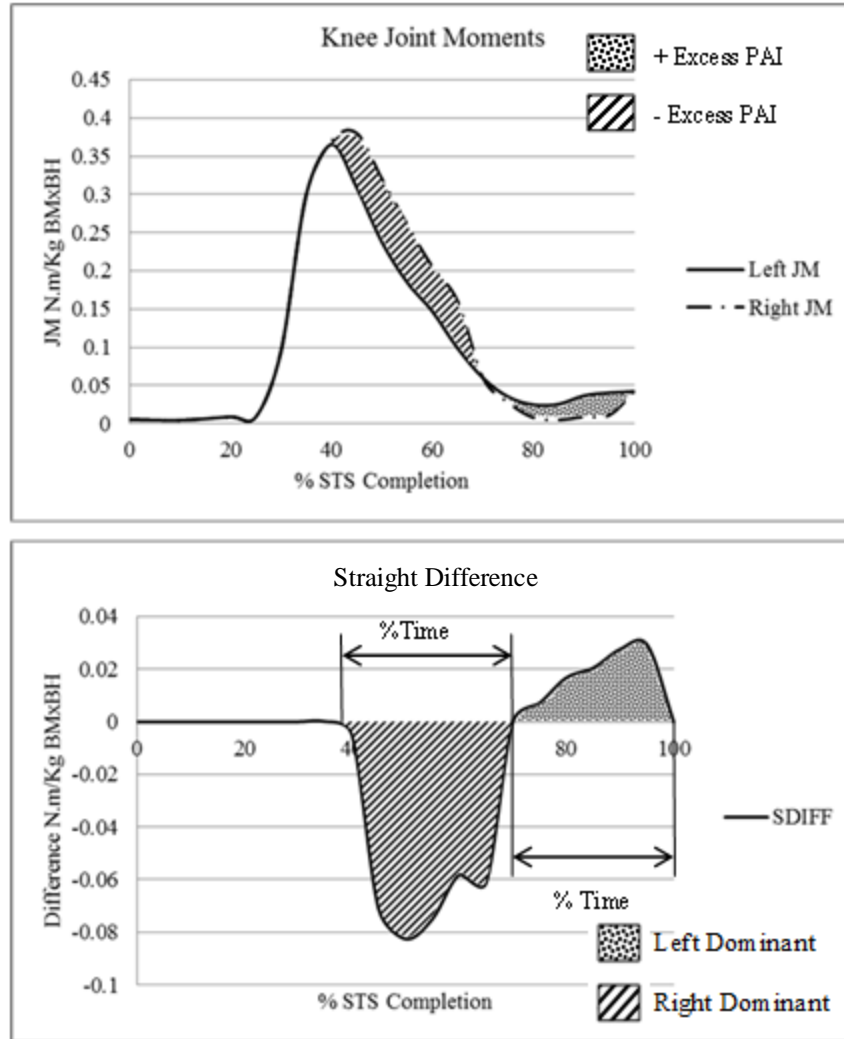
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The time period over which these areas of excess occur are highlighted in the figure.

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Table 2 Average JM and JP Peak Offset Values and Corresponding P-values

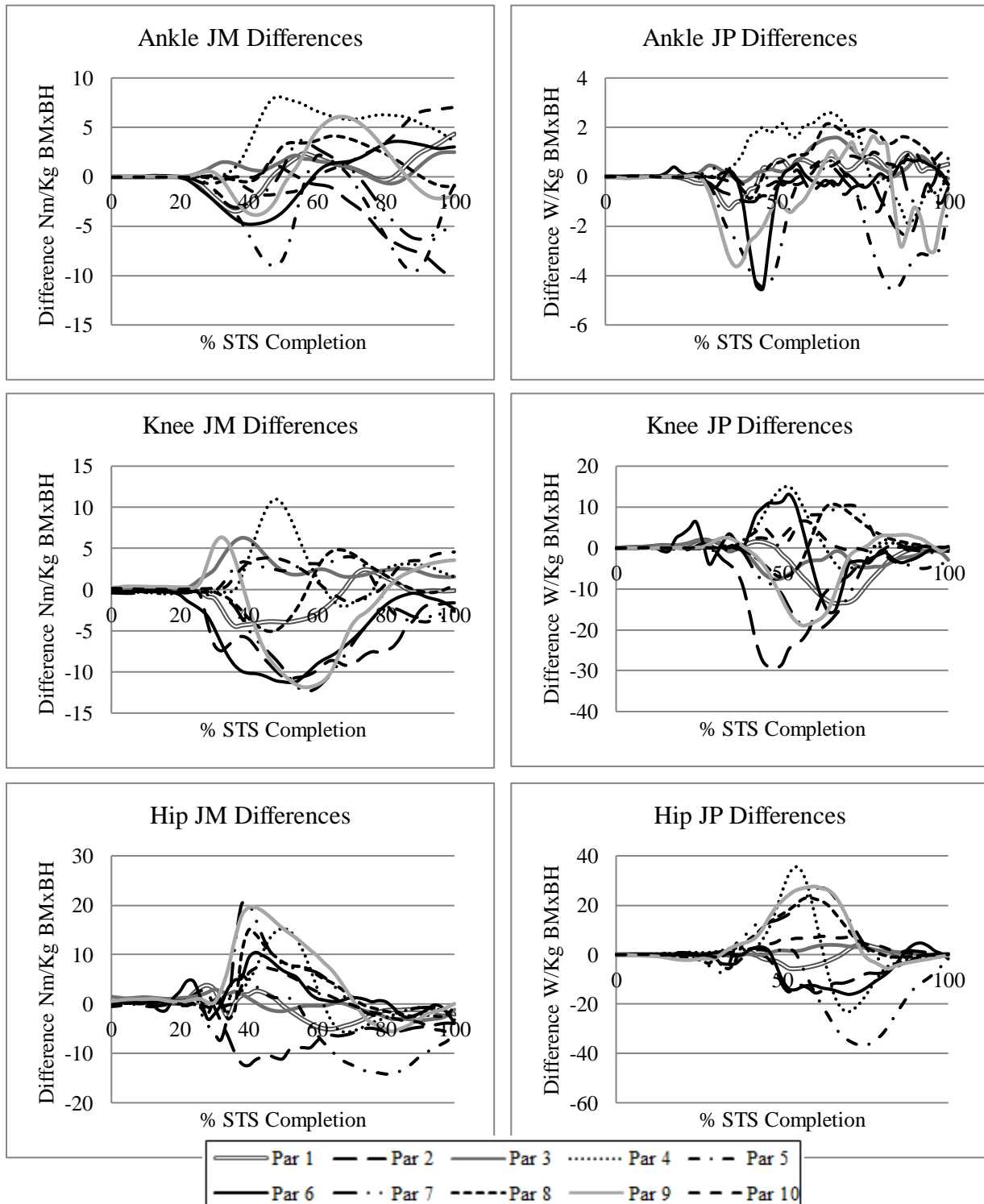
JM and JP are the average joint moment and joint power offset values in %time of the STS cycle. SD is the standard deviation of these values. P-value shows the results from the t-test of first to peak compared to last to peak. P<0.05 was assumed to show a significant difference in these mean times

Joint	JM (%)	SD (%)	p-value	JP (%)	SD (%)	p-value
Ankle	3.60	5.15	0.027	12.00	14.30	0.017
Knee	0.80	1.03	0.018	1.00	1.05	0.047
Hip	2.00	4.99	0.118	4.40	7.99	0.049

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Figure 3 Straight Difference Plots for Each Participant According to Joint

305 Where JM, JP and SDIF represent joint moment, joint power and straight difference respectively, units are given in
306 Newton or watts meters per kilogram (Nm/Kg) or (W/Kg) normalized to body mass (BM) and body height (BH).
307 Par # denotes an individual participant's SDIF data.
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Table 3 Slope Changes in Joint Moment and Joint Power Data

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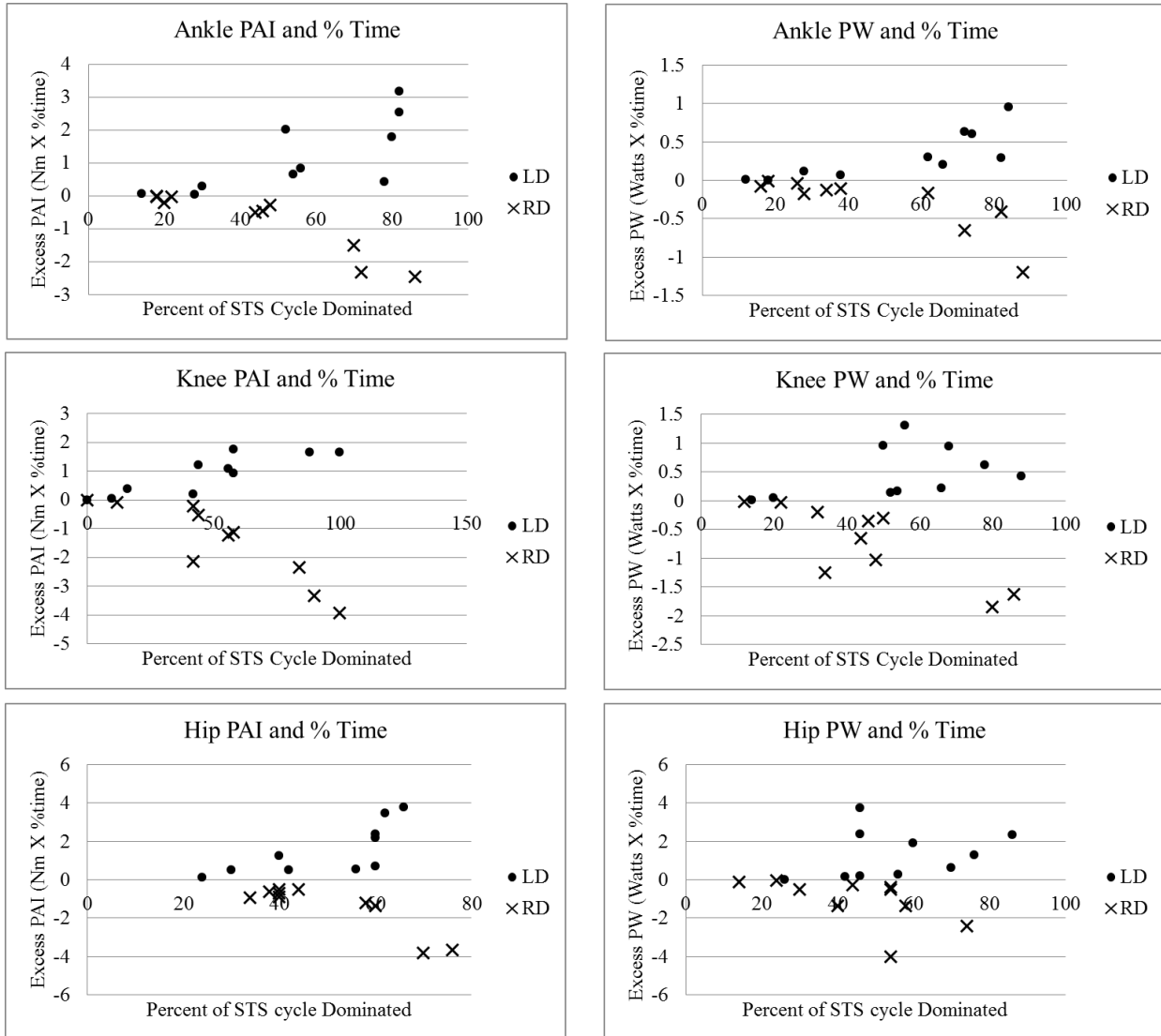
The number of slope changes is organized by participant and joint. JM represents joint moment data and JP, joint power. Groups indicate the number of slope reversal categories seen in the participant. Average and SD show the mean number of slope reversals at each joint and the corresponding standard deviation.

		Number of Slope Reversals										Groups	Average	SD
	Participant	1	2	3	4	5	6	7	8	9	10			
Ankle	JM	3	0	2	1	3	3	3	2	2	1	4	2.00	1.05
	JP	6	6	4	2	3	6	5	2	6	6	5	4.60	1.71
Knee	JM	2	1	2	3	3	1	1	2	2	2	3	1.90	0.74
	JP	2	1	2	2	3	1	1	2	2	2	3	1.80	0.63
Hip	JM	4	1	2	2	2	4	2	2	2	1	3	2.20	1.03
	JP	4	1	3	2	2	4	2	2	2	1	4	2.30	1.06

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Figure 4 Positive PAI and PW Plotted Against %Time Positive or Negative

318 The circles represent the positive PAI (or PW) plot against time the JM SDIF (or JP) remain positive respectively.
 319 Since these values are positive, LD is an abbreviation for left side dominant. Inversely the crosses represent the
 320 negative equivalents. Since these values are negative, RD is an abbreviation for right side dominant.
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